



# Final Sanitary Sewer Discharge Plan

2012 MODIFICATION: MAY 2014  
VOLUME 3 OF 3



LOUISVILLE AND JEFFERSON COUNTY  
METROPOLITAN SEWER DISTRICT  
700 WEST LIBERTY STREET  
LOUISVILLE, KY 40203

**RESOLUTION OF  
THE BOARD OF THE LOUISVILLE AND JEFFERSON COUNTY  
METROPOLITAN SEWER DISTRICT  
AUTHORIZING THE EXECUTIVE DIRECTOR TO SUBMIT FOR APPROVAL  
THE INTEGRATED OVERFLOW ABATEMENT PLAN 2012 MODIFICATION  
TO UNITED STATES ENVIRONMENTAL PROTECTION AGENCY, THE  
KENTUCKY DEPARTMENT FOR ENVIRONMENTAL PROTECTION AND THE  
UNITED STATES DEPARTMENT OF JUSTICE**

**WHEREAS**, the Board of the Louisville and Jefferson County Metropolitan Sewer District (“MSD”) entered into a Consent Decree with United States Environmental Protection Agency, the Kentucky Department for Environmental Protection and the United States Department of Justice on August 12, 2005, and subsequently amended on April 15, 2009 (“Amended Consent Decree”); and

**WHEREAS**, the Amended Consent Decree requires that MSD prepare and submit plans to comply with KPDES permits and upgrade the separate sewer system, combined sewer system and water quality treatment centers (WQTCs) to adequately address sanitary sewer overflows (“SSOs”) and unauthorized discharges, and discharges from combined sewer overflows (“CSOs”) locations identified in the Morris Forman WQTC KPDES permit; and

**WHEREAS**, MSD previously prepared and submitted an Integrated Overflow Abatement Plan (“IOAP”) to control SSOs, unauthorized discharges, and CSOs as required by the Amended Consent Decree, and state and federal law, which was subsequently approved by the United States Department of Justice on September 30, 2009; and

**WHEREAS**, MSD’s Wet Weather Team which includes a broad range of community stakeholders, MSD staff and consultants has identified the need for modifications to the IOAP to incorporate through an adaptive management process additional information developed from continued flow monitoring, enhanced hydraulic modeling, and a detailed review of project types, size, location, and schedule; and



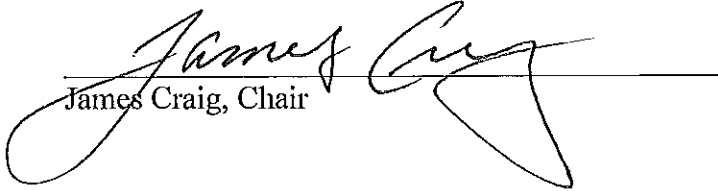
**WHEREAS**, the staff of MSD presented the proposed IOAP 2012 Modification to the Board on February 11, 2013; and

**WHEREAS**, the staff of MSD presented the proposed IOAP 2012 Modification at several public meetings Between September 27, 2011, and February 5, 2013; held a public hearing to receive both written and oral public comments on the IOAP 2012 Modification on March 26, 2013; received oral and written public comments during the period starting on March 13, 2013, and concluding on April 12, 2013;


**THEREFORE BE IT HEREBY RESOLVED** that the Executive Director is hereby authorized to submit to the United States Environmental Protection Agency, the Kentucky Department for Environmental Protection and the United States Department of Justice, the IOAP 2012 Modification as presented to the Board on May 13, 2013.

Adopted in open session this 13<sup>th</sup> day of May, 2013.

LOUISVILLE & JEFFERSON COUNTY  
METROPOLITAN SEWER DISTRICT

  
James Craig, Chair

Attest:

  
Chad Collier, Secretary-Treasurer

**RESOLUTION OF  
THE BOARD OF THE LOUISVILLE AND JEFFERSON COUNTY  
METROPOLITAN SEWER DISTRICT  
AUTHORIZING THE EXECUTIVE DIRECTOR TO SUBMIT THE  
INTEGRATED OVERFLOW ABATEMENT PLAN FOR APPROVAL  
TO UNITED STATES ENVIRONMENTAL PROTECTION AGENCY, THE  
KENTUCKY DEPARTMENT OF ENVIRONMENTAL PROTECTION AND THE  
UNITED STATES DEPARTMENT OF JUSTICE**

**WHEREAS**, the Board of the Louisville and Jefferson County Metropolitan Sewer District (“MSD”) entered into a Consent Decree, as may be amended, with United States Environmental Protection Agency, the Kentucky Department of Environmental Protection and the United States Department of Justice on August 12, 2005; and

**WHEREAS**, the Consent Decree requires that MSD prepare and submit plans to control combined sewer overflows (“CSOs”) and sanitary sewer overflows (“SSOs”); and

**WHEREAS**, MSD has prepared an Integrated Overflow Abatement Plan (“IOAP”) to control both CSOs and SSOs as required by the Consent Decree, and state and federal law; and

**WHEREAS**, the IOAP was drafted by MSD’s Wet Weather Team which includes a broad range of community stakeholders, MSD staff and consultants; and

**WHEREAS**, the staff of MSD presented the IOAP to the Board on October 27, 2008; and

**WHEREAS**, the staff of MSD presented the IOAP at several public meetings on November 10, 12, and 20, 2008; and

**WHEREAS**, the staff of MSD held a public hearing to receive both written and oral public comments on the IOAP on December 2, 2008; and

**WHEREAS**, the staff of MSD received written public comments during the period starting on October 1, 2008, and concluding on December 5, 2008; and

**WHEREAS**, the IOAP must be submitted to the USEPA and the Commonwealth by



December 31, 2008, as required by the Consent Decree;

**THEREFORE BE IT HEREBY RESOLVED** that the Executive Director is hereby authorized to submit to the USEPA and the Commonwealth by December 31, 2008, the IOAP as presented to the Board on October 27, 2008, as modified after the public hearing on December 2, 2008, and the conclusion of the public comment on December 5, 2008, and with the following scope:

The Louisville and Jefferson County Metropolitan Sewer District's Integrated Overflow Abatement Plan is a long-term plan to control combined sewer overflows (CSOs) and sanitary sewer overflows (SSOs) in the community. The IOAP is expected to improve water quality in both Jefferson County streams and the Ohio River. The expected water quality benefits of the IOAP include: (a) reductions in the peak levels of bacteria in the Ohio River, the Beargrass Creek and other Jefferson County waterways; and (b) a reduction in the duration of wet weather impairment of local waterways (i.e., the number of days that bacteria levels exceed water quality standards during periods of wet weather). The IOAP—in coordination with other community water quality initiatives (further described below)—will also improve water quality under ambient conditions.

The specific benefits anticipated from the IOAP include the following:

- The suite of projects selected for the Long Term Control Plan (LTCP) for CSOs will result in approximately 96 percent capture and treatment of wet weather combined sewage during an average year. (As a point of reference, the “presumptive approach” in EPA’s CSO Control Policy is based on a minimum of 85 percent wet weather capture.)
- Remaining CSO loads (after removing background) will no longer cause water quality standard violations in the Ohio River.

Peak fecal coliform counts are modeled to be reduced by 54 percent.

- At the mouth of Beargrass Creek, peak fecal coliform counts are modeled to be reduced by 18 percent. The control level associated with these reductions exceeds the EPA CSO Control Policy “presumptive approach” 85 percent wet weather capture threshold and reflects a point of significantly diminishing returns under the “knee of the curve” benefit-cost analysis.
- The suite of projects selected for the Sanitary Sewer Discharge Plan (SSDP) for SSOs will result in the elimination of capacity-related SSOs up to the site-specific level of protection (described below).
- The SSO projects are anticipated to eliminate an average of 145 SSO events per year, based on 2005–2007 data.
- In terms of water quality, SSO projects are estimated to eliminate an average of 290 million gallons of overflow volume per year (average of 2005–2007 normalized for rainfall), eliminating 100 tons of 5-day biochemical oxygen demand (BOD5) and almost 200 tons of solids annually.

Along with delivering water quality improvements from sewer overflow control, MSD participates in other community water quality improvement efforts. Sewer overflow control is essential to improving water quality, but overflow control alone is not enough to meet water quality standards. In light of this challenge, MSD will continue to leverage its role in supporting broader water quality improvement efforts in the community. The IOAP will be one of the key elements of MSD’s participation in those water quality improvement efforts. In particular, the IOAP will be complementary to other wet weather and water quality programs managed by MSD and/or by other community partners. These complementary efforts include, but are not limited to, the Mayor’s “Go Green Louisville” Initiative, the Partnership for a Green City, Metro Louisville’s Municipal Separate Storm Sewer System (MS4)



discharge permit, and initiatives of Jefferson County Public Schools (JCPS), private developers, and other entities.

The specific ways in which MSD is collaborating with other entities on community water quality improvement initiatives include the following:

- Partnership for a Green City: MSD is actively working with Louisville Metro Government, JCPS, and the University of Louisville to improve water quality through the Partnership for a Green City. The Partnership has established a Stormwater Committee that will be identifying opportunities to improve water quality associated with planned capital projects.
- Louisville Metro Government: MSD is an active participant in the Mayor's Go Green Louisville Initiative, which includes in its vision a commitment to focus on financially sustainable measures that improve air and water quality, land use, and energy efficiency. In coordination with this initiative, MSD is partnering with Louisville Metro Government on several green infrastructure demonstration projects in the IOAP.
- MS4 Program: MSD will coordinate IOAP implementation with the agencies that share implementation of the MS4 Program—including Metro Louisville government, small cities that handle their own drainage, and the Kentucky Department of Transportation. The MS4 program will draw upon the opportunities identified through the green infrastructure analysis conducted by MSD's IOAP technical team and the ideas suggested by WWT members during the development of the IOAP. MSD further anticipates implementing demonstration projects, such as rain gardens in the separate sewer area, under the MS4 as part of a coordinated effort with the IOAP to test and evaluate green infrastructure approaches to wet weather management.

The IOAP—as part of MSD's consent decree response—will be a federally enforceable action plan for sewer overflow abatement. Although many IOAP projects and programs will provide multiple benefits to the community, the scope of the IOAP is limited to commitments that directly relate to MSD programs and activities to

address combined sewer overflow (CSO) and sanitary sewer overflow (SSO) issues. Other community water quality programs, which may be partly or completely out of MSD's control, can provide synergistic benefits with the IOAP, but they do not fall under the same federal enforcement. These programs may, however, have different mechanisms for ensuring accountability (e.g., the State of Kentucky oversees the MS4 stormwater permit that MSD and several other agencies hold). As noted above, MSD anticipates coordinating IOAP implementation with the water quality improvement initiatives of Louisville Metro Government and other public and private entities, even though these broader initiatives may not explicitly be part of the IOAP.

Adopted in open session this 15<sup>th</sup> day of December, 2008.

LOUISVILLE & JEFFERSON COUNTY  
METROPOLITAN SEWER DISTRICT

  
Beverly Wheatley, Chairperson of the Board

  
Dana Price, Board Secretary



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Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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# Glossary



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### DEFINITIONS

**Amended Consent Decree (ACD)** - Specific to this document, a federal judicial order expressing a voluntary agreement ordered on April 10, 2009 and filed on April 15, 2009 that incorporates all elements of the original Consent Decree (see Consent Decree definition) as well as imposing new requirements to cease activities alleged by the government to be illegal.

**Average Annual Overflow Volume (AAOV)** - The total volume of overflow predicted to occur from a specific location or consolidation of locations, calculated using a continuous simulation of precipitation that occurs in a “typical year.” For the purpose of this Integrated Overflow Abatement Plan (IOAP), calendar year 2001 represents the typical year, based on an evaluation of precipitation patterns in that year compared to long-term meteorological averages.

**Average Daily Flow (ADF)** - The calculated or assumed average daily flow within the sewer system attributed to users without rainfall derived inflow and infiltration (I/I) within a 24-hour period.

**Avoidable** - A legal term of art meaning that a consequence could have been prevented with the exercise of reasonable engineering judgment in facilities planning and implementation, and/or adequate management, operations, and maintenance practices.

**Baseline** - The existing conditions. An initial set of observations or data used as a comparison or starting point from which the magnitudes of an alternative’s effects are measured.

**Benefit - Cost Analysis** - A formal process used to help appraise, or assess, the cost effectiveness of different alternatives. The higher the Benefit-Cost Ratio, the more effective the alternative is.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**Best Management Practices (BMPs)** - Schedules of activities, prohibitions of practices, maintenance procedures, and other management practices to prevent or reduce the discharge of pollutants to Waters of the United States. BMPs also include treatment requirements, operating procedures, and practice to control plant site runoff, spillage or leaks, sludge or waste disposal, or drainage from raw material storage.

**Biochemical Oxygen Demand (BOD)** - A measurement of the amount of oxygen used by the decomposition of organic material over a specified time period (usually 5 days) in a wastewater sample. Used as a measurement of the readily decomposable organic content of water.

**Bypass** - The intentional diversion of waste streams from any portion of a treatment facility as set forth in 40 Code of Federal Regulations (CFR), § 122.41(m)(1) and 401 Kentucky Administrative Regulations (KAR) 5:002, Section 1(36). The practice of bypassing secondary treatment units and recombining the bypass flow with the secondary effluent prior to discharge, known commonly as blending, recombination, or diversion, constitutes a "Bypass." The term Bypass shall specifically exclude (1) practices at MSD's Morris Forman Wastewater Treatment Plant (WWTP) that are in accordance with the KPDES permit and the CSO Control Policy and (2) any flow that exceeds the design capacity of a tertiary process at any WWTP in accordance with a Kentucky Pollutant Discharge Elimination System (KDPEs) permit.

**Chemical Treatment** - Any water or wastewater treatment process involving the addition of chemicals to obtain a desired result, such as precipitation, coagulation, flocculation, sludge conditioning, disinfection, or odor controls.

**Combined Sewer Overflow (CSO)** - an outfall identified as a combined sewer overflow or CSO in MSD's KPDES permit for the Morris Forman WWTP from which MSD is authorized to discharge during wet weather.

- **Dry Weather CSO** - An overflow from a permitted outfall identified as a combined sewer overflow or CSO in MSD's Morris Forman WWTP KPDES permit that is not the result of a wet weather event.
- **Wet Weather CSO** - An overflow from a permitted outfall identified as a combined sewer overflow or CSO in MSD's Morris Forman WWTP KPDES permit that is the result of a wet weather event.

**Combined Sewer System (CSS)** - the portion of MSD's Sewer System designed to convey municipal sewage (domestic, commercial, and industrial wastewaters) and stormwater runoff through a single-pipe system to MSD's Morris Forman WWTP or CSOs.

**Consent Decree** - A judicial decree expressing a voluntary agreement between parties to a suit, especially an agreement by a defendant to cease activities alleged by the government to be illegal in return for an end to the charges.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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**Controls** - Processes and/or activities which contribute to removal of pollutants from wastewater or to containing and conveying wastewater for treatment and discharge.

**Dissolved Oxygen (DO)** - A measurement of the amount of oxygen dissolved in water.

**Fats, Oils, and Grease (FOG)** – A general category of lipid-based wastewater constituents that often are responsible for sewer blockages and resulting back-ups or overflows.

**Feasible Alternatives** - The legal term of art used in the “Bypass” regulation to identify alternative controls which are both technically achievable and affordable (40 CFR 122.42m).

**Fecal Coliform** - Bacteria present in the feces of warm blooded animals typically used as an indicator of fecal contamination and the potential presence of pathogens.

**Flow Equalization** - Transient storage of wastewater for release to a sewer system or treatment process at a controlled rate to provide a reasonably uniform flow.

**Geographic Information System (GIS)** - A computer based system that is capable of storing, managing, and analyzing geographic spatial data. This capability includes producing maps, displaying the results of data queries, and conducting spatial analysis.

**Gray Infrastructure** - Constructed structures such as treatment facilities, sewer systems, stormwater systems, or storage basins. The term “gray” refers to the fact that such structures are typically made of, or involve the use of concrete.

**Green Infrastructure** - An adaptable term used to describe an array of materials, technologies, and practices that use natural systems—or engineered systems that mimic natural processes—to enhance overall environmental quality and provide utility services. As a general principal, green infrastructure techniques use soils and vegetation to infiltrate, evapotranspire, and/or recycle stormwater runoff. Examples of green infrastructure include green roofs, porous pavement, rain gardens, and vegetated swales.

**Infiltration** - Groundwater that enters a wastewater system through such means as defects in pipes, pipe joints, connections, or manholes.

**Inflow** - Water other than wastewater that enters a wastewater system from sources such as stormwater, runoff, and drainage. Inflow is generally derived from surface water, as compared to infiltration that is generally derived from groundwater.

**InfoWorks Collection Systems (CS)** - Hydraulic modeling software developed by Wallingford Software used by MSD for collection system modeling.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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**Kentucky Department for Environmental Protection (KDEP)** - Agency responsible for administering KPDES permits and receiving permit-related reports.

**Kentucky Pollutant Discharge Elimination System (KPDES) Permit** - Any National Pollutant Discharge Elimination System permit issued to MSD by the Cabinet pursuant to the authority of the Clean Water Act and Kentucky Revised Statutes (KRS) Chapter 224 and the regulations promulgated thereunder.

**Leadership in Energy and Environmental Design (LEED)** - A rating system that is administered by the US Green Building Council (USGBC) and is currently the most accepted benchmark for the design, construction, and operation of high performance green buildings and neighborhood developments in the U.S. The five key areas include sustainable site development, water savings, energy efficiency, materials selection, and indoor environmental quality.

**Louisville and Jefferson County Metropolitan Sewer District (MSD)** - The agency responsible for providing wastewater, stormwater, and flood protection services in Jefferson County. MSD is also responsible for response, mitigation, notification, and reporting of overflows, including unauthorized discharges.

**Lower Gauge (LG)** - A measure of the Ohio River's stage (elevation) below the McAlpine Lock and Dam. Gauge 0 is equal to an elevation of 373.2' above mean sea level. Normal pool elevation for the Ohio River is 384.5' or a lower gauge of 11.3.

**National Pollutant Discharge Elimination System (NPDES)** - A national program under the Clean Water Act that regulates discharges of pollutants from point sources to Waters of the United States. Discharges are illegal unless authorized by an NPDES permit.

**Overflow** - Any release of wastewater from MSD's sanitary or combined sewer system at locations not specified in any KPDES permit. This includes any Unauthorized Discharge and releases to public or private property that do not reach Waters of the United States, such as basement backups. However, wastewater backups into buildings caused by blockages, flow conditions, or malfunctions in a building lateral, other piping or conveyance system that is not owned or operationally controlled by MSD are not overflows for the purposes of the IOAP.

**Pathogen** - An organism capable of causing disease, including disease-causing bacteria, protozoa, and viruses.

**Peak Flow** - The maximum flow that occurs over a specific length of time (e.g., daily, hourly, instantaneous).

**Peak Wet Weather Flow** - The anticipated, calculated, or monitored maximum flow within the sewer system during an actual or synthetic rainfall event.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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**Primary Treatment** - The practice of treatment by screening, sedimentation, and skimming adequate to remove at least 30 percent of both the biochemical oxygen demanding material and the suspended solids, as defined in 40 CFR Part 125.58(r). Primary treatment may also include disinfection, where appropriate or required.

**Reasonable Engineering** - As a legal term of art, this is the statutory and regulatory standard for judgment evaluating engineering practices.

**Rim Elevation** - The elevation of the top of a manhole cover. If the water surface elevation in a manhole is higher than the rim elevation, a sewer overflow will occur.

**Risk Management** - The process of identification, analysis and either acceptance or mitigation of risk. Essentially, risk management occurs anytime one analyzes the probability and consequences of an event happening, thereby quantifying the potential for losses and then takes the appropriate action (or inaction) given their objectives and risk tolerance.

**Sanitary Sewer** - A pipe or conduit (sewer) intended to carry wastewater or water-borne wastes from homes, businesses, and industries to the publicly owned treatment works.

**Sanitary Sewer Overflow (SSO)** - Any discharge of wastewater to waters of the United States from MSD's Sewer System through a point source not authorized by a KPDES permit, as well as any release of wastewater from MSD's Sewer System to public or private property that does not reach Waters of the United States, such as a release to a land surface or structure that does not reach Waters of the United States; provided, however, that releases or wastewater backups into buildings that are caused by blockages, flow conditions, or malfunctions in a building lateral, or in other piping or conveyance system that is not owned or operationally controlled by MSD are not SSOs.

**Sanitary Sewer System (SSS)** - The portion of MSD's sewer system designed to convey only municipal sewage (domestic, commercial, and industrial wastewaters) to MSD's WWTPs.

**Secondary Treatment** - A biological wastewater treatment technology required by the Clean Water Act for discharges from Publicly Owned Treatment Works, as that term is defined in 40 CFR Part 403.3(q). The minimum level of effluent quality attainable through the application of secondary treatment is established in 40 CFR Part 133.102 in terms of the parameters for 5-day biochemical oxygen demand ("BOD5") concentration and percent removal, total suspended solids ("TSS") concentration and percent removal, and pH.

**Sensitive Areas** - Areas of particular environmental significance or sensitivity as determined by the KPDES permitting authority in coordination with State and Federal agencies, that include Outstanding National Resources Waters, waters with threatened or endangered species and their habitats, waters with primary contract recreation, public drinking water intakes or their designated protection areas.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**Sewer System** - The wastewater collection, retention, and transmission system that MSD owns or operates, that are designed to collect, retain and convey municipal sewage (domestic, commercial and industrial wastewaters) to MSD's WWTPs or CSOs which is comprised of the CSS and the SSS.

**Solids and Floatables (S&F)** – Materials in sewage that are large enough to be visibly recognizable. Most solids and floatables in combined sewage are comprised of street litter and debris, but some plastic and paper products flushed down toilets stay in a visibly recognizable form, and are objectionable to some people.

**Solution** - A set of modifications to existing conditions in the hydraulic model developed to satisfy the overflow and surcharging requirements. Solutions are generally developed by trial and error modifications to the hydrological and hydraulic system at a given design storm. Modifications may include minimizing inflow and infiltration, modifications to conveyance (pipe diameter or pump capacity), added storage, system diversions or combinations thereof.

**Surcharge** - The condition within the sewer when the hydraulic grade line (water surface level) within the sewer system exceeds the crown of pipe elevation. The System Capacity Assurance Program (SCAP) defines a wet weather surcharge condition as a water surface level within the sewer that is less than two feet from the manhole rim elevation. If the sewer system is in an area of chronic backup complaints, then a surcharge condition is considered to be a water surface level within five feet of the manhole rim.

**Upper Gauge (UG)** - A measure of the Ohio River's stage (elevation) above the McAlpine Lock and Dam. Gauge 0 is equal to an elevation of 407.5' above mean sea level. Normal pool elevation for the Ohio River is 420.0' or an upper gauge of 12.5.

**U.S. Environmental Protection Agency (EPA)** - The federal agency responsible for enforcing the Clean Water Act, Safe Drinking Water Act and other federal environmental regulations.

**Unauthorized Discharge** - (a) any discharge of wastewater to waters of the United States from MSD's Sewer System or WWTPs through a point source not authorized by a KPDES permit and (b) any Bypass at MSD's WWTPs prohibited pursuant to the provisions of 40 CFR § 122.41(m)(2) and (4) or 401 KAR 5:065, Section 1(13)(a) and (c).

**Water Quality Standards (WQS)** - Standards that set the goals, pollution limits, and protection requirements for each waterbody. These standards are composed of designated (beneficial) uses, numeric and narrative criteria, and antidegradation policies and procedures.

**Water Quality Treatment Center (WQTC)** - The devices or systems used in the storage, treatment, recycling, and reclamation of municipal sewage that MSD owns or operates, and for which KPDES permits have been or will be issued to MSD. Treatment facilities may be referenced as Wastewater Treatment Plants (WWTPs) on enclosed maps or within the IOAP appendices due to MSD's transition to the WQTC terminology during IOAP development.

**Waters of the United States** - As defined in 40 CFR 122.2:

- (a) All waters which are currently used, were used in the past, or may be susceptible to use in interstate or foreign commerce, including all waters which are subject to the ebb and flow of the tide;
- (b) All interstate waters, including interstate “wetlands,”
- (c) All other waters such as intrastate lakes, rivers, streams (including intermittent streams), mudflats, sandflats, “wetlands,” sloughs, prairie potholes, wet meadows, playa lakes, or natural ponds the use, degradation, or destruction of which would affect or could affect interstate or foreign commerce including any such waters:
  - (1) Which are or could be used by interstate or foreign travelers for recreational or other purposes; or
  - (2) From which fish or shellfish are or could be taken and sold in interstate or foreign commerce; or
  - (3) Which are used or could be used for industrial purposes by industries in interstate commerce;
- (d) All impoundments of waters otherwise defined as waters of the United States under this definition;
- (e) Tributaries of waters identified in paragraphs (a) through (d) of this definition;
- (f) The territorial sea; and
- (g) “Wetlands” adjacent to waters (other than waters that are themselves wetlands) identified in paragraphs (a) through (f) of this definition.

Note that the intent of the regulations cited above excludes waste treatment systems, manmade ponds, and prior converted cropland from the definition of “Waters of the US.” With respect to prior converted cropland, EPA maintains jurisdiction for purposes of the Clean Water Act.

**Watershed Approach** - A flexible framework used for managing water resources within a specified drainage area, or watershed. This approach includes stakeholder involvement and management actions supported by sound science and appropriate technology.

**Watershed** - Land area that drains to a common waterway, such as a stream, lake, estuary, wetland, or ultimately the ocean.

**Wet Weather Event** - A discharge from a combined or sanitary sewer system that occurs in direct response to rainfall or snowmelt.

**Wet Weather Team (WWT)** - An advisement group for MSD composed of four subgroups: The Stakeholder Group, MSD employees, a Technical Team, and the Facilitation Team. A WWT is required by the Consent Decree.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

## ACRONYMS AND ABBREVIATIONS

AAOV	Average annual overflow volume
ACD	Amended Consent Decree
ADF	Average daily flow
BG	Billion gallons
BGCMF	Beargrass Creek Middle Fork
BGCMU	Beargrass Creek Muddy Fork
BGCSF	Beargrass Creek South Fork
BMP	Best management practice
BOD	Biochemical oxygen demand
CCTV	Closed-circuit television
CDS	Continuous Deflection Separator
CFR	Code of Federal Regulations
cfs	Cubic feet per second
cfu	Colony forming unit
CMF	Central Maintenance Facility
CMOM	Capacity, Management, Operations, and Maintenance
COD	Chemical oxygen demand
CSO	Combined sewer overflow
CSS	Combined sewer system
CWA	Clean Water Act
DMR	Discharge monitoring report
DO	Dissolved oxygen
DWF	Dry weather flow
E. Coli	Escherichia Coli
EAP	Early Action Plan
ENR-CCI	Engineering News Record – Construction Cost Index
EPA	U.S. Environmental Protection Agency
FOG	Fats, oils, and grease
FY	Fiscal year
GIS	Geographic Information System
gpd	Gallons per day
GPS	Global Positioning Satellite
HEC RAS	hydraulic water flow modeling software
I&FP	Infrastructure and Flood Protection
I/I	inflow and infiltration

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

IOAP	Integrated Overflow Abatement Plan
IWD	Industrial Waste Department (also known as ICAM)
JCPS	Jefferson County Public Schools
JTown	Jeffersontown
KDEP	Kentucky Department of Environmental Protection
KPDES	Kentucky Pollutant Discharge Elimination System
KRS	Kentucky Revised Statute
LEED	Leadership in Energy and Environmental Design
LF	Linear feet
LG	Lower gauge
LG&E	Louisville Gas & Electric
LOJIC	Louisville and Jefferson County Information Consortium
LS	Lift station
LTCP	Long-Term Control Plan
LTMN	Long Term Monitoring Network
LWC	Louisville Water Company
MHI	Median Household Income
MG	Million gallons
mgd	Million gallons per day
mg/l	Milligrams per liter
ml	Milliliter
MOP	Modeled overflow point
MS4	Municipal Separate Storm Sewer System
MSD	Louisville and Jefferson County Metropolitan Sewer District
NEXRAD	Next-Generation Radar
NMC	Nine Minimum Controls
NOAA	National Oceanographic and Atmospheric Administration
NPDES	National Pollutant Discharge Elimination System
O&M	Operations and Maintenance
OR	Ohio River
ORFM	Ohio River Force Main
ORSANCO	Ohio River Sanitation Commission
OSHA	Occupational Safety and Health Administration
PE	Professional Engineer
PM	Preventive maintenance
POTW	Publicly owned treatment works
Project DRI	Project Drainage Response Initiative



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Project WIN	Project Waterway Improvements Now
PS	Pump station
PIO	Public Information and Outreach
PVC	Polyvinyl chloride
QA/QC	Quality Assurance / Quality Control
QAPP	Quality Assurance Project Plan
RBP	Stream Rapid Bioassessment Protocol
RDI/I	Rainfall-derived infiltration and inflow
ROW	Right-of-way
RTC	Real time control
S&F	solids and floatables
SAP <sup>TM</sup>	Systems Analysis Program (MSD's financial management software)
SCADA	Supervisory Control and Data Acquisition
SCAP	Louisville Metro Sewer Capacity Assurance Plan
SED	Southeastern Diversion Structure
SIU	Significant Industrial User
SOP	Standard Operating Procedure
SORP	Sewer Overflow Response Protocol
SSDP	Sanitary Sewer Discharge Plan
SSES	Sanitary Sewer Evaluation Survey
SSO	Sanitary sewer overflow
SSOP	Sanitary Sewer Overflow Plan
SSS	Sanitary sewer system
SWMM	Stormwater and Wastewater Management Model
TMDL	Total maximum daily load
TSS	Total suspended solids
UAA	Use Attainability Analysis
UG	Upper Gauge
USACE	United States Army Corps of Engineers
USGS	United States Geological Survey
WDR	Waste Discharge Regulations
WEF	Water Environment Federation
WERF	Water Environment Research Foundation
WQT	water quality tool
WQTC	Water Quality Treatment Center (formerly WWTP)
WWT	Wet Weather Team

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**MODELING AND FLOW MONITORING BASINS**

BB	Buechel Branch	MC	Mill Creek
CC	Cedar Creek	MF	Middle Fork Beargrass Creek
FF	Floyds Fork	ND	Northern Ditch
HC	Hite Creek	ORFM	Ohio River Force Main
HP	Hikes Point	PC	Pond Creek
JT	Jeffersontown		

**REGIONAL WATER QUALITY TREATMENT CENTERS**

	<b>KPDES No.</b>	<b>MSD No.</b>
Cedar Creek	KY0098540	MSD0289
Floyds Fork	KY0102784	MSD0294
Hite Creek	KY0022420	MSD0202
Jeffersontown	KY0025194	MSD0255
Morris Forman	KY0022411	MSD0278
Derek R. Guthrie	KY0078956	MSD0277

(Formerly known as the West County Wastewater Treatment Plant)

**SMALL WATER QUALITY TREATMENT CENTERS**

	<b>KPDES No.</b>	<b>MSD No.</b>
Bancroft	KY0039021	MSD0290
Berrytown	KY0036501	MSD0209
Chenoweth Hills	KY0029459	MSD0263
Glenview Bluff	KY0044261	MSD0207
Hunting Creek North	KY0029106	MSD0291
Hunting Creek South	KY0029114	MSD0292
Ken Carla	KY0022497	MSD0208
Lake Forest / Beckley Woods	KY0042226	MSD0403
Lake of the Woods	KY0044342	MSD0251
McNeely Lake	KY0029416	MSD0228
Shadow Wood	KY0031810	MSD0404
Silver Heights	KY0028801	MSD0258
Starview	KY0031712	MSD0247
Timberlake	KY0043087	MSD0293
Yorktown	KY0036323	MSD0271



## **INTEGRATED OVERFLOW ABATEMENT PLAN**

### **EXECUTIVE SUMMARY**



### **SCOPE AND DESIRED OUTCOMES**

On August 12, 2005, the Louisville and Jefferson County Metropolitan Sewer District (MSD) entered into a Consent Decree in Federal Court with the United States Environmental Protection Agency (EPA) and the Kentucky Environmental and Public Protection Cabinet. The Consent Decree was developed in response to an enforcement action taken by EPA and the Kentucky Department of Environmental Protection (KDEP) alleging violations of the Clean Water Act (CWA) primarily related to sewer overflows. The stated objective of the Consent Decree is to further the objectives of the CWA; eliminate unauthorized discharges from MSD's separate sewer system (SSS), combined sewer system (CSS), and water quality treatment centers (WQTCs); and to address discharges from MSD's combined sewer overflow (CSO) locations identified in the Kentucky Pollutant Discharge Elimination System (KPDES) permit for the Morris Forman WQTC. The Consent Decree outlines the compliance program and schedules for achieving specific objectives, including the development of discharge abatement plans.

On December 1, 2008, a draft Amended Consent Decree (ACD) was released for public comment. The draft ACD addressed alleged violations of the CWA primarily related to WQTC performance, record-keeping, and reporting. The public comment period closed on the draft ACD December 31, 2008. The ACD was entered into Federal Court on April 15, 2009.

The Consent Decree amendments were negotiated over several months, and the terms of the draft amendments were known to MSD during the final stages of development of this Integrated Overflow Abatement Plan (IOAP). For the purposes of the IOAP, except where specifically noted otherwise, the term "Consent Decree" will be understood to mean the ACD as it was entered into Federal Court April, 15, 2009.

This IOAP is a major part of MSD's response to the Consent Decree. The IOAP is a long-term plan to control CSOs and eliminate sanitary sewer overflows (SSOs) and other unauthorized discharges from MSD's sewerage system. The IOAP is expected to improve water quality in both Beargrass Creek and the Ohio River through and below Jefferson County. The expected water quality benefits of the IOAP include: (a) reductions in the peak levels of bacteria in the Ohio River and Beargrass Creek; and (b) a reduction in the amount of time that average bacteria levels to exceed water quality standards.

## **ADAPTIVE MANAGEMENT**

Recognizing the long-term nature of the IOAP, MSD committed to an approach of adaptive management, intending to make mid-course corrections as we learn more about the performance of our projects and the related response of our sewerage system. In 2011, MSD took advantage of four more years of flow monitoring data to perform a planned recalibration of the hydraulic models used to develop, evaluate, and design overflow abatement projects. As a result of this recalibration MSD found opportunities to revise the proposed suite of projects, providing increased levels of overflow abatement, faster, and for approximately the same cost. The 2012 IOAP Modification incorporated herein describes the project changes in technology, size, and schedule, and the resultant benefits of making those changes.

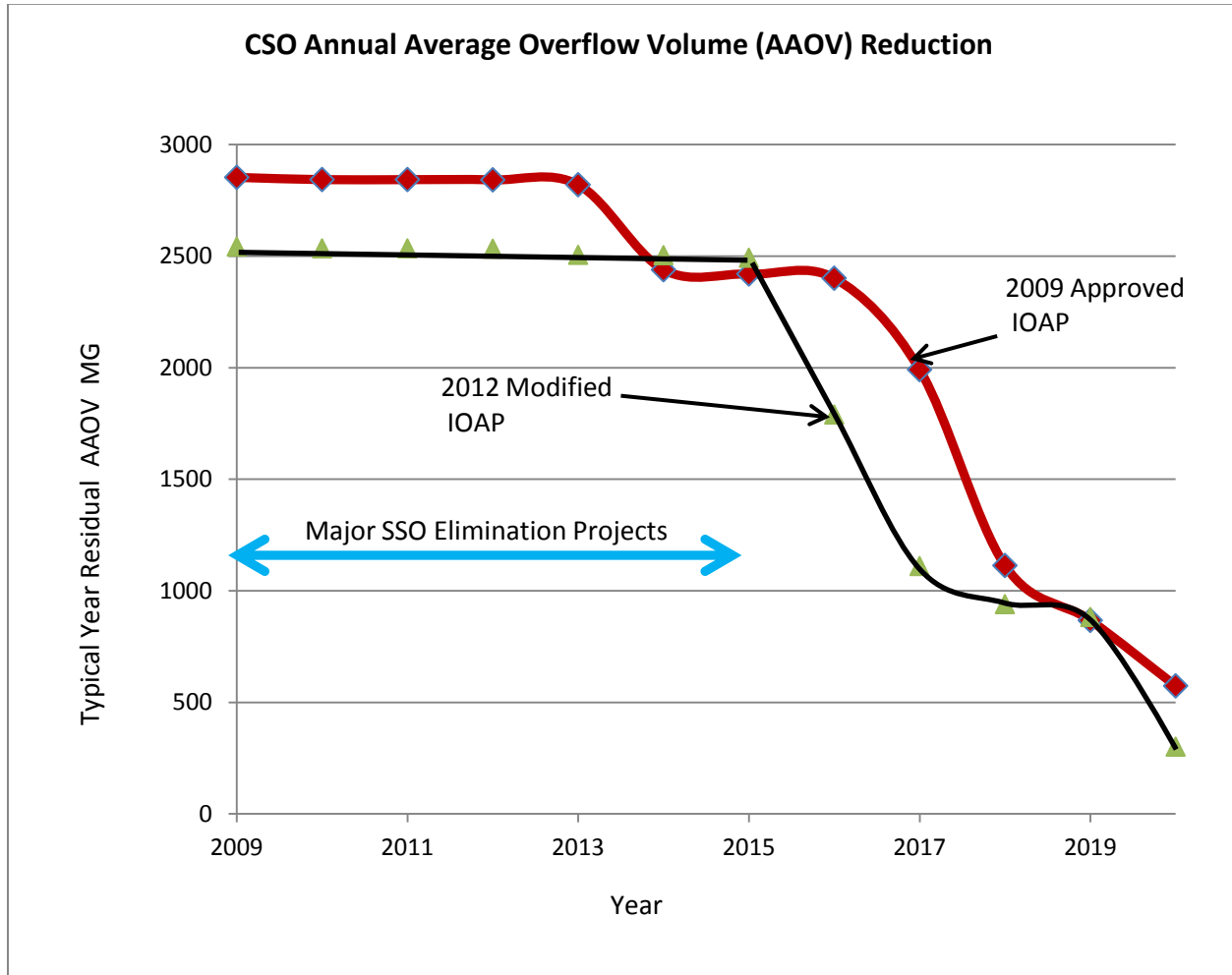
MSD developed a programmatic justification for this 2012 IOAP Modification utilizing the same benefit/cost methodology defined by the Wet Weather Team for the 2009 approved plan, as outlined in Volume 1 Chapter 2. This justification demonstrates the proposed modifications achieve a higher overall benefit to the community through earlier overflow reduction, increased use of green infrastructure and acknowledgement of pertinent public input.

A table showing the complete list of LTCP projects comparing the level of control, facility size, cost, and schedule for each of the projects in the 2009 approved IOAP and the 2012 IOAP Modification is included as Table ES.1 at the end of this Executive Summary. A similar table for the SSDP projects is included as Table ES.2 at the end of this Executive Summary. A schedule for all the projects in the LTCP and SSDP is also included at the end of this Executive Summary as Figure ES.1.

MSD has evaluated the impacts of the proposed modifications on the overflow reduction timing and overall overflow reduction performance as compared to the 2009 IOAP. Figure ES.2 below illustrates the effect of the proposed modifications on the timing of CSO elimination. The curve labeled "2009 Approved IOAP" shows the timing of average annual overflow volume (AAOV) reductions for the approved plan. The curve labeled "2012 Modified IOAP" shows that the proposed modifications achieve AAOV reductions earlier than was projected in the 2009 approved IOAP. In addition, residual AAOV is significantly lower in the 2012 Modified IOAP, reflecting a higher overall level of CSO control. Note that the apparent delay in achieving significant AAOV reductions is due to the need to focus initially on major SSO reductions required by the ACD and described in the Interim Sanitary Sewer Discharge Plan. Significant AAOV reductions were achieved prior to 2009 through the implementation of the first two phases of the Real Time Control (RTC) project, early action sewer separations, etc.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

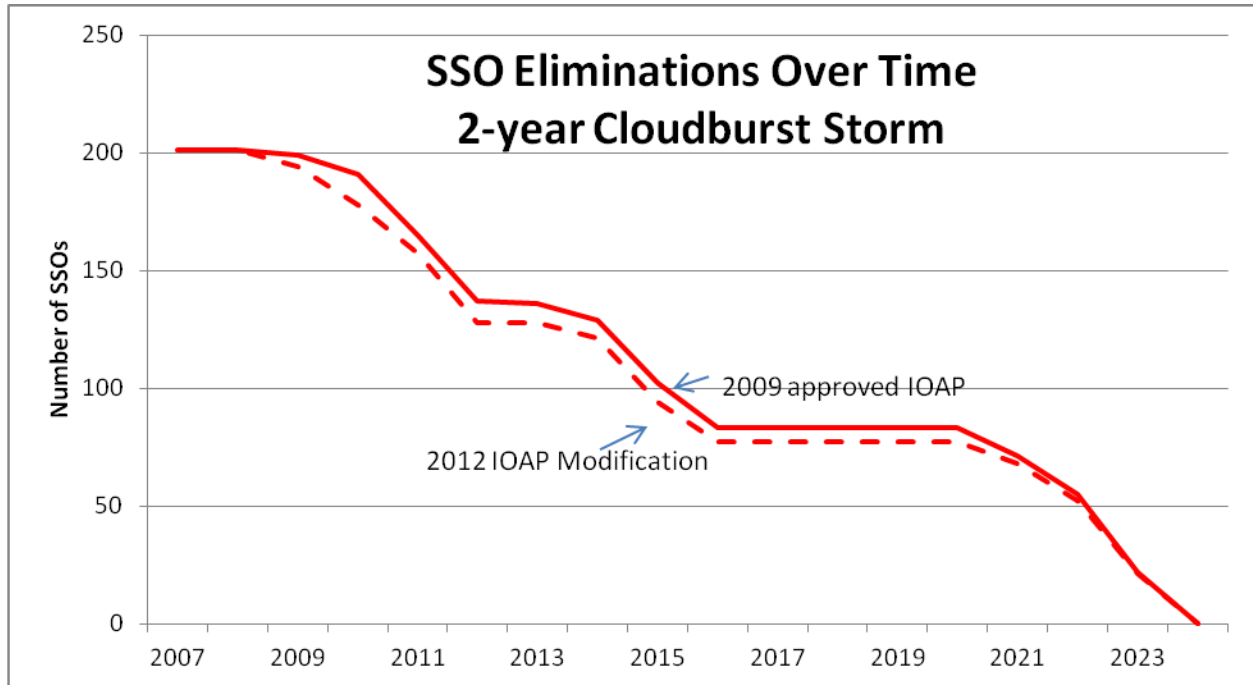
**FIGURE ES.2 - CSO AAOV REDUCTION THRU 2020**



MSD has similarly evaluated the impacts of the proposed modifications on the SSO overflow reduction timing and overall overflow reduction performance as compared to the 2009 IOAP. Figure ES.3 illustrates the effect of the proposed modifications on the timing of SSO elimination for the 1.82-inch cloudburst storm. Figure ES.3 shows that the number of SSO locations eliminated is the same, and the SSO eliminations occur quicker than originally proposed. In addition, more SSOs are eliminated to a higher level of control than proposed in 2009.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE ES.3 – SSO LOCATION REDUCTION THRU 2024**



Figures ES.2 and ES.3 demonstrate that the proposed changes result in a more effective overflow abatement program with higher community benefit and more expeditious overflow reduction as a program.

**CSO Benefits**

The suite of projects selected for the Final CSO Long-Term Control Plan (LTCP) will result in approximately 98 percent capture and treatment of wet weather combined sewage during an average year. This benefit represents an 89 percent reduction in CSO volume compared to conditions in 2008. As a point of reference, the presumptive approach for compliance with water quality standards in EPA’s CSO Control Policy is based on a minimum of 85 percent capture and treatment of wet weather combined sewage. Of the wet weather combined sewage captured and treated, approximately 70 percent receives secondary treatment at either the Morris Forman WQTC or the Derek R. Guthrie WQTC. The remainder of the wet weather flow receives primary treatment only.

Remaining CSO loads will no longer cause fecal coliform water quality standards violations in the Ohio River. Downstream from Morris Forman WQTC, peak fecal coliform counts are modeled to be reduced by 54 percent, from 100,000 colony-forming units (cfu) per 100 milliliter



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

(cfu/100mL) to 46,000 cfu/100 mL. If CSOs were eliminated, background sources (e.g. upstream Ohio River, stormwater runoff, and other sources) would continue to cause standards to be exceeded 33 percent of the recreation contact season (May to October).

Remaining CSO loads (after removing background) will result in 100 percent compliance with fecal coliform water quality standards in Beargrass Creek. At the mouth of Beargrass Creek, peak fecal coliform counts are modeled to be reduced by 18 percent, from 44,300 cfu/100mL to 37,400 cfu/100 mL. Reducing fecal coliform loads from CSO sources by 85 percent (compared to 2008 levels) results in a reduction of total loads on Beargrass Creek of approximately 30 percent. This is reflective of the preponderance of loads from stormwater runoff and other sources unrelated to CSOs.

### **SSO Benefits**

The suite of projects selected for the Final Sanitary Sewer Discharge Plan (SSDP) for SSO control will result in the elimination of capacity-related SSOs up to the site-specific level of protection. The SSO projects are anticipated to eliminate an average of 145 SSO events per year (290 million gallons {MG} of overflow volume), based on 2005–2007 data normalized for rainfall. In terms of water quality, SSO projects will eliminate 100 tons of five-day biochemical oxygen demand (BOD<sub>5</sub>) and approximately 200 tons of suspended solids annually.

Along with delivering water quality improvements from sewer overflow control, MSD participates in other community water quality improvement efforts. Sewer overflow control is essential to improving water quality, but overflow control alone is not sufficient to meet water quality standards. In light of this challenge, MSD continues to leverage its role in supporting broader water quality improvement efforts in the community. The IOAP will be one of the key elements of MSD's participation in those water quality improvement efforts.

### **Integration with Other Water Quality Programs**

The IOAP is a part of MSD's Consent Decree response and will be a federally enforceable action plan for sewer overflow abatement. Although many IOAP projects and programs will provide multiple benefits to the community, the scope of the IOAP is limited to commitments that directly relate to MSD programs and activities to address CSO and SSO issues. Other community water quality programs, which may be partly or completely out of MSD's control, can provide synergistic benefits with the IOAP, but they do not fall under the same federal enforcement. These programs may, however, have different enforcement mechanisms. As noted above, MSD anticipates coordinating IOAP implementation with the water quality improvement initiatives of Louisville Metro Government and other public and private entities, even though these broader initiatives may not explicitly be part of the IOAP.

The ancillary information provided by MSD that is not related to overflow abatement projects or the specific requirements of the Consent Decree is being provided and should be considered as supplemental, background information. It is not being submitted in response to any

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

requirements, obligations or commitments to any specific actions or time frames that are required under the provisions of the Consent Decree. This supplemental information should not be considered as a commitment by MSD to any project not required by the Consent Decree.

**Values-Based Performance Evaluation Framework**

In accordance with the Consent Decree, MSD established a Wet Weather Team (WWT) comprised of a broad range of community stakeholders, MSD staff, and consultants. Through a series of 23 meetings over the course of more than two years, the WWT developed a values-based performance evaluation framework to use in evaluating, selecting, and prioritizing alternative approaches to overflow abatement. This analytic framework includes both a robust benefit-cost scoring methodology for evaluating and selecting project alternatives and a systematic process for evaluating the IOAP programmatically. The WWT identified and agreed upon the following eleven community values that underpin the analysis and selection of alternatives for the IOAP.

Project-Specific Values	Programmatic Value
<ul style="list-style-type: none"> <li>• Asset protection</li> <li>• Eco-friendly solutions</li> <li>• Environmental enhancement</li> <li>• Public health enhancement</li> <li>• Regulatory performance</li> </ul>	<ul style="list-style-type: none"> <li>• Customer Satisfaction</li> <li>• Economic vitality</li> <li>• Education</li> <li>• Environmental justice and equity</li> <li>• Financial equity</li> <li>• Financial stewardship</li> </ul>

Using the structured decision-making process as framed by the WWT, MSD developed and evaluated overflow abatement control options for the IOAP centered on managing risks to these community values. In particular, MSD’s technical team analyzed each project alternative considered for the IOAP in terms of potential benefits and costs, where “benefits” are quantified using the anticipated reduction in risks to the community values, and “costs” reflect the total capital and operational costs of the alternative. The benefit-cost analysis influences the selection of site-specific abatement approaches or technologies, site-specific levels of protection (within the boundary conditions for CSOs and SSOs described below), and the relative priority of projects for implementation.

In developing the 2012 IOAP Modification, MSD continued to use the same benefit-cost analysis approach for alternative selection, level of control analysis, and project prioritization. The technical team maintained close contact with the WWT Stakeholder Group, and met with them during development of the modifications to ensure that the intent of the decision making process was adhered to.

Several of the WWT’s community values relate to financial considerations, including the cost-effectiveness of individual solutions and the program as a whole (financial stewardship), the

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

affordability of the program's total costs for the community (economic vitality), and how the costs are allocated among different segments of the population (financial equity). The WWT used the results of the values-based benefit-cost analysis of project alternatives to provide context to discussions about the appropriate level of investment in the IOAP.

The WWT's discussions about total program costs and the selection of projects for the IOAP have considered, as directed in EPA's CSO Control Policy, a "knee of the curve" analysis to determine where the increment of pollution reduction achieved in the receiving water diminishes compared to the increased costs (59 Code of Federal Regulations {CFR} 18688). In addition to this analysis, the community's level of investment in the IOAP has been considered in the context of anticipated future requirements and other needs for MSD services, including stormwater compliance needs associated with Louisville Metro's MS4 stormwater permit and requirements to meet the forthcoming total maximum daily load (TMDL) allocations for Beargrass Creek. This consideration of other water quality investment needs is important since sewer overflow control alone will not be sufficient to meet water quality standards.

The technical team's analysis of the IOAP according to the WWT's programmatic values yielded the following conclusions.

Customer Service: The IOAP ensures service continuity by eliminating several small WQTCs and pump stations and by incorporating redundant equipment and standby generators in the proposed projects. Odor control guidelines have been consistently applied across all projects. Most storage basins proposed in the IOAP will be covered to minimize odors. Other storage basin and pump station improvement projects incorporate odor control equipment.

Economic Vitality: MSD's current rates are near the national average. The anticipated annual rate increases of 5 to 6.5 percent are consistent with initial estimates of program costs, and they include allowances for future MSD programs as well as IOAP implementation. Even with these rate increases, MSD's rates are anticipated to remain at or near the national average, assuming other communities face similar inflation and regulatory pressures. These estimates are based on current data; many unknown factors (such as, bond market, construction market conditions, etc.) will also affect future rates.

Education: Education is an integral and essential component of the IOAP. It supports a number of IOAP objectives, including promoting and sustaining participation in green infrastructure and source control efforts, and building a sense of personal responsibility and support for clean water initiatives.

Environmental Justice and Equity: The site selection process followed uniform criteria across the county, with most solutions placed near overflow points and with no homes or private businesses permanently displaced. Furthermore, the configuration of facilities was based on a uniform application of written design criteria and odor control criteria. Other nuisance conditions, such as noise, dust, and traffic disruptions will be minimized during the design and construction phases of projects.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Financial Equity: MSD's rate structure is based on a cost-of-service model tempered by consideration of customers' ability to pay. The rate increases proposed to fund the IOAP and other MSD programs will continue to be based on the cost of service, but the MSD Board supports the existing low income, senior citizen discount program, and has discussed the possibility that this discount program be expanded. The MSD Board also implemented subsidies and incentives for green infrastructure and inflow and infiltration (I/I) control based on their business value for overflow abatement.

Financial Stewardship: As described above, the IOAP is based upon a rigorous benefit-cost analysis that considered a broad range of technology alternatives and different levels of control that met or exceeded regulatory guidelines. The "knee of the curve" evaluations of IOAP projects demonstrated that the IOAP provides a high level of control, but does not exceed the point of diminishing returns.

As noted previously, the WWT included a diverse group of community stakeholders. This WWT Stakeholder Group included 20 community opinion leaders from local government, industry WWT environmental advocacy groups, education, public health and many other areas of interest. The Stakeholder Group played a key role in developing the framework for alternative evaluation, selection, and prioritization. Prior to final submittal of the IOAP, the WWT Stakeholder Group developed a memorandum expressing support for the IOAP. This WWT Support Memorandum is attached at the end of this Executive Summary (Attachment 1). The support from the WWT Stakeholder Group is based on their understanding of the plan as represented by an "IOAP Vision." The IOAP Vision is also attached at the end of the Executive Summary (Attachment 2). The WWT Stakeholder Group continues to meet and provide input relative to IOAP implementation. They also had the opportunity to review the 2012 IOAP Modifications, and developed a similar memorandum expressing support for this submittal. The updated WWT Support Memorandum was approved by the WWT Stakeholder Group on January 30, 2013. This Memorandum is included at the end of the Executive Summary as Attachment 3.

### **Control Levels for CSOs and SSOs**

Under the CWA, CSOs are permitted discharges in wet weather, as long as they are managed to avoid degradation of water quality in the receiving streams. EPA's CSO Control Policy<sup>1</sup> has guidelines for establishing abatement targets for CSOs, one of which is the presumptive approach of establishing controls that provide for the elimination or capture and treatment of at least 85 percent of wet weather combined sewage. Under this approach, CSOs are presumed to be adequately controlled to comply with water quality standards. Regardless of the approach

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<sup>1</sup> EPA's Combined Sewer Overflow Control Policy is available at <http://cfpub1.epa.gov/npdes/cso/cpolicy.cfm>.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

that the community follows to establish abatement targets, implementation of the plans should provide that CSOs, in the absence of other loads, do not by themselves cause a violation of water quality standards.

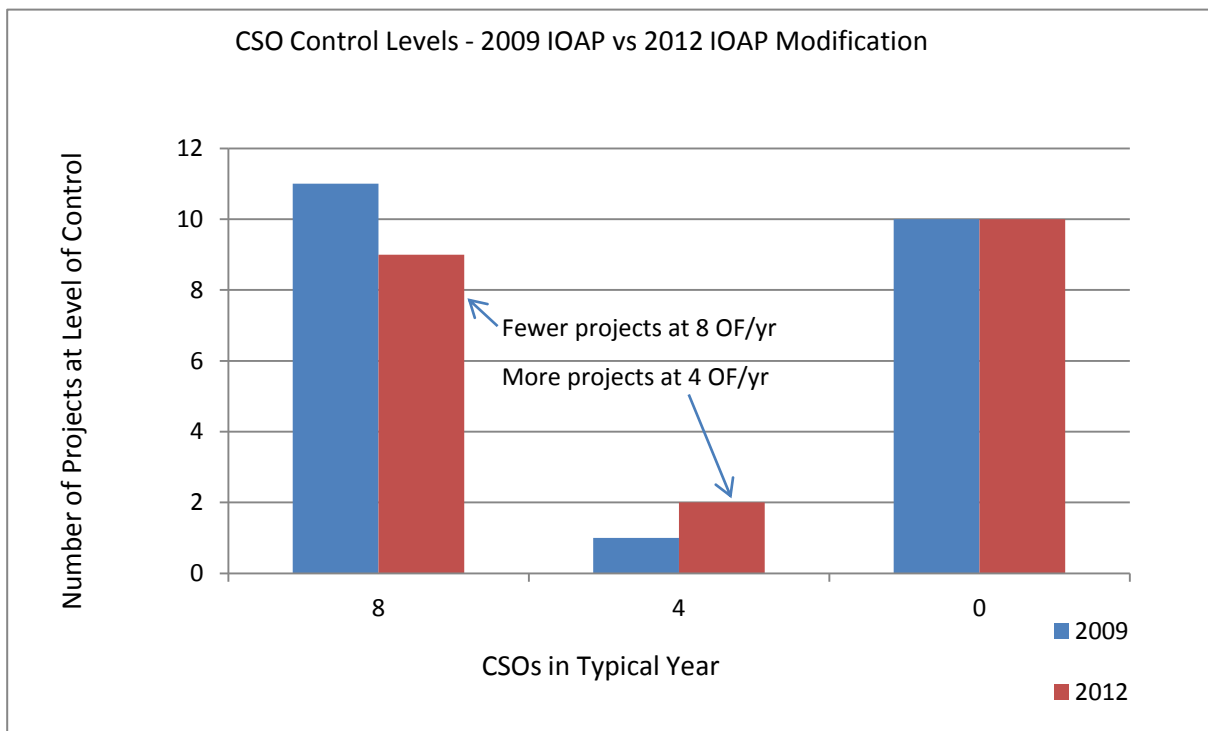
Using the values-based performance evaluation and risk management decision process described previously, MSD has elected to provide a level of CSO control that greatly exceeds EPA's presumptive approach of 85 percent capture of wet weather combined sewage. This level of overflow control represents a 96 percent capture of wet weather combined sewage, and an 85 percent reduction in overflow volumes as compared to 2008 levels.

CSO projects in the 2012 IOAP Modification have the following levels of control:

- Ten projects result in no overflows in a typical year; these locations would only overflow as a result of very large storms.
- Two projects would result in four overflows per year in a typical year.
- Nine projects result in eight overflows per year in a typical year.

Figure ES.4 below illustrates the improvement in level of protection offered by the projects of the 2012 IOAP Modification as compared to the 2009 approved IOAP.

**FIGURE ES.4**





Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

MSD's strategy for SSO control reflects the fact that SSOs, unlike wet-weather CSOs, are considered to be unauthorized discharges that must be eliminated according to EPA. Given the variable impacts of rainfall on sewage flows, elimination of unauthorized discharges must be framed in the context of a "design storm" that will be community-specific.

In the IOAP, the values evaluation framework has been used to evaluate a range of site-specific design storms to establish the appropriate level of control of SSOs. Consistent with an analysis of sixty years of historical weather patterns for Louisville Metro, the IOAP uses a three-hour "cloudburst" storm, with a statistically anticipated rainfall of 1.82-inches, as the minimum design storm considered. There is a 50 percent probability that a storm this large will occur in this area in any given year. The Cities of Atlanta, Cincinnati, and Knoxville used similar statistically probable design storms as the minimum protection level for SSO control. The approach of using the values evaluation framework to determine the SSO control level means that solutions to address certain SSOs have been designed to protect against larger storms (such as, a 2.25-inch cloudburst storm instead of a 1.82-inch cloudburst storm) because they yield a higher benefit-cost ratio in the analysis of project alternatives.

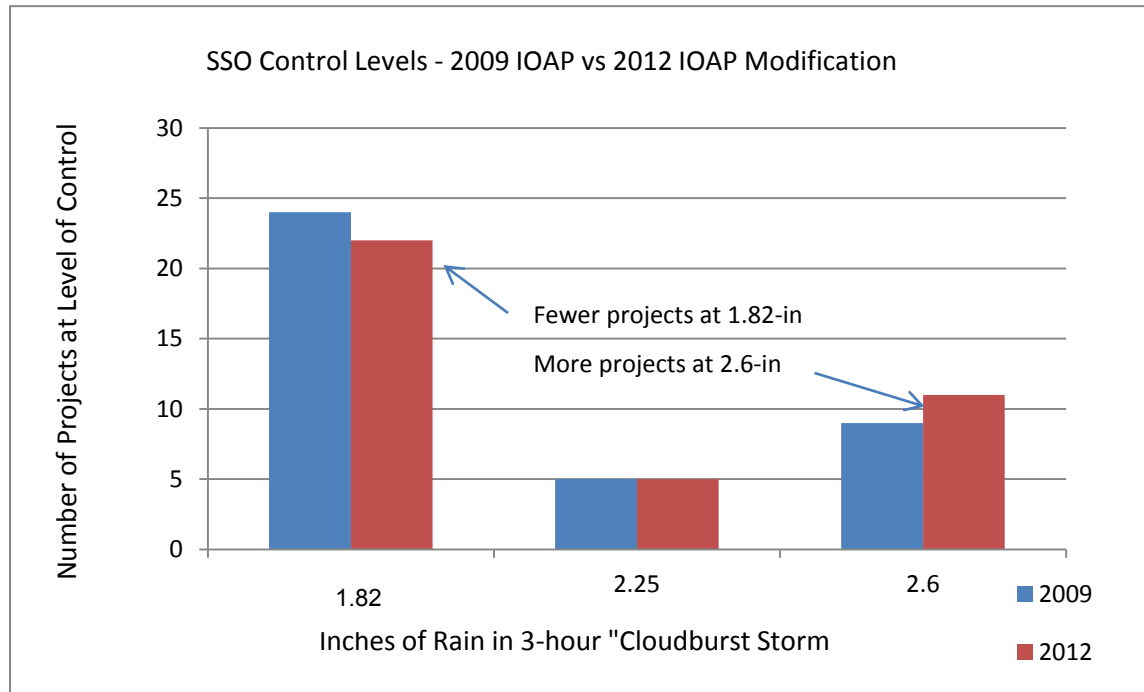
SSO projects in the 2012 IOAP Modification have the following levels of control:

- Twenty-two projects eliminate overflows up to a 1.82-inch cloudburst storm.
- Five projects eliminate overflows up to a 2.25-inch cloudburst storm.
- Eleven projects eliminate overflows up to a 2.60-inch cloudburst storm.

Figure ES.5 below illustrates the improvement in level of protection offered by the projects of the 2012 IOAP Modification as compared to the 2009 approved IOAP. Note that SSES projects are not included in this level of control analysis.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE ES.5**



**COMPONENTS OF MSD’S INTEGRATED OVERFLOW ABATEMENT PLAN**

Control options in the IOAP, known as the IOAP toolkit, include source control such as green infrastructure and I/I reduction efforts, storage, conveyance/transport, treatment, and sewer separation. MSD’s technical team used the benefit-cost tool to compare the project alternatives and program elements considered for inclusion in the IOAP. The specific mix of control options for individual CSO or SSO locations in the IOAP is driven by the benefit-cost analysis of how the project alternatives affect the WWT’s community values and site-specific considerations. Project alternatives are built around MSD’s existing infrastructure such as large diameter pipes and WQTCs and draw on synergistic benefits from other MSD projects (for instance the Interim SSDP projects). Furthermore, project budgets include an enhanced site restoration allowance to fund localized opportunities to reduce historical overflow impacts on aquatic and riparian environments near the sites of overflow abatement projects.

**Green Infrastructure and Gray Solutions, Initiatives and Programs in the Final CSO LTCP**

Driven by the values-based benefit-cost analysis, the IOAP reflects a balanced mix of green infrastructure and gray solutions to prevent and control sewer overflows. “Green infrastructure” solutions include options such as vegetated roofs, rain gardens, rain barrels, porous pavement, and bioretention, while “gray” solutions include options such as storage, treatment, conveyance/transport, and sewer separation. As a guiding principle, MSD’s IOAP has been developed based on front-end consideration of source control and green infrastructure. This means that more traditional “gray” infrastructure in the IOAP has been sized after considering both (1) the anticipated flow-reduction benefits of programmatic and site-specific green infrastructure solutions and (2) the anticipated effectiveness of other source control approaches, including reduction of private sources of I/I.

Green solutions in the IOAP will be implemented as soon as possible, to allow data to be gathered on the flow reduction benefits that occur. Approximately 17 percent of the Final CSO LTCP budget is allocated to green infrastructure, and most of that is planned to support projects in the first six years of IOAP implementation. Prior to the final design of supporting gray solutions, the actual flow reduction performance will be documented and compared against the estimated targets. The final sizing of the gray solutions will then be based on actual documented performance of green infrastructure solutions, as well as any further green and source control investments justified by performance information. Green infrastructure investments are estimated to reduce the initial costs of CSO gray infrastructure projects by \$40 million; potential future savings could double or triple this amount. A more detailed discussion of the green infrastructure program is presented in Volume 2.

Table ES.3 shows the 22 gray infrastructure projects to control CSOs defined in the IOAP.

**TABLE ES.3**  
**GRAY INFRASTRUCTURE PROJECTS TO CONTROL CSOS (2012 MODIFICATION)**

Number of Projects	Project Type
3	Sewer separation projects
14	Storage basin projects includes in-line and off-line storage. Most in-line storage projects have a RTC component
1	Replacement and expansion of the Nightingale Sanitary Pump Station
2	Conveyance expansion projects
1	“Green infrastructure only” project (with one other under consideration)
1	One high-rate wet weather treatment (screening, settling, and disinfection) with in-line and off-line storage.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

In addition to these 22 CSO control projects, MSD will implement five projects at flood pump stations. These projects will eliminate a major cause of dry weather overflows related to operation of the flood pump stations in compliance with the U.S. Army Corps of Engineers (USACE) Flood Protection System Pumping Operations Manual.

### **Green Infrastructure Program**

The IOAP includes both an annual Green Infrastructure Program and an initial set of green infrastructure demonstration projects. The Green Infrastructure Program is front-end loaded to maximize benefits on downsizing future gray infrastructure. For example, the IOAP project schedule calls for a \$40 million investment in green infrastructure programs and projects during the first six years.

Programmatic green infrastructure components in the IOAP include a downspout disconnect program, green roof construction subsidies or incentives, green roads and alleys partnership incentives, and pervious pavement sidewalks and parking. MSD has based the proposed incentives and subsidies on a “business case” analysis of the financial benefit of green infrastructure in terms of costs per gallon of flow removed from the CSS. Through the anticipated green infrastructure partnership, incentive, and education programs, MSD’s initial \$40 million investment in green infrastructure has the potential to leverage \$60 million more from other private and public funding sources, thereby yielding up to \$100 million in green infrastructure projects.

MSD plans to construct a series of new green infrastructure demonstration projects across Louisville Metro. The proposed green infrastructure projects in the CSS area will be part of MSD’s IOAP, while the proposed green infrastructure projects outside the CSS area will be a part of the community’s MS4 stormwater program and not a part of this IOAP. These demonstration projects are designed to achieve three main objectives: (1) improve water quality and reduce sewer overflows, (2) provide data on green infrastructure effectiveness, and (3) educate the community about the value and benefits of green infrastructure.

All proposed green infrastructure demonstration projects will incorporate a monitoring component, so that the effectiveness of the pilot projects can be regularly tracked. Project reports will document lessons learned and successes and be the mechanism for reporting to regulators and the public. MSD will use these monitoring results to guide future IOAP implementation, under the IOAP’s adaptive management plan (further described below).

This IOAP vision currently reflects a minimum commitment to 19 green infrastructure demonstration projects. A complete list of demonstration projects completed and other green infrastructure projects completed and underway as of October 2012 can be found in Volume 2, Chapter 5. Source Control and Gray Solutions, Initiatives and Programs in the Final SSDP.

Similar to the integrating of green infrastructure with gray infrastructure in the Final CSO LTCP, MSD will implement an annually-funded I/I reduction program to reduce clear water intrusion

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

into the sewers. I/I is one of the main causes of SSOs, so eliminating the source can be an effective way of reducing SSOs. To be effective, an I/I elimination program must deal with collection system defects in both the public and the privately owned portions of the sewer system. MSD’s program includes an active private side I/I reduction approach currently implemented through voluntary, subsidized programs.

Prior to the final design of supporting gray solutions, the actual flow reduction performance from source control programs will be documented and compared against the estimated targets. The final sizing of the gray solutions will then be based on actual documented performance of source control solutions. Approximately 15 percent of the Final SSDP budget is allocated to I/I reduction and other source control programs. In addition, the Final SSDP includes eight specific I/I reduction projects targeting overflows that appear to be controllable through source control alone.

Table ES.4 shows the technology components of the 47 gray infrastructure projects to control SSOs defined in the Final SSDP. Note that some projects have multiple components, so those projects will be counted in more than one category.

**TABLE ES.4**  
**GRAY INFRASTRUCTURE PROJECT COMPONENTS TO CONTROL SSOS (2012 MODIFICATION)**

Number of Projects Including Component	Project Type
19	Conveyance capacity upgrades and interceptor relief projects
9	Storage projects (in-line and off-line storage, many with pipe upgrades also)
13	Pump station upgrades or replacements.
12	Pump Station eliminations
7	Small WQTC eliminations including 5 in the Prospect Area
<p><b>Note:</b> Final SSDP projects also include the potential elimination of the Jeffersontown WQTC. Interim SSDP projects include the replacement of the SSS in the Beechwood Village area, the decommissioning of the Highgate Springs Pump Station, construction of an interceptor to eliminate pumped overflows in the Hikes Point area, construction of a relief sewer and a diversion interceptor to route wet weather flows to the Derek R. Guthrie WQTC (formerly known as the West County Wastewater Treatment Plant), and an expansion of the wet weather capacity of the Derek R. Guthrie WQTC.</p>	

### Control of Private Sources of I/I

MSD’s technical team analyzed methods to control private sources of I/I into the SSS and proposed several potential options. This analysis indicates that private-side I/I control must be an essential part of the IOAP implementation, because it will reduce the overall anticipated costs of overflow abatement.

Private source options include mitigating building laterals, downspouts, sump pumps, and foundation drains. The technical team also analyzed options requiring inspections of private properties. The required inspection options include: during the property transfer process, when building permits are issued, when contractors install roof and gutter systems, when plumbers connect sump pumps, and/or at other times. MSD would seek some form of cost share as well as conduct an aggressive education campaign. The MSD Board approved changes to the Wastewater and Stormwater Discharge Regulations that allow MSD to take specific action in this regard. MSD will develop specific policies to guide implementation of these measures.

### **Public Information, Education, and Involvement Program**

Education and public involvement are critical to the long-term implementation success of the IOAP. MSD uses the term “Project WIN” (Waterway Improvements Now) to describe its Consent Decree response activities to the public.

The ongoing public information, education, and involvement program for Project WIN is designed to accomplish the following objectives:

- Generate a sense of personal ownership and responsibility for clean water;
- Promote and sustain participation in critical voluntary programs in the IOAP, including private-side I/I control and green infrastructure;
- Promote public acceptance and support for the financial investments required to achieve consent decree and CWA compliance; and
- Encourage support for other agency programs or legislation that supports overflow abatement efforts.

To achieve these objectives, the Project WIN education and public involvement program uses a wide range of communication media. These public involvement efforts are focused on several key audiences; including property owners, schools and children, and target groups such as, project neighborhoods, builders, and restaurants. Focusing education efforts on children is important to ensure the long-term sustainability of voluntary programs in the IOAP. MSD uses five key messages to promote Project WIN:

1. Value clean water.
2. Your investment is paying dividends, and our water is getting cleaner.
3. Protecting public health is critically important.
4. MSD and many community partners are working hard to improve water quality.
5. You can make a difference in improving water quality.



## **Post-Construction Compliance Monitoring**

MSD's IOAP will use an adaptive management implementation approach based on monitoring and evaluation efforts. MSD's post-construction compliance monitoring and evaluation plan for the IOAP includes: (a) water quality monitoring, (b) sewer flow monitoring, (c) overflow events analysis, (d) gray and green infrastructure project performance monitoring, and (e) measurement of the effectiveness of source control and behavior-change efforts. A part of the post-construction compliance monitoring program will be a periodic recalibrating of sewer system models that will support project performance evaluation and resultant project re-sizing based on monitoring results.

In 2011, MSD took advantage of four more years of flow monitoring data to perform a planned recalibration of the hydraulic models used to develop, evaluate, and design overflow abatement projects. As a result of this recalibration MSD found opportunities to revise the proposed suite of projects, providing increased levels of overflow abatement, faster, and for approximately the same cost. The 2012 IOAP Modification incorporated herein describes the project changes in technology, size, and schedule, and the resultant benefits of making those changes.

MSD will continue to adapt the CSO management and SSO elimination approaches based on the monitoring and evaluation results. Adjustments may include recalibrating models, "right-sizing" gray solutions, reevaluating the effectiveness of green solutions, and adjusting the types and characteristics of projects planned for later phases of implementation, supplementing existing control projects with additional storage or conveyance, and including additional investments in green infrastructure or source control beyond those proposed in the initial program. At this time, there is recognition that historical weather trends may not be as reliable as in the past due to potential changes in the climate. The IOAP's adaptive management approach will allow MSD to continue to monitor rain events and weather pattern developments and adjust its plans as more technical data become available.

## **Future Development Considerations**

Solutions in the IOAP consider future development based on the community's long-term landuse plan, Cornerstone 2020.<sup>2</sup> IOAP solutions are designed to accommodate the anticipated impacts of population growth and landuse development. The solutions consider the effects of growth on connections to existing infrastructure that is upstream from existing overflow points. However, the IOAP is not intended to provide capacity for all future growth that is predicted by Cornerstone 2020. Cases where the growth outlined in Cornerstone 2020 would logically be provided by new infrastructure and is not hydraulically dependent on or connected

<sup>2</sup> For more information about the Cornerstone 2020 plan, see [www.louisvilleky.gov/PlanningDesign/Cornerstone+2020.htm](http://www.louisvilleky.gov/PlanningDesign/Cornerstone+2020.htm).

to the IOAP solution, have not been considered part of the IOAP. Moreover, the IOAP solutions are designed and sized to account for the impacts of anticipated growth on existing infrastructure, but the IOAP itself is not intended to build the capacity needed for growth.

### **IOAP Funding Plan**

To meet the requirements of the Consent Decree, the funding plan is designed to cover the IOAP capital projects that will be constructed to improve MSD's sewer infrastructure. The IOAP funding plan is based on the following four principles:

1. Rates and fees for the IOAP must pay MSD's operating costs and debt service.
2. MSD's current bond rating (AA) should, at a minimum, be maintained.
3. Rates and fees should allow for continued economic development in the community and a strong local economy.
4. Rates must be affordable for MSD's customers.

For IOAP implementation, these funding plan principles affect the amount of money MSD may borrow at one time and the level of increases in rates and fees needed to fund capital and operating expenses.

MSD will fund the IOAP primarily through a combination of annual rate increases and bond issues or other loans. MSD also plans to pursue grants, line-item appropriations, and public/private partnerships (e.g., recapture agreements) to help pay for capital construction costs, as appropriate; however, the funding plan is not built around these funding sources since they are less certain. By estimates, the Consent Decree will cost \$843 million in capital expenditures; as a result, average sewer bills for residential customers are expected to increase from 5.5 to 6.5 percent annually through 2025. Due to the Consent Decree capital construction expenses, this means that the average monthly residential sewer and Consent Decree surcharge bill would increase from \$29.58 in 2008 to approximately \$77.42 by 2025. Along with these rate increases, MSD expects to borrow approximately \$938 million between 2009 and 2025 based on the estimates of capital costs; this would increase MSD's debt service payments from \$94 million annually to \$127 million annually by 2025, assuming interest rates at four percent for new issues. A mixture of fixed and variable rate borrowings is anticipated. These rate increases and loans would be used to address both IOAP construction costs and other MSD capital needs for infrastructure renewal, replacement, and expansion.

Estimates of IOAP costs appear to be within the community's ability to pay, as indicated by affordability analysis completed using EPA guidelines. MSD recognizes, however, the rate increases could nevertheless be difficult for some segments of the population to afford, especially in the context of other living expenses. For this reason, the WWT considered potential discount options to customers that face financial hardship. The MSD Board adopted a

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

discount program for low-income senior citizens that provided over \$600,000 of rate assistance in FY 2012. The MSD Board has also considered other discount programs for other impacted groups, but has not implemented them at the time of this 2012 IOAP Modification preparation.

As noted above, MSD will construct the capital projects to meet the regulatory requirements of the Consent Decree and achieve compliance with the CWA. Many of the elements of the IOAP—including the Project WIN education program, operations and maintenance of IOAP projects, and monitoring and evaluation programs—will also continue past the construction phase of the IOAP. MSD is committed to making sure that the IOAP programs and projects provide for long-term improvements in water quality in Louisville Metro.

### **An Approvable IOAP**

MSD has developed the IOAP in conformance with the Consent Decree, the CSO Control Policy, and other applicable regulations. The following presents the “road map” of compliance factors for both the Final CSO LTCP and the Final SSDP.

### **An Approvable Final CSO LTCP**

The MSD Final CSO LTCP as submitted on June 19, 2009, is fully compliant with the Consent Decree and the requirements of the CSO Policy. This 2012 IOAP Modification provides a higher level of CSO control and a lower final residual AAOV, confirming that it is also fully compliant with the Consent Decree and the CSO Control Policy. MSD’s water quality compliance approach is based on EPA’s Demonstration Approach in that water quality modeling demonstrates that both Beargrass Creek and the Ohio River would be in full compliance with existing water quality standards if all background loads were removed. The IOAP projects, when fully implemented, are projected to capture 96 percent of the wet weather combined sewage generated in the service area. This flow will be treated with at least the equivalent of primary clarification, control of solids and floatables, and disinfection. The innovative and site-specific approach includes implementation of green infrastructure and public education. The Final CSO LTCP is also fully compliant with the three goals required in the Consent Decree [paragraph 25. (b) (2) A (i); (ii) and (iii)].

Both the Consent Decree and the CSO Policy require specific elements of the Final CSO LTCP as noted in the Table ES.5; MSD has fully complied with both the Consent Decree and the CSO Policy through the full inclusion of each of these elements in the Final CSO LTCP.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE ES.5**  
**FINAL CSO LTCP ELEMENTS AS REQUIRED BY THE CONSENT DECREE**

Requirement Per Consent Decree Paragraph 25 (b) (2)	IOAP and Final CSO LTCP Chapters and Sections	Compliance with CSO Policy and Consent Decree
(i) Results of characterization, monitoring, modeling activities and design parameters as the basis for selection and design of effective CSO controls (including controls to address those discharges resulting from MSD’s compliance with the requirements of the USACE Ohio River Flood Protection System Pumping Operations Manual, dated 1954 and revised 1988).	Volume 2 - Final CSO LTCP: Chapter 2 for an evaluation of the controls to address flood pumping issues, Chapter 3 for the alternative analysis Chapter 4 and 5 for the selection of effective CSO Controls including modifications to the flood pumping system, where required, to implement revised operating procedures at the flood pump stations.	<b>Yes</b> – the proposed plan is based on an extensive process in which every alternative accounted for data and was reviewed by WWT.
(ii) Results of an evaluation of WQTC peak flow treatment capacity for any WQTC other than the Morris Forman WQTC that will receive additional flow based on any LTCP project. Such evaluation shall be consistent with the EPA publications “Improving POTW Performance Using the Composite Correction Approach and “Retrofitting POTWs”	No existing treatment plants other than the Morris Forman WQTC will receive any additional flow as a result of the Final CSO LTCP. Volume 2, Chapter 3.3 Evaluation of CSO Control Alternatives; Table 3.1.1 shows treatment alternatives; Chapter 3.2.7.5 Utilization of Morris Forman WQTC; Chapter 3.2.7.5 Satellite treatment alternatives; Table 3.3.1.	<b>Yes</b> – peak flow treatment capacity will be available with use of storage, real time control (RTC), and treatment.
(iii) Report on the Public Participation Process	Volume 1 - IOAP, Chapter 3	<b>Yes</b> – the WWT and the general public were actively involved in the decision making to select the long-term CSO controls.
(iv) Identification of how the LTCP addresses sensitive areas as the highest priority for controlling overflows	Volume 2, Chapter 1.6.6.7; Chapter 2.8; and Chapter 3.2.7.6.	<b>Yes</b> – while all receiving waters considered in the Final CSO LTCP are categorized sensitive under CSO Policy criteria, MSD performed further prioritization of stream reaches based on ecological characteristics.
(v) Report on the cost analyses of the alternatives considered	Volume 1, Chapter 2 Volume 1, Chapter 6 presents rate and affordability impacts Volume 2, Chapter 3.3.2, and Chapter 4 and 5.	<b>Yes</b> – application of cost to community value framework for a cost-benefit and a knee of the curve analysis were part of the development of project alternatives and choices. Affordability and phases were also accounted in the development of the schedule.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE ES.5**  
**FINAL CSO LTCP ELEMENTS AS REQUIRED BY THE CONSENT DECREE**

Requirement Per Consent Decree Paragraph 25 (b) (2)	IOAP and Final CSO LTCP Chapters and Sections	Compliance with CSO Policy and Consent Decree
(vi) Operational plan revisions to include agreed upon long term controls	Volume 1, Chapter 6	<b>Yes</b> – operational plan budgets adequate resources to operate and maintain the Final CSO LTCP projects.
(vii) maximization of treatment and evaluation of treatment capacity at Morris Forman WQTC	Volume 2, Chapter 3.2.7.5 Utilization of Morris Forman WQTC Chapter 3.3 Evaluation of CSO Control Alternatives Appendix 3.2.20 Morris Forman WQTC Wet Weather SOP Procedures Appendix 3.2.21 Morris Forman WQTC Expansion Tech Memo;	<b>Yes</b> – Wet Weather flow capacity has been maximized and verified through extensive testing. Additional peak flow treatment capacity will be available with use of storage, RTC and a new retention treatment basin.
(viii) Identification of an implementation schedule for the selected CSO control	Volume 2, Chapter 4 and 5, Final CSO LTCP and selected Project Final Recommended Project List	<b>Yes</b> – All projects completed by Consent Decree deadline of December 31, 2020.
(ix) A post-construction compliance monitoring program adequate to verify compliance with water quality-based CWA requirement and ascertain the effectiveness of CSO controls	Volume 1 Chapter 6.5.	<b>Yes</b> – a full suite of monitoring will be implemented in order to determine efficacy and adapt plan as appropriate.

## **An Approvable Final SSDP**

The MSD Final SSDP as submitted on June 19, 2009, is fully compliant with all the requirements of the Consent Decree under paragraph 25 (a) (3) A. and B, as shown in Table ES.6. The 2012 IOAP Modifications provide a higher level of control (as indicated by the design events used for project sizing) and is therefore also fully compliant with the Consent Decree. The combined, sustained and phased implementation includes both a gray infrastructure plan and a source control program including a private sewer program intended to reduce I/I. This SSDP, in conjunction with the Sewer Overflow Response Protocol (SORP) and public education aimed at individual responsibility and behavior modification (as it relates to fats, oil and grease {FOG}, private sewer maintenance and rehabilitation and illicit cross connections and drainage) will eliminate unauthorized discharges from the SSS, CSS and WQTCs by December 31, 2024.

In addition, the Consent Decree requires that the results of an evaluation of the WQTC peak flow treatment capacity for any WQTC that will receive additional flow based on any Interim SSDP or Final SSDP project. These analyses were fully developed and can be found in Volume 1, Chapter 4.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE ES.6**  
**FINAL SSDP ELEMENTS AS REQUIRED BY THE CONSENT DECREE**

Requirement Per Consent Decree Paragraph 25(a)(3)	IOAP and Final SSDP Chapters and Sections	Compliance With Consent Decree
(3) The long-term SSDP projects, including schedules, milestones, and deadlines	Volume 1 – IOAP, Chapter 4.3, Chapter 6.3; Volume 3 – Final SSDP, Chapter 4 1 and Chapter 5.	<b>Yes</b> – The Final SSDP describes 41 gray infrastructure projects, I/I reductions studies, and a source control program to eliminate 214 documented, suspected, and modeled SSOs. The project schedule shows milestones and completion dates for each of these projects.
(3) Results of an evaluation of WQTC peak flow treatment capacity for any WQTC that will receive additional flow based on any Interim or Final SSDP project. Such evaluation shall be consistent with the EPA publications “Improving POTW Performance Using the Composite Correction Approach and “Retrofitting POTWs”	Volume 1, Chapter 4.4	<b>Yes</b> - All the plants that could receive additional flow as a result of SSO elimination have been evaluated.
(A) A map that shows the location of all known Unauthorized Discharges. The map shall include the areas and sewer lines that serve as a tributary to each Unauthorized Discharge. Smaller maps of individual tributary areas also may be included to show the lines involved in more detail.	Volume 3 – Final SSDP, Chapter 2.5, Figures 2.5.3 through 2.5.15.	<b>Yes</b> – The network branch maps show all 214 SSOs, with sufficient detail to see tributary sewers.
(B.i) A description of each Unauthorized Discharge location that includes the frequency of the Unauthorized Discharge	Volume 3 – Final SSDP, Appendix 4.5.1 - SSO Fact Sheets as well as in the Project Fact Sheets.	<b>Yes</b> – Discharge location as well as frequency is listed for each individual documented SSO in Appendix 4.5.1. Additionally, discharge location is located in the Project Fact Sheets.
(B.ii) The annual volume released from the Unauthorized Discharge	Volume 3 Final SSDP, Appendix 4.5.1 - SSO Fact Sheets.	<b>Yes</b> – Total annual volume is listed for each individual documented SSO in Appendix 4.5.1.
(B.iii) A description of the type of Unauthorized Discharge location	Volume 3 Final SSDP, Chapter 2.4, Table 2.4.2 as well as in the Project Fact Sheets.	<b>Yes</b> – Table 2.4.2 contains this information and in the Project Fact Sheets.
(B.iv) The receiving stream	Volume 3 Final SSDP, Chapter 2.4, Table 2.4.2 as well as in the Project Fact Sheets.	<b>Yes</b> – Table 2.4.2 contains this information and in the Project Fact Sheets.
(B.v.) The immediate and downstream land use, including the potential for public health concerns	Volume 3 – Final SSDP, Chapter 2.2.1, Appendix 4.5.1 - SSO Fact Sheets	<b>Yes</b> – Descriptions of the WQTC service areas describe landuse and the history of sewer system development in the area. Downstream landuse acreage is listed for each individual documented SSO in Appendix 4.5.1

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE ES.6**  
**FINAL SSDP ELEMENTS AS REQUIRED BY THE CONSENT DECREE**

Requirement Per Consent Decree Paragraph 25(a)(3)	IOAP and Final SSDP Chapters and Sections	Compliance With Consent Decree
(B.vi) A description of any previous (within the last 5 years) current, or proposed studies to investigate the Unauthorized Discharge	IOAP Volume 3 – Final SSDP, Chapter 1.3.	<b>Yes</b> – Chapter 1 summarizes MSD’s previous and current SSO elimination efforts.
(B.vii) A description of any previous (within the last 5 years) current or proposed rehabilitation or construction work to remediate or eliminate the Unauthorized Discharge	Volume 3 – Final SSDP, Chapter 1.3. Chapter 2.2 and 2.3.	<b>Yes</b> – Chapter 1 summarizes MSD’s previous rehabilitation efforts. In Chapter 2, The descriptions of the WQTC service areas include summary descriptions of previous construction work, and the descriptions of the model development describes those on-going or currently planned projects that contribute to SSO elimination.
(C) A prioritization of Unauthorized Discharge locations based on the frequency, volume, and impact on the receiving stream and upon public health, in coordination with CMOM programs	Volume 1, Chapter 6.3, Volume 3 – SSDP Chapter 4.2.1.	<b>Yes</b> – The referenced chapters describe the schedule prioritization process, based in part on the benefit-cost ratio that includes the required parameters in the benefit calculation.
(C) Schedules for design and construction, phased based on sound engineering judgment, and in no case extending beyond December 31, 2024	Volume 1, Chapter 6.3, Volume 3 Final SSDP, Chapter 4.2 and Chapter 5.	<b>Yes</b> – Schedules are included that show the required phases, and this schedule shows completion by December 31, 2024.
(D) A plan to involve stakeholders in the planning, prioritization and selection of projects.	Volume 1, Chapter 3.2, Volume 3 – Final SSDP, Chapter 4.3	<b>Yes</b> – The IOAP included a robust stakeholder involvement process that included participation in decisions on selection and prioritization of projects.

## **“NO SURPRISES” FOR APPROVING AGENCIES**

Throughout the development of the IOAP, meetings were scheduled with those regulatory agencies having jurisdiction over the program to facilitate open communication between MSD and the regulators regarding progress and compliance with Consent Decree requirements. Electronic reporting updates requested by KDEP and EPA have been developed and implemented to provide current information. Additionally, reports are prepared for each of the four quarters of the calendar year and are submitted to EPA and KDEP within 30 days of the end of the new quarter and are posted on MSD’s Project WIN website in Library section for public review. These reports include specific information about activities consistent with the requirements of the Consent Decree and the progress toward the development of the Final CSO LTCP.

In addition to these reports, MSD initiated periodic face-to-face meetings with technical team members from the KDEP and EPA to discuss the progress of the Project WIN Overflow Abatement Program. The intent of these meetings was to ensure that there are no surprises when the IOAP was submitted, and that the IOAP met all the parameters to allow approval.

## **SUPPORTING INFORMATION**

Attachment 1 WWT Support Memorandum

Attachment 2 IOAP Stakeholder Group Vision

Attachment 3 Updated WWT Support Memorandum January 30, 2013



# Tables

## ES.1 and ES.2



TABLE ES.1 2012 FINAL LTCP PROJECT SUITE

ACD Project Number	Project Name	Receiving Stream	2009 Overflows Controlled	2009 Level of Control	2009 Size (MG)	2009 Cost	2012 Overflows Controlled	2012 LOC	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
L_OR_MF_172_S_09B_B_A_0	Adams Street Sewer Separation	Ohio River	CSO172	0	0.12	\$983,000	CSO172	0	Sewer Separation	\$20,000	12/31/2012	12/31/2012	Project modification request to revise this project to a sewer separation has been previously submitted and accepted. Upon inspection of the sewer system, all but two catch basins were found to have been separated already during recent redevelopment. Project Completed - Monitoring Ongoing
L_OR_MF_058_S_08_A_A_0	CSO058 In-line Storage and Green Infrastructure	Ohio River	CSO058	0	Sewer Separation	\$1,361,000	N/A	8	Weir Modifications As Part of 13th & Rowan Solution	N/A	12/31/2014	12/31/2014 (Weir Modification) 12/21/2020 (w/ 13th & Rowan Solution)	The overflow from this CSO will be addressed in the 13th & Rowan storage basin. Modeling indicates that the overflow is caused by interceptor surcharging. Separation of the small drainage area upstream of the CSO would be ineffectual. Weir modifications for CSO058 will be performed in 2014. Costs associated with modifications and CSO058 are included in the 13th & Rowan solution.
L_SO_MF_093_S_08_A_A_0	CSO093 Structural Modifications & Green Infrastructure	South Fork	CSO093	0	Sewer Separation	\$952,000	CSO093	0	Structural Modifications & Green Infrastructure	\$488,000	12/31/2015	12/31/2015	The project modification involves the re-construction of the CSO structure to replace the existing leaping weir with a more conventional overflow weir.
L_ML_MF_140_S_08_A_A_0	CSO140 In-Line Storage & Green Infrastructure Controls	Middle Fork	CSO140	0	Sewer Separation	\$3,150,000	CSO140	0	Pipe upgrade & Green Infrastructure	\$574,000	12/31/2015	12/31/2015	The project modification involves the re-construction of the CSO structure to increase the low flow line to a 42-inch diameter opening which will increase the conveyance capacity.
L_OR_MF_160_S_08_A_A_0	CSO160 In-Line Storage & Green Infrastructure	Ohio River	CSO160	0	Sewer Separation	\$237,000	CSO160	0	Inline Storage & Weir Modifications	\$231,000	12/31/2015	12/31/2015	The project modification involves the creation of in-line storage provided by a combination of raising the existing overflow weir and installing 88 feet of 72-inch diameter pipe.
L_MI_MF_127_M_09B_B_A_8	I-64 and Grinstead Drive Storage Basin**	Middle Fork	CSO125, CSO126, CSO127, CSO166	8	2.74	\$12,950,000	CSO125, CSO126, CSO127, CSO166	4	8.5 plus stormwater diversions	\$38,590,000	12/31/2014	12/31/2020	Public comments received requested serious consideration for green infrastructure utilization in the basin drainage area along with intensive public involvement. Due to the size of the drainage area and the increased size and cost of the basin, additional time is needed to evaluate green infrastructure opportunities and right-size this project appropriately.
L_OR_MF_015_M_13_B_B_8	Bells Lane Wet Weather Treatment Facility (formerly known as Paddy's Run)	Ohio River	CSO015, CSO191	8	50 MGD	\$24,940,000	CSO015, CSO191	8	50 MGD/ 25 MG Storage	\$68,472,000	12/31/2014	12/31/2016	Optimization of flow through Morris Forman's Main Diversion Structure and MSD's Real Time Control strategy added storage volume requirements. Additional time for construction is being requested due to size increase, moving the site, offline storage and integration of Southwestern Pump Station.
L_OR_MF_020_S_09B_B_A_8	Story Avenue and Main Street Storage Basin	Ohio River	CSO020	8	0.13	\$1,580,000	CSO020	8	5.42	\$12,576,000	12/31/2013	12/31/2020	Story and Main & 13th and Rowan basins are linked together functionally. Story & Main grew substantially in size due to more conservative operational assumptions for Starkey PS. MSD proposes to split out and accelerate the schedule of CRD/CSO 22/CSO 23/CSO054 projects using green infrastructure and localized storage. Additional time is requested to right size the Story/Main and 13th/Rowan basins once the impacts of green infrastructure and upstream storage are realized and monitored.
L_SO_MF_130_S_09B_B_A_8	Story Avenue and Spring Street Storage Basin	South Fork	CSO130	8	0.01	\$1,077,000	CSO130	8	Green Infrastructure	\$896,000	12/31/2016	12/31/2016	A project modification request to use a suite of green infrastructure projects in lieu of the storage basin is anticipated in early 2012. No schedule change for overflow reduction is anticipated.
L_OR_MF_155_M_09B_B_B_4	13th Street and Rowan Street Storage Basin	Ohio River	CSO022, CSO023, CSO050, CSO051, CSO052, CSO053, CSO054, CSO055, CSO056, CSO150, CSO155 and Central Relief Drain CSO's (11 total w/ AAOV)	4	14.44	\$49,680,000	CSO022, CSO023, CSO050, CSO051, CSO052, CSO053, CSO054, CSO055, CSO056, CSO058, CSO150, CSO155	8	4.36	\$27,863,000	12/31/2020	12/31/2020	MSD proposes to split CRD & 13th and Rowan projects into separate projects. The storage basin and CRD projects are proposed to remain on the same schedule. CSO 58 will also be included with this project and weir modifications for CSO 58 are included with the revised cost.
L_OR_MF_211_M_13_B_A_8	Southern Outfall In-line Storage (SOR1) at 43rd Street	Ohio River	N/A	N/A	NA	NA	CSO016/210	8	11.4	\$3,544,000	12/31/2018	12/31/2018	New stand-alone project. Optimized operating rules between Paddy's Run HRT and Morris Forman's Main Diversion Structure demonstrated that only inline storage was needed at Southern Outfall Retention 1 and Southern Outfall Retention 2. MSD proposes eliminate the Algonquin storage basin portion of the project and complete the two inline storage basins by the original completion date. Costs of the total SOR1 and SOR2 projects combined were developed with the costing tool and split evenly amongst the 2 projects in this spreadsheet.



TABLE ES.1 2012 FINAL LTCP PROJECT SUITE

ACD Project Number	Project Name	Receiving Stream	2009 Overflows Controlled	2009 Level of Control	2009 Size (MG)	2009 Cost	2012 Overflows Controlled	2012 LOC	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
L_OR_MF_211_M_13_B_A_8	Southern Outfall In-line Storage (SOR2) at 12th Street and Wilson	Ohio River	N/A	N/A	NA	NA	CSO211	8	4.7	\$3,544,000	12/31/2018	12/31/2018	New stand-alone project. Optimized operating rules between Paddy's Run HRT and Morris Forman's Main Diversion Structure demonstrated that only inline storage was needed at Southern Outfall Retention 1 and Southern Outfall Retention 2. MSD proposes eliminate the Algonquin storage basin portion of the project and complete the two inline storage basins by the original completion date. Costs of the total SOR1 and SOR2 projects combined were developed with the costing tool and split evenly amongst the 2 projects in this spreadsheet.
L_OR_MF_211_M_13_B_A_8	Algonquin Parkway Storage Basin/In-line Storage	Ohio River	CSO016, CSO210, CSO211	8	4.84	\$17,300,000	N/A	N/A	N/A	N/A	12/31/2018	Eliminated	Offline storage eliminated. Optimized operating rules between Paddy's Run HRT and Morris Forman's Main Diversion Structure demonstrated that only inline storage was needed at Southern Outfall Retention 1 and Southern Outfall Retention 2. MSD proposes to eliminate the Algonquin storage basin portion of the project.
L_SO_MF_097_M_13_A_A_8	Beargrass Creek Parallel Interceptor	N/A	N/A	N/A	N/A	\$12,994,000	N/A	N/A	N/A	N/A	12/31/2017	Eliminated	Consolidation of Calvary/Creekside Basin with Logan Street Basin makes the parallel interceptor unnecessary.
L_SO_MF_097_M_09B_B_D_8	Calvary Creekside Storage Basin	South Fork	CSO097, CSO106, CSO110, CSO111, CSO137, CSO148, CSO151	8	3.46	\$13,720,000	N/A	N/A	N/A	N/A	12/31/2017	Eliminated	Basin volume now addressed through Logan Street. Project is proposed to be eliminated.
L_OR_MF_155_M_09B_B_B_4	Central Relief Drain (CRD) CSO In-Line Storage, Green Infrastructure & Distributed Storage	Ohio River	N/A	N/A	N/A	N/A	Central Relief Drain CSOs (13 total with an AAOV: CSO028, CSO029, CSO034, CSO036, CSO178, CSO181, CSO193, CSO195, CSO196, CSO197, CSO199, CSO200, CSO202)	8	Diversion, Weir Modifications & Green Infrastructure	\$2,184,000	N/A	12/31/2018	New project. MSD proposes to split CRD & 13th and Rowan projects into separate projects. The storage basin and CRD projects are proposed to remain on the same schedule.
L_MU_MF_154_M_09B_B_A_8	Clifton Heights Storage Basin	Muddy Fork	CSO132, CSO154, CSO167	8	6.55	\$13,870,000	CSO088, CSO131, CSO132, CSO154, CSO167	4	7	\$19,575,000	12/31/2018	12/31/2018	No changes are proposed for this project schedule.
L_SO_MF_083_M_09B_B_A_8	Lexington Road and Payne Street Storage Basin	South Fork	CSO082, CSO084, CSO118, CSO119, CSO120, CSO121, CSO141, CSO153	8	7.31	\$25,200,000	CSO082, CSO083, CSO084, CSO118, CSO119, CSO120, CSO121, CSO141, CSO153	0	8.18	\$25,904,000	12/31/2020	12/31/2020	No changes are proposed for this project schedule.
L_SO_MF_092_M_09B_B_D_8	Logan and Breckinridge Street Storage Basin	South Fork	CSO091, CSO113, CSO117, CSO146, CSO149, CSO152	8	11.83	\$30,320,000	CSO091, CSO097, CSO106, CSO110, CSO111, CSO113, CSO117, CSO137, CSO146, CSO148, CSO149, CSO151, CSO152	8	16.6	\$48,243,000	12/31/2017	12/31/2017	A review of project approach and benefit/cost results eliminated the Calvary Creekside basin, consolidating storage to the Logan Street basin location. No changes to schedule are proposed.
L_SO_MF_018_S_03_A_A	Nightingale Pump Station Replacement & Storage	South Fork	CSO018	0	60 MGD/0 MG	\$15,710,000	CSO018	0	33 MGD/7.7 MG	\$22,123,000	12/31/2016	12/31/2016	Pump Station size was reduced as a result of adding storage.
L_OR_MF_190_S_09B_B_A_8	18th and Northwestern Pky. Storage Basin	Ohio River	CSO190	8	1.31 MG	\$4,514,000	CSO190	8	1.24	\$4,486,000	12/31/2017	12/31/2017	Project slightly smaller
L_OR_MF_105_M_13_B_A_0	Southwestern Parkway Storage Basin	Ohio River	CSO104, CSO105, CSO189	0	5.08	\$17,620,000	CSO104, CSO105, CSO189	0	11.07	\$30,937,000	12/31/2018	12/31/2018	No changes are proposed for this project schedule.
<b>NO CHANGE</b>													
L_SO_MF_108_S_09A_B_A_4	CSO108 Dam Modification	South Fork	CSO108	N/A	N/A	\$150,000	CSO108	N/A	N/A	\$150,000	12/31/2010	12/31/2010	Project Completed - Monitoring Ongoing
L_MI_MF_123_S_08_A_A_0	CSO123 Downspout Disconnection	Middle Fork	CSO123	N/A	N/A	\$315,000	CSO123	N/A	N/A	\$315,000	12/31/2012	12/31/2012	Project Completed - Monitoring Ongoing
L_MI_MF_206_S_08_A_A_0	CSO206 Sewer Separation	Middle Fork	CSO206	N/A	N/A	\$3,842,000	CSO206	N/A	N/A	\$3,842,000	12/31/2013	12/31/2013	Project Completed - Monitoring Ongoing
L_OR_MF_019_S_13_B_A_8	Portland Wharf Storage Basin	Ohio River	CSO019	8	6.37 MG	\$20,000,000	CSO019	8	6.37	\$20,000,000	12/31/2019	12/31/2019	



TABLE ES.1 2012 FINAL LTCP PROJECT SUITE

ACD Project Number	Project Name	Receiving Stream	2009 Overflows Controlled	2009 Level of Control	2009 Size (MG)	2009 Cost	2012 Overflows Controlled	2012 LOC	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
L_OR_MF_019_S_03_A_B	34th Street Flood Pump Station	Ohio River	CSO019	N/A	N/A	\$541,000	CSO019	N/A	N/A	\$541,000	12/31/2012	12/31/2012	Project Completed - Monitoring Ongoing
L_OR_MF_022_M_03_A_A	4th Street Flood Pump Station	Ohio River	CSO022, CSO023	N/A	N/A	\$944,000	CSO022, CSO023	N/A	N/A	\$944,000	12/31/2012	12/31/2012	Project Completed - Monitoring Ongoing
L_OR_MF_019_S_03_A_A	27th Street Flood Pump Station	Ohio River	CSO019	N/A	N/A	\$476,000	CSO019	N/A	N/A	\$476,000	6/30/2013	6/30/2013	Project Completed - Monitoring Ongoing
L_OR_MF_189_M_03_A_A	Shawnee Flood Pump Station	Ohio River	CSO104, CSO105, CSO189	N/A	N/A	\$411,000	CSO104, CSO105, CSO189	N/A	N/A	\$411,000	6/30/2013	6/30/2013	Project Completed - Monitoring Ongoing
L_OR_MF_190_S_03_A_A	17th Street Flood Pump Station	Ohio River	CSO190	N/A	N/A	\$625,000	CSO190	N/A	N/A	\$625,000	12/31/2014	12/31/2014	

Table ES.2 2012 SSDP Final Project Suite

ACD Project Number	Project Name	Receiving Stream	Overflows Controlled	2009 Level of Control Depth (in)	2009 Level of Control Storm	2009 Size (MG)	2009 Cost	2012 Level of Control Depth (in)	2012 Level of Control Storm	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
<b>CEDAR CREEK AREA</b>														
S_CC_CC_70158_M_09A_C	Idlewood Inline Storage	CEDAR CREEK	28998, 28984, 63094, 63095, 70158	1.82	2-Year, 3-Hour	N/A	\$2,317,000	1.82	2-Year, 3-Hour	N/A	\$2,317,000	12/31/2023	12/31/2023	
S_FF_CC_81316_M_03_C_A	Fairmount Road Pump Station Off-Line Storage	BIG RUN	Fairmount Road PS (81316 & 97362)	N/A	N/A (New Project)	N/A	N/A	1.82	2-Year, 3-Hour	3.4 MG	\$13,439,000	N/A	12/31/2015	Project needed to accommodate flows from eliminated Jeffersontown WQTC and acknowledge capacity at Cedar Creek WQTC.
S_CC_CC_67997_M_01_C	Little Cedar Creek Interceptor Improvements	LITTLE CEDAR CREEK	67997, 67999, 86423, 86424, 89195, 89196, 89197	1.82	2-Year, 3-Hour	Pipe Upgrades	\$1,875,000	1.82	2-Year, 3-Hour	N/A	\$1,875,000	12/31/2024	12/31/2024	
S_CC_CC_MSD1025_S_03_B	Bardstown Rd. PS Improvements	BIG RUN	88545	2.25	5-Year, 3-Hour	N/A	\$281,000	2.25	5-Year, 3-Hour	N/A	\$281,000	12/31/2021	12/31/2021	
S_CC_CC_MSD1080_S_01_C	Running Fox PS Elimination	LITTLE CEDAR CREEK	MSD1080-LS	1.82	2-Year, 3-Hour	N/A	\$96,000	1.82	2-Year, 3-Hour	N/A	\$77,000	12/31/2010	12/31/2010	Project Completed
<b>HITE CREEK AREA</b>														
S_HC_HC_MSD1082_S_09A_C	Meadow Stream Pump Station & Force Main Upgrade	FLOYDS FORK, SOUTH FORK HARRODS CREEK	Meadow Steam PS (91087, MSD1082-PS)	1.82	2-Year, 3-Hour	0.5	\$974,000	2.60	10-Year, 3-Hour	3.89 MGD PS & New 18" Force Main	\$974,000	12/31/2016	12/31/2012	Project changed from a small storage basin to a pump station upgrade and new force main due to the capacity needs of Crestwood. The City paid the additional costs beyond MSD's overflow control commitment. Project Completed - Monitoring Ongoing
S_HC_HC_MSD1086_M_07_C_A	Floydsburg Rd. SSES, Rehabilitation and Pump Station Upgrade	FLOYDS FORK	Floydsburg Road (MSD1086-PS, 90776, 108956, 108957, 108958)	1.82	2-Year, 3-Hour	N/A	\$57,000	1.82	2-Year, 3-Hour	N/A	\$57,000	12/31/2010	12/31/2010	Project Completed - Monitoring Ongoing
S_HC_HC_MSD1085_S_03_A	Kavanaugh Rd. PS Improvements	HITE CREEK	Kavanaugh Rd (MSD1085-PS)	2.60	10-Year, 3-Hour	N/A	\$1,110,000	2.60	10-Year, 3-Hour	N/A	\$1,110,000	12/31/2024	12/31/2024	
<b>FLOYDS FORK AREA</b>														
S_FF_FF_NB01_S_01_C_A	Woodland Hills PS Diversion	POPE LICK	33003, 65531	1.82	2-Year, 3-Hour	N/A	\$20,000	1.82	2-Year, 3-Hour	N/A	\$20,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing
S_FF_FF_NB02_S_13_C	Eden Care PS SSO Investigation	FLOYDS FORK	Eden Care PS (MSD1105-PS)	N/A	N/A (Monitor)	N/A	N/A	N/A	N/A	N/A	\$0	N/A	Eliminated	Only one overflow had been documented at this location. MSD cleaned the sewers in the vicinity and has not documented an overflow in over 3 years. No further action is deemed necessary.
S_FF_FF_NB03_M_01_C_A	Ashburton PS Improvements & Diversion	FLOYDS FORK	Olde Copper Court PS (MSD0165-PS), Ashburton PS (MSD0166-PS)	1.82	2-Year, 3-Hour	N/A	\$118,000	1.82	2-Year, 3-Hour	N/A	\$118,000	12/31/2021	12/31/2021	Project Completed
<b>JEFFERSONTOWN AREA</b>														
S_JT_JT_NB01_M_01_C_A	Jeffersontown WQTC Elimination	CHENOWETH RUN	28390, 28391, 28392, 28395, 28551, 31733, Jeffersontown WQTC (28173 & 64505 & MSD0255 & IS028-SI)	1.82	2-Year, 3-Hour	N/A	\$23,737,000	1.82	2-Year, 3-Hour	N/A	\$23,737,000	12/31/2015	12/31/2015	
S_JT_JT_NB01A_M_03_C	Chenoweth Hills WQTC Elimination & PS Improvements	CHENOWETH RUN	Chenoweth Run PS (MSD0196-PS & 86052 & 64096), Chippewa PS (92061), Chenoweth Hills WQTC PS (MSD0263A-PS), Chenoweth Hills WQTC (MSD0263)	1.82	2-Year, 3-Hour	N/A	\$3,140,000	1.82	2-Year, 3-Hour	N/A	\$3,140,000	12/31/2015	12/31/2015	
S_JT_JT_NB02_M_01_C	Dell Rd & Charlane Project Pkwy Interceptor	BEATTY BROOK	Charlane Pkwy (28250, 28249, 28340, 28336, 104289), Dell Rd. (28413, 28414, 28415, 28416, 28417)	1.82	2-Year, 3-Hour	Pipe Upgrades	\$917,000	1.82	2-Year, 3-Hour	N/A	\$917,000	12/31/2022	12/31/2022	
S_JT_JT_NB03_M_01_C	Raintree & Marian Ct PS Eliminations and Pipe Upgrades (2 Phases)	BEATTY BROOK	28719, 28711, Marian Court PS (28729), Raintree PS (MSD0149-PS)	1.82	2-Year, 3-Hour	N/A	\$1,005,000	1.82	2-Year, 3-Hour	N/A	\$1,005,000	12/31/2021	12/31/2021	
S_JT_JT_NB04_M_01_A	Monticello PS Elimination	FERN CREEK	Monticello Place PS (MSD0151-PS & 27969)	2.60	10-Year, 3-Hour	N/A	\$207,000	2.60	10-Year, 3-Hour	N/A	\$207,000	12/31/2022	12/31/2022	

Table ES.2 2012 SSDP Final Project Suite

ACD Project Number	Project Name	Receiving Stream	Overflows Controlled	2009 Level of Control Depth (in)	2009 Level of Control Storm	2009 Size (MG)	2009 Cost	2012 Level of Control Depth (in)	2012 Level of Control Storm	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
<b>MIDDLE FORK AREA</b>														
S_MISF_MF_NB01_M_01_C_A1	Middle Fork Relief Interceptor, Wet Weather Storage, and Upper Middle Fork LS Diversion (2 Phases)	MIDDLE FORK BEARGRASS CREEK	02932, 02933, 02935, 08537, 23211, 23212, 27005, 51180, 51221, 51160, 51161, 45835, 47583, 47593, 47596, 47603, 47604, 90700, IS021A-SI, Middle Fork at Breckenridge (08935-SM)	1.82	2-Year, 3-Hour	1.6	\$26,333,500	1.82	N/A	N/A	\$26,333,500	12/31/2013, 12/31/2023	12/31/2013, 12/31/2023	
S_MI_MF_NB04_M_03_B	Goose Creek PS Improvements & Wet Weather Storage (2 Phases)	GOOSE CREEK	Devondale PS (21628-W), Goose Creek PS (46891, 62418, 62420, 91629, 91630, 105936), Saurel PS (43472)	2.25	5-Year, 3-Hour	0.5	\$7,558,000	2.25	5-Year, 3-Hour	N/A	\$7,558,000	12/31/2024	12/31/2024	
S_MI_MF_NB06_M_01_A_A - 1, S_MI_MF_NB06_M_01_A_A - 2	Anchor Estates PS Eliminations (2 Phases)	MIDDLE FORK BEARGRASS CREEK	Vannah PS (01106), Anchor Estates #1 PS (00746 & 00056-W), Anchor Estates #2 PS (MSD0057-LS)	2.60	10-Year, 3-Hour	N/A	\$1,909,000	2.6	10-Year, 3-Hour	N/A	\$1,909,000	12/31/2013, 12/31/2016	12/31/2013, 12/31/2016	Phase 1 Completed - Vannah PS Eliminated
S_MI_MF_NB07_S_07_C	Hurstbourne I/I Investigation & Rehabilitation	HURSTBOURNE CREEK	01793	1.82	2-Year, 3-Hour	N/A	\$536,000	1.82	2-Year, 3-Hour	N/A	\$536,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing
<b>SOUTHEAST DIVERSION AREA</b>														
S_SD_MF_NB03_S_07_C	Parkview Estates I/I Investigation & Rehabilitation	SOUTH FORK BEARGRASS CREEK	47250	1.82	2-Year, 3-Hour	N/A	\$285,000	1.82	2-Year, 3-Hour	N/A	\$285,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing
S_SD_MF_NB04_S_01_B_A	Klondike Interceptor	SOUTH FORK BEARGRASS CREEK	25676 (Alcona), 26650, 26651	2.25	5-Year, 3-Hour	Pipe Upgrades	\$558,000	2.25	5-Year, 3-Hour	N/A	\$558,000	12/31/2015	12/31/2015	
S_SD_MF_NB05_M_01_A	Sutherland Interceptor	SOUTH FORK BEARGRASS CREEK	Sutherland (16649)	2.60	10-Year, 3-Hour	Pipe Upgrades	\$412,000	2.60	10-Year, 3-Hour	N/A	\$412,000	12/31/2023	12/31/2023	
S_SD_MF_NB06_S_13_C	Beargrass Interceptor Rehab Ph. 2	SOUTH FORK BEARGRASS CREEK	51594	1.82	2-Year, 3-Hour	N/A	\$57,000	1.82	2-Year, 3-Hour	N/A	\$57,000	12/31/2010	12/31/2010	Monitoring Ongoing
<b>POND CREEK AREA</b>														
S_PO_WC_PC03_M_01_C	Charleswood Interceptor Extension	FISHPOOL CREEK	25477, 25478, Cooper Chapel PS (25480 & MSD0130-PS)	1.82	2-Year, 3-Hour	Pipe Upgrades	\$603,000	1.82	2-Year, 3-Hour	N/A	\$1,600,000	12/31/2022	12/31/2022	
S_PO_WC_PC04_M_01_C	Cinderella PS Elimination	FISHPOOL CREEK	Cinderella PS (60679 & MSD1013-PS), 35309	1.82	2-Year, 3-Hour	N/A	\$2,205,000	1.82	2-Year, 3-Hour	N/A	\$2,205,000	12/31/2023	12/31/2023	
S_PO_WC_PC05_M_07_C	Lantana PS I/I Investigation & Rehabilitation	PENNSYLVANIA RUN	Lantana Drive #1 PS (25484 & 93719 & MSD0101-PS)	1.82	2-Year, 3-Hour	N/A	\$20,000	N/A (SSES/Rehab)	N/A (SSES/Rehab)	N/A	\$20,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing
S_PO_WC_PC06_M_01_C	Government Center PS Elimination	PENNSYLVANIA RUN	Government Center PS (MSD0180-PS)	1.82	2-Year, 3-Hour	N/A	\$1,225,000	1.82	2-Year, 3-Hour	N/A	\$1,225,000	12/31/2024	12/31/2024	Project Completed - Monitoring Ongoing
S_PO_WC_PC07_M_01_A	Avanti PS Elimination	LITTLE CEDAR CREEK	Avanti PS (21229-W)	2.60	10-Year, 3-Hour	N/A	\$31,000	2.6	10-Year, 3-Hour	N/A	\$31,000	12/31/2010	12/31/2010	Project Completed - Monitoring Ongoing
S_PO_WC_PC08_M_01_C	Lea Ann Way System Improvements	FERN CREEK	19360, 19369, 29933, 29948, 29943, 31083, 31084, 79076, Lea Ann Way PS (MSD1010-PS)	1.82	2-Year, 3-Hour	Pipe Upgrades	\$827,000	1.82	2-Year, 3-Hour	Additional Pipe Upgrades	\$827,000	12/31/2015	12/31/2015	Additional overflows have been occurring in recent years. Therefore, additional sewer inspection and rehabilitation are underway. Contingency plans have been developed and are dependent upon the efficacy of rehabilitation of wet weather flows.
S_PO_WC_PC09_M_09B_C	Outer Loop Wet Weather Storage	FISHPOOL CREEK	70212, 17724	1.82	2-Year, 3-Hour	1.42	\$4,280,000	2.60	10-Year, 3-Hour		\$0	12/31/2024	Eliminated	Due to improvements in the Pond Creek hydraulic model calibration, this storage basin is no longer necessary.
S_PO_WC_PC09_M_09B_C	Caven Ave Pump Station Elimination	FISHPOOL CREEK	27116, Caven Ave PS (MSD0133-PS)	1.82	2-Year, 3-Hour	0.21	\$731,000	2.60	10-Year, 3-Hour	PS Elimination	\$1,800,000	12/31/2024	12/31/2016	Recent new pipeline constructed to eliminate a nearby package treatment plant makes the elimination of the pump station the most cost effective overflow solution.
S_PO_WC_PC10_M_01_C	Leven PS Elimination	PENNSYLVANIA RUN	Leven PS (36419 & MSD1019-PS)	1.82	2-Year, 3-Hour	N/A	\$376,000	1.82	2-Year, 3-Hour	N/A	\$376,000	12/31/2022	12/31/2022	
S_PO_WC_PC11_M_07_C	Edsel PS I/I Investigation & Rehabilitation	FERN CREEK	Edsel PS (92098 & MSD1048-PS)	1.82	2-Year, 3-Hour	N/A	\$367,000	1.82	2-Year, 3-Hour	N/A	\$367,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing

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ACD Project Number	Project Name	Receiving Stream	Overflows Controlled	2009 Level of Control Depth (in)	2009 Level of Control Storm	2009 Size (MG)	2009 Cost	2012 Level of Control Depth (in)	2012 Level of Control Storm	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
<b>ORFM AREA</b>														
S_OR_MF_NB01_M_01_B	Mellwood PS and Forcemain Improvements, System Improvements & PS Eliminations (2 Phases)	MUDDY FORK BEARGRASS CREEK	26752, 41374, 41416, Mockingbird Valley PS (MSD0007-PS), Winton PS (MSD0010-PS), Mellwood Avenue PS (24472 & MSD0023-PS), Canoe Lane PS (24152-W & MSD0024-PS)	2.25	5-Year, 3-Hour	N/A	\$3,055,000	2.25	5-Year, 3-Hour	N/A	\$3,055,000	12/31/2012, 12/31/2024	12/31/2012, 12/31/2024	Phase 1 Project Completed - Monitoring Ongoing
S_OR_MF_NB02_S_13_C	Leland Road SSO Investigation	CHERRYWOOD CREEK	96020	N/A	N/A	N/A	N/A	N/A (Rehab & Monitoring)	N/A (Rehab & Monitoring)	N/A	\$0	N/A	Eliminated	Only one overflow had been documented at this location. MSD cleaned the sewers in the vicinity and has not documented an overflow in over 3 years. No further action is deemed necessary.
S_OR_MF_NB03_S_07_C	Derington Ct. PS I/I Investigation & Rehabilitation	GOOSE CREEK	Derington Court PS (MSD0095-PS)	1.82	2-Year, 3-Hour	N/A	\$265,000	1.82	2-Year, 3-Hour	N/A	\$265,000	12/31/2012	12/31/2012	Project Completed - Monitoring Ongoing
S_OR_MF_NB04_M_03_B_B	Prospect WQTC Eliminations, Harrods Creek PS, and ORFM System Improvements (3 Phases)	LITTLE GOOSE CREEK	40870, 40871, 40872, 89646, Barbour Lane PS (42680, 65633, 65635, MSD0192-PS), West Goose Creek PS (22436 & MSD0123-PS), Phoenix Hill PS (MSD1044-PS), Glenview Hills PS (MSD0183-PS), New Market PS (MSD0193-PS), Deep Creek PS (MSD1063-PS), Hunting Creek South WQTC (MSD0292)	2.25	5-Year, 3-Hour	N/A	\$31,368,000	2.25	5-Year, 3-Hour	N/A	\$31,368,000	12/31/2015, 12/31/2016	12/31/2015, 12/31/2016	
<b>MILL CREEK AREA</b>														
S_MC_WC_NB01_M_01_A	Shively Interceptor	LYNNVIEW DITCH	04498, 04542, Pioneer PS (81814-W), Fern Lea PS (MSD0047-PS), Garr's Lane PS (MSD0050-PS)	2.60	10-Year, 3-Hour	Pipe Upgrades	\$16,419,000	2.6	10-Year, 3-Hour	N/A	\$16,419,000	12/31/2014	12/31/2014	Project Completed - Monitoring Ongoing
S_MC_WC_NB02_S_03_C	East Rockford PS Relocation	MILL CREEK	East Rockford PS (04699-W)	1.82	2-Year, 3-Hour	N/A	\$1,044,000	1.82	2-Year, 3-Hour	N/A	\$1,044,000	12/31/2021	12/31/2021	Project Completed
<b>SMALL WQTC AREA</b>														
S_FF_BT_NB01_S_09A_C_A	Lucas Ln. PS Inline Storage	GOOSE CREEK	Lucas Lane PS (MSD0199-LS)	1.82	2-Year, 3-Hour	N/A	\$183,000	1.82	2-Year, 3-Hour	N/A	\$183,000	12/31/2021	12/31/2021	
S_HC_HN_NB01_S_03_C_A	Riding Ridge PS Improvements	HARRODS CREEK	Riding Ridge PS (MSD1060-LS)	1.82	2-Year, 3-Hour	N/A	\$27,000	1.82	2-Year, 3-Hour	N/A	\$27,000	12/31/2014	12/31/2014	
S_HC_HN_NB02_S_09A_C_B	Gunpowder PS Inline Storage	HARRODS CREEK	Gunpowder PS (MSD1055-LS)	1.82	2-Year, 3-Hour	N/A	\$176,000	1.82	2-Year, 3-Hour	N/A	\$176,000	12/31/2021	12/31/2021	
S_HC_HN_NB03_S_09A_A_A	Fox Harbor Inline Storage	HARRODS CREEK	Fox Harbor #1 and #2 PS (62769)	2.60	10-Year, 3-Hour	N/A	\$328,000	2.60	10-Year, 3-Hour	N/A	\$328,000	12/31/2021	12/31/2021	
S_HC_HS_NB01_S_03_C_A	Fairway View PS Improvements	HARRODS CREEK	Fairway View PS (MSD1065-PS)	1.82	2-Year, 3-Hour	N/A	\$87,000	1.82	2-Year, 3-Hour	N/A	\$167,000	12/31/2014	12/31/2014	
S_FF_LF_NB01_S_13_C_A	Lake Forest PS SSO Investigation	CHENOWETH RUN	Lake Forest PS (MSD1169-LS)	N/A	N/A	N/A	N/A	N/A (Monitoring)	N/A (Monitoring)	N/A	\$77,000	12/31/2012	12/31/2012	Monitoring Ongoing
S_FF_CH_NB01_S_09A_C_A	St. Rene Rd. PS Inline Storage	CHENOWETH RUN	94187	1.82	2-Year, 3-Hour	N/A	\$30,000	1.82	2-Year, 3-Hour	N/A	\$30,000	12/31/2021	12/31/2021	
<b>CSS AREA</b>														
S_OR_MF_42007_S_07_C	Sonne PS I/I Investigation	PADDY RUN	Sonne Avenue PS (MSD0042-PS)	1.82	2-Year, 3-Hour	N/A	\$265,000	1.82	2-Year, 3-Hour	N/A	\$265,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing
S_SF_MF_30917_M_09_A	Camp Taylor System Improvements (Four Phases)	MUDDY FORK BEARGRASS CREEK	08717, 13931, 13943, 36763, 44396, 44397, 66349, 104223, 104231	2.60	10-Year, 3-Hour	Pipe Upgrades	\$28,279,000	2.60	10-Year, 3-Hour	Pipe Upgrades	\$28,279,000	Dec 31, 2012, 2013, 2017 & 2024	Multiple (Same as 2009)	Project approach is similar to 2009, but the project area targeted for inspection and rehabilitation is larger.
S_MC_MF_55665_S_07_C	Hazelwood PS I/I Investigation & Rehabilitation	MANSLICK BRANCH	Hazelwood PS (55665)	1.82	2-Year, 3-Hour	N/A	\$173,000	1.82	2-Year, 3-Hour	N/A	\$173,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing

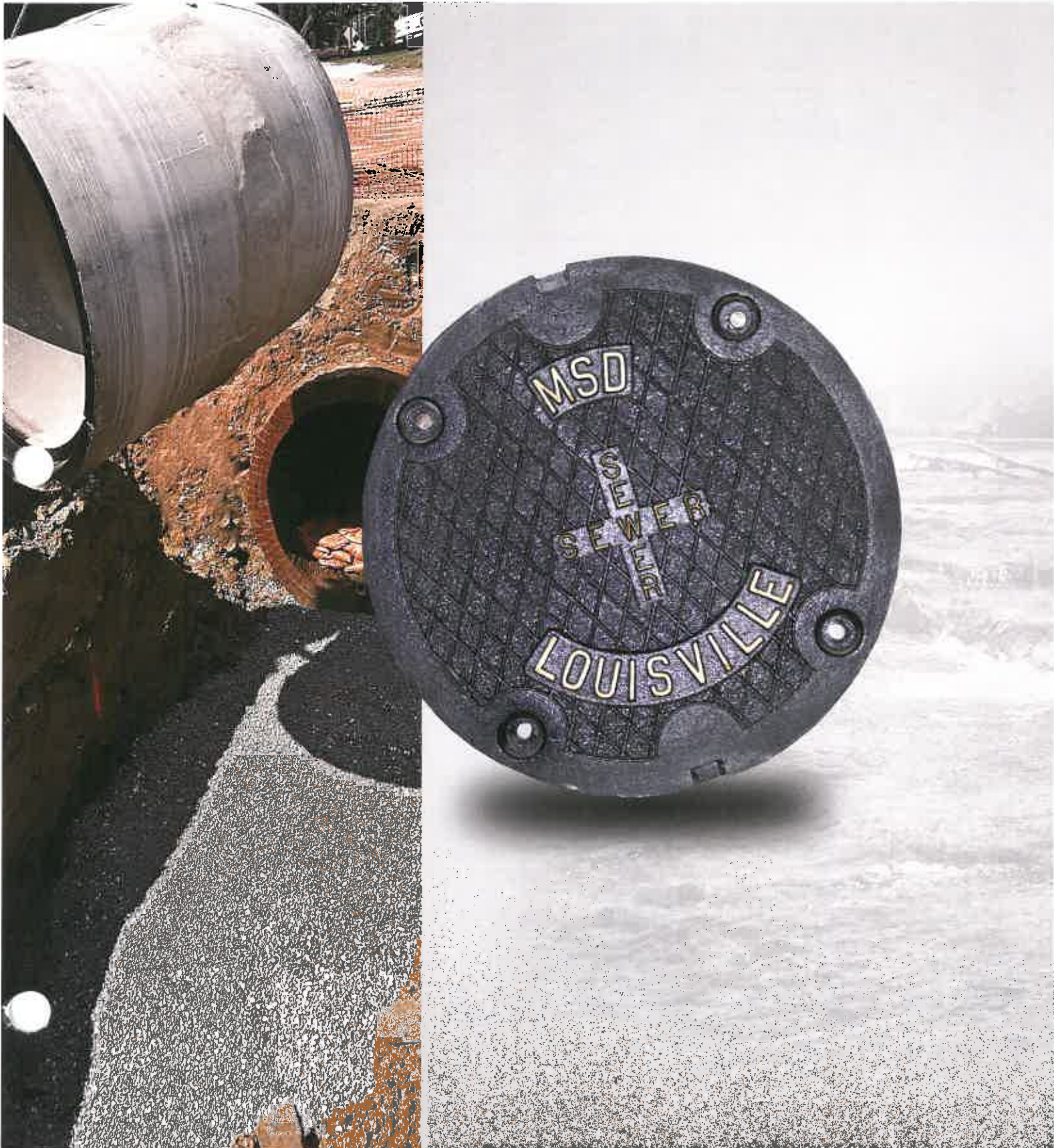
Table ES.2 2012 SSDP Final Project Suite

ACD Project Number	Project Name	Receiving Stream	Overflows Controlled	2009 Level of Control Depth (in)	2009 Level of Control Storm	2009 Size (MG)	2009 Cost	2012 Level of Control Depth (in)	2012 Level of Control Storm	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
<b>INTERIM SSDP</b>														
HIKES LANE INTERCEPTOR /HIGHGATE SPRINGS PS	<b>Hikes Lane Interceptor and Highgate Springs</b>	SOUTH FORK BEARGRASS CREEK AND WEDGEWOOD DITCH	18134, 18298, 18302, 18434, 18471, 18483, 18505, 18595, 49224, 49236, 49672, 49673, MSD0012-PS								\$21,216,000		11/27/2012	This project includes improvements to the Hikes Point Sewer System and eliminates the Highgate Springs Pump Station. In the general Hikes Point area includes improvements of 3,500 LF of new or replacement sewers, and decommissioning the Highgate Springs Pump Station. The new Hikes Lane Interceptor consists of 10,000 LF of 72-inch sewer that connects to Southeastern Interceptor. Project Completed - Monitoring Ongoing
SOUTHEASTERN DIVERSION STRUCTURE & INTERCEPTOR	<b>Southeastern Diversion Structure and Interceptor</b>	SOUTH FORK BEARGRASS CREEK	08426, 08427, 08430, 08431, 30680, 30681, 49647								\$1,744,000		5/12/2012	This project includes improvements to the Southeast Diversion Structure for increased flows due to the Hikes Lane Interceptor and other Final SSDP projects. The project consists of a new parallel Southeastern Interceptor relief sewer, two flow control junction boxes, and modifications to the existing Southeastern Diversion Structure (including removing control weirs and reprogramming Real Time Control gates). Project Completed - Monitoring Ongoing
NORTHERN DITCH DIVERSION INTERCEPTOR	<b>Northern Ditch Diversion Interceptor</b>	NORTHERN DITCH	MSD0271 (Yorktown)								\$20,397,000		7/31/2011	This project includes construction of a new Northern Ditch Diversion Interceptor which will allow flow from upstream projects to reach the Derek R. Guthrie WQTC. The project consists of 13,000 LF of 84-inch pipe constructed long Greasy Ditch. Project Completed - Monitoring Ongoing
SINKING FORK RELIEF SEWER	<b>Sinking Fork Relief Sewer</b>	MIDDLE FORK BEARGRASS CREEK AND UPPER SINKING FORK	21103, 25012, 63319								\$1,690,000		12/23/2009	This project includes conveying flow from some of the new Beechwood Village sewers and providing additional wet weather capacity downstream of the Beechwood Village East area to accommodate upstream SSDP projects. The project includes installing 2,800 LF of 24-inch relief sewer. Project Completed
BEECHWOOD VILLAGE SANITARY SEWER REPLACEMENT	<b>Beechwood Village Sanitary Sewer Replacement</b>	UPPER SINKING FORK	21061, 21089, 21101, 21153, 21156								\$11,800,000		4/27/2011	This project includes replacing or rehabilitating the entire local system, including 23,700 LF of sewer pipe and 580 homeowner's service connections. The project will be completed in two phases, East and West. Project Completed
DEREK R GUTHRIE WATER QUALITY TREATMENT CENTER	<b>Derek R. Guthrie WQTC</b>	OHIO RIVER, BLACK POND CREEK, ALVEY DITCH, MENDORA BRANCH, MILL CREEK	Wet Weather SSOs	4.50	10-Year, 24-Hour	100 MGD HRT	\$102,700,000	4.50	10-Year, 24-Hour	100 MGD HRT	\$102,700,000	12/31/2011	11/27/2012	Full high rate treatment capacity not yet available for flows to be seen by 2024 due to extreme wet weather in 2011, but current flows and overflow eliminations can be accommodated with current treatment capacity. Project Completed - Monitoring Ongoing



# Figure

ES.1





## MSD Integrated Overflow Abatement Plan Implementation Schedule (01 Jan 2009- 31 Dec 2024 )

Activity Name	Scheduled Finish	2009 IOAP Completion	2012 IOAP Modification	2009				2010				2011				2012				2013				2014				2015				2016				2017				2018				2019				2020				2021				2022				2023				2024			
				Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q												
<b>MSD IOAP ANNUAL SCHEDULE</b>	31-Dec-24	31-Dec-24	31-Dec-24																																																																
<b>LONG TERM CONTROL PLAN</b>	01-Jan-21	31-Dec-20	31-Dec-20																																																																
<b>GREEN DEMONSTRATION PROJECTS</b>	31-Dec-20	31-Dec-20	31-Dec-20																																																																
<b>GREEN INFRASTRUCTURE DEMONSTRATION PROJECTS</b>	31-Dec-11 A	31-Dec-11	31-Dec-11																																																																
GREEN INFRASTRUCTURE DEMONSTRATION PROJECTS	31-Dec-11 A	31-Dec-11	31-Dec-11																																																																
<b>GREEN INFRASTRUCTURE PROGRAM</b>	31-Dec-20	31-Dec-20	31-Dec-20																																																																
GREEN INFRASTRUCTURE PROGRAM	31-Dec-20	31-Dec-20	31-Dec-20																																																																
<b>GRAY INFRASTRUCTURE PROJECTS</b>	01-Jan-21	31-Dec-20	31-Dec-20																																																																
<b>CSO 123 DOWNSPOUT DISCONNECTION</b>	31-Dec-12	31-Dec-12	31-Dec-12																																																																
CSO 123 DOWNSPOUT DISCONNECTION	31-Dec-12	31-Dec-12	31-Dec-12																																																																
<b>I-64 AND GRINSTEAD DRIVE STORAGE BASIN</b>	31-Dec-20	21-Dec-14	31-Dec-20																																																																
I-64 AND GRINSTEAD DRIVE STORAGE BASIN	31-Dec-20	21-Dec-14	31-Dec-20																																																																
<b>CSO 140 INCREASE PIPE CONVEYANCE</b>	31-Dec-15	31-Dec-15	31-Dec-15																																																																
CSO 140 INCREASE PIPE CONVEYANCE	31-Dec-15	31-Dec-15	31-Dec-15																																																																
<b>CSO 206 SEWER SEPARATION</b>	30-Dec-13	31-Dec-13	30-Dec-13																																																																
CSO 206 SEWER SEPARATION	30-Dec-13	31-Dec-13	30-Dec-13																																																																
<b>CLIFTON HEIGHTS STORAGE BASIN</b>	31-Dec-18	31-Dec-18	31-Dec-18																																																																
CLIFTON HEIGHTS STORAGE BASIN	31-Dec-18	31-Dec-18	31-Dec-18																																																																
<b>BELL'S LANE WET WEATHER TREATMENT FACILITY AND IN LINE STORAGE</b>	31-Dec-16	31-Dec-14	31-Dec-16																																																																
BELL'S LANE WET WEATHER TREATMENT FACILITY AND IN LINE STORAGE	31-Dec-16	31-Dec-14	31-Dec-16																																																																
<b>PORTLAND WHARF STORAGE BASIN</b>	31-Dec-19	31-Dec-19	31-Dec-19																																																																
PORTLAND WHARF STORAGE BASIN	31-Dec-19	31-Dec-19	31-Dec-19																																																																
<b>STORY AVENUE AND MAIN STREET STORAGE BASIN</b>	31-Dec-20	31-Dec-13	31-Dec-20																																																																
STORY AVENUE AND MAIN STREET STORAGE BASIN	31-Dec-20	31-Dec-13	31-Dec-20																																																																
<b>CSO 058 IN-LINE STORAGE AND GREEN INFRASTRUCTURE CONTROLS</b>	31-Dec-14	31-Dec-14	31-Dec-14																																																																
CSO 058 IN-LINE STORAGE AND GREEN INFRASTRUCTURE CONTROLS	31-Dec-14	31-Dec-14	31-Dec-14																																																																
<b>SOUTHWESTERN PARKWAY STORAGE BASIN</b>	31-Dec-18	31-Dec-18	31-Dec-18																																																																
SOUTHWESTERN PARKWAY STORAGE BASIN	31-Dec-18	31-Dec-18	31-Dec-18																																																																
<b>13TH STREET AND ROWAN STREET STORAGE BASIN</b>	01-Jan-21	31-Dec-20	31-Dec-20																																																																
13TH STREET AND ROWAN STREET STORAGE BASIN	01-Jan-21	31-Dec-20	31-Dec-20																																																																
<b>13TH STREET AND ROWAN STREET STORAGE BASIN</b>	31-Dec-20		31-Dec-20																																																																
13TH STREET AND ROWAN STREET STORAGE BASIN	31-Dec-20		31-Dec-20																																																																
<b>CENTRAL RELIEF DRAIN IN-LINE STORAGE, GREEN INFRASTRUCTURE AND DISTRIBUTED STORAGE</b>	01-Jan-21		31-Dec-18																																																																
CENTRAL RELIEF DRAIN IN-LINE STORAGE, GREEN INFRASTRUCTURE AND DISTRIBUTED STORAGE	01-Jan-21		31-Dec-18																																																																
<b>CSO 160 IN-LINE STORAGE AND GREEN INFRASTRUCTURE CONTROLS</b>	31-Dec-15	31-Dec-15	31-Dec-15																																																																
CSO 160 IN-LINE STORAGE AND GREEN INFRASTRUCTURE CONTROLS	31-Dec-15	31-Dec-15	31-Dec-15																																																																
<b>ADAMS STREET SEWER SEPARATION AND STORAGE BASIN</b>	31-Dec-12	31-Dec-12	31-Dec-12																																																																
ADAMS STREET SEWER SEPARATION AND STORAGE BASIN	31-Dec-12	31-Dec-12	31-Dec-12																																																																
<b>18TH AND NORTHWESTERN PKY STORAGE BASIN</b>	31-Dec-17	31-Dec-17	31-Dec-17																																																																
18TH AND NORTHWESTERN PKY STORAGE BASIN	31-Dec-17	31-Dec-17	31-Dec-17																																																																
<b>ALGONQUIN PARKWAY STORAGE BASIN</b>	01-Jan-19	31-Dec-18	31-Dec-18																																																																
ALGONQUIN PARKWAY STORAGE BASIN	01-Jan-19	31-Dec-18	31-Dec-18																																																																
<b>SOUTHERN OUTFALL IN-LINE STORAGE (SOR 1)</b>	31-Dec-18		31-Dec-18																																																																
SOUTHERN OUTFALL IN-LINE STORAGE AT 43RD ST. (SOR 1)	31-Dec-18		31-Dec-18																																																																
<b>SOUTHERN OUTFALL IN-LINE RETENTION (SOR 2)</b>	01-Jan-19		31-Dec-18																																																																
SOUTHERN OUTFALL IN-LINE RETENTION AT 13TH AND WILSON AVE. (SOR 2)	01-Jan-19		31-Dec-18																																																																
<b>NIGHTINGALE PUMP STATION AND STORAGE BASIN</b>	31-Dec-16	31-Dec-16	31-Dec-16																																																																
NIGHTINGALE PUMP STATION AND STORAGE BASIN	31-Dec-16	31-Dec-16	31-Dec-16																																																																
<b>LEXINGTON ROAD AND PAYNE STREET STORAGE BASIN</b>	31-Dec-20	31-Dec-20	31-Dec-20																																																																
LEXINGTON ROAD AND PAYNE STREET STORAGE BASIN	31-Dec-20	31-Dec-20	31-Dec-20																																																																
<b>LOGAN STREET AND BRECKENRIDGE ST STORAGE BASIN</b>	31-Dec-17	31-Dec-17	31-Dec-17																																																																
LOGAN STREET AND BRECKENRIDGE ST STORAGE BASIN	31-Dec-17	31-Dec-17	31-Dec-17																																																																
<b>CSO 093 STRUCTURAL MODIFICATIONS AND GREEN INFRASTRUCTURE CONTROLS</b>	31-Dec-15	31-Dec-15	31-Dec-15																																																																
CSO 093 STRUCTURAL MODIFICATIONS AND GREEN INFRASTRUCTURE CONTROLS	31-Dec-15	31-Dec-15	31-Dec-15																																																																
<b>CSO 108 DAM MODIFICATIONS</b>	31-Dec-10 A	31-Dec-10	31-Dec-10																																																																
CSO 108 DAM MODIFICATIONS	31-Dec-10 A	31-Dec-10	31-Dec-10																																																																
<b>STORY AVENUE AND SPRING STREET GREEN INFRASTRUCTURE CONTROLS</b>	31-Dec-16	31-Dec-16	31-Dec-16																																																																
STORY AVENUE AND SPRING STREET GREEN INFRASTRUCTURE CONTROLS	31-Dec-16	31-Dec-16	31-Dec-16																																																																
<b>FLOOD PUMP STATION PROJECTS</b>	31-Dec-14	31-Dec-14	31-Dec-14																																																																
<b>27TH STREET FLOOD PUMP STATION</b>	30-Jun-13	30-Jun-13	30-Jun-13																																																																
27TH STREET FLOOD PUMP STATION	30-Jun-13	30-Jun-13	30-Jun-13																																																																
<b>34TH STREET FLOOD PUMP STATION</b>	31-Dec-12	31-Dec-12	31-Dec-12																																																																
34TH STREET FLOOD PUMP STATION	31-Dec-12	31-Dec-12	31-Dec-12																																																																
<b>4TH STREET FLOOD PUMP STATION</b>	31-Dec-12	31-Dec-12	31-Dec-12																																																																
4TH STREET FLOOD PUMP STATION	31-Dec-12	31-Dec-12	31-Dec-12																																																																

XXXXXX Approved 2009 IOAP   
   Remaining Work  
  Completed Work

MSD Integrated Overflow Abatement Plan Implementation Schedule (01 Jan 2009- 31 Dec 2024 )

Activity Name	Scheduled Finish	2009 IOAP Completion	2012 IOAP Modification	2009		2010		2011		2012		2013		2014		2015		2016		2017		2018		2019		2020		2021		2022		2023		2024					
				Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q					
<b>SHAWNEE FLOOD PUMP STATION</b>	30-Jun-13	30-Jun-13	30-Jun-13																																				
SHAWNEE FLOOD PUMP STATION	30-Jun-13	30-Jun-13	30-Jun-13																																				
<b>17TH STREET FLOOD PUMP STATION</b>	31-Dec-14	31-Dec-14	31-Dec-14	[X]																																			
17TH STREET FLOOD PUMP STATION	31-Dec-14	31-Dec-14	31-Dec-14	[X]																																			
<b>SANITARY SEWER DISCHARGE PLAN</b>	31-Dec-24	31-Dec-24	31-Dec-24																																				
<b>BEARGRASS CREEK MIDDLE FORK AREA</b>	31-Dec-24	31-Dec-24	31-Dec-24																																				
<b>GOOSE CREEK PUMP STATION</b>	31-Dec-24	31-Dec-24	31-Dec-24																																				
GOOSE CREEK PUMP STATION	31-Dec-24	31-Dec-24	31-Dec-24																																				
GOOSE CREEK PS PH1 - DEVONDALE PS WW STORAGE	31-Dec-24	31-Dec-24	31-Dec-24																												[X]								
GOOSE CREEK PS PH1 - DEVONDALE PS WW STORAGE	31-Dec-24	31-Dec-24	31-Dec-24																												[X]								
GOOSE CRK PS PH2 - PS & WET WEATHER STORAGE	31-Dec-24	31-Dec-24	31-Dec-24																												[X]								
GOOSE CRK PS PH2 - PS & WET WEATHER STORAGE	31-Dec-24	31-Dec-24	31-Dec-24																												[X]								
<b>ANCHOR ESTATES- ANCHOR ESTS PS 1 &amp; 2 PS ELIMINATIONS</b>	31-Dec-16	31-Dec-16	31-Dec-16																																				
ANCHOR ESTATES- ANCHOR ESTS PS 1 & 2 PS ELIMINATIONS	31-Dec-16	31-Dec-16	31-Dec-16																			[X]																	
<b>ANCHOR ESTATES- VANNAH PS ELIMINATION</b>	15-Oct-11 A	31-Dec-13	31-Dec-13	[X]																																			
ANCHOR ESTATES- VANNAH PS ELIMINATION	15-Oct-11 A	31-Dec-13	31-Dec-13	[X]																																			
<b>HURSTBOURNE I&amp;I INVESTIGATION &amp; REHABILITATION</b>	27-Dec-11 A	31-Dec-11	31-Dec-11																																				
HURSTBOURNE I&I INVESTIGATION & REHABILITATION	27-Dec-11 A	31-Dec-11	31-Dec-11	[X]																																			
<b>MIDDLE FORK RELIEF INTERCEPTOR, WET WEATHER STORAGE, AND UMFLS DIVERSION 1 -</b>	31-Dec-13	31-Dec-13	31-Dec-13																																				
MIDDLE FORK RELIEF INTERCEPTOR, WET WEATHER STORAGE, AND UMFLS DIVERSION 1 - BUECHEL BASIN	31-Dec-13	31-Dec-13	31-Dec-13	[X]																																			
<b>MIDDLE FORK RELIEF INTERCEPTOR, WET WEATHER STORAGE, AND UMFLS DIVERSION 2 F</b>	31-Dec-23	31-Dec-23	31-Dec-23																																				
MIDDLE FORK RELIEF INTERCEPTOR, WET WEATHER STORAGE, AND UMFLS DIVERSION 2 PS & WET WEATHER STORAGE	31-Dec-23	31-Dec-23	31-Dec-23																			[X]																	
<b>CEDAR CREEK AREA</b>	31-Dec-24	31-Dec-24	31-Dec-24																																				
<b>LITTLE CEDAR CREEK INTRECEPTOR IMPROVEMENTS</b>	31-Dec-24	31-Dec-24	31-Dec-24																																				
LITTLE CEDAR CREEK INTRECEPTOR IMPROVEMENTS	31-Dec-24	31-Dec-24	31-Dec-24																												[X]								
<b>IDLEWOOD INLINE STORAGE</b>	31-Dec-23	31-Dec-23	31-Dec-23																																				
IDLEWOOD INLINE STORAGE	31-Dec-23	31-Dec-23	31-Dec-23																												[X]								
<b>BARDSTOWN RD PS IMPROVEMENTS</b>	31-Dec-21	31-Dec-21	31-Dec-21																																				
BARDSTOWN RD PS IMPROVEMENTS	31-Dec-21	31-Dec-21	31-Dec-21																												[X]								
<b>RUNNING FOX PS ELIMINATION</b>	05-Apr-10 A	31-Dec-10	31-Dec-10	[X]																																			
RUNNING FOX PS ELIMINATION	05-Apr-10 A	31-Dec-10	31-Dec-10	[X]																																			
<b>FAIRMOUNT RD PS IMPROVMENTS</b>	01-Jan-15	31-Dec-23	31-Dec-23																																				
FAIRMOUNT RD PS IMPROVMENTS	31-Dec-14	31-Dec-23	31-Dec-23																			[X]																	
FAIRMOUNT RD PS IMPROVMENTS	24-Apr-12 A	31-Dec-23	31-Dec-23	[X]																																			
FAIRMOUNT RD PS IMPROVMENTS	24-Apr-12 A	31-Dec-23	31-Dec-23	[X]																																			
FAIRMOUNT RD PS IMPROVEMENT PH 2	01-Jan-15	31-Dec-15	31-Dec-15																																				
FAIRMOUNT STORAGE BASIN	01-Jan-15	31-Dec-15	31-Dec-15																																				
<b>COMBINED SEWER SYSTEM AREA</b>	31-Dec-23	31-Dec-23	31-Dec-23																																				
<b>HAZELWOOD PS I&amp;I INVESTIGATION &amp; REHABILITATION</b>	30-Jun-11 A	30-Jun-11	30-Jun-11																																				
HAZELWOOD PS I&I INVESTIGATION & REHABILITATION	30-Jun-11 A	30-Jun-11	30-Jun-11	[X]																																			
<b>SONNE PUMP STATION I&amp;I INVESTIGATION &amp; REHABILITATION</b>	30-Jun-11 A	30-Jun-11	30-Jun-11																																				
SONNE PUMP STATION I&I INVESTIGATION & REHABILITATION	30-Jun-11 A	30-Jun-11	30-Jun-11	[X]																																			
<b>CAMP TAYLOR SSES</b>	08-Jul-11 A	31-Dec-11	31-Dec-13																																				
CAMP TAYLOR SSES	08-Jul-11 A	31-Dec-11	31-Dec-13	[X]																																			
<b>CAMP TAYLOR SANITARY SEWER #1A</b>	31-Dec-12	31-Dec-13	31-Dec-13																																				
CAMP TAYLOR SANITARY SEWER #1A	31-Dec-12	31-Dec-13	31-Dec-13	[X]																																			
<b>CAMP TAYLOR SANITARY SEWER #1B</b>	31-Dec-13	31-Dec-13	31-Dec-13																																				
CAMP TAYLOR SANITARY SEWER #1B	31-Dec-13	31-Dec-13	31-Dec-13	[X]																																			
<b>CAMP TAYLOR SANITARY SEWER #2</b>	31-Dec-13	31-Dec-13	31-Dec-13																																				
CAMP TAYLOR SANITARY SEWER #2	31-Dec-13	31-Dec-13	31-Dec-13	[X]																																			
<b>CAMP TAYLOR #3- SEWER REHABILITATION</b>	31-Dec-17	31-Dec-17	31-Dec-17																																				
CAMP TAYLOR #3- SEWER REHABILITATION	31-Dec-17	31-Dec-17	31-Dec-17																			[X]																	
<b>CAMP TAYLOR #4-SEWER REHABILITATION &amp; REPLACEMENT</b>	31-Dec-23	31-Dec-23	31-Dec-23																																				
CAMP TAYLOR #4-SEWER REHABILITATION & REPLACEMENT	31-Dec-23	31-Dec-23	31-Dec-23																			[X]																	
<b>FLOYDS FORK AREA</b>	01-Apr-10 A	31-Dec-21	01-Apr-10																																				
<b>WOODLAND HILL PS DIVERSION</b>	01-Apr-10 A	30-Jun-11	01-Apr-10																																				
WOODLAND HILL PS DIVERSION	01-Apr-10 A	30-Jun-11	01-Apr-10	[X]																																			
<b>ASHBURTON PS IMPROVEMENTS AND DIVERSION</b>	22-Jan-10 A	31-Dec-21	22-Jan-10																																				
ASHBURTON PS IMPROVEMENTS AND DIVERSION	22-Jan-10 A	31-Dec-21	22-Jan-10																												[X]								
<b>HITE CREEK AREA</b>	31-Dec-24	31-Dec-24	31-Dec-24																																				
<b>MEADOW STREAM PS AND FORCE MAIN</b>	31-Dec-12	31-Dec-16	31-Dec-16																																				
MEADOW STREAM PS AND FORCE MAIN	31-Dec-12	31-Dec-16	31-Dec-16	[X]																																			
<b>KAVANAUGH RD PS IMPROVEMENTS</b>	31-Dec-24	31-Dec-24	31-Dec-24																																				

[X] Approved 2009 IOAP   [Green Box] Remaining Work  
 [Blue Box] Completed Work





## MSD Integrated Overflow Abatement Plan Implementation Schedule (01 Jan 2009- 31 Dec 2024 )

Activity Name	Scheduled Finish	2009 IOAP Completion	2012 IOAP Modification	2009		2010		2011		2012		2013		2014		2015		2016		2017		2018		2019		2020		2021		2022		2023		2024	
				Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q	Q
AVANTI PS ELIMINATION	28-Jul-09	A 31-Dec-10	31-Dec-10	██████████																															
<b>CHARLESWOOD INTERCEPTOR EXTENSION</b>	31-Dec-22	31-Dec-22	31-Dec-22																																
CHARLESWOOD INTERCEPTOR EXTENSION	31-Dec-22	31-Dec-22	31-Dec-22																																
<b>LANTANA PS I/I INVESTIGATION &amp; REHABILITATION</b>	29-Dec-11	A 31-Dec-11	29-Dec-11																																
LANTANA PS I/I INVESTIGATION & REHABILITATION	29-Dec-11	A 31-Dec-11	29-Dec-11																																
<b>LEVEN PS ELIMINATION</b>	31-Dec-22	31-Dec-22	31-Dec-22																																
LEVEN PS ELIMINATION	31-Dec-22	31-Dec-22	31-Dec-22																																
<b>CAVEN AVENUE WW STORAGE</b>	31-Dec-16	31-Dec-24	31-Dec-16																																
CAVEN AVENUE PS ELIMINATION	31-Dec-16	31-Dec-24	31-Dec-16																																
<b>SMALL WWTP AREA</b>	31-Dec-21	31-Dec-21	31-Dec-21																																
<b>RIDING RIDGE PS IMPROVEMENTS</b>	31-Dec-14	31-Dec-14	31-Dec-14																																
RIDING RIDGE PS IMPROVEMENTS	31-Dec-14	31-Dec-14	31-Dec-14																																
<b>LUCAS LN PS INLINE STORAGE</b>	31-Dec-21	31-Dec-21	31-Dec-21																																
LUCAS LN PS INLINE STORAGE	31-Dec-21	31-Dec-21	31-Dec-21																																
<b>ST. RENE RD PS INLINE STORAGE</b>	31-Dec-21	31-Dec-21	31-Dec-21																																
ST. RENE RD PS INLINE STORAGE	31-Dec-21	31-Dec-21	31-Dec-21																																
<b>LAKE FOREST PS IMPROVEMENTS</b>	31-Dec-12	31-Dec-12	31-Dec-12																																
LAKE FOREST PS IMPROVEMENTS	31-Dec-12	31-Dec-12	31-Dec-12																																
<b>GUNPOWDER PS INLINE STORAGE</b>	31-Dec-21	31-Dec-21	31-Dec-21																																
GUNPOWDER PS INLINE STORAGE	31-Dec-21	31-Dec-21	31-Dec-21																																
<b>FOX HARBOR INLINE STORAGE</b>	31-Dec-21	31-Dec-21	31-Dec-21																																
FOX HARBOR INLINE STORAGE	31-Dec-21	31-Dec-21	31-Dec-21																																
<b>FAIRWAY VIEW PS IMPROVEMENTS</b>	31-Dec-14	31-Dec-14	31-Dec-14																																
FAIRWAY VIEW PS IMPROVEMENTS	31-Dec-14	31-Dec-14	31-Dec-14																																
<b>SOUTHEASTERN DIVERSION AREA</b>	31-Dec-23	31-Dec-23	31-Dec-23																																
<b>PARKVIEW ESTATES I/I INVESTIGATION &amp; REHABILITATION</b>	28-Jun-11	A 30-Jun-11	30-Jun-11																																
PARKVIEW ESTATES I/I INVESTIGATION & REHABILITATION	28-Jun-11	A 30-Jun-11	30-Jun-11																																
<b>SUTHERLAND INTERCEPTOR</b>	31-Dec-23	31-Dec-23	31-Dec-23																																
SUTHERLAND INTERCEPTOR	31-Dec-23	31-Dec-23	31-Dec-23																																
<b>BEARGRASS INTERCEPTOR REHABILITATION PH 2</b>	14-Dec-10	A 31-Dec-10	31-Dec-10																																
BEARGRASS INTERCEPTOR REHABILITATION PH 2	14-Dec-10	A 31-Dec-10	31-Dec-10																																

  Approved 2009 IOAP    
   Remaining Work  
  Completed Work



# Executive Summary

## Attachment 1



## MEMORANDUM

**TO:** Louisville and Jefferson County Metropolitan Sewer District Board

**FROM:** Stakeholder Members of the Wet Weather Team

**DATE:** December 10, 2008

**SUBJECT:** Draft Integrated Overflow Abatement Plan

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As stakeholder members of MSD's Wet Weather Team (WWT), we wish to indicate our support for the Final Integrated Overflow Abatement Plan (IOAP) as MSD transmits the plan to the U.S. Environmental Protection Agency (EPA) and the Kentucky Environmental and Public Protection Cabinet. The attached document, "Vision for MSD's Integrated Overflow Abatement Plan," summarizes the Wet Weather Team's common understanding of the high-level architecture and components of the IOAP. As stakeholder members of the WWT, we played an active role in developing the IOAP Vision. Our support for the IOAP is based on the expectation that the complete plan is fully reflective of and consistent with the IOAP Vision. We support this vision for improving wet weather sewer overflow management in our community. In this memorandum, we review the composition and charge of the Wet Weather Team, describe the results of the stakeholder subgroup's deliberations, and outline our support for the IOAP.

### **Wet Weather Team Composition and Charge**

The Wet Weather Team consists of community representatives, elected officials, MSD personnel, and technical consultants. The nineteen stakeholders on the Wet Weather Team include individuals recognized as community opinion leaders associated with environmental advocacy, business and industry, elected officials, local government, community neighborhood, recreation, public health, environmental justice, and organized labor interests. WWT stakeholders have not formally represented their specific affiliated organizations as part of the team, but rather have provided input reflective of the broad interest areas in which they lead.

MSD chartered the stakeholder subgroup of the Wet Weather Team to "provide guidance on the development of an integrated Wet Weather Program that will comply with applicable regulatory requirements and will minimize the impacts of wet weather discharges on water quality, aquatic biota, and human health." Through MSD's consent decree with EPA and the Kentucky Environmental and Public Protection Cabinet, the WWT was charged with two primary tasks: (1) preparing a plan for funding MSD's overflow abatement program and (2) developing a program for public information, education, and involvement. In addition to these tasks, MSD sought guidance from WWT stakeholders on MSD's overall investment, policy, and performance choices in the development of the IOAP.

### **Results of the Wet Weather Team's Deliberations**

The Wet Weather Team met 22 times from July 2006 through December 2008 and provided input on all major components of the IOAP, as well as the analytic framework and the public involvement process MSD used to develop the IOAP. The WWT also met to review the public comments submitted on the Draft IOAP and discuss the changes proposed for the Final IOAP. There are four areas of the WWT stakeholder subgroup's deliberations that we would like to highlight, as follows.

1. Development of the Analytic Framework: The WWT stakeholders, along with other WWT members, identified and agreed upon a set of community values to use in the development of MSD's IOAP. We also advised MSD's technical team on a performance evaluation framework for using those values to evaluate project alternatives for MSD's IOAP. The performance evaluation framework includes both a benefit-cost scoring methodology for selecting the best alternatives at the project level and a systematic process for considering values that relate to the program as a whole. (This analytic framework is further described in the attached Vision.) We believe that this analytic framework is rigorous, transparent, and replicable, and that it provides an effective way to understand and balance tradeoffs among potentially conflicting community interests.
2. Application of the Analytic Framework: The WWT stakeholder subgroup has reviewed examples of how MSD's technical team has used the values-based performance evaluation framework to evaluate project alternatives to address combined sewer overflow (CSO) and sanitary sewer overflow (SSO) problems in our community. Moreover, we have also reviewed and provided input on how the technical team has evaluated the IOAP according to the WWT's programmatic community values—customer satisfaction, economic vitality, education, environmental justice and equity, financial equity, and financial stewardship. We believe that the analytic framework has been applied consistent with the WWT's expectations in the development of the IOAP and has produced a robust, replicable, and transparent analysis.
3. IOAP Vision: We helped develop the attached "Vision for MSD's Integrated Overflow Abatement Plan" along with the MSD personnel and technical consultants who are on the Wet Weather Team. The IOAP Vision summarizes the WWT's common understanding of the high-level architecture and components of the IOAP, and it documents the WWT's consensus about several crucial aspects of the IOAP. The Vision outlines and provides highlights of the expected water quality benefits of the IOAP; the levels of control for CSOs and SSOs in our community; the range of control options in the IOAP; the analytic framework and process used to select control options; the public information, education, and involvement program (known as "Project WIN"); the monitoring, evaluation, and adaptive management plan; future development considerations relevant to the IOAP; and the IOAP funding plan. As stakeholder members of the WWT, we support this vision for improving wet weather sewer overflow management in our community.
4. Summary of IOAP Projects: We believe the project mix and outcomes that form the backbone of the IOAP (as captured in the attached IOAP Vision) reflect responsiveness to MSD's consent decree and provide for a critical, first increment of water quality improvement for our community, while ensuring wise and effective use of our community's resources. The IOAP Vision draws on front end consideration of and investment in green infrastructure and other source control approaches, including "private side" inflow and infiltration (I&I) control. These early investments will act to test and demonstrate the effectiveness of these approaches, creating the prospect, based on demonstrated performance, for expanding their role and lowering community costs as MSD implements the IOAP. We understand that MSD, consistent with the Post-Construction Compliance Monitoring Plan, will closely monitor and report on the efforts for both regulatory and public education purposes. We further understand that MSD, over the coming months, will work with community members to further articulate and enhance the scope and scale of its IOAP public education and outreach program, including developing a robust approach for measuring the effectiveness of the program.

As MSD moves forward in coming years with IOAP implementation, we do anticipate the program will face, as all programs of this type do, project-specific challenges related to local community understanding and acceptance. In this context, we understand MSD is committed to using focused and sustained neighborhood education and outreach efforts to support project-specific and overall program implementation and will strive to address localized needs consistent with overall IOAP requirements. At the same time, we believe all localities throughout the MSD system must keep in mind that individual IOAP project locations and types have emerged from a rigorous and consistently applied technical analysis. The IOAP projects exist as critical building blocks for an overall community program framed by federal and state regulatory requirements, community water quality and public health improvement objectives, and overall rate payer capacity.

The stakeholder subgroup of the Wet Weather Team appreciates the opportunity to have contributed to MSD's IOAP development efforts. During our final meeting on December 4, 2008, we discussed the importance of an overarching, sustained community water quality education initiative directed at enhancing appreciation for water quality improvements and building understanding of the actions all members of the community can take to improve water quality. We understand this effort is substantially broader in scope than the CSO and SSO improvements addressed by the IOAP, but we believe it is important to take this opportunity to raise awareness for this need, particularly as our community turns its attention to stormwater management in the context of the multi-jurisdictional Municipal Separate Storm Sewer System (MS4) permit. We appreciate MSD's willingness to be a contributor to such an effort, even as we recognize the need for broader involvement and leadership throughout the Louisville community and across Louisville Metro Government.

We look forward to the MSD Board's review of the Final IOAP and MSD's submittal of the Final IOAP to EPA and the State of Kentucky by December 31, 2008. Thank you for the opportunity to contribute to this critical community improvement initiative. Please feel free to contact us individually or collectively with any questions or perspectives you may have.

### Stakeholder Members of the Wet Weather Team

<b><u>Member</u></b>	<b><u>Organization*</u></b>
Steve Barger	Labor
Susan Barto	Mayor of Lyndon
Stuart Benson	Louisville Metro Council, District 20
Charles Cash	Louisville Metro Planning & Design Services
Allan Dittmer	University of Louisville
Laura Douglas	E.ON U.S. LLC
Faye Ellerkamp	City of Windy Hills
Arnita Gadson	West Jefferson County Community Task Force / Kentucky Environmental Quality Commission
Mike Heitz	Louisville Metro Parks Department
Tom Herman	Zeon Chemicals
Rick Johnstone	Deputy Mayor, Louisville Metro Mayor's Office
Bob Marrett	CMB Development Company, LLC
Kurt Mason	Jefferson County Soil and Water Conservation District
Judy Nielsen	Louisville Metro Department of Public Health and Wellness
Lisa Santos	Irish Hill Neighborhood Association
Bruce Scott	Kentucky Waterways Alliance
David Tollerud	University of Louisville, School of Public Health and Information Sciences
Tina Ward-Pugh	Louisville Metro Council, District 9
David Wicks	Jefferson County Public Schools

\*Stakeholders on the Wet Weather Team do not formally represent their specific affiliated organizations, but rather seek to provide input reflective of the broad interest areas in which they lead. Along with the stakeholder subgroup, the Wet Weather Team includes MSD personnel and technical consultants.



# Executive Summary

## Attachment 2



## **Vision for MSD's Integrated Overflow Abatement Plan December 10, 2008**

*This document summarizes the vision for MSD's Integrated Overflow Abatement Plan (IOAP), as understood and endorsed by the Wet Weather Team (WWT).*

### **Scope of the Integrated Overflow Abatement Plan and Expected Water Quality Benefits**

The Louisville and Jefferson County Metropolitan Sewer District's Integrated Overflow Abatement Plan is a long-term plan to control combined sewer overflows (CSOs) and sanitary sewer overflows (SSOs) in the community. The IOAP is expected to improve water quality in both Jefferson County streams and the Ohio River. The expected water quality benefits of the IOAP include: (a) reductions in the peak levels of bacteria in Beargrass Creek and other Jefferson County waterways; and (b) a reduction in the duration of wet weather impairment of local waterways (i.e., the number of days that bacteria levels exceed water quality standards during periods of wet weather). The IOAP—in coordination with other community water quality initiatives (further described below)—will also improve water quality under ambient conditions.

The specific benefits anticipated from the IOAP include the following:

- The suite of projects selected for the Long Term Control Plan (LTCP) for CSOs will result in approximately 95 percent capture and treatment of wet weather combined sewage during an average year. (As a point of reference, the “presumptive approach” in EPA’s CSO Control Policy is based on a minimum of 85 percent wet weather capture.)
- Remaining CSO loads (after removing background) will no longer “cause or contribute” (as defined in EPA’s CSO Control Policy) to water quality standard violations in the Ohio River. Peak fecal coliform counts are modeled to be reduced by 54 percent, from 100,000 colony forming units per 100 milliliter (cfu/100mL) to 46,000 cfu/100 mL (downstream from Morris Forman Wastewater Treatment Plant).
- In Beargrass Creek peak fecal coliform counts are modeled to be reduced by 18 percent, from 44,300 cfu/100mL to 37,400 cfu/100 mL (at the mouth of Beargrass Creek). The control level associated with these reductions exceeds the EPA CSO Control Policy “presumptive approach,” 85 percent wet weather capture threshold and reflects a point of significantly diminishing returns under the “knee of the curve” benefit-cost analysis.
- The suite of projects selected for the Sanitary Sewer Discharge Plan (SSDP) for SSOs will result in the elimination of capacity-related SSOs up to the site-specific level of protection (described below).
- The SSO projects are anticipated to eliminate an average of 145 SSO events per year, based on 2005–2007 data.
- In terms of water quality, SSO projects will eliminate an average of 290 million gallons of overflow volume per year (average of 2005–2007 normalized for rainfall), eliminating 100 tons of 5-day biochemical oxygen demand (BOD5) and almost 200 tons of solids annually.

Along with delivering water quality improvements from sewer overflow control, MSD participates in other community water quality improvement efforts. Sewer overflow control is essential to improving water quality, but overflow control alone is not enough to meet water quality standards. In light of this challenge, MSD will continue to leverage its role in supporting broader water quality improvement efforts in the community. The IOAP will be one of the key elements of MSD’s participation in those water quality improvement efforts. In particular, the IOAP will be complementary to other wet weather and water quality programs managed by MSD and/or by other community partners. These complementary

efforts include, but are not limited to, the Mayor’s “Go Green Louisville” Initiative, the Partnership for a Green City, Metro Louisville’s Municipal Separate Storm Sewer System (MS4) discharge permit, and initiatives of Jefferson County Public Schools (JCPS), private developers, and other entities.<sup>1</sup>

The specific ways in which MSD is collaborating with other entities on community water quality improvement initiatives include the following:

- **Partnership for a Green City:** MSD is actively working with Louisville Metro Government, JCPS, and the University of Louisville to improve water quality through the Partnership for a Green City. The Partnership has established a Stormwater Committee that will be identifying opportunities to improve water quality associated with planned capital projects.
- **Metro Government:** MSD is an active participant in the Mayor’s Go Green Louisville Initiative, which includes in its vision a commitment to focus on financially sustainable measures that improve air and water quality, land use, and energy efficiency. In coordination with this initiative, MSD is partnering with Louisville Metro Government on several green infrastructure demonstration projects in the IOAP.
- **MS4 Program:** MSD will coordinate IOAP implementation with the agencies that share implementation of the MS4 Program—including Metro Louisville government, small cities that handle their own drainage, and the Kentucky Department of Transportation. The MS4 program will draw upon the opportunities identified through the green infrastructure analysis conducted by MSD’s IOAP technical team and the ideas suggested by WWT members during the development of the IOAP. MSD further anticipates implementing demonstration projects, such as rain gardens in the separate sewer area, under the MS4 as part of a coordinated effort with the IOAP to test and evaluate green infrastructure approaches to wet weather management.

The IOAP—as part of MSD’s wet weather consent decree response—will be a federally enforceable action plan for sewer overflow abatement. Although many IOAP projects and programs will provide multiple benefits to the community, the scope of the IOAP is limited to commitments that directly relate to MSD programs and activities to address combined sewer overflow (CSO) and sanitary sewer overflow (SSO) issues. Other community water quality programs, which may be partly or completely out of MSD’s control, can provide synergistic benefits with the IOAP, but they do not fall under the same federal enforcement. These programs may, however, have different mechanisms for ensuring accountability (e.g., the State of Kentucky oversees the MS4 stormwater permit that MSD and several other agencies hold). As noted above, MSD anticipates coordinating IOAP implementation with the water quality improvement initiatives of Louisville Metro Government and other public and private entities, even though these broader initiatives may not explicitly be part of the IOAP.

## **Values-Based Performance Evaluation Framework Used to Develop the IOAP**

MSD developed the IOAP using a values-based performance evaluation framework established by the Wet Weather Team. This analytic framework includes both a robust benefit-cost scoring methodology for evaluating and selecting project alternatives and a systematic process for evaluating the IOAP programmatically. The Wet Weather Team identified and agreed upon the following eleven community values that underpin the analysis and selection of alternatives for the IOAP.

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<sup>1</sup> More information about these initiatives is available on the following websites: Go Green Louisville ([www.louisvilleky.gov/GoGreen](http://www.louisvilleky.gov/GoGreen)), Partnership for a Green City ([www.partnershipforagreencity.org](http://www.partnershipforagreencity.org)), and MS4 program ([www.msdlouky.org/insidemsd/wwwq/ms4](http://www.msdlouky.org/insidemsd/wwwq/ms4)).

### *Project-Specific Values*

- Asset protection
- Eco-friendly solutions
- Environmental enhancement
- Public health enhancement
- Regulatory performance

### *Programmatic Values*

- Customer satisfaction
- Economic vitality
- Education
- Environmental justice and equity
- Financial equity
- Financial stewardship

Using the structured decision-making process as framed by the Wet Weather Team, MSD developed and evaluated overflow abatement control options for the IOAP based on managing risks to these community values. In particular, MSD's technical team analyzed each project alternative considered for the IOAP in terms of potential benefits and costs, where "benefits" are quantified based on the anticipated reduction in risks to the community values and "costs" reflect the total capital and operational costs of the alternative. The benefit-cost analysis influences the selection of site-specific abatement approaches or technologies, site-specific levels of protection (within the boundary conditions for CSOs and SSOs described below), and the relative priority of projects for implementation.

Several of the Wet Weather Team's community values relate to financial considerations, including the cost-effectiveness of individual solutions and the program as a whole (financial stewardship), the affordability of the program's total costs for the community (economic vitality), and how the costs are allocated among different segments of the population (financial equity). The Wet Weather Team has used the results of the values-based benefit-cost analysis of project alternatives to provide context to discussions about the appropriate level of investment in the IOAP.

The WWT's discussions about total program costs and the selection of projects for the IOAP have considered, as directed in EPA's CSO Control Policy, a "knee of the curve" analysis to determine where the increment of pollution reduction achieved in the receiving water diminishes compared to the increased costs. In addition to this analysis, the community's level of investment in the IOAP has been considered in the context of anticipated future requirements and other needs for MSD services, including stormwater compliance needs associated with Metro Louisville's MS4 permit and requirements to meet the forthcoming total maximum daily load (TMDL) allocations for Beargrass Creek. This consideration of other water quality investment needs is important since sewer overflow control alone will not be sufficient to meet water quality standards.

The technical team's analysis of the IOAP according to the WWT's programmatic values yielded the following conclusions.

- **Customer Satisfaction:** The IOAP ensures service continuity by eliminating several small wastewater treatment plants and pump stations and by incorporating redundant equipment and standby generators. Odor control guidelines have been consistently applied across all projects. Most storage basins proposed in the IOAP will be covered. Other storage basin and pump station improvement projects incorporate odor control equipment.
- **Economic Vitality:** MSD's current rates are near the national average. The anticipated annual rate increases of 5–6.5 percent are consistent with initial estimates of program costs, and they include allowances for future MSD programs as well as IOAP implementation. Even with these rate increases, MSD's rates are anticipated to remain at or near the national average, assuming other communities face similar inflation and regulatory pressures. These estimates are based on current data; many unknown factors (e.g., bond market, climate change, etc.) will also affect future rates.

- **Education:** Education is an integral and essential component of the IOAP. It supports a number of IOAP objectives, including promoting and sustaining participation in green infrastructure and source control efforts, and building a sense of personal responsibility and support for clean water initiatives.
- **Environmental Justice and Equity:** The site selection process followed uniform criteria across the county, with most solutions placed near overflow points and with no homes or private businesses permanently displaced. Furthermore, the configuration of facilities was based on a uniform application of written design criteria and odor control criteria. Other nuisance conditions will be minimized during the design and construction phases of projects.
- **Financial Equity:** MSD's rate structure is based on a cost-of-service model tempered by consideration of customers' ability to pay. The rate increases proposed to fund the IOAP and other MSD programs will continue to be based on the cost of service, but MSD will recommend to the Board that the existing low income, senior citizen discount program be expanded. The IOAP also proposes subsidies and incentives for green infrastructure and infiltration and inflow (I&I) control based on their business value for overflow abatement.
- **Financial Stewardship:** As described above, the IOAP is based upon a rigorous benefit-cost analysis that considered a broad range of technology alternatives and different levels of control that met or exceeded regulatory guidelines. The "knee of the curve" evaluations of IOAP projects demonstrated that the IOAP provides a high level of control, but does not exceed the point of diminishing returns.

## **Control Levels for Combined Sewer Overflows and Sanitary Sewer Overflows**

Under the Clean Water Act, CSOs are permitted discharges in wet weather, as long as they are managed to avoid degradation of water quality in the receiving streams. EPA's CSO Control Policy<sup>2</sup> sets specific abatement targets for CSOs. To be permitted, wet-weather CSOs must be controlled so that either water quality standards are achieved or the permit-holder can show that the CSO discharges do not cause or contribute to exceedances of water quality standards. Based on EPA's CSO Control Policy, EPA may respond to MSD's proposed strategy for controlling wet weather CSO discharges indicating a need for a temporary variance or suspension of water quality standards during wet weather. Variances are temporary, not permanent, solutions to achieve compliance with the Clean Water Act. As stated in EPA's CSO Control Policy, variances are reviewable generally every three years.

CSO projects in the IOAP have the following levels of control:

- 6 projects result in no overflows in a typical year; these locations would only overflow as a result of very large storms.
- 1 project would result in four overflows per year in a typical year.
- 11 projects result in eight overflows per year in a typical year.

MSD's strategy for SSO control reflects the fact that SSOs, unlike wet-weather CSOs, are unauthorized discharges that must be "eliminated" under the Clean Water Act. In the IOAP, the values evaluation framework has been used to evaluate a range of site-specific design storms to establish the appropriate level of control of SSOs. Consistent with an analysis of sixty years of historical weather patterns for Jefferson County, the IOAP uses a three-hour "cloud burst" storm, with a statistically anticipated rainfall of 1.82 inches, as the minimum design storm considered. The Cities of Atlanta, Cincinnati, and Knoxville used similar design storms as the minimum protection level for SSO control. The approach of using the values evaluation framework to determine the SSO control level means that solutions to address certain SSOs have been designed to protect against larger storms (e.g., a 2.25-inch cloudburst storm

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<sup>2</sup> EPA's Combined Sewer Overflow Control Policy is available at <http://cfpub1.epa.gov/npdes/cso/cpolicy.cfm>.



instead of a 1.82-inch cloudburst storm) because they yield a higher benefit-cost ratio in the analysis of project alternatives.

SSO projects in the IOAP have the following levels of control:

- 30 projects eliminate overflows up to a 1.82-inch cloudburst storm.
- 9 projects eliminate overflows up to a 2.25-inch cloudburst storm.
- 7 projects eliminate overflows up to a 2.60-inch cloudburst storm.

### **Components of MSD's Integrated Overflow Abatement Plan**

Control options in the IOAP (the IOAP “toolkit”) include source control (including green infrastructure and infiltration and inflow [I&I] reduction efforts), storage, conveyance/transport, treatment, and sewer separation. MSD’s technical team has used the benefit-cost tool to compare the project alternatives and program elements considered for inclusion in the IOAP. The specific mix of control options for individual CSO or SSO locations in the IOAP is driven by the benefit-cost analysis of how the project alternatives affect the WWT’s community values and site-specific considerations. Project alternatives are built around MSD’s existing infrastructure (e.g., large diameter pipes and wastewater treatment plants) and draw on synergistic benefits from other MSD projects (e.g., the “Big Four” SSO projects). Furthermore, project budgets include an enhanced site restoration allowance to fund localized opportunities to reduce historical overflow impacts on aquatic and riparian environments near the sites of overflow abatement projects.

Driven by the values-based benefit-cost analysis, the IOAP reflects a balanced mix of green and gray solutions to prevent and control sewer overflows. “Green” solutions include options such as green roofs, rain gardens, rain barrels, porous pavement, and bioretention, while “gray” solutions include options such as storage, treatment, conveyance/transport, and sewer separation. As a guiding principle, MSD’s IOAP has been developed based on front-end consideration of source control and green infrastructure. This means that more traditional “gray” infrastructure in the IOAP has been sized after considering both (1) the anticipated flow-reduction benefits of programmatic and site-specific green infrastructure solutions and (2) the anticipated effectiveness of other source control approaches, including reduction of private sources of I/I. Green solutions in the IOAP will be implemented as soon as possible, to allow data to be gathered on the flow reduction benefits that occur. Prior to the final design of supporting gray solutions, the actual flow reduction performance will be documented and compared against the estimated targets. The final sizing of the gray solutions will then be based on actual documented performance of green solutions, as well as any further green and source control investments justified by performance information. Green infrastructure investments are estimated to reduce the initial costs of CSO gray infrastructure projects by \$40 million; potential future savings could double or triple this figure.

As defined in the IOAP, the 19 gray infrastructure projects to control CSOs include:

- 4 sewer separation projects;
- 13 storage basin projects (This includes in-line and off-line storage; most in-line storage projects have a Real-Time Control component.);
- Replacement and expansion of the Nightingale Sanitary Pump Station; and
- 1 high-rate wet weather treatment project (screening, settling, and disinfection).

The 46 gray infrastructure projects to control SSOs in the IOAP include:

- 15 conveyance capacity upgrades and interceptor relief projects;
- 19 storage projects (in-line and off-line storage, many with pipe upgrades also);
- 1 sewer replacement project for Beechwood Village (one of the “Big 4 SSOs”);and
- 11 pump station and wastewater treatment plant upgrades, eliminations, or replacements. These projects include expanding the wet weather capacity of the Derek R. Guthrie Water Quality Treatment Center, elimination of 5 small wastewater treatment plants in the Prospect area, and potentially the elimination of the Jeffersontown Wastewater Treatment Plant.

The IOAP includes both an annual green infrastructure program and an initial set of green infrastructure demonstration projects. The green infrastructure program is front-end loaded to maximize benefits on downsizing future gray infrastructure. For example, the IOAP project schedule calls for a \$40 million investment in green infrastructure programs and projects during the first six years. Programmatic green infrastructure components in the IOAP include a downspout disconnect program, green roof construction subsidies or incentives, green roads and alleys partnership incentives, and pervious pavement sidewalks and parking. MSD has based the proposed incentives and subsidies on a “business case” analysis of the financial benefit of green infrastructure in terms of costs per gallon of flow removed from the combined sewer system. Through the anticipated green infrastructure partnership, incentive, and education programs, MSD’s initial \$40 million investment in green infrastructure has the potential to leverage \$60 million more from other private and public funding sources, thereby yielding up to \$100 million in green infrastructure projects.

MSD plans to construct a series of new green infrastructure demonstration projects across Jefferson County. The proposed green infrastructure projects in the combined sewer area will be part of MSD’s IOAP, while the proposed green infrastructure projects outside the combined sewer area will be a part of the community’s MS4 stormwater program. These demonstration projects are designed to achieve three main objectives: (1) improve water quality and reduce sewer overflows, (2) provide data on green infrastructure effectiveness, and (3) educate community members about the value and benefits of green infrastructure. All green infrastructure demonstration projects in the IOAP will incorporate a monitoring component, so that the effectiveness of the projects can be tracked over time and regularly reported to regulators and the public. MSD will then use these monitoring results to guide future IOAP implementation, under the IOAP’s adaptive management plan (further described below).

This vision currently reflects a minimum commitment to 18 green infrastructure demonstration projects in the IOAP. These proposed new green infrastructure demonstration projects (which are subject to partnership and regulatory approval) include:

- 6 bioswale and biofiltration projects (e.g., green parking lots and green streets);
- 4 rain gardens;
- 3 pervious concrete alleys; and
- 5 infiltration dry wells.

MSD plans to expand and enhance this proposed suite of demonstration projects in response to feedback from WWT members that the initial projects might not be sufficient to achieve the objective of educating the public and building support for green infrastructure. In particular, MSD will look to enhance the distribution of demonstration projects in Jefferson County (including considering green infrastructure projects in each Metro Council District) and the numbers of individual project types.

MSD's technical team has analyzed potential options to control private sources of I/I into the sanitary sewer system, including building laterals, downspouts, sump pumps, and foundation drains. This analysis indicates that private-side I/I control is an essential part of the IOAP, and it will reduce the overall anticipated costs of overflow abatement. The technical team has analyzed options for adopting a requirement for inspections of private properties (e.g., during the property transfer process, when building permits are issued, when contractors install roof and gutter systems, when plumbers connect sump pumps, and/or at other times), along with providing some form of cost share and conducting an aggressive education campaign. MSD will work with Metro Government to support further development and adoption of an ordinance supporting these requirements. Although I&I reduction is particularly relevant to SSO control (since the sanitary sewer system was not designed to accept inflow), it may be useful to have similar requirements for the combined sewer system.

## **Public Information, Education, and Involvement Program**

Education and public involvement are critical to the long-term implementation success of the IOAP. MSD uses the term "Project WIN" (Waterway Improvements Now) to describe its consent decree response activities to the public. The ongoing public information, education, and involvement program for Project WIN is designed to accomplish the following objectives:

1. Generate a sense of personal ownership and responsibility for clean water;
2. Promote and sustain participation in critical voluntary programs in the IOAP, including private-side I&I control and green infrastructure;
3. Promote public acceptance and support for the financial investments required to achieve consent decree and Clean Water Act compliance; and
4. Encourage support for other agency programs or legislation that supports overflow abatement efforts.

To achieve these objectives, the Project WIN education and public involvement program uses a wide range of communication media. In particular, the program includes the following elements:

- Public meetings and community events;
- Enhanced web portal for Project WIN;
- Speaker's bureau and technical support;
- Print and electronic media (e.g., print advertisements, press releases, targeted brochures and pamphlets, reports, newsletters, billing inserts, public TV video, radio announcements, etc.);
- Recognition programs;
- Demonstration projects;
- Tours, demonstrations, and workshops;
- Enhanced school partnerships; and
- Annual effectiveness monitoring through direct mail and phone surveys.

These public involvement efforts are focused on several key audiences, including the general public, schools and children, and target groups such as property owners, project neighborhoods, builders, and restaurants. Focusing education efforts on children is important to ensure the long-term sustainability of voluntary programs in the IOAP. For the general public, MSD is using five key messages:

1. Value clean water.
2. Your investment is paying dividends, and our water is getting cleaner.
3. Protecting public health is critically important.

4. MSD and many community partners are working hard to improve water quality.
5. You can make a difference in improving water quality.

## **Post-Construction Compliance Monitoring**

MSD's IOAP will use an adaptive management implementation approach based on monitoring and evaluation efforts. MSD's post-construction compliance monitoring and evaluation plan for the IOAP includes: (a) water quality monitoring, (b) sewer flow monitoring, (c) overflow events analysis, (d) gray and green infrastructure project performance monitoring, and (e) measurement of the effectiveness of source control and behavior-change efforts. MSD will prepare both required regulatory and public education reports from these data and adapt the CSO management and SSO elimination approaches based on the monitoring and evaluation results. Adjustments may include recalibrating models, "right-sizing" gray solutions, reevaluating the effectiveness of green solutions, and adjusting the types and characteristics of projects planned for later phases of implementation, including additional investments in green infrastructure and source control beyond those proposed in the initial program. At this time there is recognition that historical weather trends may not be as reliable as in the past due to potential changes in the climate. The IOAP's adaptive management approach will allow MSD to monitor evolving weather pattern developments and adjust its plans as more data become available.

## **Future Development Considerations**

Solutions in the IOAP consider future development based on the community's long-term land-use plan, Cornerstone 2020.<sup>3</sup> IOAP solutions are designed to accommodate the anticipated impacts of population growth and land-use development in that the solutions consider the effects of growth on connections to existing infrastructure that is upstream from existing overflow points. The IOAP is not, however, intended to provide capacity for all future growth predicted by Cornerstone 2020. Cases where the growth outlined in Cornerstone 2020 would logically be provided by new infrastructure, and not hydraulically dependent on or connected to the IOAP solution, have not been considered part of the IOAP. In summary, the solutions in the IOAP have been designed and sized to account for the impacts of anticipated growth on existing infrastructure, but the IOAP itself is not intended to build the capacity needed for growth.

MSD's Capacity, Management, Operations, and Maintenance (CMOM) Program, which is part of MSD's Consent Decree response but separate from the IOAP, includes standard operations and maintenance activities practices designed to, among other things, investigate capacity-constrained areas of the sewer system. The CMOM program also includes a System Capacity Assurance Program focused on providing capacity for current and future service needs.

Continued development in the community will require MSD to implement measures to reduce wet-weather flows. MSD will use a three-to-one offset of wet-weather flows from new development. This means that existing flows entering MSD's sanitary sewer systems will be reduced at a ratio of three gallons for every new gallon added. MSD's flow reduction efforts will be designed to correct deficiencies in the existing sewer system in the same geographic areas (sewersheds) of the system affected by the flows from new development. MSD will track flow reduction "credits" to ensure that the flow reductions occur in the appropriate geographic locations to offset the new flows. (This three-to-one offset approach is based on the City of Knoxville's Capacity Assurance Program.) The MSD Board will develop the fee structure for the offset plan.

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<sup>3</sup> For more information about the Cornerstone 2020 plan, see [www.louisvilleky.gov/PlanningDesign/Cornerstone+2020.htm](http://www.louisvilleky.gov/PlanningDesign/Cornerstone+2020.htm).

## Funding Plan

The funding plan for the IOAP is designed to cover the 15-year period over which IOAP capital projects will be constructed to improve MSD's sewer infrastructure to meet the requirements of the consent decree. The IOAP funding plan is based on the following three principles:

- Rates and fees for the IOAP must pay MSD's operating costs and debt service.
- MSD's current bond rating (AA) should, at a minimum, be maintained.
- Rates and fees should allow for continued economic development in the community and a strong local economy.

These principles for the funding plan affect the amount of money MSD may borrow at any one time and the level of increases in rates and fees needed to fund capital and operating expenses for IOAP implementation.

MSD will fund the IOAP primarily through a combination of annual rate increases and bond issues or other loans. MSD also plans to pursue grants, line-item appropriations, and public/private partnerships (e.g., recapture agreements) to help pay for capital construction costs, as appropriate; however, the funding plan is not built around these funding sources since they are less certain. Using the estimate that the consent decree will cost \$843 million in capital expenditures, average bills for residential customers are expected to increase from 5 to 6.5 percent annually through 2021. This means that the average residential bill would increase from \$29.58 in 2008 to approximately \$63.12 by 2024 due to the consent decree capital construction expenses. Along with these rate increases, MSD expects to borrow approximately \$1.25 billion by 2024 based on the estimates of capital costs; this would increase MSD's debt service payments from \$94 million annually to \$163 million annually by 2025.<sup>4</sup> A mixture of fixed and variable rate borrowings is anticipated. These rate increases and loans would be used to address both IOAP construction costs and other MSD capital needs for infrastructure renewal, replacement, and expansion.

Estimates of IOAP costs appear to be within community tolerance for rate increases; however, the rate increases could nevertheless be difficult for some segments of the population to afford, especially in the context of other expenses. For this reason, the Wet Weather Team has considered potential ways to provide discounts to customers that face financial hardship. In the IOAP funding plan, MSD proposes a few changes to MSD's existing rate structure for the Board to consider. These changes are designed to accomplish two objectives: (1) provide discounts for low-income populations and (2) ensure steady and predictable revenue flows overall. The specific rate structure changes currently under study and reflected in the IOAP funding plan include the following:

- Residential customer billing based on winter consumption;
- Potentially billing customers on a monthly basis (in coordination with the Louisville Water Company).
- Expansion of the senior citizens discount program.

As noted above, MSD will construct the capital projects in the IOAP over a 15-year period, in order to meet the regulatory requirements of the consent decree and achieve compliance with the Clean Water Act. Many of the elements of the IOAP—including the Project WIN education program, operations and maintenance of IOAP projects, and monitoring and evaluation programs—will also continue past the construction phase of the IOAP. MSD is committed to making sure that the IOAP programs and projects provide for long-term improvements in water quality in Louisville and Jefferson County.

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<sup>4</sup> This estimate assumes that interest rates are in the 5 to 6 percent range.



# Executive Summary

## Attachment 3



## MEMORANDUM

**TO:** Louisville and Jefferson County Metropolitan Sewer District Board

**FROM:** Stakeholder Members of the Wet Weather Team

**DATE:** January 30, 2013

**SUBJECT:** Draft Integrated Overflow Abatement Plan 2012 Modifications

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As stakeholder members of MSD's Wet Weather Team (WWT), we wish to indicate our support for the Final Integrated Overflow Abatement Plan (IOAP) 2012 Modifications as MSD transmits the plan modifications to the U.S. Environmental Protection Agency (EPA) and the Kentucky Environmental and Public Protection Cabinet. The attached documents, "Vision for MSD's Integrated Overflow Abatement Plan," and "2012 IOAP Project Modifications" summarize the Wet Weather Team's common understanding of the high-level architecture and components of the IOAP and the proposed 2012 Modification. As stakeholder members of the WWT, we played an active role in developing the IOAP Vision and are pleased to see that the principles of this Vision have been retained in the 2012 Modification. Our support for the IOAP and the 2012 Modification is based on the expectation that the complete plan is fully reflective of and consistent with the IOAP Vision and the 2012 IOAP Project Modifications documents attached. We support this vision for improving wet weather sewer overflow management in our community. In this memorandum, we review the composition and charge of the Wet Weather Team, describe the results of the stakeholder subgroup's deliberations, and outline our support for the IOAP.

### **Wet Weather Team Composition and Charge**

The WWT consists of community representatives, elected officials, MSD personnel, and technical consultants. The stakeholders on the WWT include individuals recognized as community opinion leaders associated with environmental advocacy, business and industry, elected officials, local government, community neighborhood, recreation, public health, environmental justice, and organized labor interests. WWT stakeholders have not formally represented their specific affiliated organizations as part of the team, but rather have provided input reflective of the broad interest areas in which they lead.

MSD chartered the stakeholder subgroup of the WWT to "provide guidance on the development of an integrated Wet Weather Program that will comply with applicable regulatory requirements and will minimize the impacts of wet weather discharges on water quality, aquatic biota, and human health." Through MSD's consent decree with EPA and the Kentucky Environmental and Public Protection Cabinet, the WWT was charged with two primary tasks: (1) preparing a plan for funding MSD's overflow abatement program and (2) developing a program for public information, education, and involvement. In addition to these tasks, MSD sought guidance from WWT stakeholders on MSD's overall investment, policy, and performance choices in the development of the IOAP.

### **Results of the Wet Weather Team's Deliberations**

The WWT met 22 times from July 2006 through December 2008 and provided input on all major components of the IOAP, as well as the analytic framework and the public involvement process MSD used to develop the IOAP. The WWT also met to review the public comments submitted on the Draft

IOAP and discuss the changes proposed for the Final IOAP. There are four areas of the WWT stakeholder subgroup's deliberations that we would like to highlight, as follows.

1. Development of the Analytic Framework: The WWT stakeholders, along with other WWT members, identified and agreed upon a set of community values to use in the development of MSD's IOAP. We also advised MSD's technical team on a performance evaluation framework for using those values to evaluate project alternatives for MSD's IOAP. The performance evaluation framework includes both a benefit-cost scoring methodology for selecting the best alternatives at the project level and a systematic process for considering values that relate to the program as a whole. (This analytic framework is further described in the attached Vision.) We believe that this analytic framework is rigorous, transparent, and replicable, and that it provides an effective way to understand and balance tradeoffs among potentially conflicting community interests.
2. Application of the Analytic Framework: The WWT stakeholder subgroup has reviewed examples of how MSD's technical team has used the values-based performance evaluation framework to evaluate project alternatives to address combined sewer overflow (CSO) and sanitary sewer overflow (SSO) problems in our community. Moreover, we have also reviewed and provided input on how the technical team has evaluated the IOAP according to the WWT's programmatic community values—customer satisfaction, economic vitality, education, environmental justice and equity, financial equity, and financial stewardship. We believe that the analytic framework has been applied consistent with the WWT's expectations in the development of the IOAP and has produced a robust, replicable, and transparent analysis.
3. IOAP Vision: We helped develop the attached "Vision for MSD's Integrated Overflow Abatement Plan" along with the MSD personnel and technical consultants who are on the Wet Weather Team. The IOAP Vision summarizes the WWT's common understanding of the high-level architecture and components of the IOAP, and it documents the WWT's consensus about several crucial aspects of the IOAP. The Vision outlines and provides highlights of the expected water quality benefits of the IOAP; the levels of control for CSOs and SSOs in our community; the range of control options in the IOAP; the analytic framework and process used to select control options; the public information, education, and involvement program (known as "Project WIN"); the monitoring, evaluation, and adaptive management plan; future development considerations relevant to the IOAP; and the IOAP funding plan. As stakeholder members of the WWT, we support this vision for improving wet weather sewer overflow management in our community.
4. Summary of IOAP Projects: We believe the project mix and outcomes that form the backbone of the IOAP (as captured in the attached IOAP Vision) reflect responsiveness to MSD's consent decree and provide for a critical, first increment of water quality improvement for our community, while ensuring wise and effective use of our community's resources. The IOAP Vision draws on front end consideration of and investment in green infrastructure and other source control approaches, including "private side" inflow and infiltration (I&I) control. These early investments will act to test and demonstrate the effectiveness of these approaches, creating the prospect, based on demonstrated performance, for expanding their role and lowering community costs as MSD implements the IOAP. We understand that MSD, consistent with the Post-Construction Compliance Monitoring Plan, will closely monitor and report on the efforts for both regulatory and public education purposes. We further understand that MSD, over the coming months, will work with community members to further articulate and enhance the scope

and scale of its IOAP public education and outreach program, including developing a robust approach for measuring the effectiveness of the program.

After IOAP approval in September 2009, the WWT Stakeholder Group continued to meet twice per year for progress reports and updates. When the need for the 2012 IOAP Modifications became apparent, MSD invited the original members of the WWT Stakeholder Group to continue to serve as a sounding board, ensuring the modifications to the plan and specific project designs remain true to values, priorities and financial plan that was originally developed. Most of the original members chose to continue their active participation in the process.

As MSD moves forward in coming years with IOAP implementation, we do anticipate the program will face, as all programs of this type do, project-specific challenges related to local community understanding and acceptance. In this context, we understand MSD is committed to using focused and sustained neighborhood education and outreach efforts to support project-specific and overall program implementation and will strive to address localized needs consistent with overall IOAP requirements. At the same time, we believe all localities throughout the MSD system must keep in mind that individual IOAP project locations and types have emerged from a rigorous and consistently applied technical analysis that has been continued through the 2012 IOAP Modifications. The IOAP projects exist as critical building blocks for an overall community program framed by federal and state regulatory requirements, community water quality and public health improvement objectives, and overall rate payer capacity.

The stakeholder subgroup of the WWT appreciates the opportunity to have contributed to MSD's IOAP development efforts. During our meeting on December 4, 2008, we discussed the importance of an overarching, sustained community water quality education initiative directed at enhancing appreciation for water quality improvements and building understanding of the actions all members of the community can take to improve water quality. We understand this effort is substantially broader in scope than the CSO and SSO improvements addressed by the IOAP, but we believe it is important to take this opportunity to raise awareness for this need, particularly as our community turns its attention to stormwater management in the context of the multi-jurisdictional Municipal Separate Storm Sewer System (MS4) permit. We appreciate MSD's willingness to be a contributor to such an effort, even as we recognize the need for broader involvement and leadership throughout the Louisville community and across Louisville Metro Government.

We look forward to the MSD Board's review of the 2012 IOAP Modifications and MSD's submittal of the 2012 IOAP Modifications to EPA and the State of Kentucky. Thank you for the opportunity to contribute to this critical community improvement initiative. Please feel free to contact us individually or collectively with any questions or perspectives you may have.

**Unanimously Adopted at the January 30, 2013 WWT Meeting  
Stakeholder Members of the Wet Weather Team**

<b><u>Member</u></b>	<b><u>Organization*</u></b>
Steve Barger	Labor (retired)
Susan Barto	Mayor of Lyndon
Stuart Benson	Louisville Metro Council, District 20
Jim Mims	Louisville Metro Planning & Design Services
Allan Dittmer	University of Louisville
Arnita Gadson	Kentucky Environmental Quality Commission
Mike Heitz	Louisville Metro Parks Department
Tom Herman	Zeon Chemicals
Rick Johnstone	Deputy Mayor, Louisville Metro Mayor's Office (retired)
Bob Marrett	CMB Development Company, LLC
Kurt Mason	Jefferson County Soil and Water Conservation District
Lisa Santos	Irish Hill Neighborhood Association
Bruce Scott	Kentucky Waterways Alliance
David Tollerud	University of Louisville, School of Public Health and Information Sciences
Tina Ward-Pugh	Louisville Metro Council, District 9
David Wicks	Jefferson County Public Schools (retired)

\*Stakeholders on the Wet Weather Team do not formally represent their specific affiliated organizations, but rather seek to provide input reflective of the broad interest areas in which they lead. Along with the stakeholder subgroup, the Wet Weather Team includes MSD personnel and technical consultants.





Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

## CHAPTER 1: INTRODUCTION

**Special Note:** This chapter was developed in 2008. The statistical data for the SSO’s reported, specifically related to individual SSO volumes and frequency in a typical rainfall year, were derived from the hydraulic models calibrated in 2007. Since then, a more detailed calibration and validation effort has adjusted the average annual overflow volumes and frequencies in the typical year. This information is provided in Chapter 5. The vast majority of the physical system characterization in this chapter is still accurate.

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**SUPPORTING INFORMATION**

Appendix 1.3.1 Plumbing Modifications Program and Downspout Disconnection Program packet

## **CHAPTER 1: INTRODUCTION**

### **1.1 BACKGROUND**

On August 12, 2005, the Louisville and Jefferson County Metropolitan Sewer District (MSD) entered into a Consent Decree in Federal Court with the United States Environmental Protection Agency (EPA) and the Kentucky Environmental and Public Protection Cabinet. The Consent Decree was developed in response to an enforcement action taken by EPA and Kentucky Department of Environmental Protection (KDEP) alleging violations of the Clean Water Act (CWA) primarily related to sewer overflows. One of the requirements of the Consent Decree is the development and submittal of a Final Sanitary Sewer Discharge Plan (Final SSDP).

On December 1, 2008, a draft Amended Consent Decree (ACD) was released for public comment. The draft ACD addressed alleged violations of the CWA primarily related to water quality treatment center (WQTC) performance, record-keeping, and reporting. The public comment period closed on the draft ACD December 31, 2008. The ACD was entered into Federal Court on April 15, 2009.

The Consent Decree amendments were negotiated over several months, and the terms of the draft amendments were known to MSD during the final stages of development of this Integrated Overflow Abatement Plan (IOAP). For the purposes of the IOAP, except where specifically noted otherwise, the term "Consent Decree" will be understood to mean the ACD as it was entered into Federal Court April, 15, 2009.

MSD is required to prepare and submit a Final SSDP designed to eliminate unauthorized discharges in the separate sanitary sewer system (SSS). The Consent Decree requires the Final SSDP to include consideration of conventional and innovative or alternative designs as part of the plan, including, but not limited to, sewer rehabilitation, sewer separation, relief sewers, above ground or below ground storage, high rate secondary treatment, illicit connection removal, remote wet weather secondary treatment facilities, and other appropriate alternatives. As interim milestones, MSD was also required to update its existing Sanitary Sewer Overflow Plan (SSOP) and to prepare an Interim SSDP identifying remedial measures to eliminate specific unauthorized discharges.

The Consent Decree requires that the Interim SSDP identify remedial measures to eliminate the unauthorized discharges identified in the Consent Decree for the Interim SSDP. These discharges include those resulting from MSD's use of portable pumps within the Hikes Point and Beechwood Village areas, and to eliminate unauthorized discharges at the Highgate Springs Pump Station and the Southeastern Diversion Structure.

The Final SSDP is intended to identify remedial measures to eliminate unauthorized discharges from the separate SSS locations not previously addressed in the Interim SSDP. The Final SSDP contains the long-term projects including schedules, milestones, and deadlines as

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

required by the Consent Decree. The Final SSDP also includes the results of an evaluation of WQTC peak flow treatment capacity for the Jeffersontown WQTC and any WQTC that will receive additional flow as a result of any Final SSDP project. Such evaluations are consistent with the EPA publications "Improving POTW Performance Using the Composite Correction Approach," EPA CERL, October 1984, and "Retrofitting POTWs," EPA CERL, July 1989.

The Final SSDP is in coordination with elements of the Capacity, Management, Operations, and Maintenance (CMOM) programs. The Final SSDP includes the following elements and descriptions:

- Maps of known unauthorized discharges (capacity related), including the areas and sewer lines that serve as a tributary to each unauthorized discharge
- Each known unauthorized discharge location including:
  - Discharge frequency
  - Type of discharge and the receiving stream
  - Annual volume of the discharge
  - Immediate area and downstream landuse (including the potential for public health concerns)
  - Studies to investigate the discharge (previously performed within the last five years, current, or proposed)
  - Rehabilitation or construction work to remediate or eliminate the discharge (previously performed within the last five years, current, or proposed)
- Prioritization of unauthorized discharge locations based upon frequency, volume, impact on receiving streams and public health
- Involvement of stakeholders in the planning, prioritization, and selection of projects
- Documentation of the prioritization process including:
  - Hydraulic modeling, including calibration, validation, addressing wet-weather inflow and infiltration (I/I) and accounting for future growth (build-out)
  - Baseline or existing conditions
  - Rules for abating SSOs and surcharged areas
  - Preliminary or initial solutions
  - Ground-truthing or field verification of preliminary locations
  - Sizing of facilities (solutions) and determining benefits and costs for facilities
  - Level of protection
  - Final costs and descriptions of preferred solutions



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

- Source Control, including targeted I/I reduction and plumbing modification programs
- Measures of success including: Elimination of SSOs, Reduction or elimination of basement flooding and Reduction in I/I
- Remedial measures, expeditious budgets, and schedules for design, initiation of construction and completion of construction. The schedules are phased based upon sound engineering judgment and do not extend beyond December 31, 2024
- Continuous modifications, including plans for measuring success via flow monitoring and modeling and addressing newly discovered SSOs

## **1.2 FINAL SSDP DOCUMENT ORGANIZATION**

As the third volume of the IOAP, the Final SSDP focuses on the control and mitigation of SSOs. The following text outlines the Final SSDP with a brief description on the focus of each chapter.

### **Chapter 1 Introduction**

This chapter presents summaries of previous/ongoing projects and programs, describing the relationship to the current planning process. Previous/ongoing projects and programs include the Updated SSOP, CMOM, Sewer Overflow Response Protocol (SORP), and Interim SSDP. This chapter reviews the role of public participation and agency interaction with specific Final SSDP issues. The final section of the chapter describes in general terms the approach used to evaluate the projects and programs of the Final SSDP.

### **Chapter 2 System Characterization**

This chapter defines the goals of the system characterization program and provides an extensive compilation and analysis of unauthorized discharges in the separate SSS. This chapter includes MSD service area maps showing the unauthorized discharge areas and associated WQTCs, collection system modeling, and system monitoring. This chapter also includes a description of the computer models used to simulate separate SSS areas.

### **Chapter 3 Development and Evaluation of Alternatives for SSO Abatement**

This chapter presents the methodologies used to evaluate the various discharge elimination solutions. The chapter defines and discusses strategies and technologies available to control and eliminate unauthorized discharges in the separate SSS. Discussions include alternatives for discharge elimination in each area of an unauthorized discharge. Finally, this chapter provides a summary of the evaluation for each discharge abatement alternative. The evaluation criterion includes feasibility screening, computer modeling, quality control, level of protection, cost estimates, and a benefit-cost analysis.

## **Chapter 4 Selection of the Sanitary Sewer Discharge Plan**

This chapter includes an explanation of the values-based risk management process used to select and prioritize the Final SSDP alternatives. This chapter examines the various issues associated with implementation of the alternative(s) selected as integral to the Final SSDP. Issues discussed include community values, benefit-cost analysis, environmental impact, technical concerns, prioritization of projects, and implementation schedules compatible with the Consent Decree requirements.

## **Chapter 5 2012 Project Modifications**

This chapter includes requested project modifications to the approved 2009 IOAP project suite resulting from the ongoing adaptive management strategy. The project modification approach centers around the utilization of monitoring data, improved modeling and a better operation understanding of MSD's sewer system. The full project suite related to the Final SSDP is defined including all proposed schedule and budget revisions.

### **1.3 PREVIOUS / ONGOING PROGRAMS**

This section provides a summary of previous and ongoing programs relative to SSO control. These programs and studies serve as the foundation for the current planning effort of the Final SSDP. The following plans and programs are summarized in this section.

- Updated SSOP
- CMOM Programs
- SORP
- Interim SSDP

#### **1.3.1 Updated Sanitary Sewer Overflow Plan (SSOP)**

MSD has been active in the SSO planning area for years and has focused collection system repair and rehabilitation efforts on wet weather I/I issues that contribute to SSOs. The projects have been successful in reducing SSO volume and frequencies, but have not completely eliminated SSOs. Prior to the development of the Final SSDP, the SSOP was MSD's centralized program for managing the investigation, prioritization, and rehabilitation of the separate SSS. The program goals were to reduce SSOs, basement backups, and other unauthorized discharges. This program represented MSD's proactive approach toward eliminating excess I/I from the separate SSS. The SSOP was submitted on February 10, 2006, to the EPA and KDEP; however, no review or approval was required by the Consent Decree.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

The previous studies have been divided into the following phases and are further described in the sections that follow:

- Flow Monitoring
- Sanitary Sewer Evaluation Study (SSES) and Other Sewer Investigation/Study Projects
- Hydrologic and Hydraulic Modeling
- Rehabilitation, Repair or Replacement Projects
- Post-Rehabilitation Flow Monitoring and Results

### **1.3.1.1 Flow Monitoring**

The goal of flow monitoring is to collect sufficient dry and wet weather data to assess I/I levels, provide calibration data to models and to assess the success of any rehabilitation. During the flow monitoring phase, sewersheds are divided into sub-basins which often coincide with key hydraulic features or SSO locations. To collect data, rain gauges and flow monitors are installed in each sub-basin and monitored for a specified period of time or until sufficient rainfall and flow responses has been obtained. Each sub-basin flow monitoring data is analyzed for typical parameters such as peaking factors, average dry weather flow, and wet weather flow characteristics in order to determine the nature of the I/I problem. This flow data serves as the basis for prioritizing projects in the sewershed, calibration of models for further study, and assessing rehabilitation. Flow-monitoring studies performed from 1997 to 2008 are summarized in Table 1.3.1.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 1.3.1**  
**FLOW MONITORING STUDIES (1997-2008)**

Service Area	Project Name	Flow Monitoring Beginning Date	Flow Monitoring Ending Date	Collection Period (days)	No. of Sub-basins	No. of Flow Monitors used	No. Significant Rain Events	I/I Found?	Results Developed Into	Project Completion Date
MF	Beechwood Village Flow Monitoring	6-Mar-98	9-Aug-98	157	--	5	6	Yes	SSES Project	July-99
MF	Ohio River Force Main/Muddy Fork Flow Monitoring	15-Jan-99	12-Mar-99	56	44	7	2	Yes	SSES Projects	December-99
MF	Priority SSO Flow Monitoring Part 1: Middle Fork Beargrass Creek	19-Feb-99	4-Apr-99	45	60	1	2	Yes	SSES Projects	February-99
MF	Beechwood Village Chimney Seal and Cured-in-place Pipe Installation: Post-rehab Flow Monitoring	12-Feb-01	16-Apr-01	64	--	6	2	Reductions Found	Post-Rehab Flow Monitoring	June-01
MF	Hikes Point Chimney Seal and Cured-in-place Pipe Installation: Post-rehab Flow Monitoring	12-Feb-01	16-Apr-01	64	--		2	Reductions Found	Post-Rehab Flow Monitoring	June-02
MF	Buechel Branch Chemical Root Control: Post-rehab Flow Monitoring	3-Jan-02	3-Mar-02	60	--		2	Reductions Found	Post-Rehab Flow Monitoring	June-02
MF	Buechel Branch (and Northern Ditch) Real-Time Control Flow Monitoring	1-Jan-02	16-May-02	120 (2 waves)	--	12	12	Yes	RTC Model Calibration	November-02
MF	Hikes Point Real-Time Control Flow Monitoring	17-Jan-02	16-May-02	120	--	5	12	Yes	RTC Model Calibration	November-02
MF	Middle Fork Flow Monitoring	9-Dec-03	16-Feb-04	70	--	23	2	--	Model Calibration	May-04
MF	County-wide Flow Monitoring	15-Jan-07	8-Jun-07	144	--	86	--	--	--	--
MF	County-wide Flow Monitoring	3-Nov-05	24-Jul-07	628	--	15	--	--	--	--

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 1.3.1**  
**FLOW MONITORING STUDIES (1997-2008)**

Service Area	Project Name	Flow Monitoring Beginning Date	Flow Monitoring Ending Date	Collection Period (days)	No. of Sub-basins	No. of Flow Monitors used	No. Significant Rain Events	I/I Found?	Results Developed Into	Project Completion Date
DRG	Valley Village Flow Monitoring	3-Mar-98	11-May-98	68	6	6	3	Yes	System Characterization	February-99
DRG	Priority SSO Flow Monitoring Part 2: Pond Creek (and: Silver Heights, McNeely Lake) Flow Monitoring	13-Apr-98	27-May-98	45	48	48	3	Yes	SSES Projects	February-99
DRG	Mill Creek Flow Monitoring	6-Oct-98	18-Jan-99	105	--	4	4	--	System Characterization	April-99
DRG	Pond Creek Chimney Seal and Cured-in-place Pipe Installation: Post-rehab Flow Monitoring	3-Jan-02	14-Mar-02	71	--		2	Reductions Found	Post-Rehab Flow Monitoring	2003
DRG	Mill Creek Flow Monitoring	16-Dec-01	18-Mar-02	92	6		2	Yes	System Characterization	June-02
DRG	Derek R. Guthrie Flow Monitoring	23-Dec-02	5-Feb-03	45	--	13	--	--	Model Calibration	March-03
DRG	County-wide Flow Monitoring	8-Jan-07	20-Apr-07	102	--	23	--	--	--	--
DRG	County-wide Flow Monitoring	22-May-08	23-Jul-08	62	--	10	--	--	--	--
CC	Cedar Creek Flow Monitoring	16-Mar-99	6-May-99	51	6	6	4	Some	SSES Project	November-01
CC	Cedar Creek Watershed Flow Monitoring	23-Dec-02	5-Feb-03	45	8		--	--	Model Calibration	--
CC	County-wide Flow Monitoring	23-Mar-07	2-Jul-07	101	--	7	--	--	--	--
HC	Hite Creek (and Crestwood) Flow Monitoring	2-May-00	11-Jul-00	70	1	7	--	Yes	System Characterization	September-03
		14-Aug-00	23-Oct-00	70	1	1	3	Some	Flow Monitoring Data Correction	September-03
HC	County-wide Flow Monitoring	19-May-06	21-Jun-07	398	--	2	--	--	--	--
HC	County-wide Flow Monitoring	22-Mar-07	17-Jul-07	117	--	9	--	--	--	--

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 1.3.1**

**FLOW MONITORING STUDIES (1997-2008)**

Service Area	Project Name	Flow Monitoring Beginning Date	Flow Monitoring Ending Date	Collection Period (days)	No. of Sub-basins	No. of Flow Monitors used	No. Significant Rain Events	I/I Found?	Results Developed Into	Project Completion Date
FF	Pope Lick Flow Monitoring	31-Jan-98	22-Mar-98	51	6	6	2	Yes	PS Sizing & SSES Project	December-99
FF	Woodland Hills Chimney Seal and Cured-in-place Pipe Installation: Post-rehab Flow Monitoring	5-Jan-00	31-Mar-00	87	--		2	A Few Improvements	Post-Rehab Flow Monitoring	June-01
FF	Pope Lick Chimney Seal and Cured-in-place Pipe Installation: Post-rehab Flow Monitoring	12-Feb-01	16-Apr-01	64	--		2	A Few Improvements	Post-Rehab Flow Monitoring	June-01
FF	County-wide Flow Monitoring	5-Apr-07	17-Jul-07	103	--	8	--	--	--	--
FF	County-wide Flow Monitoring	16-May-07	4-Aug-07	80	--	4	--	--	--	--
JT	Jeffersontown Flow Monitoring	1-Sep-98	10-Oct-98	40	23	24	2	Yes	System Characterization	June-99
JT	Jeffersontown Chimney Seal Installation: Post-rehab Flow Monitoring	5-Jan-00	31-Mar-00	87	--		3	Reductions Found	Post-Rehab Flow Monitoring	June-00
JT	Jeffersontown Cured-in-place Pipe Installation: Post-rehab Flow Monitoring	3-Jan-02	14-Mar-02	71	--		2	No Conclusions	Post-Rehab Flow Monitoring	June-02
JT	Jeffersontown Flow Monitoring	23-Dec-02	5-Feb-03	45	--	10	--	--	Model Calibration	March-03
JT	Jeffersontown I/I Rehab Phase 3: Post-rehab Flow Monitoring	8-Dec-03	26-Jan-04	50	--		2	Improvements Found	Post-Rehab Flow Monitoring	May-04
JT	Countywide Flow Monitoring	13-Jan-07	23-May-07	130	--	19	--	--	--	--
PP	Prospect Flow Monitoring	22-Dec-99	19-Feb-00	60	10	10	2	Yes	System Characterization	June-00

**Service Areas:** MF = Morris Forman, DRG = Derek R. Guthrie (formerly West County – WC), CC = Cedar Creek, HC = Hite Creek, FF = Floyds Fork, JT = Jeffersontown, PP = Prospect  
**Note:** Derek R. Guthrie WQTC (formerly West County Wastewater Treatment Plant)



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 1.3.1.2 Sanitary Sewer Evaluation Study (SSES) and other Sewer Investigations/Studies

The goal of an SSES is to provide data to identify likely sources of I/I and to prioritize areas for repairs. An SSES is an important tool for diagnosing the condition of the sewer system and determining what types of repairs might be necessary and successful. The defects identified are often used with flow monitor data to prioritize areas for rehabilitation, construction, and maintenance activities. The SSES process includes several tests and inspections that complement each other, which are described in the following text. Table 1.3.2 at the end of the section lists the studies that have been performed by MSD from 1997 to 2008.

#### Smoke Testing

The goal of smoke testing is to identify defects by emulating water entering inflow locations. Smoke under pressure flows through inflow defects to the surface, where it can be observed and documented.

The test consists of generating nontoxic, non-staining smoke and forcing it into less-than-full sewer lines by a portable, high-volume blower. The smoke can reach distances up to 600 feet and will appear at inflow locations that lead to the surface. The location is noted and the smoke-test crew investigates the emission point. If the emission point is determined to be an inflow source (see Figure 1.3.1), the area is photographed and the pertinent data are entered into MSD's data management system.

**FIGURE 1.3.1 SMOKE INDICATING  
AN INFLOW SOURCE AT A MANHOLE**



Smoke testing is generally low cost and is a proven method for locating collection system defects, such as structurally-damaged manhole frames and damaged cleanouts, and illicit connections, such as yard connections and cross-connected storm sewers. The smoke will also identify private side defects without accessing private property. This is critical given the increasing realization that private property defects can contribute significantly to wet weather I/I sources.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

## Manhole Inspections

The goal of manhole inspections is to visually identify defects that often contribute to inflow. Inspections can be done from the surface (see Figure 1.3.2), or if safety equipment is available, within the structure itself.

Inspections generally follow a checklist which is used to note the condition of various manhole features: cover, frame, risers, corbels and walls, pipe sizes, materials of construction, evidence of corrosion, and I/I (from the surface, cross connections, and illegal connections). It is also possible to lamp (shine high intensity light between manholes) the sewer between two adjacent manholes to look for defects and evidence of clogs or sedimentation.

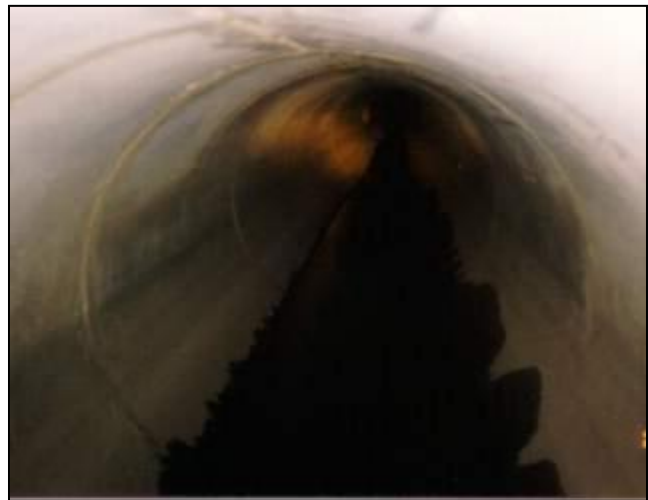
**FIGURE 1.3.2 VIEW INSIDE A MANHOLE**



## Television Inspection Review

The goal of television inspection is to provide condition assessment of sewers. The pipe is cleaned if necessary just prior to the television inspection. For television inspection review, a camera is lowered through a manhole and into the pipe and a continuous recording video inspection from within the line is completed with reference distances (See Figure 1.3.3). Inspections focus on pipe structural defects and improper connections. Beginning in 2005, the log information on each defect is used referencing Pipeline Assessment and Certification Program (PACP) codes, which is digitally linked to the video image. Inspections include noting sedimentation, pipe sags, and pipe defects.

**FIGURE 1.3.3 VIEW INSIDE SEWER PIPE FROM A TELEVISION INSPECTION**



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### Dye Testing

The goal of dye testing is to emulate inflow sources using dyed water, which, unlike normal inflow, can be readily identified. Dye testing involves injecting dyed water into a suspected inflow source and then noting the appearance (or lack thereof) of dyed water in a nearby sanitary sewer (See Figure 1.3.4). The test will confirm potential cross-connections, inflow sources and structural defects. This test is generally used as a contingency after other tests such as smoke testing cannot positively identify potential cross-connections. After the dye has penetrated the pipeline, a television inspection may be used to precisely locate the problem area.

**FIGURE 1.3.4 VIEW INSIDE SEWER PIPE FOR DYE TESTING**



### Night Flow Isolation

The goal of night-flow isolation is to determine infiltration rates during periods of time when little sanitary flow can be expected, such as, during the middle of the night or early in the morning. Night flow testing consists of installing temporary weirs or other flow measuring devices at manholes to identify areas that have relatively high nighttime flows. In addition to the flow measurements, the real-time dissolved oxygen and temperature data can be noted.

The test can be conducted rather rapidly. This allows a large area to be analyzed in the course of a single night, which greatly aids in identifying high I/I areas. Water quality and temperature are also analyzed; infiltration has better water quality and lower temperature than sewer flow. Often night-flow isolation occurs over a series of nights and the preceding night's data is used to direct the subsequent night's test areas. Night-flow isolation must occur when there is no inflow and preferably, when the groundwater is higher than the pipe. This is typically a few days after a series of rainfall or in the fall months.

### Wet Weather Inspections

The goal of wet weather inspections is to visually identify SSOs (See Figure 1.3.5) and surcharging. While the benefits of such inspections are obvious, it is very difficult to mobilize such inspections given the infrequency of overflow-causing rain events.

Tests can be aided by installing surcharge level indicators ahead of time. Surcharge level indicators are simple devices, which can indicate SSOs and surcharge conditions during wet weather. However, surcharge level indicators must be monitored frequently to minimize false

**FIGURE 1.3.5 OVERFLOW DURING WET WEATHER**





Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

readings. To indicate exfiltration of surcharged sewers inspections, dye may also be used. When time permits and where possible, inspections include estimating the timing of the SSO, the peak overflow rate, and the amount of overflow volume at each location.

### **Focused Electrode Leak Locator 41 Inspections**

The goal of Focused Electrode Leak Locator 41 inspections is to determine defect locations through non-intrusive electrical means to complement or direct other SSES tests and inspections. Focused Electrode Leak Locator 41 is a technology that generates an electrical field from a specially-constructed electrode probe called a “sonde” and uses a second electrode (a metal stake) that is put in the ground surface adjacent to the pipe being tested (see Figure 1.3.6).

The sonde is pulled through a surcharged, non-conductive sewer pipe and the magnitude of the current flow is measured by the surface electrode. Spikes in electric current identify all types of pipe defects (within inches) that are potential locations for leaks including faulty joints, pipe cracks, and defective service connections. The variation of the current is recorded and displayed as a plot of current versus distance along the pipe. The Focused Electrode Leak Locator 41 inspection also assesses the pipe defect size and continuously tests along the pipe. This inspection is simple, accurate, reliable, repeatable, and can be used at any time of the year.

**FIGURE 1.3.6 FOCUSED ELECTRODE LEAK LOCATOR SONDE AND EQUIPMENT VEHICLE FOR PIPE INSPECTIONS**



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 1.3.2**

**SANITARY SEWER EVALUATION STUDIES (SSES) 1997 - 2008**

Service Area	Project Name	Completion Date	Smoke Testing (LF)	Manhole Inspections	Television Inspections (LF)	Dye Testing	Manhole Wet Well Investigation	Focused Electrode Leak Locator -41 (LF)	Cost
CC	Cedar Creek SSES	Nov. 2001	284,000	633	134,000	N/A	20 Hours	N/A	\$246,000
FF	Pope Lick SSES	Dec. 1999	75,700	354	33,800	Yes	N/A	N/A	\$388,000
HC	North County SSES	Sept. 2003	72,100	360	8,000	Yes	N/A	N/A	\$291,000
JT	Jeffersontown Condition Assessment	Jul. 2005	86,000	N/A	56,000	N/A	N/A	N/A	\$682,000
MF	Middle Fork SSES Phase 1A	Jul. 1998	126,350	600	31,100	Yes	N/A	N/A	\$299,000
MF	Hikes Point SSES	Dec. 1998	500,000	2,143	Yes	Yes	Installed 25 flow meters and 4 rain gauges		\$1,100,000
MF	Beechwood Village SSES	Jul. 1999	34,000	147	34,000	Yes	N/A	N/A	\$117,000
MF	Buechel Branch SSES Phase 1	Mar. 2000	37,500	157	44,500	Yes	N/A	N/A	\$50,000
MF	Middle Fork SSES Phase 1B	Jun. 2000	253,600	1,004	42,000	Yes	N/A	N/A	\$434,000
MF	Middle Fork SSES Phase 2	Apr. 2002	214,814	954	38,294	Yes	N/A	N/A	\$465,000
MF	Northern Ditch SSES	Sept. 2002	N/A	459	52,791	N/A	149	4,889	\$272,000
PP	Prospect SSES	Oct. 2001	154,572	802	87,014	Yes	N/A	N/A	\$143,000
DRG	Valley Village SSES	Feb. 1999	54,000	184	35,000	Yes	N/A	N/A	\$193,000
DRG	McNeely Lake SSES	Dec. 1999	165,000	688	41,000	Yes	N/A	N/A	\$494,000
DRG	Derek R. Guthrie SSES Phase 1A	Mar. 2000	242,500	932	48,400	Yes	N/A	N/A	\$567,000
DRG	Derek R. Guthrie SSES Phase 1B	Sept. 2000	200,000	952	50,000	Yes	N/A	N/A	\$936,000
DRG	Derek R. Guthrie SSES Phase 2	Jan. 2002	234,600	978	60,000	N/A	N/A	N/A	\$491,000
DRG	Mill Creek SSES	Oct. 2002	150,000	682	30,000	Yes	N/A	N/A	\$284,000
DRG	Pond Creek SSES	Oct. 2004	193,000	1,200	16,650	N/A	23,500	N/A	\$306,000
<b>TOTALS</b>			<b>2,559,936</b>	<b>11,882</b>	<b>610,749</b>		<b>23,649</b>	<b>4,889</b>	<b>\$6,151,000</b>
<b>Service Areas:</b> CC = Cedar Creek, FF = Floyds Fork, HC = Hite Creek, JT = Jeffersontown, MF = Morris Forman, PP = Prospect, DRG = Derek R. Guthrie <b>Note:</b> Derek R. Guthrie WQTC (formerly West County Wastewater Treatment Plant)									

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### **1.3.1.3 Hydrologic and Hydraulic Modeling**

The goal of hydrologic and hydraulic modeling is to provide a computer model that mimics the function of the actual sewer system, including sanitary flow and I/I sources. Once calibrated to dry and wet weather data, the model can be used to assess existing conditions, qualify and quantify deficiencies, and evaluate potential solutions. It also can serve as a tool for future planning and capacity assurance studies.

Hydrologic and hydraulic models of the MSD separate SSS have historically been constructed using the XP-SWMM (Stormwater and Wastewater Management Model) hydrologic and hydraulic modeling software. More recently, MSD models have been converted to the Wallingford software known as InfoWorks. The models were populated with infrastructure data from MSD's Hansen Information Management System (Hansen) sewer asset database. This database includes manhole locations and depths, pipe sizes, pipe slopes, and other data. This data is supplemented with pump station data, survey data, and field investigations. The models are calibrated based on flow monitoring data and updated based on needs, resource, availability, system changes, and reporting requirements.

The hydraulic model has been used for improvement of the existing asset database, identification of significant hydraulic bottlenecks, testing rehabilitation scenarios, modeling wet weather system responses, SSO elimination alternatives, and identifying the impacts of future development scenarios. Additional detail on historic modeling, XP-SWMM model development, and future uses can be found in Volume 3, Chapter 2.

### **1.3.1.4 Plumbing Modification Program**

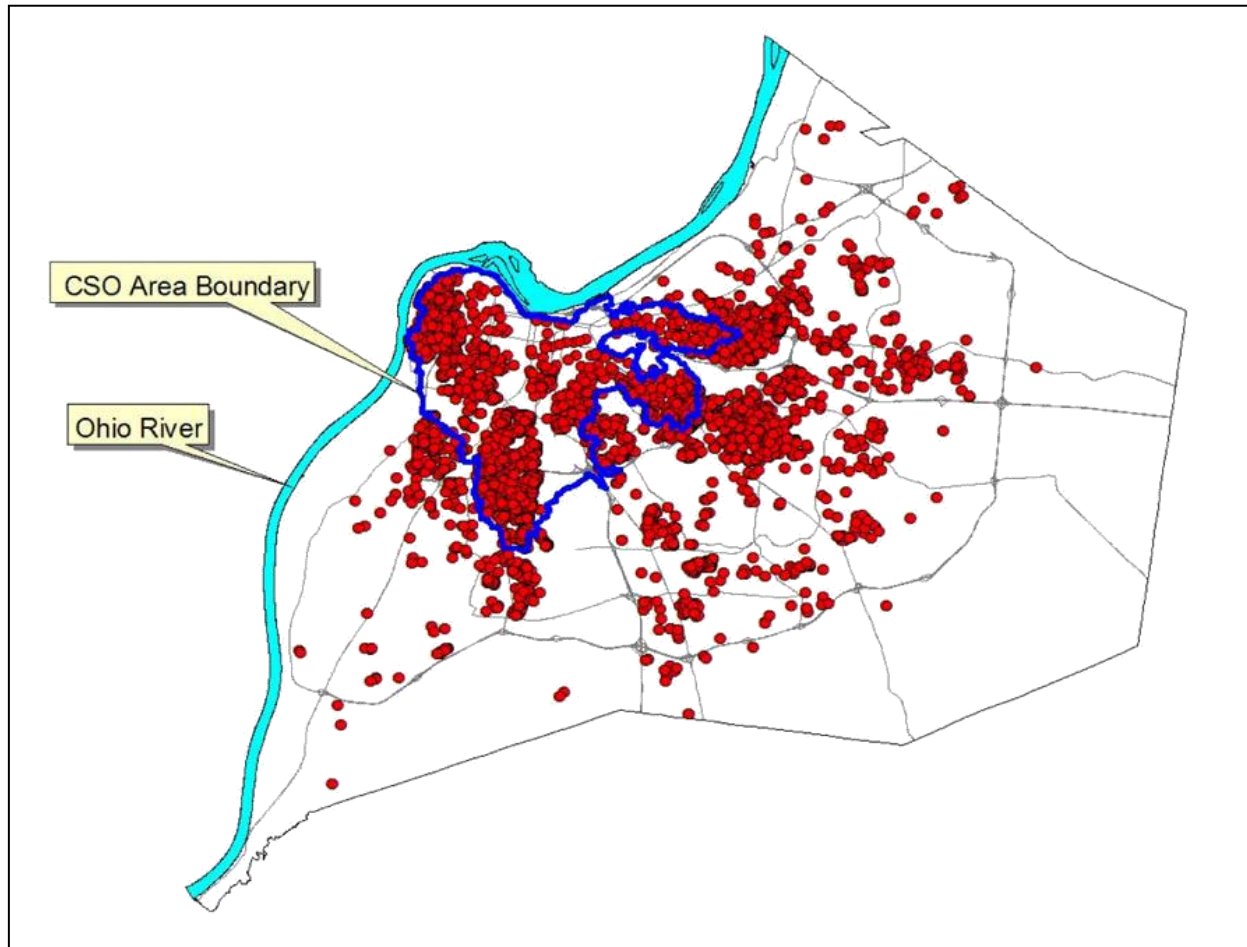
In 1994, MSD started a program to help owners of homes that experience basement backups to install backflow prevention devices at MSD's expense. For the first few years, MSD offered the program to about 450 property owners per month. After the March 1997 flood, MSD began offering a backflow prevention device to any separate SSS residential customer reporting a backup. The countywide program is now available to all MSD customers experiencing basement backups. MSD will pay up to \$3,000 per residence for plumbing modifications. Generally, installations average about \$1,600.

Since the program's inception, MSD has completed over 8,100 projects totaling approximately \$16 million dollars. See Figure 1.3.7 for a map of completed Plumbing Modification Program Projects.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 1.3.7 LOCATION OF COMPLETED PLUMBING MODIFICATION PROGRAM PROJECTS**



The two most common plumbing modifications involve a sump pump or a backwater and ball valve. A sump pump will be installed if a floor drain is present in the basement but no toilet or shower. Usually the floor drain is connected to the main sewer in the street and is the first place the main sewer could backup into the basement.

The sump pump installation consists of capping the existing floor drain, installing a sump pump, and then installing a new floor drain that will be connected to the sump pump. The new floor drain runs into the new sump pump that discharges in the outside yard.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

A backwater valve and a ball valve will be installed, if a toilet and/or shower exist in the basement. The valve installation consists of placing a backwater and ball valve between the toilet and floor drain and the main sewer in the street. Therefore, if the main sewer backs up into the basement, the backwater and ball valve will prevent the water from getting to an outlet (the toilet, shower or floor drain).

An example Plumbing Modifications Program and Downspout Disconnection Program packet available to MSD customers can be found in Appendix 1.3.1.

### 1.3.1.5 Rehabilitation, Repair or Replacement Projects

The goal of rehabilitation projects is to reduce or eliminate surcharging and SSOs through the actual repair of defects in areas of high I/I. MSD performs as-needed maintenance repairs based on planned maintenance, unplanned maintenance, and customer service requests. These repairs include mainline repairs, manhole repairs, property service connection repairs, and downspout disconnections. Table 1.3.3 summarizes the “repair required” work orders completed from 1997 - 2008.

**TABLE 1.3.3**  
**I&FP WORK (1997-2008)**

Repair Required	Work Order Count
<b>Sliplining</b>	1,559 (since October 2003)
<b>Sewer Depression Repair</b>	200
<b>Sewer Cave-in</b>	540
<b>Property Service Connection Cave-in</b>	845 (since January 2000)
<b>Service Line Repair</b>	14,407
<b>Manhole Replaced</b>	34
<b>Manhole Repair</b>	959
<b>Manhole Raised</b>	1,677
<b>Manhole Lid Replacement</b>	243
<b>Manhole Installed</b>	73
<b>Manhole Frame Repair</b>	287
<b>Mainline Sewer Repair</b>	1,171
<b>Downspout Disconnection</b>	174 (since November 2005)

Prioritization of rehabilitation areas draws on data from flow monitoring, SSES work, and computer modeling. The location and severity of the I/I issues dictates the order in which the projects are implemented. Table 1.3.4 lists the individual rehabilitation projects that have been performed by MSD from 1997 to 2008.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 1.3.4**  
**REHABILITATION WORK (1997 - 2008)**

Service Area	Project Name	Completion Date	Cured-in-place Sewer (LF)	Cured-in-place Lateral Connections	Chimney Seal Installations	Manhole Rehab.	Cost	
CC	<b>Cedar Creek Phase 1</b>	Oct. 2001	2,859	12	432	N/A	\$495,000	
CC	<b>Cedar Creek Phase 2</b>	Jun. 2002	2,115	21	1,487	N/A	\$1,015,000	
FF	<b>Woodland Hills Phase 2</b>	Dec. 1997	5,667	51	N/A	23	\$474,000	
FF	<b>Woodland Hills Phase 1</b>	Fall 1999	3,381	81	18	N/A	\$485,000	
FF	<b>Pope Lick Phase 1A</b>	Aug. 2000	5,805	99	253	5	\$941,000	
FF	<b>Pope Lick Phase 1B</b>	Dec. 2000	4,973	114	90	5	\$839,000	
HC	<b>Interceptor Manhole Rehab</b>	2004	N/A	N/A	64	21	\$202,000	
JT	<b>Jeffersontown Phase 1A</b>	Dec. 1998	3,685	N/A	N/A	11	\$188,000	
JT	<b>Jeffersontown Phase 1B</b>	Jun. 1999	N/A	N/A	408	N/A	\$280,000	
JT	<b>Jeffersontown Manhole Rehab Pilot</b>	Oct. 1999	N/A	N/A	N/A	15	\$45,000	
JT	<b>Jeffersontown Phase 1C</b>	Oct. 2001	N/A	N/A	755	N/A	\$546,000	
JT	<b>Jeffersontown Phase 2</b>	May, 2002	2,540	67	920	N/A	\$805,000	
JT	<b>Jeffersontown Phase 3</b>	Sept. 2003	3,247	38	320	120	\$1,240,000	
MF	<b>Newmarket/ Northfield</b>	1997	1,000	N/A	22	21	\$226,000	
MF	<b>Hikes Point Phase 1A</b>	Fall 1999	7,611	N/A	309	N/A	\$670,000	
MF	<b>Old Cannons Lane</b>	Fall 1999	2,153	20	12	N/A	\$213,000	
MF	<b>Hikes Point Phase 1B</b>	Fall 2000	Upsized 1,885 LF of 15" clay sewer to 21" PVC sewer main					\$656,000
MF	<b>Hikes Point Phase 2</b>	Jun. 2001	N/A	N/A	701	N/A	\$469,000	
MF	<b>Buechel Branch Phase 2</b>	Sept. 2001	Chemical root control 52,888 LF		409	N/A	\$423,000	

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 1.3.4**  
**REHABILITATION WORK (1997 - 2008)**

Service Area	Project Name	Completion Date	Cured-in-place Sewer (LF)	Cured-in-place Lateral Connections	Chimney Seal Installations	Manhole Rehab.	Cost	
MF	Hikes Point Phase 3	Oct. 2001	8,062	95	N/A	N/A	\$1,008,000	
MF	Buechel Branch Phase 1	Nov. 2001	2,782	26	N/A	N/A	\$273,000	
MF	Beechwood Village I/I remediation	Nov. 2001	10,991	29	N/A	24	\$608,000	
MF	Middle Fork Phase 2	Feb. 2002	1,872	47	382	N/A	\$435,000	
MF	ORFM chimney seal reinstallation	2004	Reinstalled chimney seals disconnected by paving operations					\$83,000
MF	Beechwood Village lateral lining	2005	Continuation of Beechwood Village Rehab Phase 1 project from FY00					\$532,000
MF	Northern Ditch Interceptor Rehab	Nov. 2008	N/A	N/A	49	55	\$120,000	
MF	Sinking Fork Interceptor Rehab	Dec. 2008	3,205	N/A	117	49	\$480,000	
MF	Middle Fork Interceptor Rehab	Dec. 2008	958	N/A	27	35	\$600,000	
MF	Beargrass Interceptor (Hikes Point)	Dec. 2008	Clean 4588 LF	N/A	152	32	\$200,000	
MF	Goldsmith Ln./Buechel Branch Int.	Dec. 2008	Clean 3737 LF	N/A	273	93	\$250,000	
DRG	McNeely Lake Phase 1A	Dec. 2000	2,709	56	644	152	\$1,068,000	
DRG	WC/Valley Village	Mar. 2001	3,326	Chemical root control 46,423 LF			\$332,000	
DRG	Derek R. Guthrie I/I Phase 2	Jun. 2001	2,574	N/A	204	N/A	\$461,000	
DRG	Derek R. Guthrie Phase 1	Oct. 2001	1,147	8	357	N/A	\$362,000	
DRG	Pond Creek Rehab	Nov. 2001	7,036	130	N/A	N/A	\$637,000	
DRG	McNeely Lake Phase 1B	Nov. 2001	4,624	27	N/A	N/A	\$299,000	
DRG	Derek R. Guthrie WQTC	May 2003	Improvements to prevent Mill Creek flood waters from entering WQTC				\$180,000	
<b>TOTALS</b>			<b>94,322</b>	<b>921</b>	<b>8405</b>	<b>661</b>	<b>\$18,140,000</b>	
<b>Service Areas:</b> CC = Cedar Creek, FF = Floyds Fork, HC = Hite Creek, JT = Jeffersontown, MF = Morris Forman, DRG = Derek R. Guthrie								

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### **1.3.1.6 Post-Rehabilitation Flow Monitoring and Results**

After each rehabilitation phase, post-rehabilitation flow monitoring is performed. The monitoring program will be based on the original sub-basin monitoring. The flow monitors are placed in the same manholes that were used for preliminary testing, and are left to collect information until adequate wet weather response flow data is acquired. This monitoring often includes a control basin (one that is not rehabilitated) to normalize post-rehabilitation flow data for any seasonal discrepancies. A combination flow monitoring and calibration provides a way for data to be accurately compared for rehabilitation effectiveness.

Historically, post rehabilitation flow monitoring indicated that, in many areas, rehabilitation (pipe and lateral lining) resulted in inconsistent I/I reduction. Sometimes post-rehabilitation monitoring showed substantial reduction, yet other times it showed almost none. Private property I/I was suspected as the primary reason that rehabilitation had not proven more effective.

As a result, MSD's design rehabilitation philosophy has focused on building system capacity controls and not strictly the rehabilitation of public-side systems. Pipeline rehabilitation, however, does continue to be implemented in an ongoing capital program.

### **1.3.1.7 Relation to Final SSDP Planning**

The SSOP was MSD's centralized program for managing the investigation, prioritization, and rehabilitation of the separate SSS to reduce unauthorized discharges. It documents the history of the MSD wet weather program and is related to the Final SSDP in this respect. The SSOP serves as a summary of historical efforts and findings to show the breadth and depth of past efforts in relation to eliminating SSOs. Since 1997, thirty-two projects costing nearly \$16.5 million have been completed and documented within the SSOP. The SSOP document serves as the obvious foundation for the Final SSDP by providing both data for evaluating current conditions and experience in adopting preferred solutions.

## **1.3.2 Capacity, Management, Operations and Maintenance (CMOM) Program**

According to the EPA, the purpose of the CMOM Program is to:

*“incorporate many of the standard operation and maintenance activities that are routinely implemented by the owner or operator with a new set of information management requirements in order to:*

- Better manage, operate, and maintain collection systems
- Investigate capacity constrained areas of the collection system
- Proactively prevent SSOs
- Respond to SSO events

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

*The CMOM approach helps the owner provide a high level of service to customers and reduce regulatory noncompliance.”*

Like other sewer districts, MSD has been using many techniques outlined in CMOM for decades to continually enhance the system. In 2003, MSD initiated a *CMOM Challenge Analysis* as the first step in a comprehensive Self-Assessment Program to provide a management-level evaluation of their organizational structure and corresponding programs, activities, and tasks.

Specific objectives of the CMOM Challenge Analysis were to:

- Provide MSD’s management staff with an overview of the fundamental components of EPA’s proposed SSO Rule and CMOM provisions.
- Inventory and compare MSD’s CMOM Program areas and activities with regards to EPA guidance material.
- Identify program activities that should be recommended for enhancement targeted at improving service or compliance performance.

The CMOM Self Assessment Report was originally submitted to the EPA and KDEP on February 10, 2006, re-submitted on May 12, 2006, and approved on August 22, 2006. The full analysis can be found on the MSD Project WIN website at: <http://www.msdlouky.org/projectwin/docs.htm>.

Through the self-assessment process MSD documented that many activities were performing well. Nevertheless, in some cases, MSD implemented changes and improvement activities to provide continuity and consistency with other activities. The management policies, operational programs, and operational activities that were found to be performing well are listed below.

- Technical Training
- Skills Training
- Safety Training
- Safety Department
- Confined Space Entry
- General Safety Procedures
- Traffic Management
- Monitoring of Street Pavement
- Mapping
- Acquisition Consideration
- Capital Improvement Program Funding
- Pretreatment Legal Support
- Septic Tank Haulers Legal Support
- “Call Before You Dig” Legal Support



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

- Lock Out/ Tag Out
- Safety Equipment
- Performance Measures
- Industrial User Permitting
- Inspection and Sampling Enforcement

The self-assessment process also identified program areas and activities that would benefit from improvement, such as:

- Program 1. Continuous Sewer System Assessment
- Program 2. Infrastructure Rehabilitation
- Program 3. System Capacity Assurance Plan (SCAP)
- Program 4. Pump Station Preventive Maintenance Program
- Program 5. Gravity Line Preventive Maintenance Program
- Program 6. Sewer Use Ordinance Legal Support Program

Through continuous improved performance, MSD expects to see benefits such as:

- Reduced incidence of SSOs due to wet weather events
- Enhanced customer service response and relations
- Optimized existing resources to meet growing demands and expectations
- Financial stability through better anticipation of capital and operations and maintenance (O&M) requirements

### **1.3.2.1 Relation to Final SSDP Planning**

As outlined above, the CMOM Self Assessment Report identified areas that needed improvement, recommended specific improvements, and set a schedule for those improvements to be implemented. Implementation of improvements is critical for other programs, including the Final SSDP and the overall IOAP. MSD staff developed performance goals for the programs and activities that needed improvement and worked throughout the organization to discuss, develop, and implement the improvements.

MSD continues to improve programs with the intent of mitigating SSOs. The next step involves development and implementation of system capacity-related solutions to address issues, which is part of the Final SSDP.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Through the CMOM Program, MSD is to coordinate capacity decision criteria under a System Capacity Assurance Plan (SCAP). These criteria will:

- Improve upon existing support for each watershed's community values including a process to confirm and document the capacity of WQTCs, pump station, and conveyance systems.
- Identify hydraulic constrictions, which are characterized by upstream system capacity that is greater than downstream system capacity.
- Propose capacity improvements that support IOAP performance objectives.
- Directly affect the modeling efforts performed under the Final SSDP and the planning of SSO elimination projects.
- Confirm that sewers are designed to handle additional flow and prevent excessive I/I as a result of new connections.
- Prevent sewers already over-capacity during dry and/or wet weather from receiving new flows.
- Identify pump station and gravity line activities to be integrated into the Final SSDP.

### **1.3.2.2 System Capacity Assurance Plan (SCAP)**

The SCAP applies to the separate sanitary system only and works in conjunction with the Final SSDP to ensure that MSD's efforts for SSO abatement are successful. The SCAP is a living, dynamic document that will continue to change due to various components. Changing components include modeling improvements, map updates, Consent Decree program implementation, reporting automation, capital improvement projects, development capacity requests, and other CMOM and MSD programs. An overview of the SCAP can be found on the MSD Project WIN website at <http://www.msdlouky.org/projectwin/docs.htm>.

The SCAP is the basis for coordinating capacity decision criteria for each separate SSS watershed. Providing wastewater collection, conveyance, and treatment that will meet the expansion needs of MSD's customers, while protecting the environment and meeting regulatory requirements, are top priorities of MSD's facility improvements efforts.

New service connections contribute additional flow that utilizes available capacity in the system. Since wet weather capacity deficiencies have been identified as the cause for a significant portion of SSOs, it is important for MSD to have a program that ensures new sanitary flow connections do not cause or contribute to SSOs.

The objective of the SCAP is to enable MSD to authorize new sewer service connections or increases in flow from existing sewer service connections while making system improvements in

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

accordance with the May 2006 CMOM recommendations. The SCAP process includes a programmatic approach for items such as confirming capacity of plants, pump stations, and conveyance systems; identifying hydraulic constrictions; and proposing capacity improvements that support interim and WQTC performance objectives. The SCAP contains technical information, methodology, and analytical techniques to be used that will:

- Calculate the peak flow capacity of system components (collector sewers, interceptor sewers, treatment plants and pump stations);
- Calculate the increase in flows from new service connections;
- Calculate the increase in peak flow capacity resulting from specific system improvements projects;
- Integrate current new development approvals, acquisition of sewers, and extension of service to un-sewered areas.

The SCAP also details the steps to approve new flow requests in areas of limited capacity through a flow credits “banking” system. This “banking” system requires that for every one gallon of new flow, three gallons of I/I must be removed from the system through rehabilitation. A presumptive approach to this removal is outlined within the SCAP document; please refer to this document for additional detail.

### **1.3.3 Sewer Overflow Response Protocol (SORP)**

The purpose of the SORP is to provide guidance to MSD personnel regarding response to SSOs, mitigation of the SSO’s impact, public notification, and reporting of the SSO. Utilizing the SORP enables MSD to respond to SSOs in a consistent and effective manner and reduces an SSO’s impact on the environment and human health.

Per Paragraph 24.d. of the Amended Consent Decree, MSD initially submitted the SORP to the EPA and KDEP on February 10, 2006 and received comments on March 13, 2006. MSD resubmitted the revised SORP on May 12, 2006, and received an approval letter on August 22, 2006. The SORP undergoes regular annual reviews and updates; the last update was approved in late 2008. The updated SORP document can be found on the MSD Project WIN website at <http://www.msdlouky.org/projectwin/docs.htm>.

#### **1.3.3.1 Preparatory Actions**

An important component of MSD’s SORP is preparing for wet weather SSO incidents before they actually occur. By assuming an SSO could occur and taking proactive measures, MSD may prevent the SSO from actually occurring. In cases where the SSO cannot be prevented, this strategy minimizes MSD’s response time, reduces the SSO’s volume, and mitigates the SSO’s impact.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

MSD's preparatory strategy has two major components. The first is wet weather monitoring which provides early warning of events that may result in SSO conditions. If wet weather monitoring indicates that SSO conditions are likely, then the second component, the pre-positioning of personnel and equipment, is implemented.

### **1.3.3.2 Overflow Management and Field Documentation**

Once MSD becomes aware of a possible SSO event, a cascade of actions and responses begin. These actions include the following:

- Initial response, identifying the origin and cause of the SSO. Determining the boundaries of the SSO's impact area and performing an initial assessment of the SSO's impact are also required during the initial response. After the initial extent and impact are assessed, a control zone is established, and public notification is completed. The responding personnel determine which method, or combination of methods, will best minimize the SSO's impact.
- Mitigation, preventing an SSO from moving into non-impacted areas, and therefore limiting the extent of the impacted area. Examples of containment technologies or mitigation include sand bags, inflatable plugs, as well as spill containment equipment.
- Clean-up of the impacted area. The immediate area around the SSO site is inspected and cleaned of residual material in order to minimize public health and environmental risks.

### **1.3.3.3 Public Notification and Communication**

When an SSO occurs, MSD utilizes an event-based public notification program. These are localized, short-term, and field-based activities designed to warn the public and limit access to areas impacted by the SSO. Event-based notification methods include the use of signage, establishment of a control zone (discussed previously), and placement of door-hangers.

In addition to the event-based notification methods, MSD also practices programmatic activities. Programmatic activities are long-term, community-wide activities designed to increase awareness of SSOs including their cause and prevention, potential health hazards, environmental impacts, and MSD's abatement activities. Examples of programmatic activities include overflow advisory signs posted at SSO locations and public access areas downstream of SSOs. MSD also posts email notices and has prepared educational videos, brochures, and billing inserts in an effort to inform the public about SSOs.

#### **1.3.3.4 Regulatory Reporting and Data Management**

The complete and accurate documentation of SSO data is required for the purpose of regulatory reporting. In addition, such data is crucial for tracking the SSO history of system assets such as manholes, sewer lines, and pump stations. MSD also utilizes this data to make decisions regarding SSO response methods, procedures, monitoring frequencies, and abatement strategies.

Personnel responsible for responding to SSOs, including unauthorized discharges, are responsible for gathering and documenting pertinent SSO data. Work orders must be initiated within 10 hours of a verified SSO. This protocol is necessary to provide transmission of the unauthorized discharge's data to KDEP and EPA within the required timeframe. In addition, MSD submits a monthly summary of all unauthorized discharges occurring by WQTC. The summary is submitted as a component of the sewershed's respective wastewater treatment plant's Discharge Monitoring Report (DMR).

#### **1.3.3.5 Staff Training and Communication**

The SORP is a dynamic document that is monitored and adjusted as new or improved procedures, practices, and technologies become available. The SORP is reviewed annually and amended as appropriate. Proposed changes to the SORP are submitted to the EPA and KDEP for review and approval. MSD continually enhances the SORP training modules, ensuring MSD staff remains current on existing and updated procedures.

Knowledge of SORP procedures and practices is transferred to MSD's employees through a comprehensive training program. MSD employees receive the SORP Overview training that discusses the purpose, objectives, and scope of the SORP as well as an understanding of the requirements for its execution. Personnel involved in overflow response activities receive additional quarterly training to ensure that they possess the knowledge and skills necessary to properly implement the SORP.

#### **1.3.3.6 Relation to Final SSDP Planning**

MSD maintains a database of documented SSOs, which is utilized to validate hydraulic models used in the Final SSDP. In turn, the hydraulic modeling efforts have identified potential SSO points at other locations, also known as Modeled Overflow Points (MOPs). These points were screened and did not include those hydraulically connected to a known SSO or have modeled overflow volumes less than 10,000 gallons to account for modeling accuracy. All other points were field verified. Refer to Chapter 2, Section 2.4.2 for a more detailed explanation of the MOP validation process.

Additionally, follow-up monitoring will be required after implementation and final construction of solution alternatives to abate known and suspected SSOs. A phasing plan will be implemented under SORP protocols to monitor the sites for three years until it is proven, under design conditions, that the SSO has been eliminated or mitigated. Periodic flow monitoring and

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

hydraulic-model recalibration will also be performed to report on systematic performance of SSO abatement efforts.

New MOPs or SSOs identified by new modeling or field inspection will be added to the database and will be subject to follow-up monitoring, especially if it occurs at less than the design level of protection. Areas upstream of these SSOs will also be targeted in the I/I Program as outlined in Volume 3, Chapter 2, Section 2.3.5.8.

### **1.3.4 Interim Sanitary Sewer Discharge Plan**

On September 28, 2007, MSD submitted to the EPA and KDEP the Interim SSDP identifying remedial measures for specific unauthorized discharges (specified in Paragraph 25(a) (2) of the Amended Consent Decree) in the separate SSS. Comments were received on January 8, 2008. The Interim SSDP was resubmitted on March 7, 2008, and approved on July 24, 2008. The Interim SSDP document can be found on the MSD Project WIN website at: <http://www.msdlouky.org/projectwin/docs.htm>.

The primary goals of the Interim SSDP are to define a plan to eliminate unauthorized pumped discharges in Beechwood Village and Hikes Point, the elimination of the pumped discharge at the Highgate Springs Pump Station, and the closure of the constructed overflow at the Southeastern Diversion. The efficiency of the proposed projects will be verified using the following categories of post construction monitoring:

- Three years of observations at current SSO locations to confirm that overflows (pumped or otherwise) have been eliminated.
- Flow monitoring within the collection system to confirm flows predicted by modeling.
- Verification of full secondary treatment of all flows received at the Derek R. Guthrie WQTC (formerly formerly West County Wastewater Treatment Plant), based on an evaluation of its first year of operation.

#### **1.3.4.1 Background**

Most of the Interim SSDP projects are interdependent. Staging their implementation, therefore, will be an important task. The sequence of projects is outlined in Chapter 3, Section 3.2 of the Interim SSDP. In general, downstream projects will have priority for implementation to allow increased levels of wastewater to be properly conveyed via the Pond Creek Interceptor and treated at the Derek R. Guthrie WQTC. If any upstream project is completed prior to a prerequisite downstream project, it will not be connected until capacity is available.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

#### **1.3.4.2 Interim SSDP Solution**

The six projects developed in the Interim SSDP are currently being designed and coordinated with Final SSDP and IOAP projects. All projects will likely require easements and/or property acquisitions, as well as construction permits. The six Interim SSDP projects are summarized below.

##### Project 1: Beechwood Village Sanitary Sewer Replacement

The entire local collection system, including homeowner's service connections, will either be rehabilitated or replaced in the city of Beechwood Village and a portion of the City of St. Matthews. This will eliminate wet weather pumping of unauthorized discharges and reduce I/I currently entering the Sinking Fork Interceptor.

The sanitary portion of the project will consist of lining 19,000 linear feet (LF) of 8-inch diameter, 700 LF of 10-inch diameter and 4,000 LF of 18-inch diameter sanitary sewer pipe. The service connections at 580 homes will be replaced and modifications made to the internal plumbing of most of the homes. The project is divided into two phases, East and West, to help ease project implementation. Final design plans were substantially complete as of March 2008. Final design contract documents will be amended to include any special conditions required by customers once residential customer negotiations have been completed and all easements have been acquired. It is assumed that no temporary easements will have to be acquired through the condemnation process.

Improvements to the Beechwood Village East and West collection systems will reduce wastewater flow by reducing I/I, thereby improving downstream conditions. The only prerequisite project is the Sinking Fork Interceptor Relief Sewer (Project 2). This relief sewer is planned to take the flow from some of the new Beechwood Village sewers and must be in operation before the Beechwood Village collection system improvements can be connected. The Beechwood Village East construction contract began in the first quarter of 2009 and be completed in the first quarter of 2011. The Beechwood Village West construction contract will begin in the second quarter of 2009 and will be completed in the second quarter of 2011.

##### Project 2: Sinking Fork Relief Sewer

The Sinking Fork Relief Sewer will convey flows from a portion of Project 1 and will provide additional wet weather capacity downstream of the Beechwood Village East area to accommodate final SSDP projects upstream. This project consists of 2,800 LF of 24-inch diameter sanitary sewer interceptor pipe, which will extend from the 18-inch diameter interceptor being installed as part of Project 1 – Beechwood Village East. Design was completed and sent for KDEP review in December 2008. Construction began in the second quarter of 2009 and will be completed in the fourth quarter of 2010.

##### Project 3: Hikes Lane Interceptor and Highgate Springs Pump Station

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Improvements to the Hikes Point sewer system will eliminate the need for wet weather pumping in the Hikes Point area. Improvements will also eliminate the Highgate Springs Pump Station and reduce wet weather flow into the Beargrass Interceptor. The Hikes Point sewer improvements will impact two sanitary sewer basins:

- One basin is northwest of the Watterson Expressway, (I-264) and flows by gravity to the Beargrass Interceptor via the Goldsmith Lane Trunk Sewer. The improvements will consist of 1,000 LF of relief sewer along Carson Way and Ribble Road pumped locations to a new connection into the Goldsmith Trunk. This part of the project is fully independent of other components, with preliminary design completed and final design in progress.
- The second basin is located in the general Hikes Point area south of I-264, where wet weather pumping occurs. Here the improvements will consist of 10,000-LF, 72-inch-diameter Hikes Lane interceptor, a total of 3,500 LF of smaller, new or replacement sewers, and the decommissioning of the Highgate Springs Pump Station. The flows from the Highgate Springs Pump Station will be diverted by gravity to the Southeastern Interceptor downstream of the Southeastern Diversion via the new Hikes Lane Interceptor. Once the Hikes Lane Interceptor is constructed, Highgate Springs Pump Station will be decommissioned.

Preliminary design including route selection, field investigations, geotechnical exploration, surveying, and utility research were completed in October 2008. The geotechnical evaluations, 50 percent of the surveying, and 50 percent of design are scheduled to be completed by September 2009. Design will be completed in April 2010. Construction will begin in the fourth quarter of 2010 and be completed in the fourth quarter of 2012.

#### Project 4: Southeastern Diversion Structure and Interceptor

Following the commissioning of the Northern Ditch Diversion Interceptor and the Derek R Guthrie WQTC, operational improvements to the Southeastern Diversion Structure will provide the necessary flexibility to increase Real Time Control (RTC) effectiveness and eliminate the need to overflow at the Southeastern Diversion Structure during wet weather. Additional work in the vicinity of the Southeastern Diversion Structure will be needed to accommodate the additional flows from the new Hikes Lane Interceptor, Project 3. This project will consist of a new Southeastern Interceptor Relief Sewer, two flow control junction boxes, and modifications to the existing Southeastern Diversion Structure. A new parallel Southeastern Interceptor Relief Sewer will run between the Southeastern Diversion and the 72-inch diameter Northern Ditch Interceptor and will transport additional flows to the Derek R. Guthrie WQTC. The Southeastern Interceptor Relief Sewer is being sized to convey flows from future Final SSDP projects and can provide in-line storage. The Southeastern Interceptor Relief Sewer sizing will accommodate other Final SSDP projects bringing additional flows to the Southeastern Diversion.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

The other improvements involve the following:

- A new junction structure located near Fountain Drive will connect the Southeastern Interceptor Relief sewer to the Hikes Lane Interceptor and Buechel Branch Interceptor.
- Another structure will be required at the junction with the Northern Ditch Interceptor. This second structure will contain RTC gates to prevent overwhelming the downstream system and to utilize the Southeastern Interceptor and Southeastern Interceptor Relief sewer for in-line storage.
- The control weir in the Southeastern Diversion will be removed after the Southeastern Interceptor Relief and junction structures are complete allowing flow from the upper Beargrass Interceptor into the Southeastern Interceptor under dry conditions.
- Other modifications will include re-programming RTC gates to prevent most flow into the Beargrass Interceptor.

Construction of the Southeastern Interceptor Relief Sewer will be completed in the second quarter of 2012. The connections at the Southeastern Diversion and the Northern Ditch Interceptor cannot be completed until the Derek R. Guthrie WQTC wet weather facilities (Project 6) are operational. Derek R. Guthrie WQTC and the Northern Ditch Interceptor provide for SSO elimination at the Southeastern Diversion Structure without modifications to the Southeastern Diversion or the Southeastern Interceptor. Preliminary design, including route selection and surveying, will be completed in the third quarter of 2009. Final design including field investigations, geotechnical exploration, wetlands delineation, and utility research, will be completed in the third quarter of 2010.

#### Project 5: Northern Ditch Diversion Interceptor

Construction of the new Northern Ditch Diversion Interceptor will allow flows from upstream projects to reach Derek R. Guthrie WQTC. The Northern Ditch Diversion Interceptor project will consist of 13,000 LF of new 84-inch-diameter pipe constructed along Greasy Ditch from the Northern Ditch Pump Station to the Pond Creek Interceptor. A new flow control structure near Enterprise Drive to divert flow from the Northern Ditch Interceptor to the new Northern Ditch Diversion Interceptor will be constructed to control flow between the Northern Ditch Pump Station and the Derek R. Guthrie WQTC using a 144-inch weir gate and 84-inch sluice gate. There are 45 private property easements that will be required along with a Section 404 Permit from the USACE.

The Northern Ditch Diversion Interceptor is scheduled for completion in the third quarter of 2011. It cannot be connected to the Pond Creek Interceptor until expansion at the Derek R. Guthrie WQTC is complete and operational. Preliminary design including route selection was completed in October 2007. Field investigations consisting of geotechnical exploration,

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

wetlands delineation, utility research, and final design were initiated in November 2007. The design was completed and sent for KDEP review in December 2008.

#### Project 6: Derek R. Guthrie WQTC

Improvements to Derek R. Guthrie WQTC will allow treatment of all wet weather flow from the other Interim SSDP improvements. The 100 million gallons per day (mgd) peak flow capacity secondary treatment facility will consist of the following:

- New influent pumps and piping modifications providing 200 mgd firm pumping capacity.
- Construction of a wet weather pump station with an initial capacity of 104 mgd and an ultimate capacity of 145 mgd to be in service when influent flow exceeds 200 mgd.
- New screening facility with three units, each with capacity of 172.5 mgd.
- Wet Weather Treatment Plant with 100 MGD capacity including a short-term detention basin, initially two channels and ultimately four channels, a new grit removal system, one new contact basin, six new secondary clarifiers and new chlorine contact basins.
- New 20 MG (million gallons) equalization basin.

These facilities will be located at the Derek R. Guthrie WQTC site. The proposed wet weather treatment facility is an expansion of the existing contact stabilization activated sludge process with one additional contact basin and six additional secondary clarifiers, sized to produce effluent that meets secondary treatment discharge standards when operating on relatively dilute wet weather flows.

Preliminary design for process selection and sizing, including field investigations for geotechnical exploration, wetlands delineation, and utility research, was completed in November 2008. Final design, initiated in November 2008, will be completed in the third quarter of 2009.

The construction period was established to provide two full warm-weather building seasons to reach substantial completion, allowing testing and start-up to be completed prior to the required completion date of December 31, 2011. Construction and commissioning of the Derek R. Guthrie WQTC wet weather flow equalization and wet weather treatment facilities are critical paths to implementing the overall Interim SSDP.

#### **1.3.4.3 Preliminary Project Schedule and Cost**

The estimated capital cost to implement the Interim SSDP is approximately \$200 million. Estimated costs were calculated using planning level cost estimating tools developed for projects associated with MSD's IOAP. The planning level costs are based on historical data from multiple cities, EPA documentation, and similar project data. The estimates prepared are

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

based on the best available data and judgments by engineering firms under contract for either the planning or design of the respective project components at the time they were developed. Refined estimates will be prepared as projects move to detailed-design stages.

In accordance with the Consent Decree, the Interim SSDP will implement the corrective measures necessary for remediation of the unauthorized discharges in the Beechwood Village area and at the Southeastern Diversion Structure by December 31, 2011. Similarly, the unauthorized discharges at Hikes Point and Highgate Springs Pump Station will be eliminated by December 31, 2013.

## **1.4 PLANNING APPROACH**

This section provides a brief summary of the Final SSDP planning approach used by MSD. The following are summarized in this section:

- Modeling Overview
- Public Participation and Agency Interaction
- Measures of Success: Performance Goals

### **1.4.1 Modeling Overview**

A hydraulic model is the mathematical representation of a sewer system in a computer. Models use basic laws of physics, such as conservation of mass and energy, to continuously model flows through sewers systems. In addition, models are used to characterize the existing sewer conditions so that the magnitude and extent of SSOs and surcharging can be assessed. The same models are used to evaluate potential solutions. However, adequate models are dependent upon the supporting databases; therefore, much effort is placed on calibrating and validating models prior to any assessment or evaluation.

Evaluating sewers with a hydraulic model is much like evaluating an airplane using a wind tunnel. First, the model is constructed to mimic known conditions, then the shortcomings are noted and finally solutions are tested. The hydraulic model, like the wind tunnel, allows the modeler to assess a wide array of conditions and possible solutions without full-scale testing. Hydraulic models can be divided into a number of important features:

- Hydrological characterization, which uses databases on land types and soils to generate mathematical representation of rainfall and stormwater flow into the sewer system.
- The hydrological model, which uses the hydrological characterization to estimate I/I based on assumed rainfall and soil conditions.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

- Base flow calculations, which estimate actual sewer flow from homes and businesses based on census data.
- Hydraulic characterization, which uses databases on manhole and sewer sizes, locations, depths and materials to generate mathematical representation of a sewer system. This characterization also includes pumps, diversions and other special structures normally found in sewer collection systems.
- The hydraulic model, which uses the I/I from the hydrological model, combines it with the base flow and uses the hydraulic characterization to predict flows and levels at any point in the system.

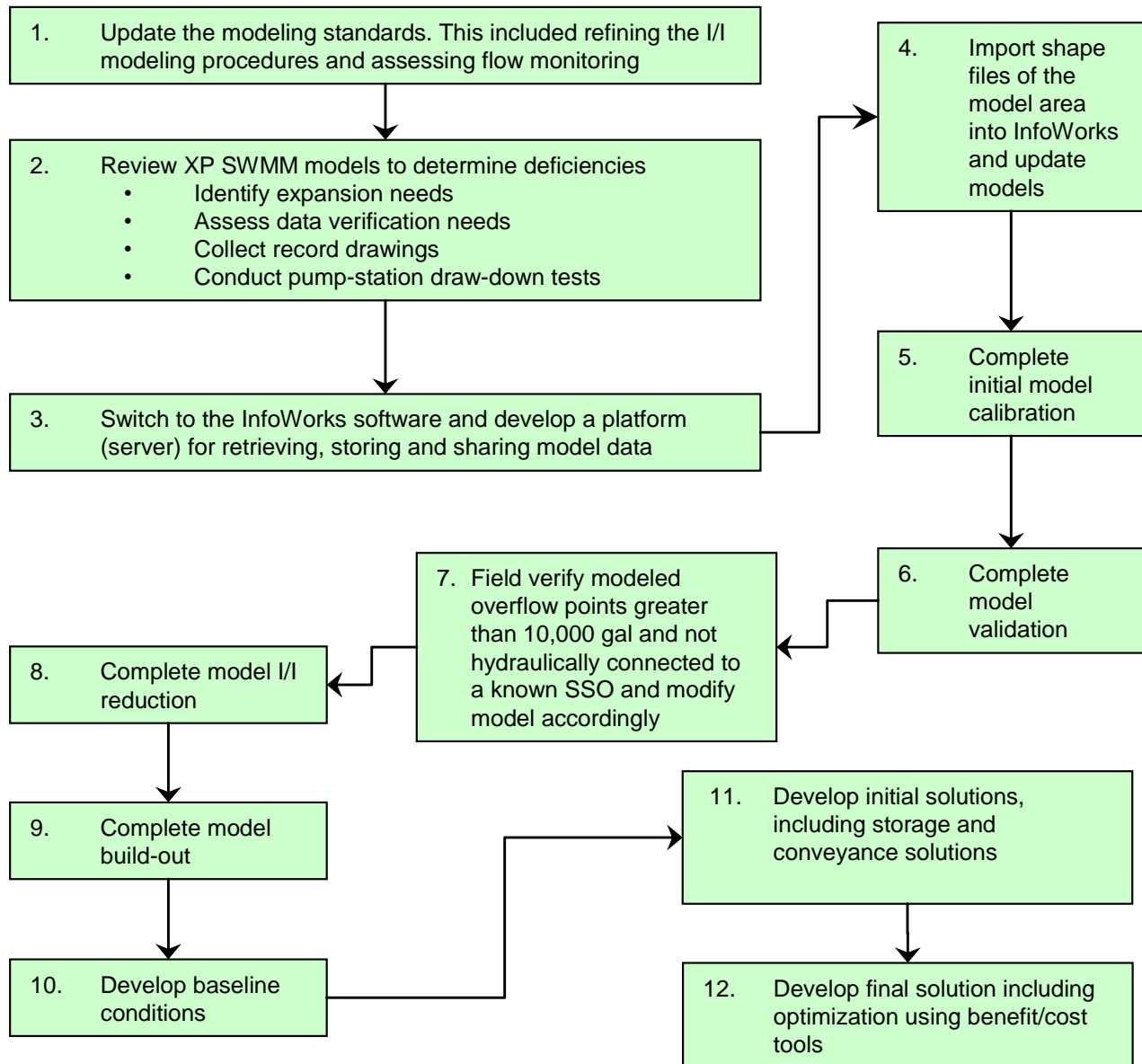
With the objective of the Final SSDP to eliminate SSOs, the sewer system hydraulic models must represent, as accurately as possible, known SSOs and surcharging within the system. Additionally, it is probable that the calibrated hydraulic models will identify new SSO locations. MSD determined that historical modeling efforts were not adequate for the detailed evaluations necessary to plan system improvements on a scale required by the Final SSDP. Therefore, MSD initiated a new sewer system modeling program using InfoWorks.

Prior to model calibration, MSD provided each modeling team with known system hydraulic information such as known SSO location, volume and duration; pump station runtime information; known surcharge areas; and other pertinent data for use in calibration and validation of the model results. The modelers validated SSOs and surcharging in the general location of the SSOs for various levels of protection as part of the calibration process. The models were then divided into model areas and further divided into branches based on SSO locations. The modeling process can be abridged into the components depicted in Figure 1.4.1.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

FIGURE 1.4.1 MODELING FLOW CHART



Modeling is a complex task and is further explained and defined in Chapter 2. Using the model, potential solutions were developed, analyzed and optimized for each branch. Chapter 3 discusses the solution development and analysis. Chapter 4 details the optimized and selected projects. Once the optimized projects were chosen, an implementation schedule was developed along with project costs and is presented in Chapter 4.

## **1.4.2 Capacity Analysis and Other Model Applications**

System capacity analyses are based on existing conditions and impacts of future population projections, reserved capacity for future assessments and new developments, and capacity requests currently being reviewed by MSD's Development Team. The hydraulic models will be used to support future evaluations of new connection requests and system capacity. The models determine the best range of feasible options for conveyance, storage, and/or treatment to abate excess wet weather flows and eliminate SSOs. MSD performed capacity assessments, compiled a range of system improvement approaches, and developed the benefit-cost evaluations for various solutions in a manner consistent with the Final SSDP.

## **1.4.3 Public Participation**

Public participation is an integral component during the planning, development, evaluation, and selection stages of SSO abatement projects. By informing the public early in the planning process, potential conflicts can be identified and addressed during the development stages. The public outreach efforts include communication media, public meetings, public hearings, workshops, and discussion panels. Key target audiences include the public, property owners, advocacy groups, builders, restaurants, industries, and schools.

The backbone of the framework is the Wet Weather Stakeholder Group involvement. Effective input of Louisville Metro's community values is essential for the elements of the IOAP. The stakeholder process has provided meaningful involvement in discharge abatement, alternative development, evaluation, and prioritization. The stakeholder involvement activities have helped establish the performance objectives for the sanitary and combined sewer systems and the associated CMOM and Nine Minimum Controls (NMC) programs. Public participation and agency interaction is discussed in full detail in Volume 1, Chapter 3 of the IOAP.

## **1.4.4 Measures of Success: Performance Goals**

The measures of success are a means to demonstrate compliance with the Consent Decree requirements and to quantify the benefits achieved from SSO elimination projects. Ongoing measurements of the system and analysis of measured results will help guide MSD by identifying specific methods that perform better or worse than predicted in time to modify future efforts. Each project's performance goals should be tailored to site-specific situations.

A review of the Final SSDP projects after completion will evaluate how well the project accomplished the performance goals that were established before the project began, and whether the project implemented was indeed the most cost effective approach. Results from the review should show that the cost-benefit analyses and risk management approach used to choose targeted deficiencies, level of protection, project alternatives and project scheduling were effective.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Deficiencies in the system addressed by the Final SSDP include wet weather capacity related problems and generally exclude maintenance issues, which are CMOM related. Therefore, these performance goals are only meant to encompass wet weather situations within the level of protection under the IOAP. Meeting these performance goals has many potential benefits including:

- Achieving Legal and Regulatory compliance
- Reducing potential negative impacts on public health
- Reducing potential negative impacts on receiving waters
- Reducing future costs of operation
- Documenting proof of project results and effectiveness.

Chapter 4 outlines the full details of the measures of success. The four performance goals for Final SSDP projects are:

1. No Wet Weather Capacity Related SSOs under the Selected Level of Protection
2. No Wet Weather Capacity Related Basement Back-ups within the Level of Protection
3. Sufficient Treatment Capacity within the Level of Protection
4. Project Flow Monitoring Performed and Documented



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

## CHAPTER 2: SYSTEM CHARACTERIZATION

**Special Note:** This chapter was developed in 2008. The statistical data for the SSO’s reported, specifically related to individual SSO volumes and frequency in a typical rainfall year, were derived from the hydraulic models calibrated in 2007. Since then, a more detailed calibration and validation effort has adjusted the average annual overflow volumes and frequencies in the typical year. This information is provided in Chapter 5. The vast majority of the physical system characterization in this chapter is still accurate.

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## **SUPPORTING INFORMATION**

Appendix 2.2.1 Pipe Material, 100-year Floodplain, and Non-conforming Slopes Maps  
Appendix 2.3.1 Selection of the Cloudburst Storm  
Appendix 2.3.2 Model Calibration/Validation Reports  
Appendix 2.3.3 Model QA/QC Documents  
Appendix 2.3.4 RDI/I Method and Modeling Techniques Technical Paper  
Appendix 2.3.5 Build-out Method and Modeling Techniques Technical Paper  
Appendix 2.4.1 MOP Investigation Findings  
Appendix 2.4.3 Hydraulic Sewer System Modeling Guideline Manual  
Appendix 2.5.1 Surcharge/Bottleneck Maps

## **CHAPTER 2: SYSTEM CHARACTERIZATION**

### **2.1 SYSTEM CHARACTERIZATION OBJECTIVES**

Objectives of system characterization within the context of the Final Sanitary Sewer Discharge Plan (SSDP) include:

- Calibrating and validating the hydraulic models.
- Identifying and verifying system deficiencies and problem areas, including sanitary sewer overflows (SSOs), by analysis of assembled data using validated hydraulic models.

The objectives are met by collecting system data and developing hydraulic models that are consistent with the data that represent Louisville and Jefferson County Metropolitan Sewer District (MSD)'s separate sanitary sewer system (SSS). This chapter serves as a framework for solution development to eliminate known or suspected capacity-related SSOs, within the established level of protection.

### **2.2 EXISTING SSDP DATA**

This section of the Final SSDP provides compilation and evaluation of data from three key areas:

- Existing Water Quality Treatment Center (WQTC) service areas and existing WQTC capacity evaluations.
- Existing collection systems, primarily gravity sewers and pump stations.
- Flow Monitoring and associated rain gauge network.

These compilations are focused on building representative hydraulic models and in determining collection system deficiencies.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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### **2.2.1 WQTC Service Areas**

This section provides a background summary of each of the six WQTC regional service areas as well as a number of small WQTCs that make up MSD's sewer service area. Table 2.2.1 includes information on service area size, design capacities, dates of construction, and lengths and diameters of sewers.

While MSD has built the regional treatment facilities and the required interceptors to treat and convey flow in each service area, much of the collection system was built by other communities or by private developers. When MSD acquired these systems beginning in the 1960s, it also acquired the system deficiencies and operations and maintenance (O&M) concerns, many of which are the root cause of current SSOs.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.2.1  
WATER QUALITY TREATMENT CENTER (WQTC) CHARACTERISTICS**

WQTC	Sub-Service Area	KPDES Permit Number	Year Built	Year Acquired by MSD	Design Capacity	Discharge To	Sanitary Sewer Pipe in Collection System (mi)	Pipe Size Range	Most Common Pipe Materials	Sanitary Pump / Lift Stations	Scheduled WQTC Diversion Date	Expected Receiving WQTC
<b>Cedar Creek</b>	--	KY0098540	1995	1995	7.5 MGD	Cedar Creek	125	8"-36"	VCP, PVC	28	N/A	N/A
<b>Hite Creek</b>	--	KY0022420	1970	1970	6.0 MGD	Hite Creek	120	8"-27"	PVC	35	N/A	N/A
<b>Floyds Fork</b>	--	KY0102784	2001	2001	3.25 MGD	Floyds Fork	98	8"-54"	VCP, PVC	20	N/A	N/A
<b>Jeffersontown</b>	--	KY0025194	1956	1990	4.0 MGD	Chenoweth Run	112	8"-36"	VCP, PVC	27	2015	To be Determined
<b>Morris Forman</b>	--	KY0022411	1958	1958	120 MGD	Ohio River	1,000	8"-72"	VCP, RCP, PVC	118	N/A	N/A
--	Middle Fork	N/A	N/A	N/A	N/A	--	348	8"-53"	VCP, RCP, PVC	19	N/A	N/A
--	Beechwood Village	N/A	N/A	N/A	N/A	--	6.8	8"-10"	VCP	--	N/A	N/A
--	Ohio River Force Main / Muddy Fork	N/A	N/A	N/A	N/A	--	185	8"-48"	VCP, PVC	30	N/A	N/A
--	Hikes Point / Highgate Springs PS	N/A	N/A	N/A	N/A	--	100	8"-36"	VCP	3	N/A	N/A
--	Buechel Branch	N/A	N/A	N/A	N/A	--	57	8"-36"	VCP	--	N/A	N/A
--	Northern Ditch	N/A	N/A	N/A	N/A	--	130	8"-72"	VCP	6	N/A	N/A
<b>Derek R. Guthrie</b>	--	KY0078956	1986	1986	30 MGD	Ohio River	852	8"-120"	VCP, PVC	68	N/A	N/A
--	Pond Creek	N/A	N/A	N/A	N/A	--	495	8"-120"	VCP, PVC	40	N/A	N/A
--	McNeely Lake	N/A	N/A	N/A	N/A	--	31	8"-24"	VCP, PVC	6	N/A	N/A



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.2.1  
WATER QUALITY TREATMENT CENTER (WQTC) CHARACTERISTICS**

WQTC	Sub-Service Area	KPDES Permit Number	Year Built	Year Acquired by MSD	Design Capacity	Discharge To	Sanitary Sewer Pipe in Collection System (mi)	Pipe Size Range	Most Common Pipe Materials	Sanitary Pump / Lift Stations	Scheduled WQTC Diversion Date	Expected Receiving WQTC
--	Mill Creek	N/A	N/A	N/A	N/A	--	309	8"-78"	VCP, PVC	20	N/A	N/A
--	Valley Village	N/A	N/A	N/A	N/A	--	17	8"-27"	VCP, PVC	2	N/A	N/A
<b>Hunting Creek North</b>	--	KY0029106	1964	1999	0.358 MGD	Harrods Creek	14	8"-15"	VCP, PVC	10	2015	HC WQTC
<b>Hunting Creek South</b>	--	KY0029114	1968	1999	0.251 MGD	Harrods Creek	11	8"-10"	VCP, PVC	8	2015	HC WQTC
<b>Ken Carla</b>	--	KY0022497	1968	1997	0.010 MGD	Harrods Creek	0.5	8"	VCP	1	2015	HC WQTC
<b>Shadow Wood</b>	--	KY0031810	1979	2008	0.085 MGD	Harrods Creek	2.0	8"-10"	PVC	3	2015	HC WQTC
<b>Timberlake</b>	--	KY0043087	1973	1999	0.200 MGD	Harrods Creek	6.0	8"-10"	PVC	11	2015	HC WQTC
<b>Berrytown</b>	--	KY0036501	1975	1995	0.075 MGD	Floyds Fork	5.9	8"-12"	VCP, PVC	5	2011	FF WQTC
<b>Chenoweth Hills</b>	--	KY0029459	1972	1990	0.200 MGD	Chenoweth Run	6.4	8"-12"	VCP, PVC	2	2015	To be Determined
<b>Silver Heights</b>	--	KY0028801	1963	1990	0.500 MGD	Mud Creek	6.8	8"-15"	VCP	1	Beyond 2014	DRG WQTC
<b>Bancroft</b>	--	KY0039021	1966	1998	0.080 MGD	Goose Creek	3.0	8"-15"	VCP	--	Beyond 2014	MF WQTC
<b>Glenview Bluff</b>	--	KY0044261	1976	1976	0.010 MGD	--	0.3	8"	VCP, PVC	--	Beyond 2014	MF WQTC
<b>Lake Forest</b>	--	KY0042226	1988	2005	0.470 MGD	Chenoweth Run	22	8"-18"	VCP, PVC	6	2011	FF WQTC
<b>Lake of the Woods</b>	--	KY0044342	1976	1989	0.044 MGD	Chenoweth Run	1.0	8"	VCP, PVC	1	Beyond 2014	To be Determined
<b>McNeely Lake</b>	--	KY0029416	1964	1986	0.205 MGD	Pennsylvania Run	4.0	8"-12"	VCP	4	Beyond 2014	DRG WQTC

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.2.1**  
**WATER QUALITY TREATMENT CENTER (WQTC) CHARACTERISTICS**

WQTC	Sub-Service Area	KPDES Permit Number	Year Built	Year Acquired by MSD	Design Capacity	Discharge To	Sanitary Sewer Pipe in Collection System (mi)	Pipe Size Range	Most Common Pipe Materials	Sanitary Pump / Lift Stations	Scheduled WQTC Diversion Date	Expected Receiving WQTC
Starview	--	KY0031712	1971	1988	0.100 MGD	Chenoweth Run	2.4	8"-10"	VCP, PVC	1	2011	FF WQTC
Yorktown	--	KY0036323	1968	1991	0.150 MGD	Northern Ditch	2.9	8"-15"	VCP, PVC	1	2010	DRG WQTC

Legend: KPDES – Kentucky Pollutant Discharge Elimination System, MGD - million gallons per day, VCP – vitrified clay pipe, RCP - reinforced concrete pipe, PVC - polyvinyl chloride  
WQTC: HC – Hite Creek, FF - Floyds Fork, DRG - Derek R. Guthrie, MF - Morris Forman

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### **2.2.1.1 Cedar Creek**

The Cedar Creek WQTC was constructed in 1995 by MSD to provide service to one of the fastest growing areas of Jefferson County. The new facility facilitated the elimination of nine small treatment plants and numerous septic systems. The plant was expanded in 2003 to its present design capacity of 7.5 million gallons per day (mgd). The Cedar Creek WQTC is located near Bardstown and Cedar Creek Roads in Southern Jefferson County. The landuse consists primarily of single-family residential with a small amount of multi-family, commercial, industrial, and vacant or undeveloped land. Refer to Exhibit 2.2.1 in Appendix 2.2.1, Pipe Material, 100-year Floodplain, and Non-conforming Slopes Maps, for a map of the Cedar Creek service area.

### **2.2.1.2 Floyds Fork**

Construction of the Floyds Fork WQTC was completed in 2001 with a design capacity of 3.25 mgd to provide service to a fast growing area of Jefferson County. It also eliminated several small treatment plants and off-loaded some areas that were previously directed to the Jeffersontown WQTC. The Floyds Fork WQTC is located at the end of Blue Heron Road off Shelbyville Road in Eastern Jefferson County. The landuse consists primarily of single-family residential housing with a small amount of apartments, commercial development, and vacant or undeveloped land. Refer to Exhibit 2.2.2 in Appendix 2.2.1 for a map of the Floyds Fork service area.

### **2.2.1.3 Hite Creek**

The Hite Creek WQTC was constructed by MSD in 1970 to provide service to the newly constructed Ford Motor Company Kentucky Truck Plant and the surrounding suburbs in eastern Jefferson County. Two expansions have occurred at the treatment plant, along with various upgrades, to increase the present design capacity to six mgd. The Ford Motor Company Kentucky Truck Plant contributes approximately 1 mgd to the treatment facility. The landuse consists primarily of single-family residential areas with a small amount of multi-family areas, commercial lots, vacant or undeveloped land, and the Ford Motor Company Kentucky Truck Plant. Refer to Exhibit 2.2.3 in Appendix 2.2.1 for a map of the Hite Creek service area.

### **2.2.1.4 Jeffersontown**

The Jeffersontown WQTC was constructed in 1956 and was expanded several times to its current design capacity of four mgd. MSD acquired the Jeffersontown WQTC in 1990. In 1998, the system was placed under an Agreed Order by the Kentucky Department of Environmental Protection (KDEP) (Case No. 97201). The Agreed Order required various rehabilitation projects and treatment plant upgrades because the average annual hydraulic load was at 90 percent of its permitted capacity and the system experienced wet weather SSOs at the siphon just upstream of the WQTCs headworks. Improvements made by MSD to the plant from 1997 to 2000 added phosphorous removal, ultraviolet (UV) disinfection, and a new return activated sludge pump station. The Jeffersontown Service Area is located at Taylorsville Road and

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Watterson Trail in central Jefferson County. The landuse consists primarily of single-family residential and industrial with a small amount of commercial and vacant or undeveloped land. Refer to Exhibit 2.2.4 in Appendix 2.2.1 for a map of the Jeffersontown service area.

### **2.2.1.5 Morris Forman**

The Morris Forman WQTC is the largest treatment plant in the MSD service area with a design capacity of 120 mgd. It was originally built in 1958 as a primary treatment plant that removed only heavy, solid wastes. The plant was rededicated in 1975 as a secondary treatment facility that treated organic matter and bacteria. The plant serves most of Louisville Metro and is the bio-solids processing facility for the entire service area.

The Morris Forman service area is the largest sewershed in the MSD collection system. The majority of the landuse in the service area is residential, with some smaller areas of commercial, industrial, and parks. Refer to Exhibits 2.2.5 through 2.2.7 in Appendix 2.2.1 for maps of the Morris Forman service area.

Within the Morris Forman service area are several key features associated with SSOs and known system deficiencies. These features are discussed below.

### **Middle Fork**

The Middle Fork service area is located within the Morris Forman Service area and primarily serves the areas within the Middle Fork of Beargrass Creek watershed. The landuse consists primarily of single-family residential area.

### **Beechwood Village**

Beechwood Village is located along the Sinking Fork Interceptor in St. Matthews, which is a part of the Middle Fork service area. The landuse consists of single-family residential area. The Beechwood Village separate SSS has experienced excessive inflow and infiltration (I/I) since the construction of the neighborhood's sanitary sewers in the early 1960s. Available data suggests that the separate SSS was constructed to substandard conditions, adding to the infiltration problems typically associated with clay pipe. The neighborhood is also located in an area with unusually high groundwater and poor drainage. MSD acquired the system in the mid-1960s and has since been working with the neighborhood to alleviate chronic basement backups. The five locations where temporary pumping occurs during wet weather are the locations called out in the Consent Decree as a part of the Beechwood Village neighborhood and are addressed in the Interim SSDP.

### **Ohio River Force Main / Muddy Fork**

The Ohio River Force Main (ORFM) / Muddy Fork service area is located along the Ohio River in northeast Jefferson County. The area consists primarily of single-family residential housing

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and vacant or undeveloped land along with a small number of apartments and commercial development. The service area is generally bounded on the northwest by the Ohio River, northeast by Gene Snyder Freeway (I-265) South, and south by Westport Road.

### **Hikes Point / Highgate Springs Pump Station**

The Hikes Point / Highgate Springs Pump Station area is located at the intersection of Hikes Lane and Goldsmith Lane. The majority of the landuse in the service area is residential, with some smaller areas of commercial and parks. MSD constructed Highgate Springs Pump Station in 1963, which was designed to relieve the Beargrass Interceptor and prevent surcharging in the Highgate Springs sewer system. During dry weather, a weir prevents flow from the 36-inch diameter Highgate Springs Interceptor from entering the station's wet well. The flow is passed through the pump station by gravity and through a 30-inch tide gate into the Beargrass Interceptor. During wet weather, the tide gate closes, and flow from the Highgate Springs Interceptor spills into the wet well of the Highgate Springs Pump Station. For small storm events, one pump discharges directly into the Beargrass Interceptor. For increasingly larger events, the remaining three pumps will turn on sequentially until three pumps are discharging to the creek and preventing basement backups to approximately 300 homes. The Highgate Springs Pump Station and five additional locations where temporary pumping occurs during wet weather are the locations called out in the Consent Decree as a part of the Hikes Point area and are addressed in the Interim SSDP.

### **Buechel Branch**

The Buechel Branch service area is located in central Jefferson County and is part of the South Fork of Beargrass Creek watershed. The landuse consists primarily of residential area with some commercial and industrial area. In the late 1970s, the Southeastern Interceptor was constructed because of a system constriction on the Beargrass Interceptor. The Southeastern Interceptor extends from the Southeastern Diversion structure to the Northern Ditch Interceptor.

### **Northern Ditch**

The Northern Ditch area is located near the intersection of I-65 and Preston Highway. The majority of the landuse in the service area is residential and industrial.

#### **2.2.1.6 Derek R. Guthrie**

Construction of the Derek R. Guthrie WQTC (formerly known as the West County Wastewater Treatment Plant) began in 1984 and the WQTC came on-line in 1986 with a design capacity of 15 mgd. The Derek R. Guthrie WQTC eliminated over 45 small WQTCs and numerous pump stations and septic systems in the Pond/Mill Creek area where water quality was significantly impaired by small WQTC permit violations and failing septic systems. As the service area and population has grown, treatment capacity has been added to increase the present design capacity to 30 mgd. The Derek R. Guthrie modeled area serves primarily single-family

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

residential customers, commercial, and vacant or undeveloped land. Refer to Exhibits 2.2.13 through 2.2.15 in Appendix 2.2.1 for maps of the Derek R. Guthrie service area.

There are four key features within the Derek R. Guthrie Service Area associated with SSOs and known system deficiencies. These features are outlined below.

### **Pond Creek**

The Pond Creek area of Derek R. Guthrie is located at the intersection of Preston Highway and the I-265. The majority of the landuse in the service area is residential and undeveloped/vacant land.

### **McNeely Lake**

The McNeely Lake sewershed is located at I-265 and Smyrna Parkway in southern Jefferson County. The majority of the landuse in the service area is residential and undeveloped/vacant land. The McNeely Lake area was acquired in stages during the late 1980s and 1990s. The area was comprised of six small WQTCs: The Pines; Pleasant Valley; Apple Valley; Maple Grove; Old Maple Grove; and McNeely Lake. In 1999, five of the small WQTCs were eliminated and directed to the Derek R. Guthrie WQTC. McNeely Lake WQTC is still in service.

### **Mill Creek**

The Mill Creek sewershed is located near the intersection of Dixie Highway and Greenwood Road. The majority of the landuse is residential and undeveloped/vacant land.

### **Valley Village**

The Valley Village sewershed is located at Dixie Highway and Watson Lane in southwestern Jefferson County. The majority of the landuse is residential and undeveloped/vacant land. The Valley Village system was acquired in 1986 and the original small WQTCs were eliminated in 1989 with the construction of a gravity interceptor to the Derek R. Guthrie WQTC.

#### **2.2.1.7 Prospect**

The Prospect area in northeastern Jefferson County contains five small WQTCs listed below and their characteristics are outlined in Table 2.2.1. These WQTCs primarily serve single-family residential customers with a small amount of multi-family residential and commercial area. Refer to Exhibit 2.2.8 in Appendix 2.2.1 for a map of the Prospect service area.

- Hunting Creek South WQTC
- Ken Carla WQTC
- North Hunting Creek WQTC



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

- Shadow Wood WQTC
- Timberlake WQTC

### **2.2.1.8 Small WQTCs**

After the 1937 flood, less floodprone suburban areas became more desirable and began to be developed at an increasing rate. Suburban expansion occurred and new homes were built to use septic tanks to dispose of their sewage. However, in many suburban areas of Jefferson County, septic tanks were not a good solution due to topography, low permeability soil types, and shallow bedrock. In wet weather, groundwater would typically rise above the level of the septic tank systems, and raw sewage would stand in the yards and drainage ditches. As a solution, the Louisville Metro Board of Health agreed to allow individual septic tanks where the land could accommodate them, and to require small "package" WQTCs where septic tanks would not work well. These package WQTCs were typically operated by the developers. By mid-1972, there were about 350 small WQTCs in Jefferson County.

MSD began to acquire these systems as the regional sewer system developed. Small WQTC acquisitions became controversial, for a time, until pressure from state and federal regulators made it clear that their owners would have to make large investments to meet new water pollution regulations. Several court decisions also affirmed that MSD had the power to take over small WQTC systems when MSD sewer lines reached the area.

The ten small WQTC service areas currently operated by MSD located outside of the Prospect area are listed below and their characteristics are outlined in Table 2.2.1. These small WQTCs primarily serve single-family residential customers in multiple areas of Jefferson County. Refer to Exhibits 2.2.9 through 2.2.12 in Appendix 2.2.1 for maps of the Small WQTC service areas.

- Berrytown WQTC
- Chenoweth Hills WQTC
- Silver Heights WQTC
- Bancroft WQTC
- Glenview Bluff WQTC
- Lake Forest WQTC
- Lake of the Woods WQTC
- McNeely Lake WQTC
- Starview WQTC
- Yorktown WQTC

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 2.2.1.9 Existing Treatment Plant Capacity Evaluation

MSD has acquired and eliminated over 300 privately owned WQTCs and six regional plants were expanded, upgraded, or constructed. The Updated SSOP outlines WQTC operation parameters such as the year of construction, year acquired by MSD, design capacity, average influent flow, collection system size, and number of customers.

Under the CMOM Programs, MSD developed the Louisville and Jefferson County System Capacity Assurance Plan (SCAP). One of the activities of the SCAP is to confirm the flow capacities of all the WQTCs and pumping stations and compare them to current base and peak flows. The following summarizes the regional and small WQTC capacity evaluations.

#### Regional WQTCs

Treatment capacities at the regional WQTCs were evaluated in 2007. Evaluation included review of the most recent engineering design and construction plans, individual site visits, and performance certifications where available. WQTC performance under 2007 loading conditions was also reviewed to validate the results of the engineering studies.

Table 2.2.2 summarizes the annual average flow capacity and the peak flow capacity of each regional WQTC.

**TABLE 2.2.2**

**SUMMARY OF REGIONAL WQTC CAPACITY EVALUATION & RESULTING LIMITATIONS**

WQTC	Rated Permitted Capacity (mgd)	Peak Hour Design Flow (mgd)	2007 Average Day Flow (mgd)	2007 Peak Day Flow (mgd)	Limiting Unit Process (Peak Flow)
Morris Forman	120	350	100	204	Clarifier
Derek R. Guthrie	30	96	24	70	Clarifier
Cedar Creek	7.5	26.0	3.7	17.4	Clarifier
Hite Creek	6.0	16.0	4.0	14.0	Aeration
Jeffersontown	4.0	9.5	3.7	17.9	Clarifier
Floyds Fork	3.25	10.4	1.80	6.77	Clarifier

#### Small WQTCs

Treatment capacities at the small WQTCs were evaluated in 2007. Evaluation included review of the most recent engineering design and construction plans, individual site visits, and performance certifications where available. WQTC performance under 2007 loading conditions was also reviewed to validate the results of the engineering studies.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Table 2.2.3 summarizes the annual average flow capacity and the peak flow capacity of each small WQTC.

**TABLE 2.2.3**  
**SUMMARY OF SMALL WQTC CAPACITY EVALUATION & RESULTING LIMITATIONS**

WQTC	Rated Permitted Capacity (gpd)	Peak Hour Design Flow (gpd)	2007 Average Day Flow (gpd)	2007 Peak Day Flow (gpd)	Limiting Unit Process (Peak Flow)	Planned Elimination Date
Bancroft	80,000	183,000	37,000	65,000	Disinfection	Beyond 2014
Berrytown	75,000	275,000	95,000	640,000	Disinfection	2011
Chenoweth Hills	200,000	576,000	147,000	738,000	Clarifier	2015
Glenview Bluff	10,000	26,000	4,000	6,000	Aeration	Beyond 2014
Hunting Creek South	251,000	630,000	180,000	768,000	Clarifier	2015
Ken Carla	10,000	50,000	3,000	29,000	Aeration	2015
Lake Forest	470,000	1,034,000	384,000	1,725,000	Aeration	2011
Lake of the Woods	44,000	161,000	31,000	285,000	Aeration	Beyond 2014
McNeely Lake	205,000	282,000	104,000	661,000	Disinfection	Beyond 2014
North Hunting Creek	358,000	792,000	325,000	786,000	Disinfection	2015
Shadow Wood	85,000	162,000	52,000	550,000	Disinfection	2015
Silver Heights	500,000	889,000	301,000	1,570,000	Disinfection	Beyond 2014
Starview	100,000	288,000	108,000	500,000	Clarifier	2011
Timberlake	200,000	646,000	76,000	606,000	Clarifier	2015
Yorktown	150,000	432,000	194,000	876,000	Clarifier	2010

## 2.2.2 Collection System Evaluation

MSD has developed detailed design models for each WQTC service area based on Louisville and Jefferson County Information Consortium (LOJIC) data, as-built drawings, and field investigation records. The models generally include sewers ranging from large interceptors to small local 8-inch lines, pump stations, and control features such as diversion weirs or interceptor flow controls.

Additionally, GIS tools were used to characterize the system, such as system connectivity, pipe material, pipe in the 100-year floodplain, and pipe with non-conforming slope (pipe slopes that do not meet minimum MSD design criteria). The calibrated and validated hydraulic models were used to establish existing system conditions such as surcharged pipes, SSO volumes, and hydraulic restrictions (outlined later in this section), as well as identify modeled overflow points (MOPs).

### 2.2.2.1 Existing Gravity-Sewer Condition Evaluation

GIS mapping and database queries were utilized to characterize the existing gravity sewer system. These evaluations were comprehensive and intended to provide initial assessments. In most cases, the evaluations were a review of the appropriate GIS mapping, especially those in the vicinity of known SSOs or MOPs, once identified.

The evaluations included the following by sewershed and shows references to relevant data and figures in this section:

- Sewer pipe material (Figure 2.2.1)
- Sewers in the 100-year floodplain (Figure 2.2.2)
- Sewers with non-conforming slopes (Figure 2.2.2)

Mapping related to these evaluations are listed and available in Appendix 2.2.1:

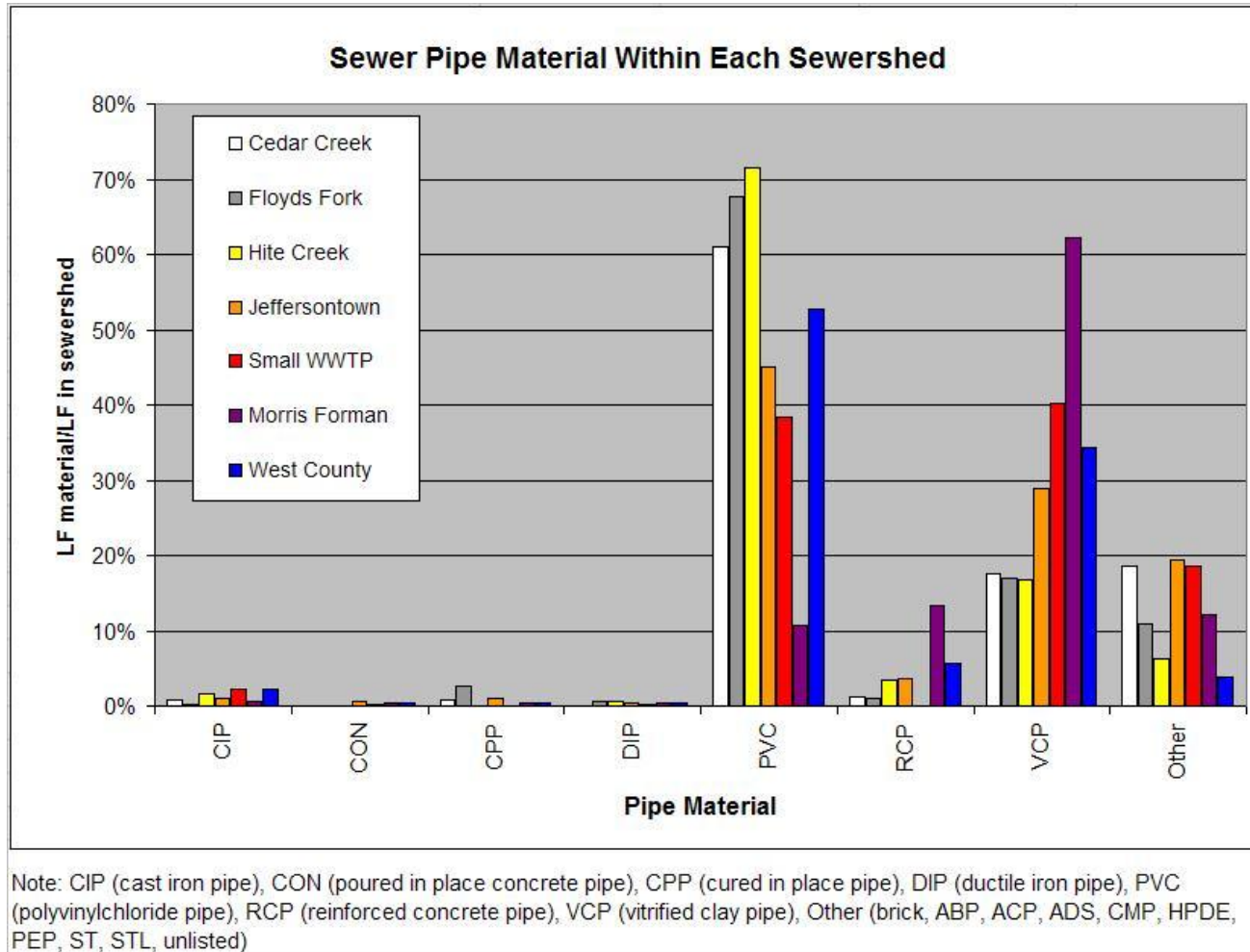
- Sewer pipe material (Exhibits 2.2.1 through 2.2.15)
- Sewers in the 100-year floodplain (Exhibits 2.2.16 through 2.2.30)
- Sewers with non-conforming slopes (Exhibits 2.2.31 through 2.2.45)

Validated models were used to develop summaries of existing conditions for the hydraulic capacity in the gravity sewer system. These evaluations are summarized in this section and include the following:

- Locations and volume of SSOs for various levels of protection
- Surcharged sewers
- Number of hydraulic bottlenecks
- The existing conditions evaluation identified specific capacity deficiencies in the system that would need to be addressed by SSO abatement solutions.

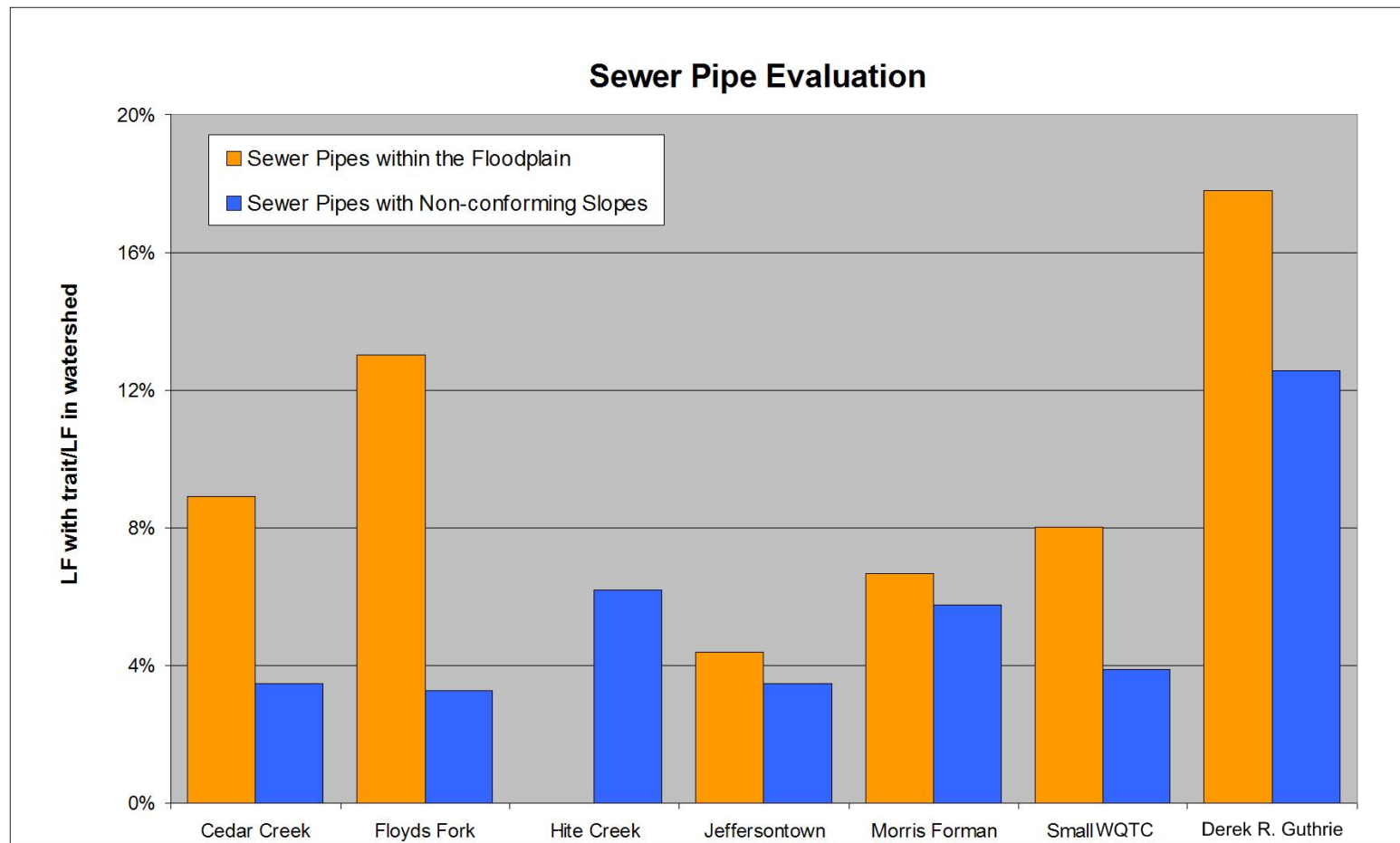
Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 2.2.1 SEWER PIPE MATERIAL BY SEWERSHED**



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 2.2.2 SEWERS LOCATED IN 100-YEAR FLOODPLAIN AND WITH NON-CONFORMING SLOPES BY SEWERSHED**





Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### **2.2.2.2 Pump Station Capacity Evaluations**

Developing pump station performance curves that represent the station's capacity under varying system conditions is a critical element for modeling a collection system. MSD maintains a set of as-built drawing and specifications that list pump capacity. While nameplate capacity and as-built drawings can list design capacity, actual in-situ testing provides the best estimate of capacity. Prior to modeling, MSD performed drawdown tests at pump stations, including all large pump stations and those associated with SSO or surcharged areas. The drawdown test consisted of measuring a pump's ability to drawdown, or drop, in the pump station wet-well volume and the corresponding time. After accounting for inflow during the test, the average pump discharge was determined. If there were several pumps, each was tested individually.

The drawdown tests results were compared to design data to note pump stations that were not performing at designed capacity. The design data was used at several small pump stations where drawdown tests were not performed.

### **2.2.3 Flow Monitoring**

MSD has been collecting environmental data sets for almost 20 years. Rain data have been collected continuously on a network of rain gauges across Jefferson County since the early 1990s. In 2003, a network of radar rainfall data was added to fill in the gaps in physical distance between the rain gauges. Rain data can be simultaneously evaluated with many of the other data sets to help determine the timing and impact of wet weather.

Sewer flow meters have been in place in various locations in the MSD collection system since the early 1990s. These meters have been used to assess existing conditions, locate I/I, determine SSO volumes, and assist sewer modeling efforts. The majority of the historical meters were temporary meters used for evaluation studies, but MSD has installed several permanent meters that are used for real time control (RTC) of storage within larger pipes to reduce SSOs. For purposes of this Volume of the IOAP, flow monitoring is essential for capturing flow data used for model calibration, testing the success of SSO abatement projects, and analyzing system performance after projects have been constructed.

#### **2.2.3.1 Flow Monitoring for SSDP Modeling**

MSD had approximately 145 flow meters temporarily installed by a contractor from January 2007 through mid-June 2007 to support hydraulic modeling and sewer system improvements planning. Approximately 45 additional flow meters were purchased by MSD to provide better coverage of the system. With the addition of these monitors, MSD will have approximately 69 permanent flow meters for use within the system.

One storm during the 2007 monitoring period was used specifically to calibrate and verify the models. This storm occurred on April 14, 2007, and rainfall gauges recorded depths of 1.2-inch to 1.54-inch over 21 hours during the storm event. A smaller storm was also recorded on April 11, 2007, and in some modeling areas this storm was used to assist in model calibration.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 2.2.3.2 Rain Gauge Network and Radar Rainfall

Rainfall data has been collected continuously on a network of rain gauges across Jefferson County since the early 1990s. During 2003, a network of radar rainfall data was added and rainfall data is currently gathered continuously at 15 rain gauge sites throughout the MSD sewer system.

The gauges are tipping-bucket type rain gauges (see Figure 2.2.3), where rainfall enters the gauge and is funneled down to a small “bucket.” The bucket will tip and empty when 0.01 inches of rain is collected. The amount of rain (tips) is accumulated and every five minutes the data is stored in MSD’s database for an accurate history of the rainstorm.

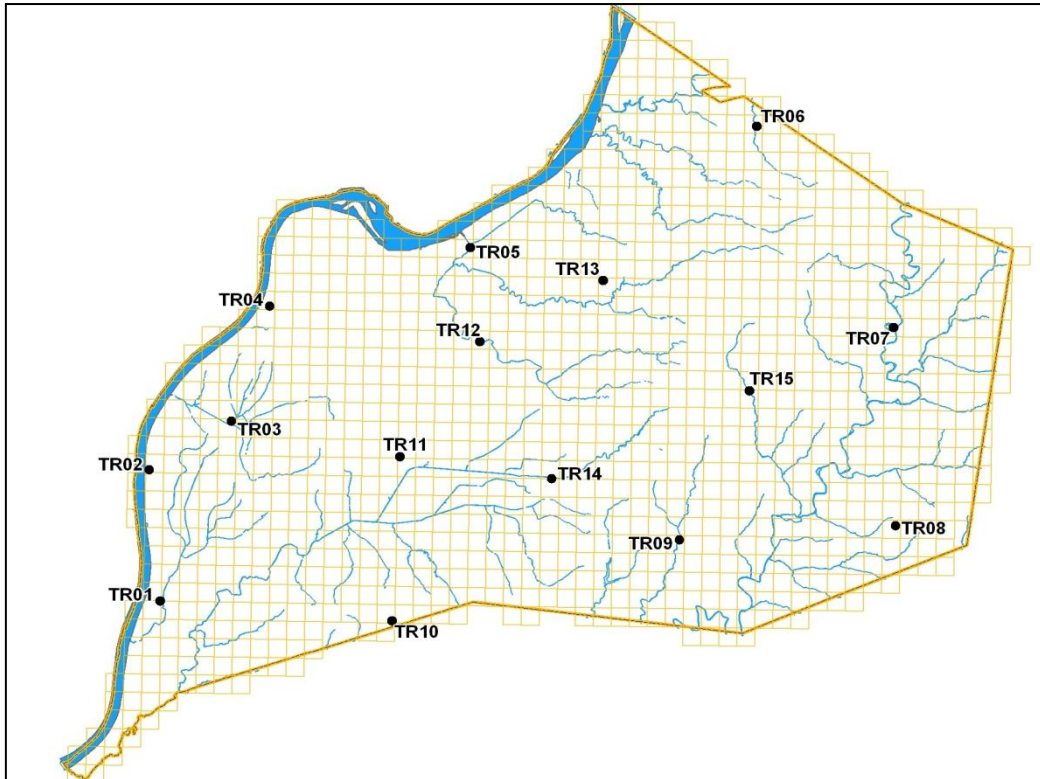
MSD currently receives radar rainfall data over a grid of approximately 1400 cells throughout the county and its immediate boundary (see Figure 2.2.4). These cells have rainfall depths reported every five minutes during wet weather and provide a thorough representation of the rainfall distribution differences across the county. Rainfall data is simultaneously evaluated with many of the other data sets to help determine the timing and impact of wet weather. Radar Rainfall and data from these gauges is used for model calibration, in determining “threshold” rainfall volumes for validation and for augmenting level of protection rainfall distributions.

FIGURE 2.2.3 RAIN GAUGE



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 2.2.4 TELEMETERED RAIN GAUGE NETWORK AND RAINFALL PIXEL GRID**



Data Source: LOJIC

Additional information on the rain gauge system can be found on MSD's website at <http://www.msdlouky.org/aboutmsd/rainfall.cfm>.

## **2.3 CONVEYANCE SYSTEM MODELING**

This section provides general background information related to model development. Detailed discussions of individual modeling efforts are discussed in Section 2.5.

### **2.3.1 Modeling History**

MSD's separate SSS system within Jefferson County is divided into three main areas: Beargrass Creek, Floyds Fork/North County, and Mill Creek/Pond Creek. The Beargrass Creek sewershed includes the Morris Forman WQTC; the Floyds Fork/North County sewershed includes the Cedar Creek, Floyds Fork, Hite Creek, and Jeffersontown WQTCs; and the Mill Creek/Pond Creek sewershed includes the Derek R. Guthrie WQTC.

The following discussion includes historic modeling efforts for the following areas:

- The Middle Fork and Beargrass Creek collection systems which flow to the Morris Forman WQTC, including Beechwood Village, ORFM/Muddy Fork, Hikes Point/Highgate Springs Pump Station, Buechel Branch, and Northern Ditch.
- The Cedar Creek collection system, which flows to the Cedar Creek WQTC.
- The Pond Creek, McNeely Lake, Mill Creek, and Valley Village collection systems, which flow to the Derek R. Guthrie WQTC.
- The Jeffersontown collection system, which flows to the Jeffersontown WQTC.
- A portion of the Prospect collection system, which includes Hunting Creek North, Hunting Creek South, and Timberlake WQTCs.

#### **2.3.1.1 Middle Fork of Beargrass Creek Collection System**

##### **Middle Fork (including Beechwood Village)**

In 2003, the Middle Fork XP-Stormwater and Wastewater Management Model (XP-SWMM) Hydraulic Model was built and calibrated to 1998-1999 flow monitoring data. This calibration was used to analyze the system for deficient sewers and SSOs for various rainfall depths. Since the original flow monitoring data was older, new flow monitoring was performed in 2003-2004 and the model was re-calibrated. The model covered an area of approximately 14,283 acres.

Both the 1998-1999 and 2003-2004 calibrated models showed similar results: the majority of the wet weather problems were occurring in the Beechwood Village/Sinking Fork and Lower Middle Fork sub-sewersheds. These two areas contain the majority of SSO locations, SSO volume, and capacity-deficient sewers in Middle Fork. The model was used to perform capacity

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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assessments and analyze potential improvements in Beechwood Village and other areas of Middle Fork.

### **Ohio River Force Main / Muddy Fork**

The ORFM XP-SWMM Hydraulic Model was built and calibrated in 2000-2001 using 1998-1999 flow monitoring data. The ORFM is a dual force main consisting of 92,000 linear feet (LF) of pipe. There are eight connected pump stations and approximately 7,600 acres covered in the model. The model was used to evaluate numerous operational scenarios to determine how the system would function with different combinations of pumps in operation and at maximum flow conditions.

### **Hikes Point / Highgate Springs**

The Hikes Point XP-SWMM Hydraulic Model was developed as part of the 1997 Sanitary Sewer Evaluation Study (SSES). This model was used to test various scenarios for in-line storage in the area affected by wet weather emergency pumped SSOs and results were used to establish design parameters for the Hikes Point Phase 1B rehabilitation project. In 2002, the model was updated and recalibrated to 2002 flow monitoring data for use with the RTC system developed by MSD. Also at this time, the system was extended to include the Southeastern Diversion Structure. In 2003, the model was used to perform analyses for several SSO sites with the goal of determining whether emergency pumps were required and if so, at what depth of flow they should be activated. The model covers an area of approximately 5,500 acres.

In 2003-2004, the model was used as the basis for the Hikes Point System Improvement Phase 1 Project. It was used to develop a solution to eliminate SSOs, both model-predicted and known. The model was also used to determine available hydraulic capacity in the system for various storm events.

In 2004-2005, the XP-SWMM model was used for the Hikes Point Capacity Assessment Project to refine solutions developed in the system improvements project and evaluate options for redirecting flows external to the Hikes Point system throughout the area. Cost estimates were refined and ground truthing was performed to help identify the most viable abatement options.

### **Southeastern Diversion Structure / Buechel Branch / Northern Ditch**

In the early 1990s, an evaluation of relief capacities of the Southeastern Diversion Structure and Southeastern Interceptor was conducted using the XP-SWMM program. The objective was to optimize the flow diversion approach to provide relief to the Hikes Point and Buechel Branch areas upstream of the diversion structure, but this created surcharging and SSOs upstream. Currently the flow diversion gate is normally closed during wet weather.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

The Buechel Branch XP-SWMM hydraulic model was built and calibrated in 2002-2003, using 2002 flow monitoring data collected during the RTC project. The Buechel Branch RTC model covers approximately 2,800 acres and is centrally located at the intersection of Breckenridge and Nachand Lanes. The Northern Ditch area was also included in the Buechel Branch RTC model. In 2003, minor updates were made to this model, which included adding a small amount of new residential development.

### **2.3.1.2 Cedar Creek Collection System**

The Cedar Creek XP-SWMM hydraulic model was originally built and calibrated in 2000-2001 using 1998-1999 flow monitoring data. This model consisted of sanitary sewers tributary to the Cedar Creek WQTC. New system infrastructure was added and system rehabilitation projects took place in 2002-2003 so the model was updated to include the changes. The model was recalibrated for wet weather flow and dry weather flow (DWF) using flow monitoring data collected in 2002-2003.

Future conditions scenarios were analyzed in conjunction with the Jeffersontown Interceptor Condition Assessment project. Areas that were proposed to be diverted to the Cedar Creek area in the Jeffersontown Action Plan were added to the model and the effects analyzed. The Cedar Creek model covers approximately 3,600 acres of area.

### **2.3.1.3 Pond Creek Collection System**

The Pond Creek XP-SWMM hydraulic model was built and calibrated in 2002-2003 using 1997-1998 flow monitoring data. The model consists of 10-inch and greater diameter sanitary sewer tributary to the Pond Creek and Mill Creek interceptors but does not include the Valley Village Interceptor. The model covers approximately 29,100 acres.

### **Derek R. Guthrie Spline Model (including Valley Village)**

The Derek R. Guthrie WQTC spline hydraulic model was built by joining the Mill Creek model with a spline model of the Pond Creek system under the Derek R. Guthrie Conveyance System Improvements Project. The Valley Village interceptor was incorporated into the model. This model was originally calibrated in 2002-2003 using 1997-1998 flow monitoring data in the Pond Creek system, and 2001-2002 flow monitoring data in the Mill Creek system. The model was updated and recalibrated after system rehabilitation using 2002-2003 flow monitoring data. The model covers approximately 43,000 acres. The Derek R. Guthrie WQTC spline model was used for analysis of the proposed Pond Creek Interceptor storage basin as well as to identify system corrections to eliminate the direct entry of Mill Creek floodwaters to the system.



## **McNeely Lake**

The McNeely Lake hydraulic model is part of the Pond Creek hydraulic model. To improve the calibration, previous flow monitoring data, pump run records, and downstream flow monitoring data were reviewed. The Derek R. Guthrie WQTC spline model was used in 2004-2005 to review hydraulic solutions on the Pennsylvania Run study area collection system due to planned and future developments.

## **Mill Creek**

The Mill Creek model was built and calibrated in 2001-2002 using 2001 flow monitoring data. The model was built to simulate dry weather and wet weather flow in the separate SSS system. This model was part of the Derek R. Guthrie WQTC spline model, which was built by joining the Mill Creek model with the Pond Creek system model.

### **2.3.1.4 Jeffersontown Collection System**

The Jeffersontown XP-SWMM hydraulic model was originally built and calibrated in 1998-1999 using 1997-1998 flow monitoring data. This model consisted of sanitary sewer tributary to the Jeffersontown WQTC. Model runs were performed to evaluate the system response to various storm events and was used to identify SSOs within the model. The project modeled approximately 4,650 acres. In 2001, this model was used to evaluate scenarios for inclusion in the Jeffersontown Facilities Plan submitted to the KDOW in August 2002.

A simple hydraulic isolation analysis was performed in 2002-2003 using 2002 flow monitoring data. This analysis created several artificial free outfalls within the system to evaluate the performance of the sub-basins independent of the primary interceptors. The model was revised to reflect the impact of the Jeffersontown Facilities Plan. The Facilities Plan was then updated to include anticipated flows from undeveloped areas. Finally, the model was used to evaluate various options to improve the system and eliminate unauthorized discharges. A report detailing this information and providing recommendations for capacity improvements for SSO eliminations was completed in September 2005.

### **2.3.1.5 Prospect Collection System**

The Prospect XP-SWMM Hydraulic Model includes the North Hunting Creek, Hunting Creek South, and Timberlake WQTCs covering approximately 1,856 acres. The Shadow Wood WQTC was not modeled because it was privately-owned at the time. The Prospect model was built to simulate dry weather and wet weather flows, and was calibrated in 2002 using 1999-2000 flow monitoring data. The model was used in conjunction with existing data and wet weather inspections to develop a comprehensive solution for the elimination of SSOs at the Gunpowder Pump Station. The project was completed in August 2004.

## 2.3.2 Objectives of the Modeling Program

Objectives and uses of the modeling program include:

- Performing alternative and solution analysis for SSO volume reduction and elimination
- Projecting capacity for new development
- Performing future analysis, with an increased investment in calibration/validation, of system upgrades due to age and asset deterioration
- Simulating storm events and system response investigation

## 2.3.3 SSDP Model Development

The hydrologic and hydraulic modeling software selected for all hydraulic modeling was InfoWorks. The InfoWorks program is designed not only to model wet weather effects on collection systems, but to also take advantage of a large GIS database provided by LOJIC. InfoWorks has the ability to import XP-SWMM models, allowing MSD to build on extensive prior modeling, as detailed in Section 2.3.1.

There are a total of 11 modeled areas in the Final SSDP (refer to Figure 2.3.1 at the end of the chapter). MSD provided each modeling team with known system hydraulic information such as known SSO location, volume and duration; pump station runtime information; known surcharge areas; and other relevant data for each modeled area. This information was used by the modeling teams in calibration and validation of the models.

### 2.3.3.1 Modeling Guidelines

As a first step in the program, MSD developed the Hydraulic Sewer System Modeling Guideline Manual (see Appendix 2.4.3 in Volume 2). These procedures improve the detail, quality, and functionality of the sewer models while providing consistent model development criteria.

The guidelines instructed the modelers how to:

- Perform the capacity assessments
- Develop a range of system improvements
- Develop the benefit/cost ratios for the various solutions in a consistent manner
- Confirm reported results are sufficient for development of the Final SSDP

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

MSD developed the Modeling Guidelines to address the following:

- Update modeling standards, including refining the I/I modeling procedures and assessing flow monitoring
- Review XP-SWMM models to determine deficiencies
  - Identify expansion needs
  - Assess data verification needs
  - Collect record drawings, and
  - Conduct pump-station drawdown tests
- Switch to the InfoWorks software and develop a platform (server) for retrieving, storing and sharing model data
- Import shape files of the model area into InfoWorks
- Develop flow monitoring basins
- Define hydrologic and hydraulic parameters
- Review modeling input and output

The following summaries provide samples of important guidelines presented in the manual related to initial model development.

### **Modeling Standards and Migration of Model Data**

MSD developed a full set of modeling standards prior to performing any separate SSS modeling. This included calibration standards, use of flow monitoring data, use of previous models, input and export standards, Quality Assurance / Quality Control (QA/QC) procedures, and modeling techniques for I/I and pump facilities. In parallel with that effort, MSD reviewed past models and determined deficiencies in data, such as inverts and pump data. They also coordinated with MSD crews who conducted drawdown tests at key pump station facilities.

InfoWorks CS is a modeling platform designed around GIS databases and is capable of importing data from other models. Thus, InfoWorks models were not designed from “scratch.”

### **Flow Monitor Basins**

MSD determined that flow monitoring basins should have no more than 100,000 LF of pipe within its boundaries, not including areas contributing flows measured by upstream monitors. As much as practical, each basin had uniform landuse and soils data.

## Hydrologic Parameters

Hydrologic parameters refer to the components of the model that are manipulated to simulate rainfall dependent inflow and infiltration (RDI/I). RDI/I is simulated as rain falling on catchments. These catchments are not real, but rather mathematical abstractions used to determine the rate and volume of RDI/I over time.

MSD system models do not account for the effects of snowmelt due to the small volume of water resulting from snowmelt for this region of the country. Likewise, evaporation is ignored due to the relatively short model runs.

DWF is a combination of groundwater infiltration, residential, industrial, and commercial user flows. DWF is defined as the flow that occurs in absence of any runoff due to precipitation. Three main features of DWF are flow volume and rate, diurnal pattern, and spatial distribution. Each is determined from flow monitoring data. DWF is allocated to individual manholes based on spatial data, such as census and landuse.

## Hydraulic Parameters

Hydraulic parameters represent the infrastructure of the model. This would include features such as pipes, manholes, pump stations, and force mains. The modeler provides dimensional and geographical information for each feature. The modeler also provides the node and link arrangement to mimic actual infrastructure connections.

MSD provided each modeler with past models and pertinent LOJIC GIS data. With this information, each modeler developed the complete sewershed model and the models were checked with InfoWorks review tools. The following represent critical components of a model's accuracy and the method used in the modeling procedure to address them.

## Pump Stations

Since pump station capacity is critical to developing an accurate model, significant effort was paid to pump station representation (see Section 2.2.2.2). Each procedure was detailed by pump size within the Modeling Guideline Manual. Large pumps are always modeled as dynamic pumps, with capacity a function of wet well and outlet conditions.

## Boundary Conditions

In most cases, a downstream boundary condition is a known hydraulic grade line elevation at the point of interface between the modeled system and a system outside of the modeled boundary (e.g. river). During periods of high flow, backwater effects in the conveyance system caused by a high hydraulic grade line at a pump station wet well were captured and modeled.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

For the Final SSDP, the following boundary conditions were used:

- For downstream branches, the boundary condition could include WQTC capacity, Interim SSDP project allotment, or existing flow to the combined sewer area.
- For upper branches not tying into a WQTC, Interim SSDP project, or combined sewer system, solutions were determined without regard to downstream impacts (i.e. no penalty for conveyance).

### **Model Input and Output**

Model input selection and the level of detail to which the model is constructed are important to confirm the model is properly constructed. Equally important is a complete review of model output prior to acceptance of model results. After the modeling teams made a thorough review, the model was reviewed by a separate modeling firm to verify accuracy. Additional detail on the quality assurance and quality control (QA/QC) procedure is described in the next section.

#### **2.3.4 Rainfall Distribution and Level of Protection**

Rainfall is characterized by temporal distribution and total volume. Both of these characteristics impact design capacity, pumping rates and optimized solutions. Level of protection is the selection of a rainfall-volume frequency or level for design. This is commonly denoted by an average interval, such as a two-year storm that has a 50 percent probability of occurring in any given year.

From a practical perspective, no sewer system can be designed to consistently convey all system flow during extreme weather events. Therefore, a “design condition” must be defined that reflects the level of protection consistent with community values. The costs for capturing wet-weather events must be balanced with the benefits to community associated with capturing that event. Section 3.2.1 in the following chapter outlines the procedure used for determining consistent costs. Section 3.2.2 outlines the procedure used for determining benefits consistent with community values, as outlined in the Stakeholder process. Section 3.2.3 outlines the procedure used for determining the best benefit-cost ratio, thus defining the preferred level of protection.

In the Final SSDP, the values evaluation framework was used to determine levels of protection that reflect an appropriate level of control of unauthorized discharges for the Louisville Metro community.

##### **2.3.4.1 Base Rainfall Distribution**

For the separate SSS modeling, MSD considered two storm distributions: 1) the Natural Resources Conservation Service (NRCS) “long duration” distribution and; 2) the National

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Oceanographic and Atmospheric Administration (NOAA) “short-duration precipitation,” often referred to as the “cloudburst” distribution. The Natural Resources Conservation Service method is a general large-area storm often used for design of large stormwater and flood control structures such as dams and detention facilities. The NOAA cloudburst distribution uses depth-area-reduction-factors derived from frequency analyses of local hourly precipitation data recorded at the Louisville International Airport. This distribution is typical of shorter duration storms that often cause SSOs in individual basins. It is also similar to the storms captured during the system flow monitoring used for model calibration.

Based on an analysis of over fifty years of historical weather patterns for Jefferson County, MSD determined that a three-hour, high-intensity cloudburst storm reflected the most appropriate storm pattern to use in SSO control evaluation. The NRCS long duration distribution is more appropriate for total system-wide modeling for larger service areas, such as inflow to regional wastewater treatment plants, since the attenuation of the peaks for the larger service area is less dramatic. However, the cloudburst storm is more appropriate for localized collection system modeling and provides for better calibration and validation of the hydraulic models to known SSO locations.

See Appendix 2.3.1, Selection of the Cloudburst Storm, for additional details on the selection of the cloudburst storm.

#### **2.3.4.2 Second Storm Distribution**

In some cases, the preferred solution for an SSO will be storage of excess wet-weather flow. Storage, however, will only be effective as an SSO abatement strategy if it can empty in short order. Otherwise, a small second storm immediately after the design storm could cause a full storage facility to overflow.

To account for this, a second smaller rainfall distribution was added after the first such that the rainfall peaks were 12 hours apart. The total rainfall depth for the second storm was consistently set at 0.46”, corresponding to a 10-day recurrence interval storm.

#### **2.3.4.3 Model Simulations**

During system characterization, a suite of design conditions was analyzed starting at the 1.27-inch cloudburst up to the 2.60-inch cloudburst. This allowed the opportunity to validate models and determine the extent of various deficiencies, such as surcharging, at each level. During solution optimization, the baseline storm was at the 1.82-inch cloudburst storm level. Once a solution had been identified at this level, the solution was then analyzed at a 2.25-inch cloudburst level and 2.60-inch cloudburst level to compare benefit-cost ratios for a modeled watershed branch. Solution optimization is discussed in detail in Volume 3, Chapter 4.



### **2.3.5 Model Calibration, Validation, and Baseline Conditions**

The following sub-sections summarize critical modeling components related to model and solution development.

#### **2.3.5.1 Model Calibration**

Model calibration is the process of comparing model-predicted results to measured flow monitoring and rainfall data from a single, significant rainfall event and to match pump station drawdown test results. The process is iterative and proceeds until the modeled results match the measured data within a pre-defined percentage level of accuracy, called action levels. Model calibration and validation reports are located in Appendix 2.3.2.

#### **Action Levels**

The action level of accuracy is 20 percent for the difference in base flow rate (minimum); the action level is 10 percent for the difference in flow volume and the difference in peak flow rate (maximum). The hydrograph shape, mean flow velocity, and water depth predicted by the model and measured by the flow monitoring is also qualitatively compared. Guidelines on adjusting models are detailed in MSD's Hydraulic Sewer System Modeling Guideline Manual, Volume 2, Appendix 2.4.3.

#### **Model Re-calibration**

Model re-calibration was required after validation and verification of modeled overflow points (MOPs). MOPs are discussed in detail later in this section. Model calibration and re-calibration was completed in accordance with MSD modeling standards and protocols. The standards can be found in the Hydraulic Sewer System Modeling Guideline Manual, Volume 2, Appendix 2.4.3.

#### **2.3.5.2 Model Validation**

Once the model is calibrated, the model is then "validated." Model validation is simply cross-checking the model performance against other recorded storm events or historical system performance data sources, such as known SSO locations, using threshold rainfall depths known to cause overflows, reported overflow volumes, and surcharged pipes. Due to lack of additional, system-wide storm events during the 2007 flow monitoring period, model validation was focused on validating the models to readily available historical overflow data. For details on future model calibration, validation, and flow monitoring procedures reference MSD's Post-Construction Compliance Monitoring Plan detailed in Volume 1, Chapter 6.

## **Known SSOs**

MSD provided threshold 24-hour rainfall and average reported SSO volume for each known SSO in MSD's service area. The calibrated model simulated the 2.2-inch, 2.7-inch, and 3.2-inch level (this corresponds roughly to the six-month, one-year, and two-year Natural Resources Conservation Service design rainfall events) and the modeled SSO locations and volumes were noted. In some cases, modeled SSOs occurred within a few manholes of known SSOs, these locations were considered to represent the known SSOs.

The results were compared to the initial SSO list with two goals in mind. The primary goal was to show overflows at each known SSO location for similar rainfall depth. A secondary goal was to have relative agreement in SSO volume; for example, the SSOs in the sewershed within the top third of the reported volumes were not in the lowest third of the modeled SSO volumes. If parameters needed to be adjusted, the model was modified in a manner similar to calibration modifications. The validated MOPs were not considered for this criterion since there were no reported SSO volumes associated with the locations. Initial validation took place prior to MOP investigations in the spring of 2008.

## **Surcharged Pipe**

MSD provided maps of areas with historical basement flooding based on complaint records and installed back-flow preventers. In most cases these areas coincided with known SSO locations and known hydraulic restrictions. In the few instances where surcharging was not noted in the model, parameters were adjusted upwards to induce surcharging for a 1.27-inch storm in a manner similar to calibration modifications.

## **Unvalidated SSOs**

In some cases, SSOs could not be induced in the model where known SSOs occurred. If the pipe slope in the area was shallow, sedimentation could be applied to the model to induce the SSO (process was performed according to modeling standards). In these cases, MSD investigated the downstream sewer system to locate blockages or other operational problems. If the problem was cleared, the SSO status was changed to "Remediated." These cases are detailed in Appendix 2.3.2, Model Calibration/Validation Reports, and the sewershed summaries in Section 2.5.

## **Recalibration**

After validation was completed, the model was reviewed to confirm it met calibration standards. If it did not, the model was recalibrated and revalidated until all action items and validation goals were met. In practice, validation and any re-calibration took place simultaneously.

## **Appropriate Rainfall Distribution**

While model calibration and validation was being conducted, MSD contracted to have a rainfall analysis performed and synthetic rainfall events produced for the Louisville Metropolitan area, based on 59 years of rainfall records at the Louisville International Airport. (See Appendix 2.3.1.) The analysis indicated that the typical storm type and duration for Louisville rainfall events is the 3-hour duration cloudburst event, especially for events over the two-year recurrence interval.

MSD compared the typical Natural Resources Conservation Service Type II 24-hour rainfall distributions with the 3-hour cloudburst distributions to determine the best synthetic rainfall event to use for further validation and additional analyses. The Natural Resources Conservation Service distributions resulted in unrealistic model results that did not match calibration and validation data from storm events of similar recurrence intervals. The results typically showed higher overflow volumes, longer overflow durations, and more modeled overflow points that did not correspond with field data. The cloudburst storm overwhelmingly showed a closer resemblance to overflow recurrence intervals, approximated overflow volumes, and documented overflow locations that had been recorded over the past five years. Because of this approximation of typical events, the cloudburst storm distribution was selected for the development of overflow abatement solutions.

### **2.3.5.3 Model QA/QC Process**

As mentioned earlier, calibrated and validated models were also subjected to a QA/QC process as discussed in the Modeling Guidelines. This QA/QC peer review involved a “swapping” of models based on a pre-determined assignment list. The process involved reviewing dry-weather and wet-weather flow surveys, comparing results for calibration storm, and reporting discrepancies in a QA/QC checklist and comments form. Reviews were then returned to the model development teams for responses and revisions. In some cases, recalibration was necessary. Table 2.3.2 is a sample of the QA/QC checklist used by modelers to verify and validate model accuracy. Full Model QA/QC documents are provided in Appendix 2.3.3.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.3.2**  
**QA/QC CHECKLIST SAMPLE**

GENERAL REQUIREMENTS		
ITEM	OK	SEE COMMENT
<b>Model Development</b>		
1. Standard Data Flags – Ensure data flags have been properly used. (Section 3.4.1)	<input type="checkbox"/>	
2. Rainfall Data – Check the rainfall data to ensure the PIXEL number has been used for the profile ID (Section 3.4.2). Ensure pixels cover the entire modeling catchment.	<input type="checkbox"/>	
3. Rainfall Data – Check rainfall data units. Rainfall data should be in inches/hour.	<input type="checkbox"/>	
4. Model Building – Check the unique IDs used for nodes and links (Table 3-2 Section 3.4.3).	<input type="checkbox"/>	
5. Model Building – Check pipe invert and manhole rim elevations. Generally these should range from 400ft to 800ft above sea level for Louisville.	<input type="checkbox"/>	
6. Model Building - Run the network validation and check to see if there are any errors or warnings that need to be addressed.	<input type="checkbox"/>	
7. Model Building – Check the simulation parameters. Generally the "Simulation: Tolerance for Volume Balance" parameter should be set to 0.01 for model stabilization. (Section 3.4.6)	<input type="checkbox"/>	
8. Standard Naming Convention – Check naming convention used for groups listed in the Guidelines. (Section 3.4.8)	<input type="checkbox"/>	
<b>Hydrologic Parameters</b>		
1. Runoff – Runoff Volume Type should be set to Fixed for all Runoff Surfaces. Can be set to SCS only if in a rural area. (Section 4.1.1)	<input type="checkbox"/>	
2. Runoff – Routing Model should be set to SWMM for all Runoff Surfaces (Section 4.1.1)	<input type="checkbox"/>	
3. Evaporation & Other Losses – For single storm event analysis evaporation losses should be set to zero. See Guidelines for continuous annual simulations. (Section 4.4)	<input type="checkbox"/>	
4. RDII – Check to ensure the model has the proper number of dummy subcatchments to simulate the fast, medium, and slow response of for RDII. A minimum of two are required. (Section 4.5)	<input type="checkbox"/>	
5. Subcatchment Areas – Check for large subcatchment areas. Ensure these areas represent the contributing area to the sewer system. For large parcels the subcatchments should only be drawn around the contributing area and not the entire parcel.	<input type="checkbox"/>	
<b>Hydraulic Parameters</b>		
1. Conduit Data – Pipe shapes should be predominately circular except in the CSS area.	<input type="checkbox"/>	
2. Datum shift – Spot check 5 pre-2002 and 5 post-2002 constructed conduits and manholes to ensure the -0.5 feet datum shift from NGVD29 to NAVD88 was properly applied. (Section 5.1)	<input type="checkbox"/>	
3. Conduit Data – Check for elevations of zero, adverse slopes, and non-standard pipe diameters. (Section 5.1)	<input type="checkbox"/>	
4. Conduit Data – Manning's N values should be set 0.013 in the Separate Sewer System and 0.013 – 0.016 in the Combined Sewer System based upon pipe material. (Section 5.1)	<input type="checkbox"/>	
5. Conduit Data – Headloss Types should be set to 'normal'. (Section 5.1)	<input type="checkbox"/>	
6. Node Data - All junction chambers and shafts should have a diameter of 4.0 feet. For pipe diameters greater than 4.0 feet the chamber diameter should equal the pipe diameter. (Section 5.2)	<input type="checkbox"/>	

#### **2.3.5.4 Modeled Overflow Points (MOPs)**

After validation and peer review, the models were simulated again at the 1.82-inch cloudburst storm level to note any modeled SSOs that were not associated with known SSOs. These SSOs were designated as MOPs. MOP locations were targeted for further analysis and field investigations. Section 2.4.2 describes the MOP investigation and validation procedures.

#### **2.3.5.5 System Deficiencies**

Once models were calibrated and validated, system deficiencies were determined for various levels of protection. The system was characterized by SSOs, surcharged pipes, and areas at or near capacity for each analyzed level, including peak flow rates, time to peak, and total SSO volumes. System deficiencies noted include hydraulic restrictions, hydraulic jumps, bottlenecks, pump limitations, flow monitoring limitations, insufficient slopes, and non-standard diameters. System deficiencies can be divided into two categories: 1) construction and 2) hydraulic, as explained below.

##### **Construction Deficiencies**

Construction deficiencies are related to operation and maintenance issues. Deficiencies may not directly cause SSOs or hydraulic issues but they require additional maintenance and, therefore, contribute to conditions that can promote the formation of SSOs. The InfoWorks Engineering Tool includes a variety of tests to identify engineering deficiencies such as pipe slopes (which can promote silting), pipes with insufficient soil cover (which may be damaged by traffic), and excessively long pipes (which are difficult to access for inspection and cleaning).

##### **Hydraulic Deficiencies**

Hydraulic deficiencies are related to physical limitations of the system. Such systems may meet specific Engineering Standards for normal flow, but are insufficient for the flows observed in the field. These deficiencies could include bottlenecks, hydraulic jumps, and surcharged pipes. While InfoWorks can identify numerous minor reductions in flow that have no impact on sewer performance, only hydraulic restrictions that result in surcharging under modeled flow are flagged as restrictions.

Hydraulic deficiencies are identified through several features integral to InfoWorks. This will take advantage of the rigorous examination of the data performed during the model construction. For example, hydraulic jumps are marked as part of the surcharge identifier. Other deficiencies require modeler evaluation. For example, pump station limitations are highlighted by surcharging upstream of the pump station, but requires the modeler to confirm the pump station capacity as the true restriction.

### **2.3.5.6 Model Branching**

Prior to the solution development process, the models were subdivided into “branches.” These branches were analyzed separately, beginning at the most upstream branches and proceeding downward toward the sewershed outlet or WQTC. During solution development, costs, benefits and benefit-cost ratios were determined for each branch separately. Once a preferred solution was determined for upstream branches, development proceeded downstream.

Ideally, each branch would address a separate hydraulic issue that caused SSOs and surcharging. In practice, branches were set by grouping hydraulically connected SSOs, surcharging and system deficiencies. These groupings often contained several SSOs and often two or more groupings would be in close proximity.

Section 2.5 provides details on the branch selection for each model area. Figures 2.3.2 through 2.3.11 at the end of the chapter provide maps of each modeled area and respective branch boundaries.

### **2.3.5.7 RDI/I Reduction**

RDI/I reduction, identified by the Wet Weather Stakeholder Group as a critical component of solution development, was an integral part of every solution. MSD developed a method to project estimated RDI/I reduction for the entire MSD service area. Appendix 2.3.4, RDI/I Method and Modeling Techniques Technical Paper, provides a technical paper outlining this application and the modeling techniques.

The RDI/I reduction projections were:

- Applied to all models prior to solution evaluation.
- Based on flow monitoring results, namely peaking factors at flow monitoring basins. The peaking factors were calculated prior to modeling by comparing monitored flow to average flow determined from a period of dry weather.
- Applied only in areas with high peaking factors (greater than four).
- Conservative in that RDI/I reduction was set at a maximum of 25 percent reduction and then only at areas with peaking factors greater than 14.

It should be noted that the projected RDI/I reduction used in the models is based on estimated values. The actual RDI/I reduction will be based on the type and comprehensiveness of the rehabilitation effort. This is not to say that actual RDI/I reduction exceeding the projected reduction values used in the models cannot be accomplished. It is expected that they will in many cases. Such successful RDI/I reduction projects will provide capacity for areas where reduction is not as successful. It is, however, prudent that overly optimistic values are not used



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

in planning and design. This is especially important in transport-based solutions where the diameter of installed piping cannot readily be changed once it is installed. The projected RDI/I reduction applied to each model is listed in the Section 2.5.

### **2.3.5.8 I/I Program**

MSD will execute an on-going I/I Program for systemic improvements in the collection system during implementation of the Final SSDP. At the behest of Stakeholders MSD committed to use RDI/I removal as the first approach to eliminate SSOs. MSD recognizes that, based on past I/I Program Projects, the degree of RDI/I removal is often difficult to predict and success is not always assured. Accordingly, MSD has committed to achievable levels of RDI/I removal in areas where success is most likely.

Projected RDI/I removal was applied to all hydraulic models prior to solution development and optimization. Details of this approach are found in Appendix 2.3.4. Once optimized solutions for all SSOs had been developed, RDI/I reduction was removed from the models. The models were re-evaluated and solutions were re-sized at the 1.82-inch cloudburst storm level. The cost differential between the two sets of solutions, one with and one without RDI/I reduction, was used to determine appropriate I/I Program costs, as presented in Chapter 3, Appendix 3.1.1, I/I Program Documentation. It is estimated that the annual cost would average \$1.6 million. This cost does not include programmatic needs for inspection and rehabilitation related to associated programs such as CMOM, SCAP, and the Nine Minimum Controls (NMCs). To provide contingency and to account for the costs to accommodate associated programs, the annual cost of the I/I program was set at \$3 million.

Appendix 3.1.1 (Table 6) lists projects dependant on RDI/I reduction as part of the SSO elimination solution. Appropriate rehabilitation for these projects will take place as part of the I/I Program prior to actual capital construction of these solutions. The earliest I/I projects will likely concentrate on areas solely dependent on RDI/I removal (such as Branch MSD1086 in Hite Creek); these projects already have funds allocated for RDI/I removal. Other early candidates include areas with the highest peaking factors and thus the highest potential for RDI/I reduction. The actual schedule will be determined by MSD in conjunction with the CMOM Program, SCAP, and other associated programs.

Given the uncertainty of RDI/I removal, monitoring and adapted management techniques are critical to success of the I/I Program. Pre- and post rehabilitation flow monitoring will take place as part of the Final SSDP (refer to Volume 2, Section 1.3.1 for a description of this program) and will include areas in the I/I program. SSOs will also be monitored under SORP guidelines (refer to Section 1.3.1.5). Post-construction monitoring will be used to demonstrate the impacts of I/I improvements on RDI/I reduction. As SSOs are eliminated they will be removed from the I/I Program. If flow monitoring and the SORP program show that RDI/I removal has been effective but insufficient, additional RDI/I removal may be implemented as part of the I/I Program or the CMOM Program. If flow monitoring and the SORP program indicate that RDI/I removal has not been effective, additional construction alternatives may occur at the SSO.

### **2.3.5.9 Capital Improvement Projects**

All MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. In some cases, the project was expanded and lengthened; in others, the project was shortened. In all cases, some portion of the capital project was included in the optimized solution, although this was not a requirement. The Capital Improvement Projects used in solution development are listed for each modeled area in Section 2.5.

### **2.3.5.10 Build-out Development**

In preparing solutions, potential future development was considered. Consequently, MSD developed a method to determine areas likely to be developed and added to existing systems.

In general, build-out was applied as additional flow using the following criteria:

- Upstream of SSOs
- Drained by gravity to the SSO
- Limited to open areas outside of 100-year floodplain, parks and recreational areas
- Limited to buildable areas (no steep slopes or shallow bedrock)
- Developable in phases consistent with planning documents
- Single-family home equivalents, with peaked wastewater flows per MSD's Design Manual
- Flow added to the existing system at an appropriately sized interceptor
- Peak flow added to the model to coincide with peak rainfall
- Additional flows from all other areas would fall under the SCAP requirements

Appendix 2.3.5, Build-out Method and Modeling Techniques, provides the full reports describing the build-out potential and the techniques used for determining the areas. Specific build-out parameters used in solution development are listed for each modeled area in Section 2.5.

### **2.3.5.11 Future Model Updates**

Following construction, calibration, and validation of models under the Final SSDP program, periodic updates to the model will be conducted. Every 12 months, each model will be reviewed internally by MSD to document any changes to the system that have occurred. Changes include new sewers, pump station eliminations, pump station upgrades, capacity upgrades, etc. With the results from this review, MSD will proceed with updating any significant changes in the

sewer models. The need for an update will vary for each model due to the unique characteristics of each model. Appropriate documentation will take place for all model updates. The scale of the necessary documentation will be related to the scale of the changes to the model, the length of time since the last full model report was prepared, and the end use of the model.

## **2.4 SSO CHARACTERIZATION**

This section discusses the initial SSO list and the process for the validation of MOPs by field investigation. It also presents the final SSO list used for Final SSDP solution development.

### **2.4.1 Initial SSOs**

Identification, validation and characterization of SSOs are a continuous process. Management of the data associated with these activities is described in the SORP.

In the Spring of 2007, flow monitoring data collected throughout the MSD collection system along with continuous rainfall data from the MSD rainfall network, were used for initial calibration of the models. The calibrated models were then validated against 126 “initial” SSOs: those known to be active, known SSOs at the beginning of the modeling process in the Fall of 2007.

For each initial SSO, the following data was developed:

- **The 24-hour “threshold rainfall” volume.** This threshold rainfall was determined by noting the minimum (non-zero) 24-hour rainfall for each SSO event at each initial SSO. The rainfall was derived from the nearest rain gauge and centered on the time the SSO was first reported to overflow.
- **Average reported volume for each initial SSO.** This data is not as dependable as threshold rainfall since SSO volumes are estimated and reported based on when the SSO was first discovered until it ceases. This data was not used in calibration. MSD used this data for general guidance in the validation phase after calibration was performed to ensure models were predicting known overflows within a reasonable range of the reported volume. Refer to Section 2.3.5.2 for a description of the Model Validation process.

As described later in this section, MOPs that became validated by field investigation were added to the initial SSO list and used in further model validation.

## **2.4.2 MOP Validation Process**

Early modeling based on initial SSOs indicated that SSOs might occur at locations other than documented SSOs. A separate category, known as MOPs, was created to classify these SSOs. A MOP corresponds to a particular manhole or pump station location.

MSD's goal was to verify the existence (or lack thereof) of the MOPs through field investigations. In particular, MSD focused on "targeted" MOPs, with the following characteristics:

- Modeled overflow volumes greater than 10,000 gallons during a 1.82-inch cloudburst storm
- Not hydraulically connected to a documented SSO

The following subsections summarize the field investigation process.

### **2.4.2.1 Investigation Procedures**

The following steps briefly describe the investigation procedures developed by MSD for validating MOPs:

- Investigation teams attended MSD training for inspecting manholes and how to document findings.
- Seventy-one targeted MOPs were divided among teams by geographical location.
- During and immediately following three significant rain events in March, April, and May 2008, investigation teams performed the following:
  - For each MOP, the surrounding area was inspected for sewer debris and other waste.
  - Each MOP manhole, if possible, was opened, checked, and marked with chalk for future investigations. The chalk was used to assist in future inspections for determining if surcharge conditions occurred within the manhole.
  - Upstream and downstream manholes were investigated if the MOP manhole could not be accessed or flow conditions in the MOP manhole could not be determined.
  - Data was documented in work orders provided by MSD.
  - MSD Customer Service was notified if an active overflow was observed.
  - Overflow Report Forms were completed for any observed overflow.

### 2.4.2.2 MOP Classification

Based on field investigation findings, MOPs were classified into one of six categories. A summary of each category is outlined in the following.

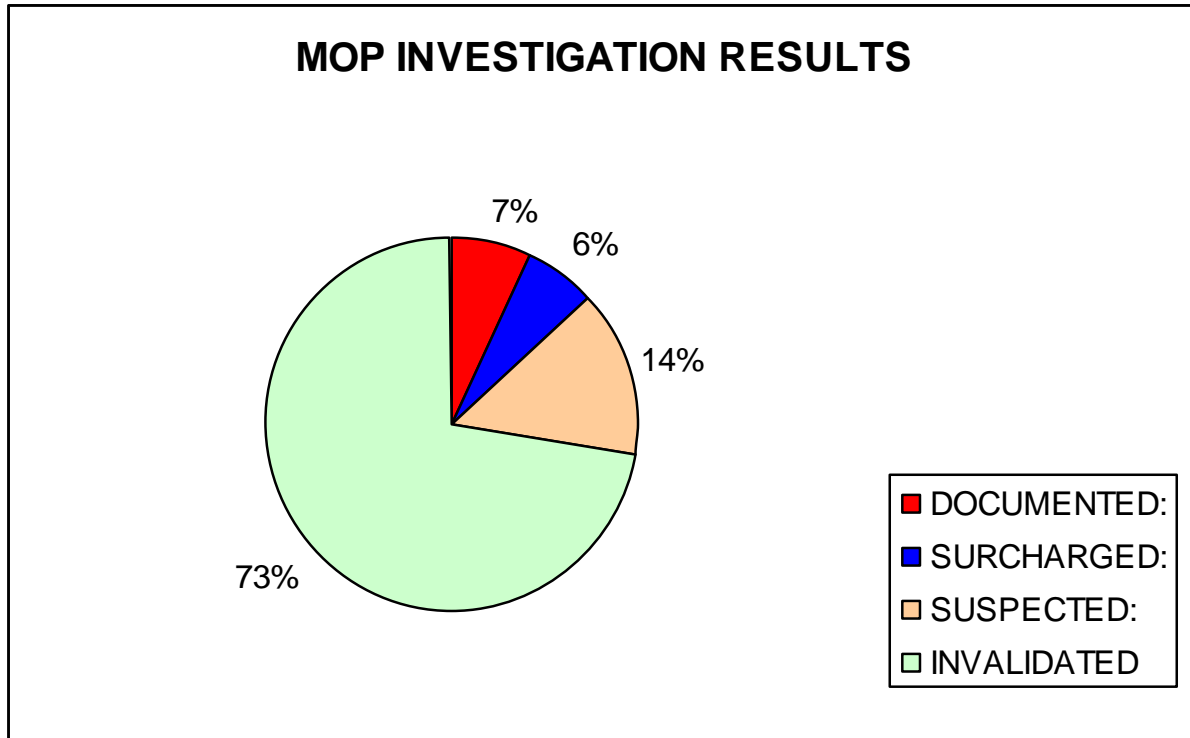
1. Documented - An overflow was witnessed. MOP locations coded as documented SSOs require solution development by the modelers and added to the documented SSO list.
2. Suspected - Evidence found indicating an overflow had occurred. MOP locations coded as suspected overflows require solution development by the modelers and are added to the suspected SSO list.
3. Surcharged - Evidence found indicating manhole surcharging but not an overflow. Solution required. MOP locations coded as surcharged should remain a MOP status and will require solution development by the modelers according to surcharge criteria specified in the System Capacity Assurance Plan, described in Volume 1.
4. Remediated – Manhole was found to have a bolt-down lid. No solution was required. These manholes are all located along major streamlines or within the 100-year floodplain. Upstream and downstream manholes were investigated and also found to have bolt-down lids.
5. Invalidated - No problems found and no solution was required. Modeling teams were provided a list of invalidated MOPs and were directed to adjust I/I factors accordingly until the MOP locations have been successfully eliminated from the hydraulic models.
6. Unconfirmed - Could not locate the MOP manhole in the field, but upstream/downstream manholes displayed no problems. No solution required. These locations had upstream and/or downstream manholes that were inspected to determine flow conditions. All respective manholes displayed good flowing conditions; therefore, the unconfirmed MOP has become invalidated.

### 2.4.2.3 Specific Findings

On March 20 and 21, 2008, two-person teams performed extensive field manhole inspections following the storm event that ended on March 19. Additionally, on April 4-5 and May 9, 2008, inspection teams revisited and field-investigated all invalidated and unconfirmed MOPs following the April 3 and 4 rain event that produced approximately four inches of rain in a 24-hour period and the May 8 rain event of similar magnitude. This was performed as follow-up reconnaissance and confirmation that invalidated MOPs were accurately categorized and unconfirmed MOPs were given a second and even third attempt to locate. In total, 211 manholes were investigated during the MOP investigation process. Detailed results from these investigations are included in Appendix 2.4.1, MOP Investigation Findings. Figure 2.4.1 summarizes the investigation results.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 2.4.1 MOP INVESTIGATION SUMMARY**



**2.4.2.4 Re-validation of Models**

After the final set of validated SSOs was developed, it was necessary to re-validate the hydraulic models to these SSOs. After this validation process was completed, the final list of targeted SSOs was compiled for project development. This list is discussed in the following section.

**2.4.3 SSOs Targeted for Solution Development**

A total of 173 SSO locations were validated within the MSD system and are considered in the Final SSDP projects (refer to Volume 3, Chapter 3). Table 2.4.2 summarizes the typical volume, receiving stream, model region, and service area of each SSO. The SSO volume information was averaged based on actual field investigation and was used to estimate life-cycle costs such as pumping, fines, and cleanup.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.4.2**

**SSOS TARGETED FOR FINAL SSDP SOLUTION DEVELOPMENT**

No.	SSO ID	SSO Name/ Address	Service Area	Receiving Stream	Model Region	Overflow Type	Avg Per Incident (gal)
1	MSD0199-LS	Lucas Lane	Berrytown	Goose Creek	Berrytown	LS	5,000
2	28984	Plumwood #1	Cedar Creek	Cedar Creek	Cedar Creek	Manhole	21,600
3	28998	Plumwood #2	Cedar Creek	Cedar Creek	Cedar Creek	Manhole	21,600
4	63094	Plumwood #4	Cedar Creek	Cedar Creek	Cedar Creek	Manhole	50
5	63095	Plumwood #5	Cedar Creek	Cedar Creek	Cedar Creek	Manhole	13
6	67997	7906 Gainsborough Court	Cedar Creek	Little Cedar Creek	Cedar Creek	Manhole	25
7	67999	7904 Shaw Court	Cedar Creek	Little Cedar Creek	Cedar Creek	Manhole	Suspected- no data
8	70158	Plumwood #3	Cedar Creek	Cedar Creek	Cedar Creek	Manhole	378,333
9	81316	Fairmount Road #1	Cedar Creek	Big Run	Cedar Creek	Manhole	500
10	86423	8314 Casualwood Way	Cedar Creek	Little Cedar Creek	Cedar Creek	Manhole	MOP - No data
11	88545	11101 Cambridge Commons Drive	Cedar Creek	Big Run	Cedar Creek	Manhole	Suspected- no data
12	89195	8104 Kimberly Way	Cedar Creek	Little Cedar Creek	Cedar Creek	Manhole	MOP - No data
13	89197	8104 Kimberly Way	Cedar Creek	Little Cedar Creek	Cedar Creek	Manhole	MOP - No data
14	97362	Fairmount Road #2	Cedar Creek	Big Run	Cedar Creek	Manhole	212,100
15	MSD1080-LS	Running Fox	Cedar Creek	Little Cedar Creek	Cedar Creek	LS	36,940
16	94187	Wet Well for St. Rene Road PS	Chenoweth Hills	Chenoweth Run	Chenoweth Hills	Manhole	4,380
17	33003	815 Tucker Station Road	Floyds Fork	Pope Lick	Floyds Fork	Manhole	Suspected- no data
18	65531	12400 Brierly Hill Place	Floyds Fork	Pope Lick	Floyds Fork	Manhole	Suspected- no data
19	MSD0165-PS	Olde Copper Court	Floyds Fork	Floyds Fork	Floyds Fork	LS	2,320
20	MSD0166-PS	Ashburton	Floyds Fork	Floyds Fork	Floyds Fork	LS	No Data
21	MSD0263	Chenoweth Hills WQTC	Floyds Fork	Chenoweth Run	Jeffersontown	Treatment Plant	2,767
22	MSD1105-PS	Eden Care	Floyds Fork	Floyds Fork	Floyds Fork	LS	200
23	90776	Floydsburg Road #1	Hite Creek	Floyds Fork	Hite Creek	Manhole	30,700
24	91087	Near Meadow Stream PS	Hite Creek	South Fork Harrods Creek	Hite Creek	Manhole	405,001
25	108956	Floydsburg Road #2	Hite Creek	Floyds Fork	Hite Creek	Manhole	75
26	108957	Floydsburg Road #3	Hite Creek	Floyds Fork	Hite Creek	Manhole	85,500
27	108958	Floydsburg Road #4	Hite Creek	Floyds Fork	Hite Creek	Manhole	13,000
28	MSD1082-PS	Meadow Stream	Hite Creek	Floyds Fork	Hite Creek	LS	51,000
29	MSD1085-PS	Kavanaugh Rd	Hite Creek	Hite Creek	Hite Creek	LS	176,000

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.4.2**

**SSOS TARGETED FOR FINAL SSDP SOLUTION DEVELOPMENT**

No.	SSO ID	SSO Name/ Address	Service Area	Receiving Stream	Model Region	Overflow Type	Avg Per Incident (gal)
30	MSD1086-PS	Floydsburg Road	Hite Creek	Floyds Fork	Hite Creek	LS	2,502
31	62769	Fox Hill Road/ Fox Hunt Court	Hunting Creek North	Harrods Creek	Hunting Creek North	Constructed	No data
32	MSD1055-LS	Gunpowder	Hunting Creek North	Harrods Creek	Hunting Creek North	Pumped	17,199
33	MSD1060-LS	Riding Ridge	Hunting Creek North	Harrods Creek	Hunting Creek North	Pumped	4,700
34	MSD0292	Hunting Creek South WQTC	Hunting Creek South	Harrods Creek	ORFM	Treatment Plant	117,436
35	MSD1063-PS	Deep Creek	Hunting Creek South	Harrods Creek	Hunting Creek South	LS	15,623
36	MSD1065-PS	Fairway View	Hunting Creek South	Harrods Creek	Hunting Creek South	LS	19,500
37	27969	4304 Rivanna Dr	Jeffersontown	Fern Creek	Jeffersontown	Manhole	Suspected- no data
38	28173	Watterson Trail	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	46,028
39	28249	Charlane Parkway/St Edwards Drive	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	14,676
40	28250	Charlane Parkway Near the Street	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	31,422
41	28336	Parking Lot Charlane Parkway	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	247,618
42	28340	Charlane Parkway at Pool	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	36,804
43	28390	10025 Grassland Road	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	MOP - No data
44	28391	Grassland #3	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	387,000
45	28392	Grassland #2	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	2,160,000
46	28395	Grassland #1	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	251,378
47	28413	3317 Dell Road	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	No Data
48	28414	3322 Dell Road	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	55,012
49	28415	3406/3404 Dell Road	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	143,920
50	28416	Marlin Drive	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	78,000
51	28417	Locust Avenue/Marlin Drive	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	15,000
52	28711	9510 Taylorsville Road	Jeffersontown	Avoca Creek	Jeffersontown	Manhole	Suspected- no data
53	28719	Intersection of Gleeson and Wendell	Jeffersontown	Avoca Creek	Jeffersontown	Manhole	MOP - No data
54	31733	10001 Grassland Road	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	Suspected- no data

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.4.2**

**SSOS TARGETED FOR FINAL SSDP SOLUTION DEVELOPMENT**

No.	SSO ID	SSO Name/ Address	Service Area	Receiving Stream	Model Region	Overflow Type	Avg Per Incident (gal)
55	64096	Chenoweth Run #1	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	51
56	64505	3200 Ruckreigel Pky	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	Suspected- no data
57	86052	4706 Chenoweth Run	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	Suspected- no data
58	92061	11804 Chippewa Ridge Lane	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	3,917
59	104289	3620 Charlane Pky	Jeffersontown	Chenoweth Run	Jeffersontown	Manhole	Suspected- no data
60	IS028-SI	Jeffersontown WQTC Siphon	Jeffersontown	Chenoweth Run	Jeffersontown	Constructed	113,000
61	MSD0151-PS	Monticello Place	Jeffersontown	Fern Creek	Jeffersontown	LS	10,000
62	MSD0196-PS	Chenoweth Run	Jeffersontown	Chenoweth Run	Jeffersontown	LS	212,117
63	MSD0255	Jeffersontown WQTC	Jeffersontown	Chenoweth Run	Jeffersontown	Treatment Plant	1,800,658
64	MSD1169-LS	Lake Forest	Lake Forest	Floyds Fork	Lake Forest	LS	MOP - No data
65	00746	Manhole Adjacent to Anchor Estates PS #1	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Pumped	10,762
66	01106	Vannah PS Wetwell Manhole	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Constructed	No Data
67	01793	9 Muirfield Place	Morris Forman	Middle Fork Beargrass Creek	Southeastern Diversion	Manhole	109,000
68	02932	Oxmoor #1	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	1,203,000
69	02933	Oxmoor #2	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	150,000
70	02935	Oxmoor #3	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	3,420
71	08537	Northern Ditch Blow-off	Morris Forman	Greasy Ditch	Middle Fork	Constructed	No data
72	08717	Fincastle #2	Morris Forman	South Fork Beargrass Creek	Combined	Manhole	100
73	13931	Camp Taylor #4	Morris Forman	South Fork Beargrass Creek	Combined	Manhole	6,000
74	13943	Camp Taylor #3	Morris Forman	South Fork Beargrass Creek	Combined	Manhole	250

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.4.2**

**SSOS TARGETED FOR FINAL SSDP SOLUTION DEVELOPMENT**

No.	SSO ID	SSO Name/ Address	Service Area	Receiving Stream	Model Region	Overflow Type	Avg Per Incident (gal)
75	16649	Wickland Road/ Sutherland Drive	Morris Forman	South Fork Beargrass Creek	Southeastern Diversion	Constructed	1,078,972
76	22436	Manhole Adjacent to West Goose Creek PS	Morris Forman	Goose Creek	ORFM	Pumped	30,275
77	23211	Peabody Lane #1	Morris Forman	South Fork Beargrass Creek	Middle Fork	Constructed	2,309,980
78	23212	Peabody Lane #2	Morris Forman	South Fork Beargrass Creek	Middle Fork	Manhole	9,720
79	24472	501 Mockingbird Valley Road	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Manhole	MOP - No data
80	25676	Alcona Lane	Morris Forman	South Fork Beargrass Creek	Southeastern Diversion	Manhole	288,969
81	26650	Briarbridge Ln at South Fork Beargrass Creek	Morris Forman	South Fork Beargrass Creek	Southeastern Diversion	Manhole	150
82	26651	Klondike Ln at South Fork Beargrass Creek	Morris Forman	South Fork Beargrass Creek	Southeastern Diversion	Manhole	2,511,000
83	26752	Brownsboro Road at Mockingbird Valley #1	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Manhole	25
84	27005	Bridge #6 - Cherokee Park	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	2,152,664
85	36763	3520 Fincastle Road	Morris Forman	Camp Taylor Ditch	Combined	Manhole	Suspected- no data
86	40870	Muddy Fork PS #1	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Manhole	41,800
87	40871	Muddy Fork PS #2	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Manhole	150,067
88	40872	Muddy Fork PS #3	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Manhole	183,400
89	41374	Brownsboro Road at Mockingbird Valley #2	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Manhole	100
90	41416	3202 Brownsboro Road	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Manhole	Suspected- no data

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.4.2**

**SSOS TARGETED FOR FINAL SSDP SOLUTION DEVELOPMENT**

No.	SSO ID	SSO Name/ Address	Service Area	Receiving Stream	Model Region	Overflow Type	Avg Per Incident (gal)
91	42680	Barbour Lane #1	Morris Forman	Little Goose Creek	ORFM	Pumped	162,000
92	43472	Near Saurel Drive PS	Morris Forman	Goose Creek	Middle Fork	Manhole	118
93	44396	Fincastle #4	Morris Forman	South Fork Beargrass Creek	Combined	Manhole	79,500
94	44397	Fincastle #3	Morris Forman	South Fork Beargrass Creek	Combined	Manhole	41,420
95	45835	Beargrass Road near Big Rock	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	456,021
96	46891	Goose Creek PS Wet Well	Morris Forman	Goose Creek	Middle Fork	Manhole	246,000
97	47250	1645 Rangeland Rd	Morris Forman	No Data	Southeastern Diversion	Capacity	MOP - No data
98	47583	Oxmoor #4	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	2,557,520
99	47593	Near LG&E Power Station	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	359,960
100	47596	7410 Steeplecrest Circle	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	Suspected- no data
101	47603	Kindercare #1	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	120
102	47604	Kindercare #2	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	17,083
103	51160	Peabody Lane #3	Morris Forman	South Fork Beargrass Creek	Middle Fork	Manhole	55,500
104	51161	Brooklawn	Morris Forman	South Fork Beargrass Creek	Middle Fork	Manhole	438,000
105	51221	Watterson Expressway at South Fork Beargrass Creek	Morris Forman	South Fork Beargrass Creek	Middle Fork	Constructed	13,500
106	51594	Trevilian Way	Morris Forman	South Fork Beargrass Creek	Southeastern Diversion	Manhole	51
107	55665	Hazelwood PS wetwell	Morris Forman	Upper Mill Creek	Combined	Manhole	28,000

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.4.2**

**SSOS TARGETED FOR FINAL SSDP SOLUTION DEVELOPMENT**

No.	SSO ID	SSO Name/ Address	Service Area	Receiving Stream	Model Region	Overflow Type	Avg Per Incident (gal )
108	62418	Goose Creek PS Near Goose Creek	Morris Forman	Goose Creek	Middle Fork	Manhole	128,000
109	65633	Barbour Lane #2	Morris Forman	Little Goose Creek	ORFM	Manhole	102,125
110	65635	Barbour Lane #3	Morris Forman	Little Goose Creek	ORFM	Manhole	25,500
111	66349	Fincastle #1	Morris Forman	South Fork Beargrass Creek	Combined	Manhole	15
112	90700	Christian Court	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	5,400
113	91629	Old Westport Road at Goose Creek PS #2	Morris Forman	Goose Creek	Middle Fork	Manhole	15,750
114	91630	Old Westport Road at Goose Creek PS #3	Morris Forman	Goose Creek	Middle Fork	Manhole	5,250
115	96020	Leland Road	Morris Forman	Cherrywood Creek	ORFM	Manhole	20
116	104223	Camp Taylor #1	Morris Forman	South Fork Beargrass Creek	Combined	Manhole	40
117	104231	Camp Taylor #2	Morris Forman	Camp Taylor Ditch	Combined	Manhole	1,217
118	105936	Old Westport Road at Goose Creek PS #1	Morris Forman	Goose Creek	Middle Fork	Manhole	10,927
119	00056-W	Anchor Estates #1 Wetwell	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Manhole	11,929
120	08935-SM	Middle Fork at Breckenridge Lane	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Constructed	3,020,300
121	21628-W	Devondale Wet Well Manhole (PS Overflow)	Morris Forman	Goose Creek	Middle Fork	Pumped	58,013
122	24152-W	3733 Canoe Lane (Wet Well for Canoe Ln PS)	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Constructed	60,750
123	IS021A-SI	Bowman Field Siphon	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	Constructed	No data
124	MSD0007-PS	Mockingbird Valley	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Constructed	10,840
125	MSD0010-PS	Winton	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Constructed	45



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.4.2**

**SSOS TARGETED FOR FINAL SSDP SOLUTION DEVELOPMENT**

No.	SSO ID	SSO Name/ Address	Service Area	Receiving Stream	Model Region	Overflow Type	Avg Per Incident (gal)
126	MSD0023-PS	Mellwood Avenue	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Constructed	287,472
127	MSD0024-PS	Canoe Lane	Morris Forman	Muddy Fork Beargrass Creek	ORFM	LS	15,769
128	MSD0042-PS	Sonne Avenue	Morris Forman	Paddy Run	Combined	Pumped	156,075
129	MSD0057-LS	Anchor Estates #2	Morris Forman	Middle Fork Beargrass Creek	Middle Fork	LS	14,519
130	MSD0095-PS	Derington Court	Morris Forman	Goose Creek	ORFM	Pumped	18,875
131	MSD0123-PS	West Goose Creek	Morris Forman	Goose Creek	ORFM	LS	36,750
132	MSD0183-PS	Glenview Hills	Morris Forman	Ohio River	ORFM	LS	73,733
133	MSD0192-PS	Barbour Lane	Morris Forman	Little Goose Creek	ORFM	LS	38,581
134	MSD0193-PS	New Market	Morris Forman	Muddy Fork Beargrass Creek	ORFM	LS	16,333
135	MSD1044-PS	Phoenix Hill	Morris Forman	Muddy Fork Beargrass Creek	ORFM	Pumped	2,252
136	28729	9100 Marian Ct (Wet Well for Marian Ct PS)	No Plant	Avoca Creek	Jeffersontown	Constructed	No data
137	21229-W	Avanti Way at Fernview Road	No plant	Little Cedar Creek	Pond Creek	Constructed	No data
138	MSD0149-PS	Raintree	No Plant	Avoca Creek	Jeffersontown	Constructed	MOP - No data
139	MSD0263A-PS	Chenoweth Hills WQTC PS	No Plant	Chenoweth Run	Jeffersontown	LS	108,767
140	04498	820 Echo Bridge Road	Derek R. Guthrie	Mill Creek	Mill Creek	Manhole	Suspected- no data
141	04542	Fern Lea PS Wet Well	Derek R. Guthrie	Heatherfield Ditch	Mill Creek	Manhole	91,500
142	17724	1096 Springview Drive	Derek R. Guthrie	Pond Creek	Pond Creek	Manhole	33
143	19360	Rockwood Dr / Monaco	Derek R. Guthrie	Northern Ditch	Pond Creek	Manhole	Suspected- no data
144	19369	5221 Layne Road	Derek R. Guthrie	Northern Ditch	Pond Creek	Manhole	Suspected- no data
145	25477	6101 Price Lane Road	Derek R. Guthrie	Fishpool Creek	Pond Creek	Manhole	Suspected- no data
146	25478	6006 Cooper Chapel Road	Derek R. Guthrie	Fishpool Creek	Pond Creek	Manhole	Suspected- no data
147	25480	6112 Cooper Chapel Rd	Derek R. Guthrie	Fishpool Creek	Pond Creek	Manhole	6,500
148	25484	Near Lantana PS	Derek R. Guthrie	Pennsylvania Run	Pond Creek	Manhole	180,875
149	27116	10306 Caven Avenue	Derek R. Guthrie	Mud Creek	Pond Creek	Manhole	Suspected- no data
150	29933	6926 Sandstone Blvd	Derek R. Guthrie	Fern Creek	Pond Creek	Manhole	Suspected- no data

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.4.2**

**SSOS TARGETED FOR FINAL SSDP SOLUTION DEVELOPMENT**

No.	SSO ID	SSO Name/ Address	Service Area	Receiving Stream	Model Region	Overflow Type	Avg Per Incident (gal)
151	29943	6906 Sandstone Blvd	Derek R. Guthrie	Fern Creek	Pond Creek	Manhole	Suspected- no data
152	29948	Sandstone Blvd	Derek R. Guthrie	Fern Creek	Pond Creek	Manhole	75
153	31083	6924 Sandstone Blvd	Derek R. Guthrie	Fern Creek	Pond Creek	Manhole	Suspected- no data
154	31084	6916 Sandstone Blvd	Derek R. Guthrie	Fern Creek	Pond Creek	Manhole	Suspected- no data
155	35309	Marjorie Drive	Derek R. Guthrie	Manslick Branch	Pond Creek	Manhole	10,825
156	36419	10601 Leven Blvd	Derek R. Guthrie	Pennsylvania Run	Pond Creek	Manhole	Suspected- no data
157	60679	Manhole Adjacent to Cinderella PS	Derek R. Guthrie	Fishpool Creek	Pond Creek	Manhole	8,100
158	70212	1095 Springview Drive	Derek R. Guthrie	Fishpool Creek	Pond Creek	Manhole	Suspected- no data
159	79076	6308 Hanses Drive	Derek R. Guthrie	Blue Spring Ditch	Pond Creek	Manhole	Suspected- no data
160	92098	7801 Edsel Lane (Upstream of Edsel Lane PS)	Derek R. Guthrie	Fern Creek	Pond Creek	Pumped	3,600
161	93719	Wet Well for Lantana PS	Derek R. Guthrie	Pennsylvania Run	Pond Creek	Manhole	5,625
162	04699-W	East Rockford PS	Derek R. Guthrie	Mill Creek	Mill Creek	Pumped	No data
163	81814-W	Pioneer Road PS	Derek R. Guthrie	Mill Creek	Mill Creek	Pumped	32,750
164	MSD0047-PS	Fern Lea	Derek R. Guthrie	Mill Creek	Mill Creek	Pumped	141,083
165	MSD0050-PS	Garrs Lane	Derek R. Guthrie	Mill Creek	Mill Creek	Pumped	72,000
166	MSD0101-PS	Lantana Drive PS #1	Derek R. Guthrie	Pennsylvania Run	Pond Creek	LS	22,300
167	MSD0130-PS	Cooper Chapel	Derek R. Guthrie	Fishpool Creek	Pond Creek	Constructed	4,442
168	MSD0133-PS	Caven Avenue	Derek R. Guthrie	Mud Creek	Pond Creek	Pumped	15,250
169	MSD0180-PS	Government Center	Derek R. Guthrie	Pennsylvania Run	Pond Creek	LS	12,381
170	MSD1010-PS	Lea Ann Way	Derek R. Guthrie	Northern Ditch	Pond Creek	Pumped	3,024,040
171	MSD1013-PS	Cinderella	Derek R. Guthrie	Fishpool Creek	Pond Creek	LS	71,356
172	MSD1019-PS	Leven	Derek R. Guthrie	Pennsylvania Run	Pond Creek	Pumped	Suspected- no data
173	MSD1048-PS	Edsel	Derek R. Guthrie	Fern Creek	Pond Creek	LS	91,500

PS- pump station, LS – lift station, CO- cleanout, SI-siphon, W-wet well, MOP – Modeled Overflow Point

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

## **2.5 FINAL SSDP WATERSHED MODEL DEVELOPMENT**

This section provides an overview of existing sewer system deficiencies and individual watershed model development, including validation, RDI/I reduction, build-out potential, and branching. System deficiencies include surcharged pipes and hydraulic bottlenecks. System deficiencies were analyzed and considered for determining causes of SSOs and SSO solution projects.

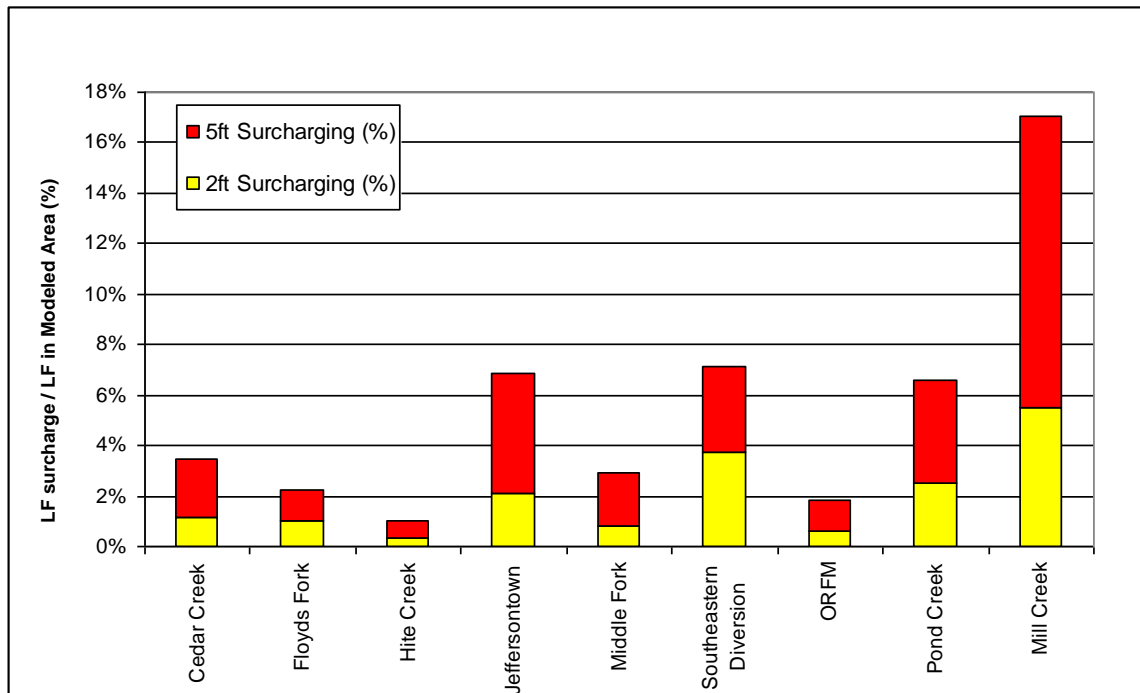
### **2.5.1 Surcharged Pipe Criteria**

For the Final SSDP, surcharged pipes were categorized and analyzed using two criteria: 1) two feet below the manhole rim; and 2) five feet below the manhole rim. This criterion was formulated based on SCAP methodology. According to the SCAP, a wet weather surcharge condition is defined as a water surface level within the sewer that is less than two feet from the manhole rim elevation. If the sewer system is in a residential area with historical capacity-related backup complaints, then a surcharge condition is considered to be a water surface level within five feet of the manhole rim. Based on this data, models were analyzed at the 1.82-inch cloudburst storm under existing system conditions to determine surcharge levels.

Figure 2.5.1 shows surcharge percentages for each modeled watershed area during the 1.82-inch cloudburst storm under existing sewer system conditions. Mapping related to these evaluations are found in Appendix 2.5.1.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 2.5.1 TOTAL SURCHARGING PERCENT BY MODELED AREA**



## 2.5.2 Hydraulic Bottlenecks

A hydraulic bottleneck is characterized by upstream system capacity that is greater than the downstream system capacity as identified by the model. The number of hydraulic bottlenecks by modeled watershed area is summarized in Table 2.5.1 and Figure 2.5.2. Most of the bottlenecks were found in the collection system, with the exception of Middle Fork where many of the bottlenecks were found in interceptor pipe (12-inch diameter and greater). Mapping related to these evaluations are found in Appendix 2.5.1, Surge/Bottleneck Maps.

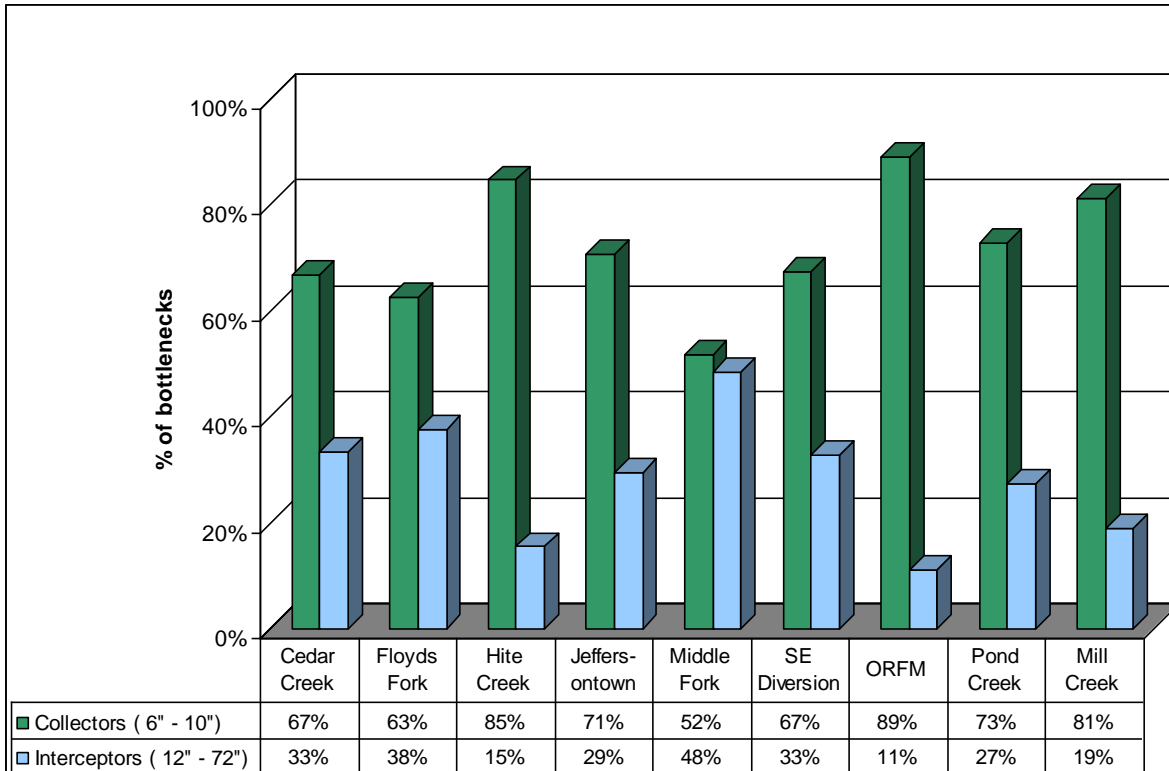
**TABLE 2.5.1**

**NUMBER OF SEPARATE SSS BOTTLENECKS BY MODELED AREA**

Modeled Bottlenecks	
Modeled Area	Number of Bottlenecks
Cedar Creek	18
Floyds Fork	8
Hite Creek	13
Jeffersontown	136
Middle Fork	64
Southeastern Diversion	58
ORFM	91
Pond Creek	92
Mill Creek	48
<b>Total</b>	<b>516</b>

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 2.5.2 SUMMARY OF SEPARATE SSS BOTTLENECKS IN MODELED AREA**



**2.5.3 Cedar Creek Model Development**

This section provides a summary of the Cedar Creek watershed model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing or proposed capital improvement projects relevant to the watershed. The full calibration/validation report is available for review in Appendix 2.3.2.

**2.5.3.1 SSO Descriptions for Cedar Creek**

Cedar Creek is divided into five branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Refer to Figure 2.5.3 for a map of the Cedar Creek branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Branch 70158 addresses five SSOs: 28984, 28998, 63094, 63095, and 70158. The SSOs are due to shallow invert levels and a hydraulic bottleneck where a 15-inch diameter sewer line combines with a 10-inch diameter sewer line, which both flow into an 8-inch diameter line. The contributing area is single-family residential.

Branch 81316 addresses two SSOs: 81316 and 97362. These SSOs are just upstream of the Fairmount Road Pump Station, MSD1022-PS. The SSOs are most likely caused by upstream flows greater than the available pump station wet weather capacity. The area surrounding the SSO is residential with open spaces.

Branch 67997 addresses five SSOs: 67997, 67999, 86423, 89195, and 89197. During wet weather, the interceptor is unable to handle peak wet weather flow rates, and lower elevation manholes that are below the hydraulic grade line are shown to overflow in the model. Peak wet weather flow is the anticipated, calculated, or monitored maximum flow within the sewer system during an actual or synthetic rainfall event. The contributing area is single-family residential.

Branch MSD1025 addresses one SSO: 88545. This SSO is just upstream of the Bardstown Road Pump Station, MSD1025-PS. It is most likely caused by upstream flows greater than the available pump station wet weather capacity. The contributing area is single-family residential.

Branch MSD1080 addresses one SSO: MSD1080-LS (Running Fox Lift Station). The SSO is located in the Fox Ridge Subdivision off Beulah Church Road. It is likely caused by upstream flows greater than the available pump station wet weather capacity. The contributing area is single-family residential.

### **2.5.3.2 Validation for Cedar Creek**

There is a modeled SSO near each known SSO at the appropriate threshold rain event (explained in Section 2.3.5.2). There were five validated SSOs in the Cedar Creek model: 28984, 28998, 70158, 81316, and 97362. 28984, 28998, and 70158 are hydraulically connected with each other and were validated by modeled SSOs at 28998, 63094, and 63095. Similarly, SSOs 81316 and 97362 are hydraulically connected and were validated by a single modeled SSO at 97365.

### **2.5.3.3 RDI/I Reduction for Cedar Creek**

The RDI/I reduction process for Cedar Creek follows the procedures described in Section 2.3.5.7. Table 2.5.2 summarizes the average peaking factor and projected RDI/I reduction for sub-catchments of Cedar Creek. Peaking factor is the peak flow (the monitored maximum flow within the sewer system during a rainfall event) at the flow monitor compared to average DWF at the flow monitor. The average peaking factor is computed from three major storms that occurred in the flow-monitoring period. The projected RDI/I reduction represents the percent of contributing area which was reduced for models used in MSD SSO evaluation modeling (see Appendix 2.3.4 for explanation of peaking factors, RDI/I reduction, and model refinements).



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.5.2**

**CEDAR CREEK PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
81316	2.3	0%
87001	2.6	1%
74696	3.1	3%
83010	3.1	3%
89176	3.2	3%
63095	3.4	4%
64023	3.8	5%
98027	8.0	23%
<b>Average Projected RDI/I Reduction</b>		<b>5.3%</b>

**2.5.3.4 Build-out for Cedar Creek**

In preparing solutions, potential future development (build-out) was considered. Build-out was only applied as additional flow upstream of known or suspected SSOs. The build-out process for Cedar Creek followed the procedures described in Section 2.3.5.10 and results are listed in Table 2.5.3. There are five general locations where additional flow was applied to the model to represent future development and corresponding flows.

**TABLE 2.5.3**

**CEDAR CREEK PROJECTED BUILD-OUT**

Build-out Areas		
Branch	Build-out Input Location (Manhole/node ID)	Future development additional DWF (gpd)
70158	28278	1,353
70158	28298	5,727
70158	28981	31,274
70158	28985	3,424
70158	28976	4,421
<b>Total Future Projected Additional Flows</b>		<b>46,129</b>

### **2.5.3.5 Capital Improvement Projects for Cedar Creek**

MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. There was one Capital Improvement Project integrated into the Cedar Creek hydraulic model.

MSD Project C94086: Fern Hill Subdivision Interceptor No. 8. The project takes flow from Holly Oaks Pump Station (MSD0161-PS) and Exhibition Court Pump Station (MSD1052-PS) to the Fern Creek / Nottingham Interceptor No. 6 near Stonybrook Drive and Hurstbourne Parkway, eliminating the SSOs at these pump stations. The Holly Oaks and Exhibition Court Pump Stations were eliminated.

### **2.5.4 Floyds Fork Model Development**

This section provides a summary of the Floyds Fork watershed model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing or proposed capital improvement projects relevant to the watershed. The full calibration/validation report is available for review in Appendix 2.3.2.

#### **2.5.4.1 SSO Descriptions for Floyds Fork**

Floyds Fork is divided into three branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Refer to Figure 2.5.4 for a map of the Floyds Fork branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Branch 1 addresses two SSOs: 33003, 65531, and several surcharged areas. These SSOs are located in Douglas Hills Subdivision on Tucker Station Road. The SSO 33003 occurs at a manhole that is part of a 15-inch interceptor that runs parallel to Tucker Station Road. The SSO 65531 occurs at a manhole that is part of the same 15-inch interceptor as 33003. The SSOs are located in a residential area along a stream, and are likely caused by inability of the interceptor to convey upstream flow.

Branch 2 addresses one SSO: MSD1105-PS (Eden Care Pump Station). The SSO is located in Martin C.B. Farm Subdivision off Blankenbaker Parkway next to the Eden Terrace Retirement Community. It is likely caused by upstream flows greater than the available pump station wet weather capacity.

Branch 3 addresses two SSOs: MSD0165-PS (Olde Copper Ct. Pump Station) and MSD0166-Pump Station (Ashburton Pump Station). These SSOs are located in Copperfield Subdivision near Beckley Station. In this branch, the Ashburton Pump Station pumps to a gravity line that drains into the Olde Copper Court Pump Station. The Olde Copper Court Pump Station is located alongside a small creek that is downhill from a residential area. The Ashburton Pump

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Station is located alongside a small creek that is downhill from a residential area. Both SSOs are most likely caused by upstream flows greater than the available pump station wet weather capacity.

#### 2.5.4.2 Validation for Floyds Fork

There is a modeled SSO near each known SSO at the appropriate threshold rain event (explained in Section 2.3.5.2) with the exception of SSO 65531. However, this SSO is hydraulically connected to SSO 33003. There were five validated SSOs in the Floyds Fork modeled area.

#### 2.5.4.3 RDI/I Reduction for Floyds Fork

The RDI/I reduction process for Floyds Fork follows the procedures described in Section 2.3.5.7. Table 2.5.4 summarizes the average peaking factor and projected RDI/I reduction for sub-catchments of Floyds Fork. Peaking factor is the peak flow (the monitored maximum flow within the sewer system during a rainfall event) at the flow monitor compared to average DWF at the flow monitor. The average peaking factor is computed from three major storms that occurred in the flow-monitoring period. The projected RDI/I reduction represents the percent of contributing area which was reduced for models used in MSD SSO evaluation modeling (see Appendix 2.3.4 for explanation of peaking factors, RDI/I reduction, and model refinements).

**TABLE 2.5.4**

**FLOYDS FORK PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
<b>96911A</b>	2.1	0%
<b>99901</b>	2.6	1%
<b>46316</b>	3.6	5%
<b>97793</b>	4.6	9%
<b>84509</b>	4.9	10%
<b>46327</b>	5.0	11%
<b>97804</b>	5.3	12%
<b>108245A</b>	6.6	17%
<b>Average Projected RDI/I Reduction</b>		<b>8.0%</b>

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

#### 2.5.4.4 Build-out for Floyds Fork

In preparing solutions, potential future development (build-out) was considered. Build-out was only applied as additional flow upstream of known or suspected SSOs. The build-out process for Floyds Fork follows the procedures described in Section 2.3.5.10 and listed in Table 2.5.5. There are two general locations where additional flow was applied to the model to represent future development and corresponding flows.

**TABLE 2.5.5**

**FLOYDS FORK PROJECTED BUILD-OUT**

Build-out Areas		
Branch	Build-out Input Location (Manhole/node ID)	Future development additional DWF (gpd)
Branch 1	33003	79,200
Branch 2	MSD1105-PS	5,500
<b>Total Future Projected Additional Flows</b>		<b>84,700</b>

#### 2.5.4.5 Capital Improvement Projects for Floyds Fork

MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design.

Middletown Recapture. This project eliminates the Berrytown, Starview, Middletown Industrial, and Chenoweth Run WQTCs by connecting to the Old Henry Road Force Main which delivers wastewater to the Floyds Fork WQTC. Additionally, a new Lake Forest Pump Station will be constructed to deliver the flow from these WQTCs to the Old Henry Road Force Main. Construction is expected to be complete by late 2011.

### 2.5.5 Hite Creek Model Development

This section provides a summary of the Hite Creek watershed model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing or proposed capital improvement projects relevant to the watershed. The full calibration/validation report is available for review in Appendix 2.3.2.

#### 2.5.5.1 SSO Descriptions for Hite Creek

Hite Creek is divided into three branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Refer to Figure 2.5.5 for a map of the Hite Creek branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Branch MSD1082 addresses two SSOs: 91087 and MSD1082-PS (Meadow Stream Pump Station). Meadow Stream Pump Station is on the south end of the city of Crestwood near I-71. The SSOs are located in a residential area along South Fork Beargrass Creek, and are likely caused by upstream flows greater than the available pump station wet weather capacity.

Branch MSD1085 addresses one SSO: MSD1085-PS (Kavanaugh Rd. Pump Station). The SSO is located on the southwest side of Crestwood, downstream of Cherry Lane Pump Station and Kavanaugh Rd. Pump Station. The site of the SSO occurrence is between two homes, and the area surrounding the SSO is residential with open spaces. This SSO is likely caused by upstream flows greater than the available pump station wet weather capacity.

Branch MSD1086 addresses five SSOs: 90776, 108596, 108957, 108958, and MSD1086-PS (Floydsburg Rd. Pump Station). These SSOs are located on the south end of Crestwood just west of Floydsburg Road. The SSOs are located at the Floydsburg Road Pump Station or just upstream of the pump station. The pump station is in an industrial area with some residential area. The SSOs are likely caused by upstream flows greater than the available pump station wet weather capacity.

#### **2.5.5.2 Validation for Hite Creek**

There is a modeled SSO near each known SSO at the appropriate threshold rain event (explained in Section 2.3.5.2). There were five validated SSOs in the Hite Creek model. SSOs MSD1086-PS, 90776, and 108956 (associated with MSD1086-PS) are hydraulically connected and were validated by a single modeled SSO at 90776.

Reported SSOs 11877 and 30520 at the Hite Creek WQTC were originally ranked in the top third of the reported SSO volumes, but were invalidated during the modeling process because the Hite Creek WQTC influent pumping station was relocated out of the 100-year floodplain which eliminated the problem. Under normal conditions, the WQTC's wet weather capacity is sufficient and there are no SSOs.

#### **2.5.5.3 RDI/I Reduction for Hite Creek**

The RDI/I reduction process for Hite Creek follows the procedures described in Section 2.3.5.7. Table 2.5.6 summarizes the average peaking factor and projected RDI/I reduction for sub-catchments of Hite Creek. Peaking factor is the peak flow (the monitored maximum flow within the sewer system during a rainfall event) at the flow monitor compared to average DWF at the flow monitor. The average peaking factor is computed from three major storms that occurred in the flow-monitoring period. The projected RDI/I reduction represents the percent of contributing area which was reduced for models used in MSD SSO evaluation modeling (see Appendix 2.3.4 for explanation of peaking factors, RDI/I reduction, and model refinements).

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.5.6**

**HITE CREEK PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
00205	0.0	0%
29526	2.2	0%
30521	2.5	0%
40943	2.6	1%
29499	2.7	1%
91122	3.1	3%
MSD1082-PS	3.1	3%
90719	7.4	20%
<b>Average Projected RDI/I Reduction</b>		<b>3.5%</b>

**2.5.5.4 Build-out for Hite Creek**

In preparing solutions, potential future development (build-out) was considered. Build-out was only applied as additional flow upstream of known or suspected SSOs. The build-out process for Hite Creek follows the procedures described earlier in Section 2.3.5.10 and listed in Table 2.5.7. There are five general locations where additional flow was added to the model to represent future development and corresponding flows.

**TABLE 2.5.7**

**HITE CREEK PROJECTED BUILD-OUT**

Build-out Areas		
Branch	Build-out Input Location (Manhole/node ID)	Future development additional DWF (gpd)
MSD1085	90781	600
MSD1085	90811	2,000
MSD1085	102897	40,000
MSD1085	90877	64,300
MSD1086	90776	25,400
<b>Total Future Projected Additional Flows</b>		<b>132,300</b>

The addition of build-out flow was considered for one other location in the Hite Creek model, areas surrounding the Meadow Stream Pump Station. Future rates amounting to 1,579,200 gpd were so large that build-out flow significantly outweighed the reported SSO amount and would have been beyond the extent of the SSO solutions development. Although portions of this flow were added at upstream locations (listed above for Kavanaugh Road and Floydsburg Road), the majority was considered outside the scope of modeling SSO solutions.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 2.5.5.5 Capital Improvement Projects for Hite Creek

MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. There were no Capital Improvement Projects integrated into the Hite Creek hydraulic model.

### 2.5.6 Jeffersontown Model Development

This section provides a summary of the Jeffersontown watershed model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing or proposed capital improvement projects relevant to the watershed. The full calibration/validation report is available for review in Appendix 2.3.2.

#### 2.5.6.1 SSO Descriptions for Jeffersontown

Jeffersontown is divided into five branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Branch 1A is a sub-section of Branch 1, created to minimize the extreme size of the branch. They were analyzed separately but combined for project solution development. Refer to Figure 2.5.6 for a map of the Jeffersontown branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Branch 1 addresses nine SSOs: 28173, 28390, 28391, 28392, 28395, 31733, 64505, MSD0025 (Jeffersontown WQTC), and ISO28-SI (Jeffersontown Siphon). The SSOs are upstream of the Jeffersontown WQTC, which is on Chenoweth Run north of Taylorsville Road. Many of the SSOs in this branch are caused by insufficient wet weather capacity in the Jeffersontown Interceptor to convey excess flow downstream. The SSO ISO28-SI is most likely caused by upstream flows greater than the available Jeffersontown WQTC wet weather capacity. The contributing area is a mix of single-family residential, industrial, and commercial.

Branch 1A addresses five SSOs: 64096, 86052, 92061, MSD0196-PS (Chenoweth Run Pump Station), and MSD0263A-PS (Chenoweth Hills WQTC Pump Station). This branch has 38,200 LF of sewer in the Chenoweth Hills WQTC service area. The SSOs 64096, 86052 and MSD0196-PS are likely caused by upstream flows greater than the available Chenoweth Run Pump Station wet weather capacity. The SSO 92061 is likely caused by upstream flows greater than the available Chippewa Pump Station wet weather capacity. The SSO MSD0236A-PS is likely caused by upstream flows greater than the available Chenoweth Hills WQTC wet weather capacity. The contributing area is single-family residential.

Branch 2 addresses ten SSOs: 28249, 28250, 28336, 28340, 28413, 28414, 28415, 28416, 28417, and 104289. The SSOs are caused by the gravity lines having insufficient wet weather capacity. The contributing area is single-family residential.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Branch 3 addresses four SSOs: 28711, 28719, 28729, and MSD0149-PS (Raintree Pump Station). The SSOs 28711 and 28719 are caused by the insufficient wet weather capacity of the interceptor. The SSOs 28729 is likely caused by upstream flows greater than the available Marian Court Pump Station wet weather capacity. MSD0149-PS is likely caused by upstream flows greater than the available Raintree Pump Station wet weather capacity. Both pump stations have constructed overflow pipes in the wet well that were constructed before MSD acquired the system in 1990. The contributing area is single-family residential.

Branch 4 addresses two SSOs: 27969 and MSD0151-PS (Monticello Place Pump Station). The SSOs are likely caused by upstream flows greater than the available Monticello Place Pump Station wet weather capacity. The contributing area is single-family residential.

### 2.5.6.2 Validation for Jeffersontown

There is a modeled SSO near each known SSO at the appropriate threshold rain event (explained in Section 2.3.5.2). There were 28 validated SSOs in the Jeffersontown model.

### 2.5.6.3 RDI/I Reduction for Jeffersontown

The RDI/I reduction process for Jeffersontown follows the procedures described in Section 2.3.5.7. Table 2.5.8 summarizes the average peaking factor and projected RDI/I reduction for sub-catchments of Jeffersontown. Peaking factor is the peak flow (the monitored maximum flow within the sewer system during a rainfall event) at the flow monitor compared to average DWF at the flow monitor. The average peaking factor is computed from three major storms that occurred in the flow-monitoring period. The projected RDI/I reduction represents the percent of contributing area which was reduced for models used in MSD SSO evaluation modeling (see Appendix 2.3.4 for explanation of peaking factors, RDI/I reduction, and model refinements).

**TABLE 2.5.8**

**JEFFERSONTOWN PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
46300	2.5	0%
93434	2.5	0%
86162	2.9	2%
42026	3.0	2%
42275	3.2	3%
28111-SM	3.4	4%
64096	3.4	4%
27668	3.6	5%
31742	3.6	5%
42273-X	3.9	6%
28564	4.1	7%
28602	4.1	7%

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.5.8**

**JEFFERSONTOWN PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
28173	4.2	7%
29386	4.4	8%
28553	4.8	10%
104337	5.0	10%
86057	5.1	11%
28351	6.9	18%
42268	29.7*	25%
<b>Average Projected RDI/I Reduction</b>		<b>7.1%</b>
*Note: High peaking factor due to minimal dry weather flow		

#### 2.5.6.4 Build-out for Jeffersontown

In preparing solutions, potential future development (build-out) was considered. This build-out evaluation assumed that the Consent Decree requirements limiting new flows to the Jeffersontown system have been removed by improvements to the system that eliminate the practice of “blending” during wet weather. This will be accomplished either by eliminating the Jeffersontown WQTC or by expanding and upgrading the WQTC to take all wet weather flows through full secondary treatment. The elimination or expansion of the Jeffersontown WQTC is required by the Consent Decree to be completed no later than December 31, 2015. For the purpose of this IOAP it is assumed that after that time adequate conveyance and treatment capacity will be provided to allow development in the current Jeffersontown WQTC service area to proceed in accordance with Louisville Metro land-use plans.

The build-out process for Jeffersontown follows the procedures described in Section 2.3.5.10 and the result is listed in Table 2.5.9. There is one general location where additional flow was added to the model to represent future development and corresponding flows. The build-out potential occurs in areas that would require pumping the flow to the Jeffersontown WQTC; therefore, a build-out inflow hydrograph was created and applied at the WQTC. No additional flow will be allowed to Jeffersontown WQTC until blending is eliminated at the plant; unless the process outlined in the Amended Consent Decree is followed.

**TABLE 2.5.9**

**JEFFERSONTOWN PROJECTED BUILD-OUT**

Build-out Areas		
Branch	Build-out Input Location (Manhole/node ID)	Future development additional DWF (gpd)
Branch 1	MSD0255	1,180,000
<b>Total Future Projected Additional Flows</b>		<b>1,180,000</b>

### 2.5.6.5 Capital Improvement Projects for Jeffersontown

MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. There was one Capital Improvement Project integrated into the Jeffersontown hydraulic model.

Rehl Road Recapture. Construct 14,250 LF of 15"-21" interceptor, 9,500 LF of 16" force main, and a regional 4.3 MGD peak flow pumping facility located near Rehl Road and Pope Lick Road. This is intended to serve 212 acres in Jefferson County proposed to be developed. Construction is complete and the interceptor, pump station, and force main are in use.

### 2.5.7 Middle Fork Model Development

This section provides a summary of the Middle Fork watershed model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing or proposed capital improvement projects relevant to the watershed. The full calibration/validation report is available for review in Appendix 2.3.2.

#### 2.5.7.1 SSO Descriptions for Middle Fork

Middle Fork is divided into four branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Refer to Figure 2.5.7 for a map of the Middle Fork branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Branch 1 addresses 19 SSOs: 02932, 02933, 02935, 08537, 23211, 23212, 27005, 45835, 47583, 47593, 47596, 47603, 47604, 51221, 51161, 51160, 90700, 08935-SM, and ISO21A-SI. Most of the SSOs are gravity SSOs to the Middle Fork of Beargrass Creek from manhole rims. They are caused by excess wet weather flows and partially by the condition of the interceptor under I-264. The SSO 08935-SM near the Upper Middle Fork Lift Station is a constructed overflow structure to Middle Fork Beargrass Creek along the Middle Fork Interceptor, and it overflows when the downstream interceptor becomes surcharged. It is located in a commercial area. The SSO ISO21A-SI is a constructed overflow structure to Middle Fork Beargrass Creek upstream of an inverted siphon and it overflows when the downstream interceptor and siphon become surcharged. The SSO 08537 is a constructed overflow structure that does not overflow during regular wet weather events. This overflow structure, better known as the Northern Ditch Blowoff, is located along the Northern Ditch Interceptor. The upstream contributing area consists of industrial, commercial, and residential area.

Branch 4 addresses seven SSOs: 21628-W, 43472, 46891, 62418, 91629, 91630, and 105936. The SSO 21628-W is a gravity manhole SSO near the Devondale Pump Station in a residential area, and it is most likely caused by upstream flows greater than the available Devondale Pump Station wet weather capacity. The SSO 43472 is a gravity manhole SSO in a residential area and is most likely caused by upstream flows greater than the available Saurel Road Pump

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Station wet weather capacity. The other SSOs in this branch are gravity SSOs from manhole rims that overflow to Goose Creek; they are likely caused by upstream flows greater than the available Goose Creek Pump Station wet weather capacity.

Branch 6 addresses four SSOs: 00056-W (Anchor Estates #1 Pump Station), 00746, 01106 (Vannah Way Pump Station), and MSD0057-LS (Anchor Estates #2 Lift Station). The SSO 01106 is a constructed overflow structure in the wet well that overflows to a storm sewer and is most likely caused by upstream flows greater than the available Vannah Way Pump Station wet weather capacity. The SSOs 00056-W and 00746 are gravity manholes located in a residential area and are most likely caused by upstream flows greater than the available Anchor Estates #1 Pump Station wet weather capacity. The SSO MSD0057-LS occurs at a gravity manhole in a residential area, and is likely caused by upstream flows greater than the available Anchor Estates # 2 Pump Station wet weather capacity.

Branch 7 addresses one SSO: 01793. This manhole is located in the Hurstbourne subdivision near Hurstbourne Country Club. The SSO at this manhole was assumed to be caused by backwater conditions in the Lower Middle Fork Interceptor due to insufficient capacity in the interceptor. In 2005, the force main at the Hurstbourne Pump Station was re-routed to relieve flow to the interceptor and the SSO did not occur again and, therefore, was believed to be eliminated. In March 2008, however, the SSO reappeared and is now assumed to be caused by insufficient wet weather capacity.

There are other SSOs in Middle Fork that are being addressed by Interim SSDP projects; these locations are described below.

SSOs 21153, 21101, 21061, 21156, and 21089 are locations that are pumped from the sanitary sewer during wet weather. These SSOs are in the Beechwood Village neighborhood and the contributing area is single family residential. The pumps are activated to eliminate residential basement backups. The cause of the overflows are downstream surcharging and significant I/I. These locations are addressed by Interim SSDP projects, namely the Beechwood Village and Sinking Fork Relief Interceptor projects.

SSOs 25012, 63319, and 21103 are gravity SSOs through manhole rims that occur during wet weather. The contributing area is mostly single family residential. The cause of the overflows are downstream surcharging and significant I/I. These locations are addressed by Interim SSDP projects, namely the Beechwood Village and Sinking Fork Relief Interceptor projects.

### **2.5.7.2 Validation for Middle Fork**

There is a modeled SSO near each known SSO at the appropriate threshold rain event (explained in Section 2.3.5.2). There were 31 validated SSOs in the Middle Fork modeled area. There was one unvalidated SSO at manhole 01793; this area was investigated by MSD Infrastructure & Flood Protection group to determine if a downstream blockage had occurred. Investigation did not identify any blockages downstream of the manhole; therefore, this SSO will be targeted for I/I reduction and an SSES will be performed upstream of the manhole.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 2.5.7.3 Sedimentation for Middle Fork

Based on validation results and a review of the interceptor condition assessment, sedimentation was needed in the model for the Middle Fork SSO validation. Sediment amounts, which are listed in Table 2.5.10, were added in the pipes downstream of the listed manhole ID in the hydraulic model. The majority of these blockages have since been removed through cleaning and rehabilitation projects completed in late 2008.

**TABLE 2.5.10**

**MIDDLE FORK SEDIMENTATION**

Sedimentation for SSO Validation	
Site (Manhole ID)	Sediment Depth (Upstream Pipe Diameter)
63324	4 inches (18 inches)
63321	6 inches (18 inches)
45443	6 inches (27 inches)
21156	6 inches (27 inches)
21150	8 inches (21 inches)
21155	8 inches (27 inches)
<b>Average Sediment Depth</b>	<b>6.3 inches</b>

### 2.5.7.4 RDI/I Reduction for Middle Fork

The RDI/I reduction process for Middle Fork follows the procedures described in Section 2.3.5.7. Table 2.5.11 summarizes the average peaking factor and projected RDI/I reduction for sub-catchments of Middle Fork. Peaking factor is the peak flow (the monitored maximum flow within the sewer system during a rainfall event) at the flow monitor compared to average DWF at the flow monitor. The average peaking factor is computed from three major storms that occurred in the flow-monitoring period. The projected RDI/I reduction represents the percent of contributing area which was reduced for models used in MSD SSO evaluation modeling (see Appendix 2.3.4 for explanation of peaking factors, RDI/I reduction, and model refinements).

**TABLE 2.5.11**

**MIDDLE FORK PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
24551	2.2	0%
45835	2.4	0%
48763	2.4	0%
02933	2.5	0%
48758	2.5	0%
45449	2.8	2%
65746	2.8	1%



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.5.11  
MIDDLE FORK PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
01793	2.9	2%
21150	3.1	3%
62425	3.1	3%
96675	3.5	4%
45381	3.6	5%
45440	3.7	5%
71004	3.7	5%
01268	3.8	6%
47098	3.8	6%
22610	4.0	6%
25012	4.4	8%
91629	5.5	13%
21155	5.6	13%
<b>Average Projected RDI/I Reduction</b>		<b>4.1%</b>

### 2.5.7.5 Build-out for Middle Fork

There was no build-out applied to the Middle Fork watershed model for future development flows because the area is fully developed.

### 2.5.7.6 Capital Improvement Projects for Middle Fork

MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. There was one Capital Improvement Project integrated into the Middle Fork hydraulic model.

MSD Project F05039: Woodlawn Road Pump Station Relocation. The project will construct 2,200 LF of gravity interceptor from the existing pump station site to the existing Muddy Fork interceptor at Foeburn Lane, as well as a diversion structure. In coordination with the widening of Westport Road the project will eliminate the existing Woodlawn Park Pump Station, which will help relieve SSO conditions at Falgate Court and in the Beechwood Village system. The project is currently under design.

### 2.5.8 Southeastern Diversion Model Development

This section provides a summary of the Southeastern Diversion watershed model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

or proposed capital improvement projects relevant to the watershed. The full calibration/validation report is available for review in Appendix 2.3.2.

### **2.5.8.1 SSO Descriptions for the Southeastern Diversion**

Southeastern Diversion was originally divided into eight branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Only four branches remain after modifications have taken place to the model and the SSO list and modeling process throughout the Final SSDP process. Refer to Figure 2.5.8 for a map of the Southeastern Diversion branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Branch 3 addresses one SSO: 47250. It is an SSO that was modeled and field verified as significantly surcharged. This manhole is on a 12-inch diameter sewer line located on a Jefferson County School property. The contributing area is mixed with single and multi-family residential. The SSO is likely caused because the entire interceptor in the local 12-inch collection system is surcharged and cannot convey peak discharges during wet weather.

Branch 4 addresses three SSOs: 25676, 26650, and 26651. The other SSOs in this branch (18134, 18298, 18302, 18318-W, 49224, 49236, 49672, and 49673) are addressed in the Interim SSDP projects. The SSOs have a mixed contributing landuse area of residential and commercial. The SSOs are likely caused due to surcharging in the Beargrass Interceptor during wet weather.

Branch 5 addresses one SSO: 16649. SSO 16649 is a constructed overflow structure in the Sutherland neighborhood, and it occurs when the local 10-inch diameter sewer becomes surcharged. The contributing area is mostly single-family residential.

Branch 6 addresses one SSO: 51594. Early field investigation of Manhole 51594 suggested that this manhole had a downstream blockage coupled with the Beargrass Interceptor surcharge effects causing the SSO. The Interceptor Condition Assessment Phase 1 project noted numerous obstructions and root masses in the Beargrass Interceptor near this location. The contributing area is mostly single-family residential.

There are other SSOs in Southeastern Diversion that are being addressed by a combination of the Interim SSDP projects, maintenance activities, and other branch solutions. These locations are described below.

SSOs 08426, 08427, 08430, 08431, 30701, 30702, 49647, and 63779 are SSOs along the Buechel Branch Trunk. These are known as the Pruitt Court SSOs. The contributing area is mostly residential with some commercial and industrial. There are two main causes of these SSOs: downstream surcharging in the Southeastern Diversion Structure and excessive blockages per the Interceptor Condition Assessment and model validation activities. These SSOs will be addressed by Interim SSDP projects and maintenance activities.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

SSOs 23211, 23212, 51160, 51161, and 51221 are SSOs at or near the confluence of the Goldsmith Lane Trunk and the Beargrass Interceptor. The Goldsmith Lane Trunk and Beargrass Interceptor exceed capacity during wet weather. SSO 23211 was originally a constructed overflow structure but has since been welded shut. In addition, the Upper Middle Fork Lift Station currently flows through this location; it peaks at 6.6 mgd for a period of nearly 48 hours during a 1.82-inch rainfall event. Due to the significant I/I at the Upper Middle Fork Lift Station, SSOs occur at these locations. These locations will be addressed by Interim SSDP projects and the solution involving the diversion of the Upper Middle Fork Lift Station to the Hikes Lane Interceptor in Middle Fork Branch 1.

SSOs 72571-X, 30680, and 30681 will also be addressed by Interim SSDP projects. SSO 72571-X is better known as the Southeastern Diversion structure which is a constructed overflow structure. SSOs 30680 and 30681 are several manholes upstream of the Southeastern Diversion structure along the Buechel Branch Trunk. These manholes overflow due to local I/I and surcharging at the Southeastern Diversion. SSO 72571-X overflows due to two influent interceptors (30-inch and 33-inch) that flow into the structure and only one interceptor exiting (30-inch) the structure. There is an additional 60-inch interceptor exiting the structure but the gate is left mostly closed due to downstream operational restrictions.

SSOs 18471, 18483, 18505, and 18595 are locations that are pumped from the sanitary sewer during wet weather. These overflows are in the Hikes Point area and the contributing area is single family residential. The pumps are activated to eliminate residential basement backups. The cause of the overflows are downstream surcharging and significant I/I. These locations are addressed by Interim SSDP projects, namely the Hikes Lane Interceptor project.

SSO 17571 is an overflow that is pumped from the sanitary sewer during wet weather. This overflow is near the Hikes Point area and the contributing area is single family residential. The pump is activated to eliminate residential basement backups. The cause of the overflow is downstream surcharging and significant I/I. This location is addressed by Interim SSDP projects.

SSOs MSD0012-PS and 18434 are located in the Hikes Point area and the contributing area is single family residential. MSD0012-PS is known as the Highgate Springs Pump Station, which overflows to Beargrass Creek during extreme wet weather. This was constructed as a wet weather relief to eliminate basement backups. SSO 18434 is located a few manholes upstream. The cause of these overflows is due to surcharging in the Beargrass Interceptor and significant I/I. These locations are addressed by Interim SSDP projects, namely the Hikes Lane Interceptor project.

SSOs 18134, 18298, 18302, 18370, 18318-W, 49224, 49236, 49672, and 49673 are overflows along the Beargrass Interceptor between the Southeastern Diversion and the Highgate Springs Pump Station. The contributing area is mostly residential with some commercial and industrial. The main cause of these SSOs is downstream surcharging at the Southeastern Diversion Structure and excessive wet weather flow in the Beargrass Interceptor. These locations are addressed by Interim SSDP projects, namely the Hikes Lane Interceptor project.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### **2.5.8.2 Validation for the Southeastern Diversion**

There is a modeled SSO near each known SSO at the appropriate threshold rain event (explained in Section 2.3.5.2). There were two validated SSOs in the Southeastern Diversion modeled area. There are three unvalidated SSOs at manholes 18134, 18370, and 51594. Manholes 18134 and 18370 are in the tributaries upstream of the Beargrass Interceptor in the Hikes Point area that will be addressed with the new Hikes Lane Interceptor (Interim SSDP project). The Interceptor Condition Assessment Phase 1 project noted numerous obstructions and root masses in the Beargrass Interceptor near Manhole 51594. This part of Beargrass Interceptor will be recommended for the next phase of the Beargrass Interceptor rehabilitation work.

### **2.5.8.3 Sedimentation for the Southeastern Diversion**

Based on validation results and a review of the interceptor condition assessment, sedimentation was needed in the model for the Southeastern Diversion SSO validation. Sediment amounts that are listed in Table 2.5.12 were added in the pipes downstream of the listed manhole ID in the hydraulic model. The majority of these blockages have since been removed through cleaning and rehabilitation projects completed in late 2008.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.5.12**  
**SOUTHEASTERN DIVERSION SEDIMENTATION**

Sedimentation for SSO Validation					
Site (Manhole ID)	Sediment Depth (Upstream Pipe Diameter)	Site (Manhole ID)	Sediment Depth (Upstream Pipe Diameter)	Site (Manhole ID)	Sediment Depth (Upstream Pipe Diameter)
72555	18 inches (36")	51147	8 inches (42")	49245-T	6 inches (33")
30703-T	15 inches (30")	51221	8 inches (42")	72552	6 inches (21")
30704	14 inches (30")	72353-T	8 inches (42")	49468	6 inches (27")
08535C-T	14 inches (72")	72354	8 inches (42")	22574	6 inches (30")
50682	13 inches (36")	72396-T	8 inches (42")	22576	6 inches (30")
51186-T	13 inches (36")	73168	8 inches (42")	49664	6 inches (30")
51147-T	13 inches (42")	51232	8 inches (36")	49778	6 inches (30")
30683-T	11 inches (30")	63832	8 inches (36")	54003	6 inches (30")
30703	11 inches (30")	30720	7 inches (30")	66205	6 inches (30")
30705	11 inches (30")	24299	7 inches (39")	28080T	5 inches (24")
50648	11 inches (30")	26640	7 inches (33")	49446	5 inches (24")
68190	11 inches (21")	18465-T	7 inches (33")	19255	5 inches (27")
51221-T	10 inches (42")	51175	7 inches (36")	49779	5 inches (27")
49767	10 inches (21")	51187-T	7 inches (36")	49781	5 inches (27")
51222	9 inches (42")	51191	7 inches (36")	49807	5 inches (27")
23249C-AG	9 inches (48")	51203	7 inches (36")	49818	5 inches (27")
51189	9 inches (36")	26645	7 inches (27")	49703	5 inches (24")
51192-T	9 inches (36")	30683SM	7 inches (30")	25345	4 inches (18")
51194	9 inches (36")	18465	6 inches (33")	112639	4 inches (21")
49473	9 inches (27")	18704	6 inches (21")	30714	4 inches (21")
24299-T	8 inches (39")	26642	6 inches (33")	30715	4 inches (21")
30685	8 inches (33")	48885	6 inches (33")	49459	4 inches (21")
49244-T	8 inches (33")	48886	6 inches (33")	49710	4 inches (18")
49810	8 inches (27")	48894	6 inches (33")	19769	3 inches (18")
<b>Average Sediment Depth</b>					<b>7.7 inches</b>

#### 2.5.8.4 RDI/I Reduction for the Southeastern Diversion

The RDI/I reduction process for Southeastern Diversion follows the procedures described in Section 2.3.5.7. Table 2.5.13 summarizes the average peaking factor and projected RDI/I reduction for sub-catchments of the Southeastern Diversion. Peaking factor is the peak flow (the monitored maximum flow within the sewer system during a rainfall event) at the flow monitor compared to average DWF at the flow monitor. The average peaking factor is computed from three major storms that occurred in the flow-monitoring period. The projected RDI/I reduction represents the percent of contributing area which was reduced for models used

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

in MSD SSO evaluation modeling (see Appendix 2.3.4 for explanation of peaking factors, RDI/I reduction, and model refinements).

There were 32 flow monitoring locations in the Southeastern Diversion modeled area. There were six flow monitoring locations that the RDI/I reduction was adjusted from what MSD provided. These were HP22, HP24, HP25A, HP31, HP32, and HP33. These were adjusted by taking an average of adjacent flow monitoring basins. This was done because the flow monitors either had volume-balancing problems or were highly influenced by an upstream pump station. There were two instances where MOPs were invalidated so the RDI/I were redistributed.

**TABLE 2.5.13**  
**SOUTHEASTERN DIVERSION PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction			
Basin	Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
Buechel Branch	25330	2.5	0%
Buechel Branch	51762	2.8	1%
Buechel Branch	25331	3.2	3%
Buechel Branch	49641	3.4	4%
Buechel Branch	25370	3.7	5%
Buechel Branch	49467	4.0	6%
Buechel Branch	68191	27.8*	25%
Hikes Point	16762	1.3	0%
Hikes Point	27293	1.4	0%
Hikes Point	49323	2.1	0%
Hikes Point	30684	2.2	0%
Hikes Point	48894	2.5	0%
Hikes Point	104816	2.5	0%
Hikes Point	18429	2.9	2%
Hikes Point	18434	2.9	2%
Hikes Point	26648	3.1	3%
Hikes Point	49546	3.4	4%
Hikes Point	49518	3.6	5%
Hikes Point	18475	4.1	7%
Hikes Point	71738	4.9	10%
Hikes Point	26642	5.3	12%
Hikes Point	104818	7.1	19%
Hikes Point	48864	7.9	23%
Hikes Point	73087	16.1*	25%
Hikes Point	23214	22.1*	25%
Hikes Point	43711	281.3*	25%
Northern Ditch	54546	4.0	6%
Northern Ditch	23278	5.0	11%
Northern Ditch	23288	5.2	11%
Northern Ditch	08531	5.7	14%
Northern Ditch	23275	5.9	14%
Northern Ditch	80515	6.6	17%
<b>Average Projected RDI/I Reduction</b>			<b>8.8%</b>

\*Note: High peaking factor due to minimal dry weather flow



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### **2.5.8.5 Build-out for the Southeastern Diversion**

There was no build-out applied to the Southeastern Diversion watershed model for future development flows because the area is fully developed.

### **2.5.8.6 Capital Improvement Projects for the Southeastern Diversion**

MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. There were three Capital Improvement Projects integrated into the Southeastern Diversion hydraulic model.

MSD Project B00234: Cavelle Avenue Sanitary Sewer. The assessment project consists of 15 residential properties in which property owners currently use on-site disposal systems. The project will construct approximately 560 LF of separate SSS.

MSD Project B98235: Newburg Road at Tartain Road Sanitary. The assessment project consists of five residential properties in which property owners currently use on-site disposal systems. The project will construct approximately 1,200 LF of gravity sewers. Alternatives to conventional sewers will be considered.

MSD Project E98307: Taylorsville Road at Six Mile Lane. The assessment project consists of 12 residential properties in which property owners have requested service in this unsewered area of Jeffersontown. The project will construct approximately 1,700 LF of separate SSS for the properties.

## **2.5.9 Ohio River Force Main Model Development**

This section provides a summary of the ORFM watershed model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing or proposed capital improvement projects relevant to the watershed. The full calibration/validation report is available for review in Appendix 2.3.2.

### **2.5.9.1 SSO Descriptions for the Ohio River Force Main**

The ORFM area is divided into four branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Refer to Figure 2.5.9 for a map of the ORFM branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Branch 1 addresses nine SSOs: 24152-W, 24472, 26752, 41374, 41416, MSD0007-PS (Mockingbird Valley Pump Station), MSD0010-PS (Winton Ave. Pump Station), MSD0023-PS (Mellwood Ave Pump Station), and MSD0024-PS (Canoe Ln Pump Station). The SSOs at MSD0007-PS, MSD0010-PS, Mellwood Avenue Pump Station (24472 and MSD0023-PS), and

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Canoe Lane Pump Station (24152-W and MSD0024-PS) are likely caused by upstream flows greater than the available pump station wet weather capacity. The SSOs at 26752, 41374, and 41416 are caused by insufficient wet weather capacity of the interceptor upstream of Mockingbird Valley Pump Station. The contributing area is mostly single-family residential.

Branch 2 addresses one SSO: 96020. The SSO is caused by a hydraulic bottleneck in the 8" gravity line. The contributing area is mostly single-family residential.

Branch 3 addresses one SSO: MSD0095-PS (Derington Ct. Pump Station). The SSO is likely caused by upstream flows greater than the wet weather capacity of the Derington Court Pump Station. The contributing area is mostly single-family residential.

Branch 4 addresses 13 SSOs in the Prospect area: 22436, 40870, 40871, 40872, 42680, 65633, 65635, MSD0123-PS (West Goose Creek Pump Station), MSD1044-PS (Phoenix Hill Pump Station), MSD0183-PS (Glenview Hills Pump Station), MSD0192-PS (Barbour Ln Pump Station), MSD0193-PS (New Market Pump Station), and MSD0292 (Hunting Creek South WQTC). The SSOs at 22436 and MSD0123-PS are caused by the head in the ORFM limiting the Goose Creek Pump Station and the insufficient wet weather capacity at the pump station to convey flow. The SSOs at 40870, 40871, and 40872 are caused by the head in the ORFM limiting the Muddy Fork Pump Station. The SSOs at 42680, 65633, 65635, and MSD0192-PS are caused by insufficient wet weather capacity at the Barbour Lane Pump Station to convey wet weather flow. The SSOs at MSD0183-PS, MSD0193-PS, and MSD1044-PS are caused by the head in the ORFM and the insufficient capacities at the pump stations to convey the wet weather flow. The SSO at MSD0292 is likely caused by upstream flows greater than the wet weather capacity at the Hunting Creek South WQTC. The contributing area at all these locations is mostly single-family residential.

### **2.5.9.2 Validation for the Ohio River Force Main**

There is a modeled SSO near each known SSO at the appropriate threshold rain event (explained in Section 2.3.5.2). There were 20 validated SSOs in the ORFM modeled area.

The SSO 22436 is currently a documented SSO but only validates to a 2.60-inch cloudburst storm; there is a possibility that excessive inflow exists in the small upstream system.

### **2.5.9.3 RDI/I Reduction for the Ohio River Force Main**

The RDI/I reduction process for ORFM follows the procedures described in Section 2.3.5.7. Table 2.5.14 summarizes the average peaking factor and projected RDI/I reduction for sub-catchments of ORFM. Peaking factor is the peak flow (the monitored maximum flow within the sewer system during a rainfall event) at the flow monitor compared to average DWF at the flow monitor. The average peaking factor is computed from three major storms that occurred in the flow-monitoring period. The projected RDI/I reduction represents the percent of contributing area which was reduced for models used in MSD SSO evaluation modeling (see Appendix 2.3.4 for explanation of peaking factors, RDI/I reduction, and model refinements).

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.5.14**

**OHIO RIVER FORCE MAIN PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
42675	2.2	0%
42742	2.2	0%
42788	2.2	0%
32191	2.5	0%
22433e	2.6	1%
66021	2.6	1%
44084	2.8	1%
48228	3.1	3%
27035	3.5	4%
43569	3.5	4%
40872	3.6	5%
22433w	4.4	8%
91799-10	4.7	10%
91799-12	4.8	10%
24077	6.3	16%
27435	6.3	16%
<b>Average Projected RDI/I Reduction</b>		<b>4.9%</b>

**2.5.9.4 Build-out for the Ohio River Force Main**

The build-out process for ORFM included Sewer Assessment Projects only. It follows the procedures described in Section 2.3.5.10 and are listed in Table 2.5.15. Additional flow was applied to the model to represent future flow based on the following assessment projects:

- D98333 - Upper River Road / Overbrook Area Sanitary Sewer Assessment Project
- D00252 – Indian Hills North - River Road Assessment Project
- D96177 – Riviera Area Sanitary Sewer Assessment Project
- D94203 – Future Upper Muddy Fork Pump Station (Boxhill Road Sanitary Sewer Assessment Project)
- D98331 – Cabin Way Sanitary Sewer Assessment Project
- D98334 – Orion / Hillsdale Sanitary Sewer Assessment Project
- D98338 – Ten Broeck Phase II Sanitary Sewer Assessment Project

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

- D98343 – Winchester Acres Sanitary Sewer Assessment Project
- D96179 – Wallbrook Subdivision Sanitary Sewer Assessment Project

**TABLE 2.5.15**

**OHIO RIVER FORCE MAIN PROJECTED BUILD-OUT**

Build-out Areas			
Branch	Assessment ID	Build-out Input Location (Manhole/node ID)	Future development additional DWF (gpd)
<b>Branch 1</b>	D98333	40388	10,800
<b>Branch 4</b>	D00252	40866	22,400
<b>Branch 4</b>	D96177	110797	34,800
<b>Branch 4</b>	D94203	Upper Muddy	32,800
<b>Branch 4</b>	D98331	44109	2,400
<b>Branch 4</b>	D98334	66019	16,800
<b>Branch 4</b>	D98338	42726	2,800
<b>Branch 4</b>	D96179	24233	6,400
<b>Branch 4</b>	D98343	42726	16,000
<b>Total Future Projected Additional Flows</b>			<b>145,200</b>

### 2.5.9.5 Capital Improvement Projects for the Ohio River Force Main

MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. There were three Capital Improvement Projects integrated into the ORFM hydraulic model. There was also a capital project completed in 2005, which eliminated the Jarvis Lane Pump Station SSO; the constructed overflow structure was sealed and the force main was upsized. Additionally, in 2003, pump replacements occurred and a permanent generator was placed at Glen Oaks Pump Station, which eliminated the SSO.

MSD Project F05039: Woodlawn Park Pump Station Relocation. The project consists of diverting flow from the Middle Fork Modeling area to the Muddy Fork Interceptor. The project will construct 2,200 LF of gravity interceptor from the existing pump station site to the existing Muddy Fork interceptor at Foeburn Lane. In coordination with the widening of Westport Road the project will eliminate the existing Woodlawn Park Pump Station, which will help relieve sewer SSO conditions at Falgate Court and in the Beechwood Village system. The project was completed on March 31, 2009.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

MSD Project F06298: Canoe Pump Station Elimination. The project consists of diverting flow from the Canoe Lane Pump Station and the Fairway Lane Pump Station to the existing Muddy Fork Interceptor. The Canoe Lane Pump Station will be eliminated. The flow currently goes to the Mellwood Pump Station, but it does not have the ability to accept all wet weather flow so this project will reduce flow to Mellwood Pump Station.

MSD directed project to upgrade Hillsdale, Barbour Lane, Glenview Hills, and New Market Pump Stations by a private party. The project includes replacing a 75 horsepower pump with a 200 horsepower pump in the Barbour Lane Pump Station; replacing the existing 8-inch force main with a 12-inch and replacing the existing pumps with two 107 horsepower pumps at Hillsdale Pump Station; replacing the existing pumps with two 65 horsepower pumps and replacing the 4-inch force main with a 6-inch force main at New Market Pump Station; installing a new wet well and two 65 horsepower pumps for Glenview Hills Pump Station. The construction plans for improvements are on file, MSD Record No. 15271.

## **2.5.10 Combined Sewer Overflow Area Model Development**

The CSO hydraulic model provides solutions for the modeling of SSOs within the combined sewer system (CSS) combined sewer overflow (CSO) area boundary. Although they are located within the CSS boundary, they are included in the Final SSDP in order to develop elimination projects for the SSOs. This section provides a summary of the CSO area model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing or proposed capital improvement projects relevant to the watershed.

### **2.5.10.1 SSO Descriptions for the CSO Model**

The CSO area is divided into three branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Refer to Figure 2.5.10 for a map of the CSO area branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Branch 42007 addresses one SSO: MSD0042-PS (Sonne Pump Station). The SSO occurs at Sonne Pump Station which is a hauling operation site during wet weather conditions. This SSO is likely caused by upstream flows greater than the available Sonne Pump Station and force main capacity during wet weather or excess wet weather flow in the system caused by excessive I/I. This pump station was recently upgraded to 225 gpm from its original design peak flow capacity of 150 gpm. The pump station upgrade appears to eliminate the 1.27-inch cloudburst event overflows, but SSOs still occur for the 1.52-inch, 1.82-inch, 2.25-inch, and 2.60-inch cloudburst events. The contributing area is single-family residential.

Branch 30917 addresses nine SSOs: 08717, 13931, 13943, 36763, 44396, 44397, 66349, 104223, and 104231. This branch (known as Camp Taylor) is near the Camp Zachary Taylor Neighborhood Association and Subdivision, west of Poplar Level and the Louisville Zoo. The available sewer system information in this area is limited; therefore, an accurate cause of the

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

SSO is unknown. It appears that the collection system is very old in some areas and the capacity is inadequate to handle excess wet weather flow.

Branch 55665 addresses one SSO: 55665 (Hazelwood Pump Station). The SSO occurs at Hazelwood Pump Station which is a hauling operation site during wet weather conditions. The SSO is most likely caused by excess wet weather flow in the system caused by excessive I/I. The contributing area is single-family residential.

#### **2.5.10.2 Validation for the CSO Model**

The Camp Taylor area was not modeled due to the lack of available data to build the hydraulic model. Record drawings were available but pertinent information was missing from the drawings. There was no flow monitoring data available to assess the system responses to various wet weather events. The alternative to modeling was to develop a regression equation using estimated SSO volume and total rainfall depth. The equation was applied to the total rainfall depth for various storm events to estimate the SSO volume.

The Sonne Pump Station (hauling operation site) is located within the CSO boundaries. The existing CSO model was expanded to include the service area for the Sonne Pump Station. Calibration of Sonne Pump Station was assumed to be part of the CSO model calibration. Validation was completed by using 1.27-inch, 1.52-inch, 1.82-inch, 2.25-inch, and 2.60-inch cloudburst storm events. Initial validation showed an SSO during the 1.27-inch cloudburst storm with original pump peak flow capacity. Based on pump upgrade information provided by MSD staff in June 2008, no SSO occurred during the 1.27-inch cloudburst storm event.

The Hazelwood Pump Station (hauling operation site) is located just outside of the CSO boundaries. The existing CSO model was expanded to include the service area for Hazelwood Pump Station. Calibration was based on estimated volume hauled and wet well level data. Validation runs reported SSO volumes at the pump station and upstream locations in the system.

#### **2.5.10.3 RDI/I Reduction for the CSO Model**

RDI/I reduction was not applied to the CSO area model.

#### **2.5.10.4 Build-out for the CSO Model**

There was no build-out applied to the CSO area model because the area is fully developed.

#### **2.5.10.5 Capital Improvement Projects for the CSO Model**

MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. One Capital



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Improvement Project was considered when designing solutions for the branches in the CSO area.

Sonne Pump Station Pump Replacement. This project was completed in 2007. The Sonne Pump Station peak flow capacity was upgraded from 150 gpm to 225 gpm.

### 2.5.11 Small WQTC Model Development

This section provides a summary of the Small WQTC watershed model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing or proposed capital improvement projects relevant to the watershed. The full calibration/validation report is available for review in Appendix 2.3.2.

#### 2.5.11.1 SSO Descriptions for Small WQTCs

The small WQTC areas are divided into eight branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Refer to Figures 2.5.11 through 2.5.13 for maps of the small WQTC branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Berrytown Branch 1 addresses one SSO: MSD0199-LS (Lucas Ln. Pump Station). The SSO is caused by limited Lucas Lane Pump Station wet weather capacity. It is located adjacent to a drainage ditch that drains to Goose Creek. The contributing area is single-family residential.

North Hunting Creek Branch 1 addresses one SSO: MSD1060-LS (Riding Ridge Lift Station). This SSO is likely caused by upstream flows greater than the available Riding Ridge Lift Station wet weather capacity. The contributing area is single-family residential.

North Hunting Creek Branch 2 addresses one SSO: MSD1055-LS (Gunpowder Lift Station). This SSO is likely caused by upstream flows greater than the available Gunpowder Lift Station wet weather capacity. The contributing area is single-family residential.

North Hunting Creek Branch 3 addresses one SSO: 62769, upstream of the Fox Harbor #2 Lift Station. This SSO is most likely caused by upstream flows greater than the available Fox Harbor #1 Lift Station (MSD1053-LS) and Fox Harbor #2 Lift Station (MSD1054-LS) wet weather capacity. The contributing area is single-family residential.

Hunting Creek South Branch 1 addresses one SSO: MSD1065-PS (Fairway View Pump Station). It is located next to the Hunting Creek golf course in a residential area. This SSO is most likely caused by upstream flows greater than the available Fairway View Pump Station wet weather capacity. The contributing areas is single-family residential.

Hunting Creek South Branch 2 addresses one SSO: MSD1063-PS (Deep Creek Pump Station). The SSO occurs at the Deep Creek Pump Station, and is located approximately 550 feet from

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Harrods Creek in a residential area. This SSO is most likely caused by upstream flows greater than the available Deep Creek Pump Station wet weather capacity. The contributing area is single-family residential.

Lake Forest Branch 1 addresses one SSO: MSD1169-LS (Lake Forest Lift Station). The SSO occurs at the Lake Forest Lift Station and is most likely caused by upstream flows greater than the available Lake Forest Lift Station wet weather capacity. The contributing area is single-family residential.

Chenoweth Hills Branch 1 addresses one SSO: 94187, which is caused by MSD1084-PS (St. Rene Road Pump Station). The SSO is likely caused by upstream flows greater than St. Rene Road Pump Station wet weather capacity. It is located in a residential area, approximately 550 feet from Chenoweth Run. The contributing area is single-family residential.

#### **2.5.11.2 Validation for Small WQTCs**

There is one validated SSO in the Berrytown WQTC modeled area (in addition to the SSO at the WQTC) located at the Lucas Lane Pump Station (MSD0199-LS). There is a modeled SSO during the 2.25-inch cloudburst storm at the Creel Lodge Pump Station (MSD1001-LS), which is upstream of the Lucas Lane Pump Station.

Excluding the SSO at the WQTC, there is one validated SSO in the Chenoweth Hills model: MSD1084-PS.

There are four validated SSOs in the North Hunting Creek model. There is a modeled SSO during the 1.52-inch cloudburst storm at manhole 66750, which is upstream of the Gunpowder Lift Station (MSD1055-LS).

Excluding the SSO at the WQTC, there are two validated SSOs in the Hunting Creek South model, and three modeled SSOs: Manhole 68563 (just upstream of Covered Cove Way Pump Station), MSD1064-PS (Westover Pump Station), both located upstream of SSO MSD1065-PS, and Manhole 66584, located upstream of SSO MSD1063-PS.

There is one validated SSO in the Lake Forest model: MSD1169-LS.

For procedures on the validation process, see Section 2.3.5.2.

#### **2.5.11.3 RDI/I Reduction for Small WQTCs**

RDI/I reduction was not applied to the Small WQTC models.

#### **2.5.11.4 Build-out for Small WQTCs**

There was no build-out applied to the Small WQTC models for future development flows.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 2.5.11.5 Capital Improvement Projects for Small WQTCs

MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. There were no Capital Improvement Projects integrated into the Small WQTC hydraulic model.

### 2.5.12 Pond Creek Model Development

This section provides a summary of the Pond Creek watershed model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing or proposed capital improvement projects relevant to the watershed. The full calibration/validation report is available for review in Appendix 2.3.2.

#### 2.5.12.1 SSO Descriptions for Pond Creek

Pond Creek is divided into nine branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Refer to Figure 2.5.14 for a map of the Pond Creek branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Branch 3 addresses four SSOs: 25477, 25478, 25480, and MSD0130-PS (Cooper Chapel Pump Station). The SSOs occur at or directly upstream of the Cooper Chapel Pump Station in a residential area and are most likely caused by upstream flows greater than the available Cooper Chapel Pump Station wet weather capacity. The contributing area is single-family residential.

Branch 4 addresses three SSOs: 35309, 60679 and MSD1013-PS (Cinderella Pump Station). The SSOs 60679 and MSD1013-PS occur at the Cinderella Pump Station in a residential area and are most likely caused by upstream flows greater than the available Cinderella Pump Station wet weather capacity. Manhole 35309 is immediately downstream of the Cinderella PS force main discharge point. Given the drawdown peak flow capacity of the pump station, there is no hydraulic reason for the line to overflow. Model-simulated sedimentation was used immediately downstream to cause the SSO. The contributing area is single-family residential.

Branch 5 addresses three SSOs: 25484, 93719, and MSD0101-PS (Lantana Drive Pump Station). The SSOs occur near the Lantana Dr. Pump Station in a residential area. They are most likely caused by upstream flows greater than the available Lantana Drive Pump Station wet weather capacity. The contributing area is single-family residential.

Branch 6 addresses one SSO: MSD0180-PS (Government Center Pump Station). The SSOs occur at the Government Center Pump Station near the parking lot of a Louisville Metro government building. They are most likely caused by upstream flows greater than the available

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Government Pump Station wet weather wet weather capacity. The contributing area is primarily single-family residential with some public landuse.

Branch 7 addresses one SSO: 21229-W, which occurs at the Avanti Pump Station in a residential area. It is most likely caused by upstream flows greater than the available Avanti Pump Station wet weather wet weather capacity. The contributing area is single-family residential.

Branch 8 addresses nine SSOs: 19360, 19369, 29933, 29943, 29948, 31083, 31084, 79076, and MSD1010-PS. The SSO MSD1010-PS occurs at the Lea Ann Way Pump Station in a residential area. MSD Operations have replaced the three existing pumps with higher peak flow capacity pumps in 2008, and a fourth pump has been installed by a contractor as a development agreement. The pump station is now rated at 22 mgd peak wet weather capacity, which eliminates the pump station wet weather capacity problems. The SSO 79076 occurs upstream of the Lea Ann Way Pump Station and is due to backwater conditions at the pump station; this SSO should be eliminated by the pump station upgrades. The other SSOs occur upstream of the Lea Ann Way Pump Station at gravity manholes in a residential area. These SSOs are caused by upstream flows greater than the available collector system wet weather capacity. The contributing area is single-family residential.

Branch 9 addresses four SSOs: 27116, 70212, 17724, and MSD0133-PS (Caven Ave. Pump Station). The SSOs 70212 and 17724 occur upstream of a hydraulic constriction at I-65 and the Outer Loop and is due to backwater conditions caused by the constriction in addition to insufficient collector system wet weather capacity. SSOs 27116 and MSD0133-PS are caused by upstream flows greater than the available Caven Avenue. Pump Station wet weather wet weather capacity. The contributing area is single-family residential.

Branch 10 addresses two SSOs: 36419 and MSD1019-PS (Leven Pump Station). The SSOs occur at the Leven Pump Station in a residential area. They are most likely caused by upstream flows greater than the available Leven Pump Station wet weather capacity. The contributing area is single-family residential.

Branch 11 addresses two SSOs: 92098 and MSD1048-PS (Edsel Pump Station). The SSOs occur at the Edsel Pump Station in a residential area. The SSOs are suspected to be caused by maintenance-related issues or excessive I/I during wet weather. They are targeted for investigation by MSD I&FP to determine if a downstream blockage has occurred.

### 2.5.12.2 Validation for Pond Creek

There is a modeled SSO near each known SSO at the appropriate threshold rain event (explained in Section 2.3.5.2). There were 32 validated SSOs in the Pond Creek modeled area. There were two unvalidated SSOs at manhole 35309 and Edsel Pump Station (MSD1048-Pump Station) and are believed to be maintenance-related issues or I/I induced.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

The SSO 35309 is immediately downstream of the Cinderella Pump Station force main. Given the drawdown peak flow capacity of the pump station, there is no hydraulic reason for the line to overflow. Model-simulated sedimentation was used immediately downstream to cause the SSO.

The Valley Village SSOs (32682 and 32688) were not validated as they are due to backwater conditions from Derek R. Guthrie WQTC and will be eliminated as part of the Interim SSDP Derek R. Guthrie WQTC improvements.

### 2.5.12.3 Sedimentation for Pond Creek

Based on validation results and a review of the interceptor condition assessment, sedimentation was needed in the model for the Pond Creek SSO validation. Sediment amounts, which are listed in Table 2.5.16, were added in the pipes downstream of the listed manhole ID in the hydraulic model.

**TABLE 2.5.16**

**POND CREEK SEDIMENTATION**

Sedimentation for SSO Validation	
Site (Manhole ID)	Sediment Depth
35308	6 inches
35309	6 inches
<b>Average Sediment Depth</b>	<b>6 inches</b>

### 2.5.12.4 RDI/I Reduction for Pond Creek

The RDI/I reduction process for Pond Creek follows the procedures described in Section 2.3.5.7. Table 2.5.17 summarizes the average peaking factor and projected RDI/I reduction for sub-catchments of Pond Creek. Peaking factor is the peak flow (the monitored maximum flow within the sewer system during a rainfall event) at the flow monitor compared to average DWF at the flow monitor. The average peaking factor is computed from three major storms that occurred in the flow-monitoring period. The projected RDI/I reduction represents the percent of contributing area which was reduced for models used in MSD SSO evaluation modeling (see Appendix 2.3.4 for explanation of peaking factors, RDI/I reduction, and model refinements).

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.5.17**

**POND CREEK PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
58046	2.4	0%
41789	2.7	1%
22349	3.5	4%
84926-42	3.7	5%
22324	3.8	6%
22340	3.8	6%
61725-21	3.8	6%
85330	4.0	7%
22304	4.4	8%
61725-36	4.4	8%
64052	4.5	8%
60325	4.8	10%
82316	5.8	14%
84926-21	7.1	19%
32685	11.6	25%
<b>Average Projected RDI/I Reduction</b>		<b>8.4%</b>

**2.5.12.5 Build-out for Pond Creek**

In preparing solutions, potential future development (build-out) was considered. Build-out was only applied as additional flow upstream of known or suspected SSOs. The build-out process for Pond Creek follows the procedures described in Section 2.3.5.10 and the result is listed in Table 2.5.18. There are four general locations where additional flow was added to the model to represent future development and corresponding flows.

**TABLE 2.5.18**

**POND CREEK PROJECTED BUILD-OUT**

Build-out Areas		
Branch	Build-out Input Location (Manhole/node ID)	Future development additional DWF (gpd)
<b>Branch 1</b>	32682	211,789
<b>Branch 4</b>	102339	3,492
<b>Branch 4</b>	35308	3,903
<b>Branch 6</b>	31300	30,904
<b>Total Future Projected Additional Flows</b>		<b>250,088</b>



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 2.5.12.6 Capital Improvement Projects for Pond Creek

MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. There were three Capital Improvement Projects integrated into the Pond Creek hydraulic model. In addition, there was a capital project completed in March 2008 that eliminated the Valley Village Pump Station SSO; a pump was repaired and placed back into service.

MSD Project C94103: Charleswood Subdivision Interceptor. The project includes 3,150 LF of sewer and a system of collector sewers along Cooper Chapel Road between Charleswood Road and Price Lane. All the improvements are planned to be constructed in conjunction with the widening of Cooper Chapel Road. The Cooper Chapel Pump Station will be eliminated and sanitary sewer service will be provided to an area currently using on-site disposal systems (58 properties). This project is scheduled to be completed in 2010.

MSD Project C06295: Zabel Way Pump Station Elimination. The project included 2,000 LF of new 10-inch sewer to eliminate the Zabel Way Pump Station. This project was completed in September 2008.

Lea Ann Way Pump Station Upgrades. MSD Operations have replaced the three existing pumps with higher peak flow capacity pumps in 2008. A fourth pump has been installed by a contractor as a development agreement. The pump station is now rated at 22 mgd peak flow capacity.

### 2.5.13 Mill Creek Model Development

This section provides a summary of the Mill Creek watershed model development including SSO descriptions, validation process, RDI/I reduction, build-out potential, and existing or proposed capital improvement projects relevant to the watershed. The full calibration/validation report is available for review in Appendix 2.3.2.

#### 2.5.13.1 SSO Descriptions for Mill Creek

Mill Creek is divided into two branches (see Section 2.3.5.6 for details on branching) based on SSO locations and system deficiencies. Refer to Figure 2.5.15 for a map of the Mill Creek branching and SSO locations at the end of this chapter. Brief descriptions of the SSOs in each branch are below.

Branch 1 addresses five SSOs: 04498, 04542, 81814-W (Pioneer Rd. Pump Station), MSD0047-PS (Fern Lea Pump Station), and MSD0050-PS (Garrs Lane Pump Station). The SSO 81814-W occurs at the Pioneer Road Pump Station in a residential area; the SSO is most likely caused by upstream flows greater than the available Pioneer Road Pump Station wet weather capacity. The SSOs at 04542 and MSD0047-PS occur at the Fern Lea Pump Station

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

in a residential area; the SSOs are most likely caused by upstream flows greater than the available Fern Lea Pump Station wet weather capacity. The SSO MSD0050-PS occurs at the Gars Lane Pump Station in a residential area; the SSO is most likely caused by upstream flows greater than the available Gars Lane Pump Station wet weather capacity. SSO 04498 occurs along the 10" sewer line between Pioneer Road. Pump Station and Fern Lea Pump Station and most likely occurs due to backwater conditions from the Fern Lea Pump Station.

Branch 2 addresses one SSO: 04699-W. The SSO occurs at the East Rockford Pump Station in a residential area. This pump station is built in an area prone to surface flooding, which most likely inundates the pump station and causes the SSO.

### 2.5.13.2 Validation for Mill Creek

There is a modeled SSO near each known SSO at the appropriate threshold rain event (explained in Section 2.3.5.2). There are four validated SSOs in the Mill Creek modeled area.

The Derek R. Guthrie SSOs (22385, 22370, 59169, and MSD0277) were not validated as they are due to backwater conditions from Derek R. Guthrie WQTC and will be eliminated as part of the Interim SSDP Derek R. Guthrie WQTC improvements.

### 2.5.13.3 RDI/I Reduction for Mill Creek

The RDI/I reduction process for Mill Creek follows the procedures described in Section 2.3.5.7. Table 2.5.19 summarizes the average peaking factor and projected RDI/I reduction for sub-catchments of Mill Creek. Peaking factor is the peak flow (the monitored maximum flow within the sewer system during a rainfall event) at the flow monitor compared to average DWF at the flow monitor. The average peaking factor is computed from three major storms that occurred in the flow-monitoring period. The projected RDI/I reduction represents the percent of contributing area which was reduced for models used in MSD SSO evaluation modeling (see Appendix 2.3.4 for explanation of peaking factors, RDI/I reduction, and model refinements).

**TABLE 2.5.19**  
**MILL CREEK PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
<b>100763</b>	2.7	1%
<b>33000</b>	3.1	3%
<b>26716-NE</b>	3.3	4%
<b>22382</b>	3.4	4%
<b>08689</b>	3.5	4%
<b>26716-NW</b>	3.6	5%
<b>81919</b>	3.8	6%

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 2.5.19**

**MILL CREEK PROJECTED RDI/I REDUCTION**

Rainfall Dependent Inflow and Infiltration Reduction		
Flow Monitoring Location (Manhole ID)	Average Peaking Factor	Projected RDI/I Reduction
96658	4.1	7%
59250	4.3	8%
56968	5.9	14%
<b>Average Projected RDI/I Reduction</b>		<b>5.6%</b>

#### 2.5.13.4 Build-out for Mill Creek

In preparing solutions, potential future development (build-out) was considered. Build-out was only applied as additional flow upstream of known or suspected SSOs. The build-out process for Mill Creek follows the procedures described in Section 2.3.5.10 and listed in Table 2.5.20. There are five general locations where additional flow was applied to the model to represent future development and corresponding flows.

**TABLE 2.5.20**

**MILL CREEK PROJECTED BUILD-OUT**

Build-out Areas		
Branch	Build-out Input Location (Manhole/node ID)	Future development additional DWF (gpd)
NB01	22370	23,500
NB01	22385	3,600
NB01	59169	17,100
NB01	MSD0047	9,600
<b>Total Future Projected Additional Flows</b>		<b>53,800</b>

#### 2.5.13.5 Capital Improvement Projects for Mill Creek

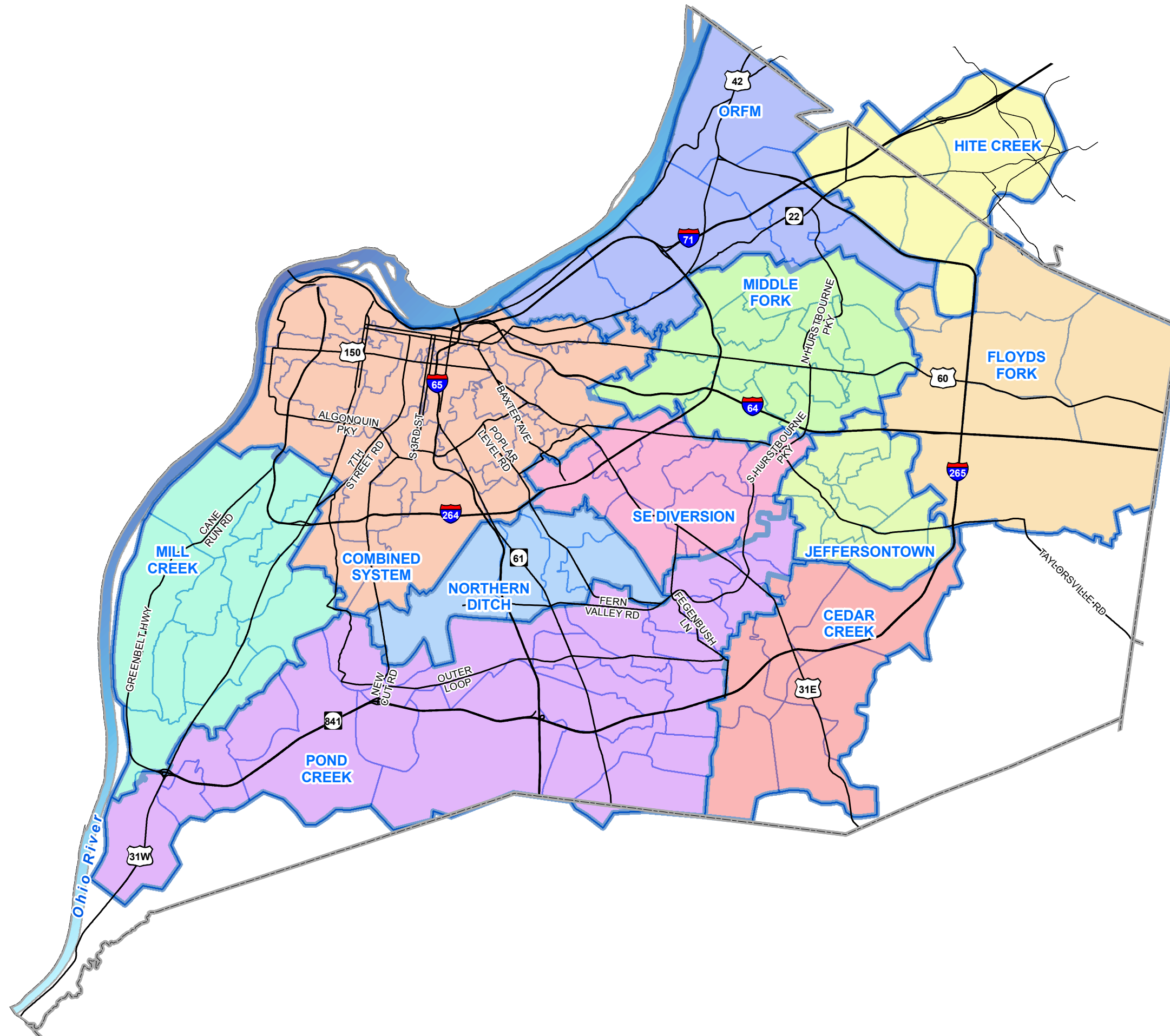
All MSD projects within the current five-year capital plan were considered in branch solutions. In considering these projects, modelers were given the latitude to modify design parameters (such as pipe diameter or pump capacity) to the extent of the preliminary project design. There was one Capital Improvement Project integrated into the Mill Creek hydraulic model.

MSD Project Budget ID B06208 Shively Interceptor. This project will eliminate five pump stations (Jacks Lane, Pioneer Road, Fern Lea, Garrs Lane, and City Park Pump Stations) to provide gravity service and eliminate SSOs due to Mechanical and/or Power failures.

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**Final SSDP Model Areas**

**Figure 2.3.1**



**Legend**

— Jefferson County Boundary

— Major Roads

**System Capacity Credit Basins**

- Cedar Creek
- Combined System
- Floyds Fork
- Hite Creek
- Jeffersontown
- Middle Fork
- Mill Creek
- Northern Ditch
- ORFM
- Pond Creek
- SE Diversion
- SCAP Sub Areas
- Ohio River

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Some boundaries are uniquely symbolized within the map.

Map Revision  
May 7, 2009

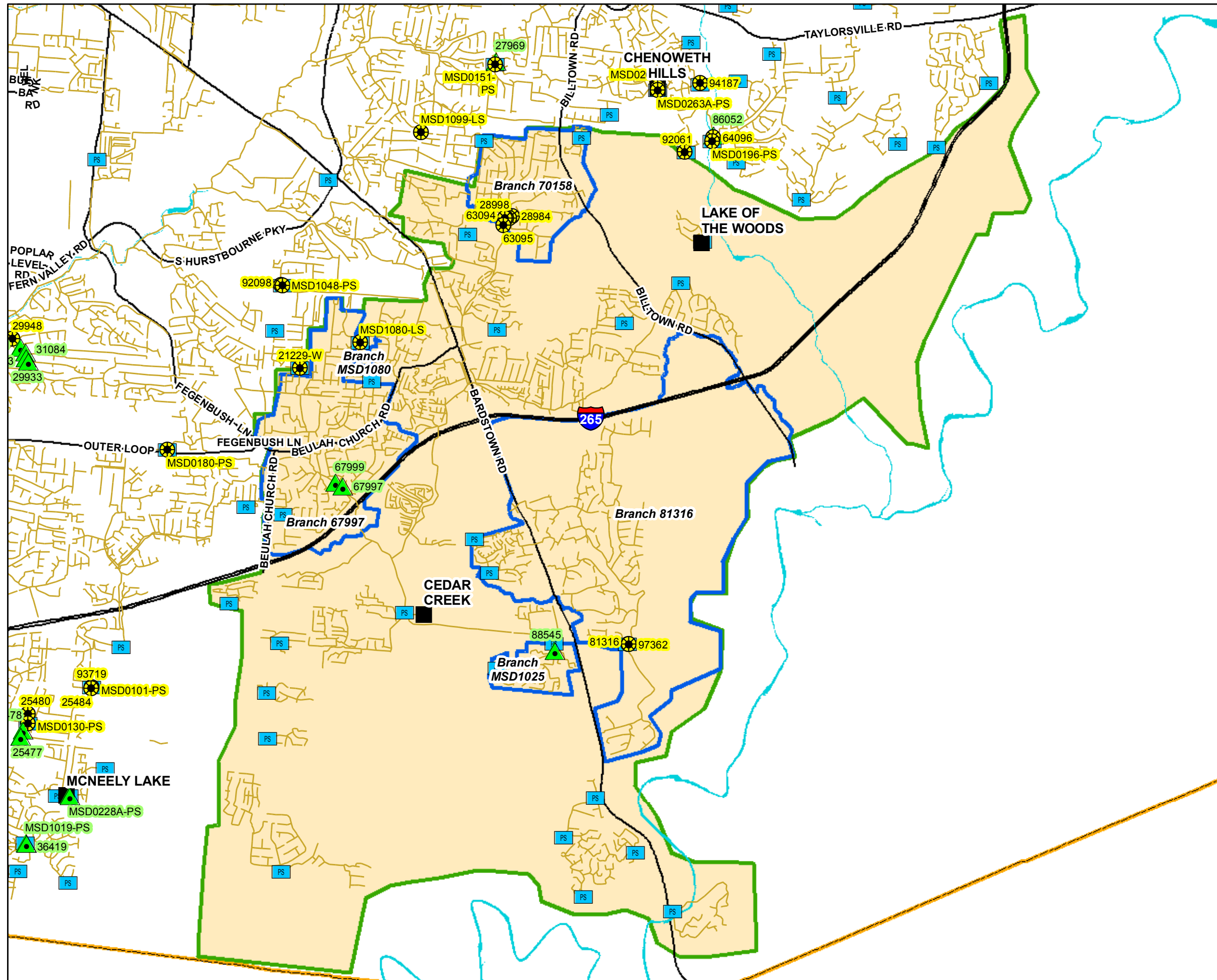


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**Cedar Creek Model Area  
and Branch Network  
Figure 2.3.2**



**Legend**

- Documented SSO
- Suspected SSO
- Pump Station
- WWTTP
- Sewer Lines
- Major Road
- Major Stream
- Credits Catchment Boundary
- CSO Area
- Branch Boundary
- County Boundary

1 inch = 4,000 feet  
Scalable when printed on 11" X 17" paper

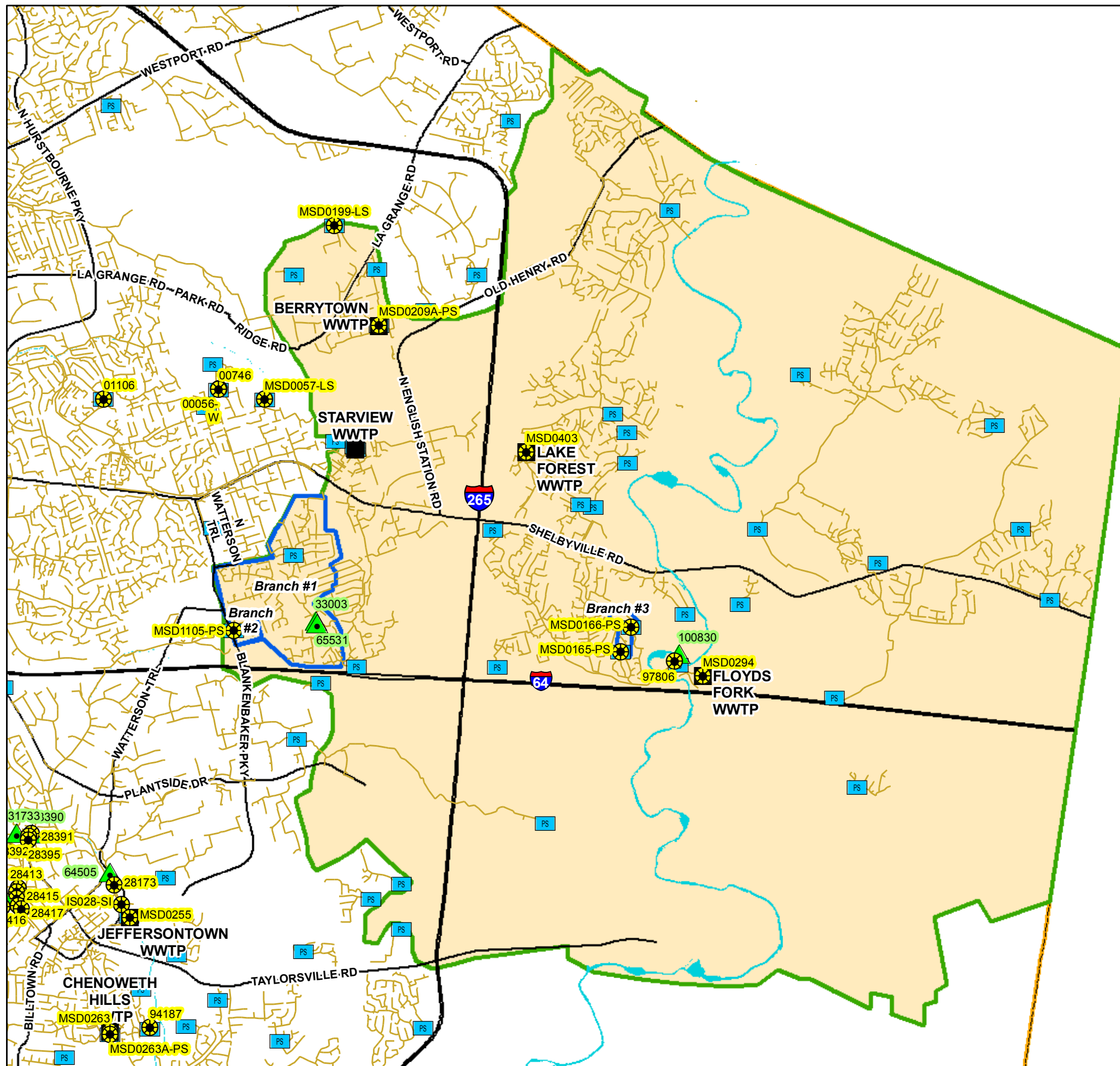
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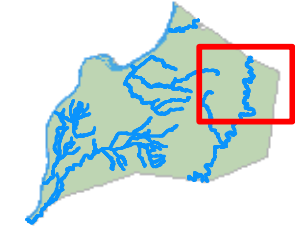
**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

**Floyd Fork Model Area  
and Branch Network  
Figure 2.3.3**



- Legend**
- Documented SSO
  - Suspected SSO
  - Pump Station
  - WWTP
  - Sewer Lines
  - Major Road
  - Major Stream
  - Credits Catchment Boundary
  - CSO Area
  - Branch Boundary
  - County Boundary

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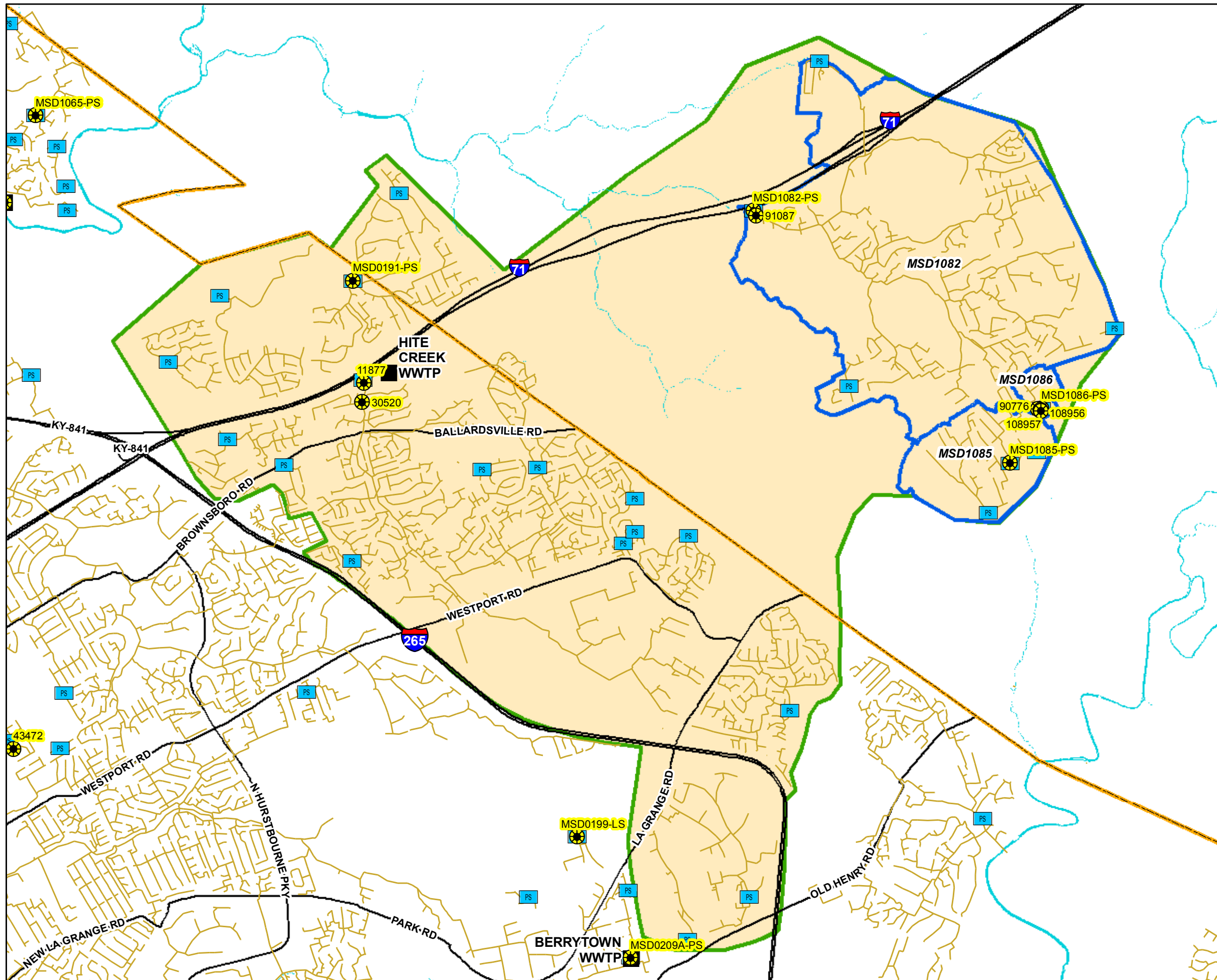


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**Hite Creek Model Area  
and Branch Network  
Figure 2.3.4**



**Legend**

- Documented SSO
- Suspected SSO
- Pump Station
- WWTP
- Sewer Lines
- Major Road
- Major Stream
- Credits Catchment Boundary
- CSO Area
- Branch Boundary
- County Boundary

1 inch = 3,500 feet  
Scalable when printed on 11" X 17" paper



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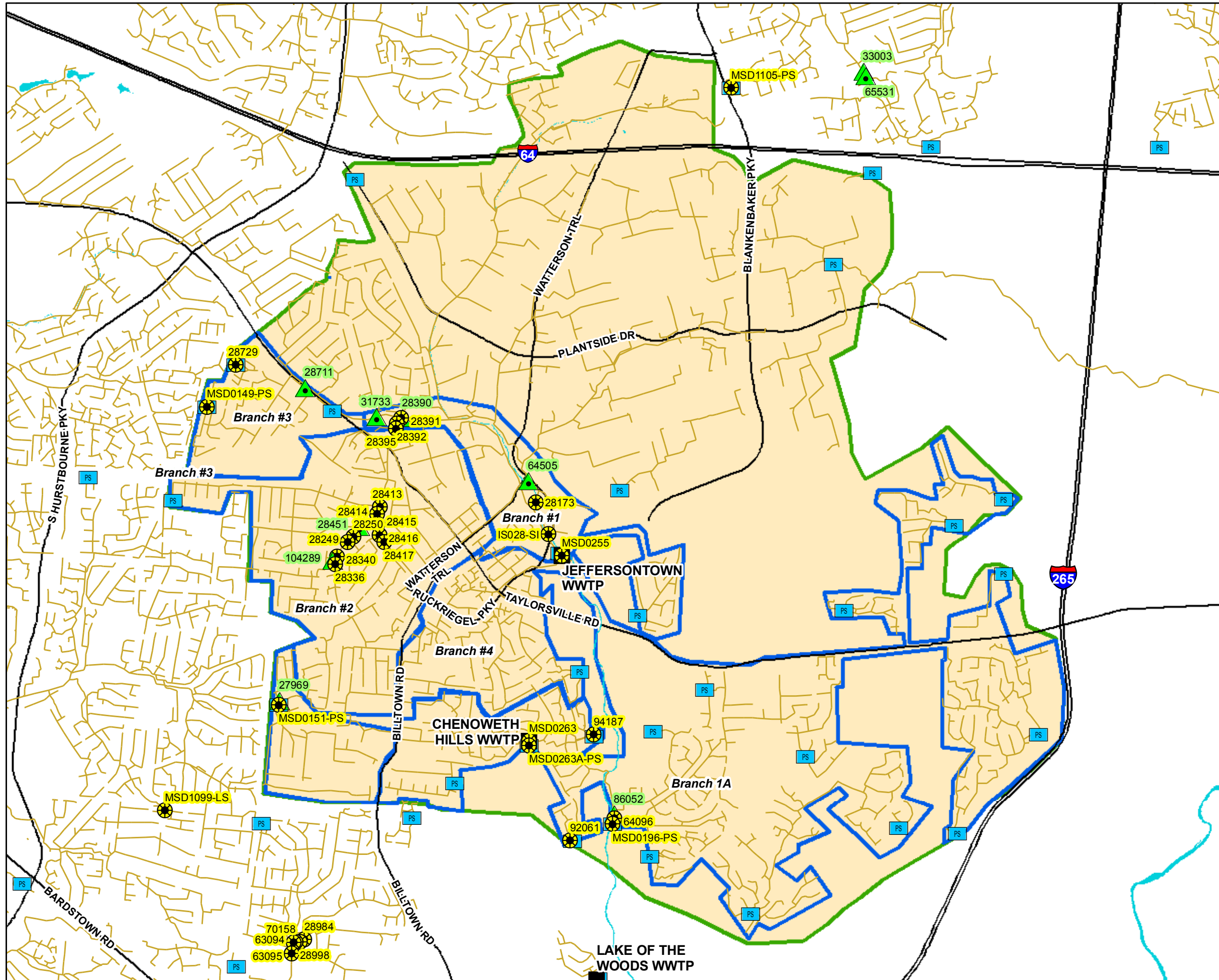
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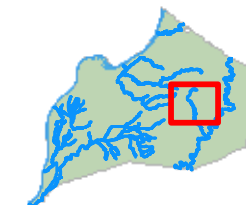
**Jeffersontown Model Area  
and Branch Network  
Figure 2.3.5**



**Legend**

- Documented SSO
- Suspected SSO
- WWTP
- Pump Station
- Sewer Lines
- Major Road
- Major Stream
- Credits Catchment Boundary
- CSO Area
- Branch Boundary
- County Boundary

1 inch = 2,600 feet  
Scalable when printed on 11" X 17" paper



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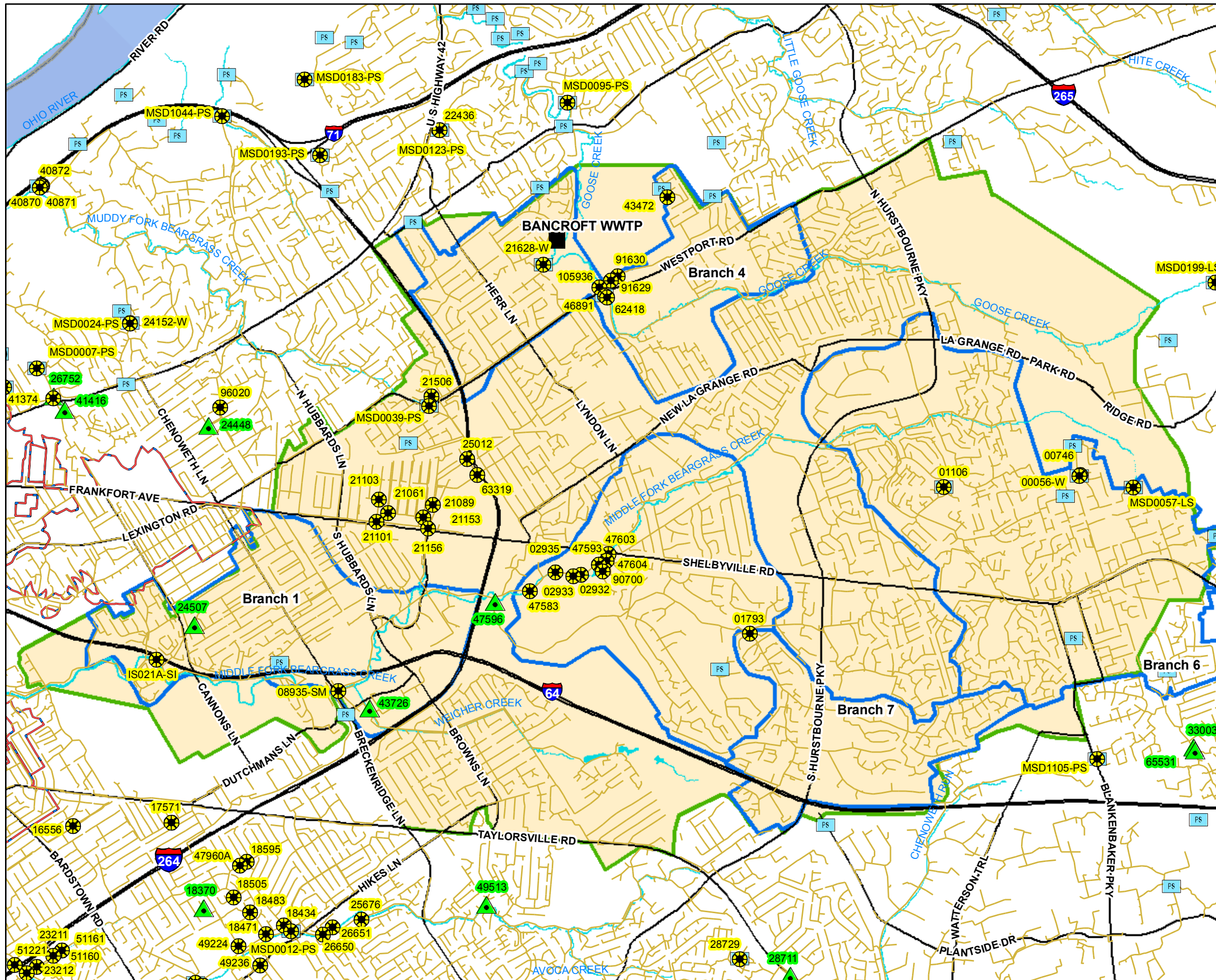


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**Middle Fork Model Area  
and Branch Network  
Figure 2.3.6**



**Legend**

- Documented SSO
- Suspected SSO
- Pump Station
- Sewer Lines
- Major Road
- Major Stream
- Credits Catchment Boundary
- CSO Area
- Branch Boundary
- County Boundary

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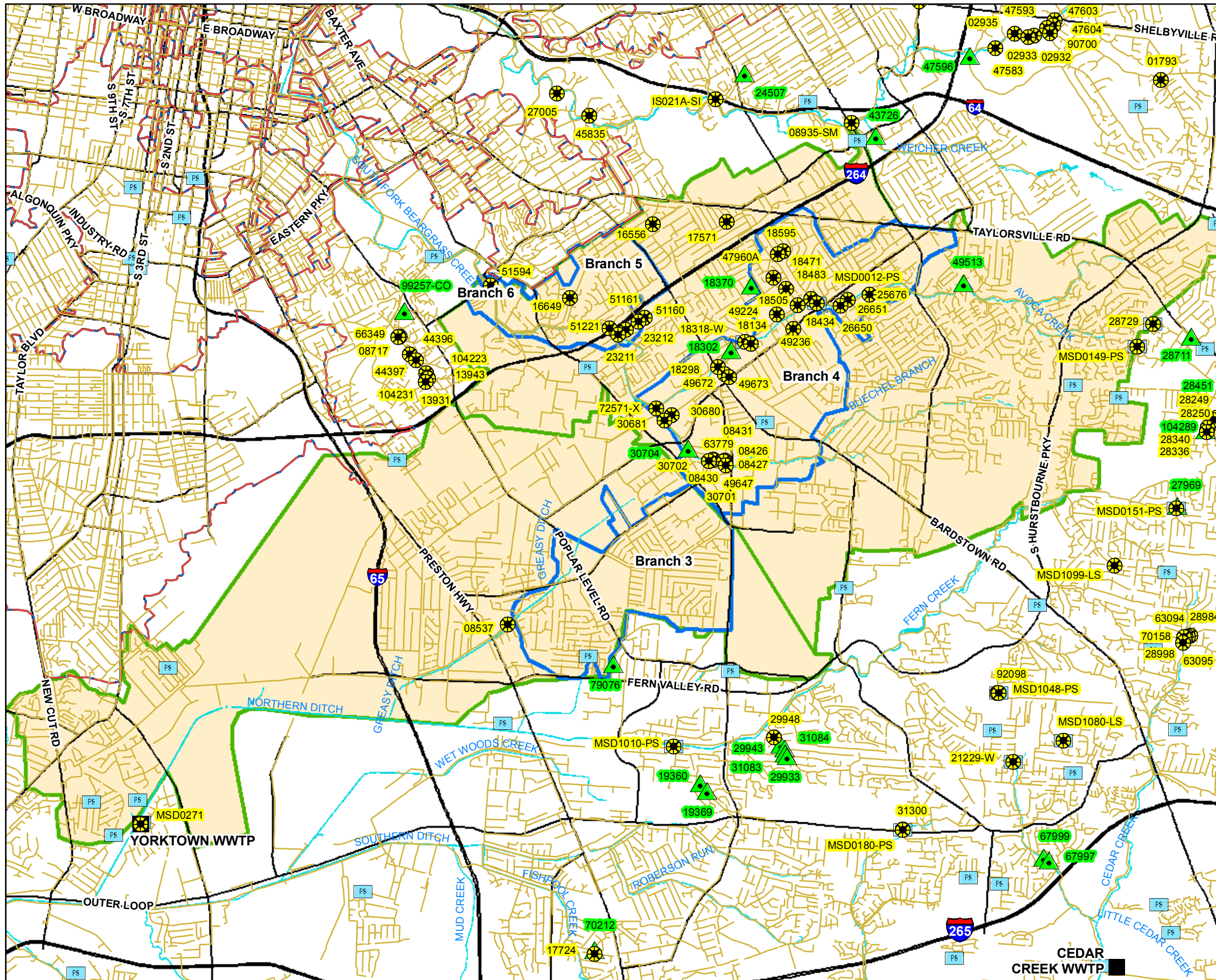


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**Southeastern Diversion  
Model Area and Branch Network  
Figure 2.3.7**



**Legend**

- Documented SSO
- Suspected SSO
- Pump Station
- Sewer Lines
- Major Road
- Major Stream
- Credits Catchment Boundary
- CSO Area
- Branch Boundary
- County Boundary

1 inch equals 4,800 feet  
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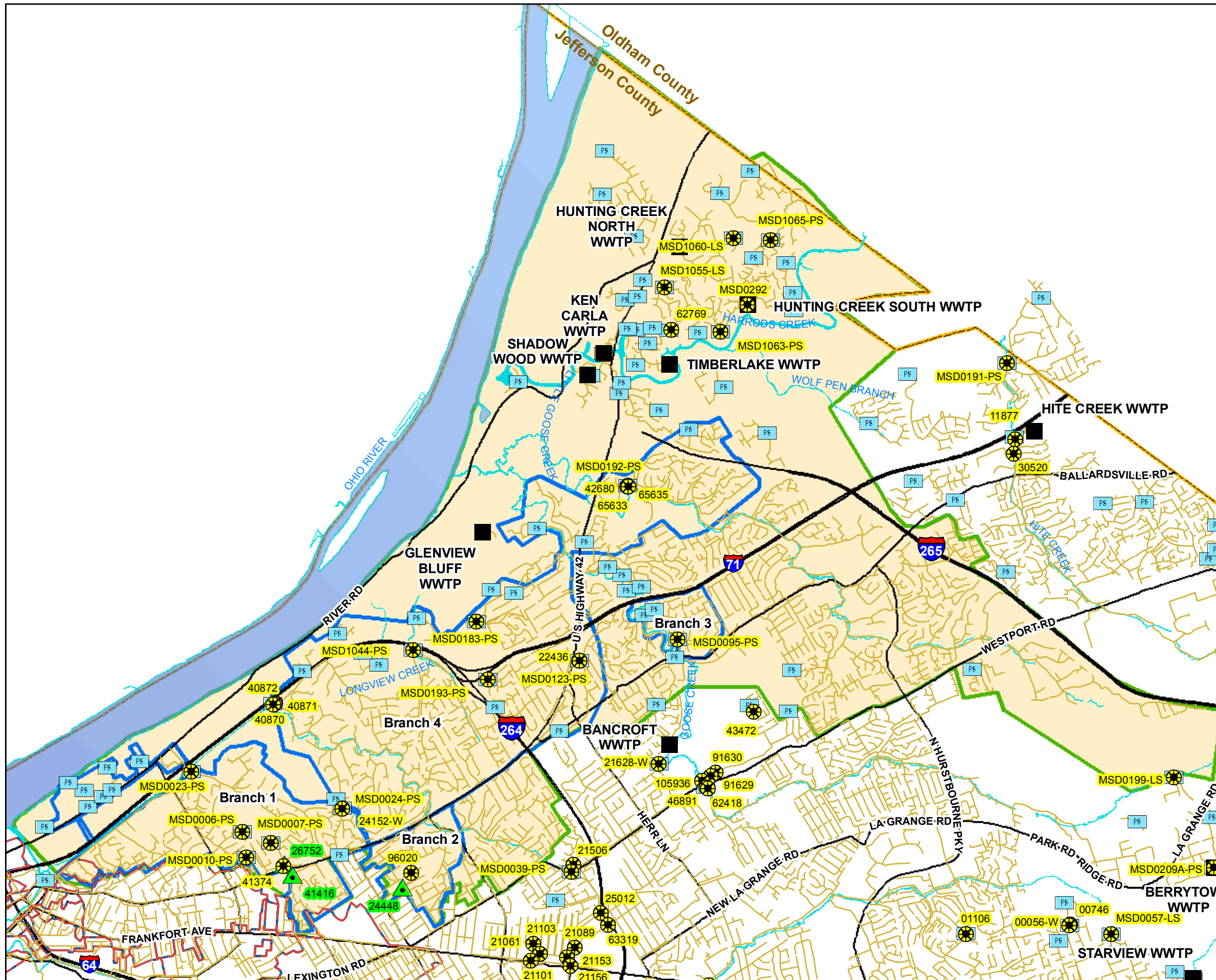


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**ORFM Model Area  
and Branch Network  
Figure 2.3.8**



**Legend**

- Documented SSD
- Suspected SSD
- Pump Station
- Sewer Lines
- Major Road
- Major Stream
- Credits Catchment Boundary
- CSO Area
- Branch Boundary
- County Boundary

1 inch equals 4,700 feet  
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**CSS Model Area  
and Branch Network  
Figure 2.3.9**



**Legend**

- Documented SSO
- Suspected SSO
- Pump Station
- Sewer Lines
- Major Road
- Major Stream
- Credits Catchment Boundary
- CSO Area
- Branch Boundary
- County Boundary

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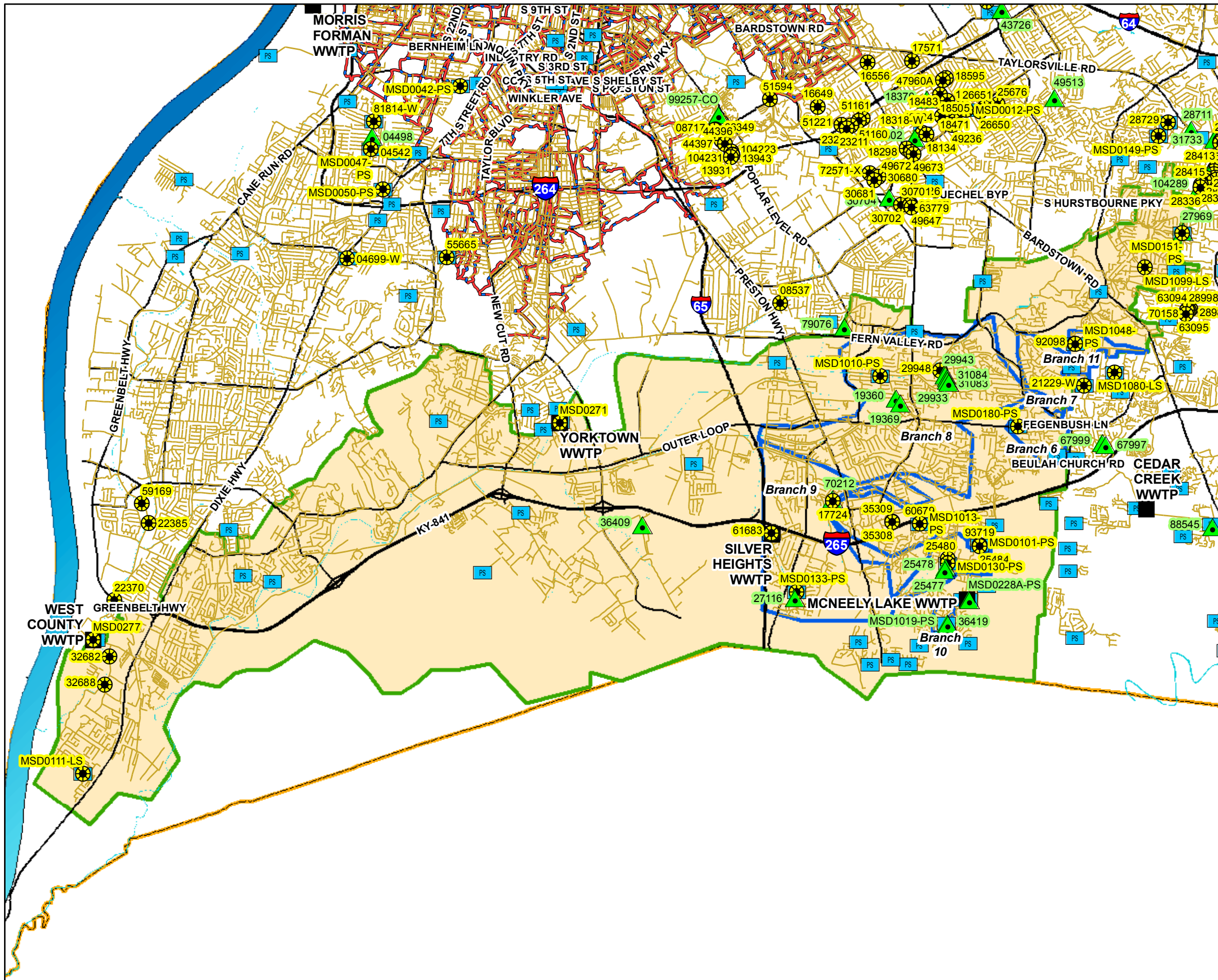


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**Pond Creek Model Area  
and Branch Network  
Figure 2.3.10**



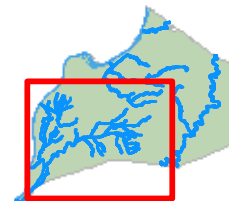
**Legend**

- Documented SSO
- Suspected SSO
- Pump Station
- WWTP
- Sewer Lines
- Major Road
- Major Stream
- Credits Catchment Boundary
- CSO Area
- Branch Boundary
- County Boundary

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**Mill Creek Model Area  
and Branch Network  
Figure 2.3.11**

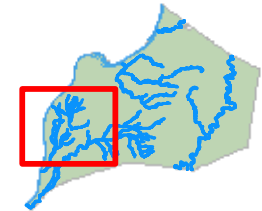


- Legend**
- Documented SSO
  - Suspected SSO
  - Pump Station
  - WWTP
  - Sewer Lines
  - Major Road
  - Major Stream
  - Credits Catchment Boundary
  - CSO Area
  - Branch Boundary
  - County Boundary

1 inch = 5,000 feet  
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nbolized within the map.

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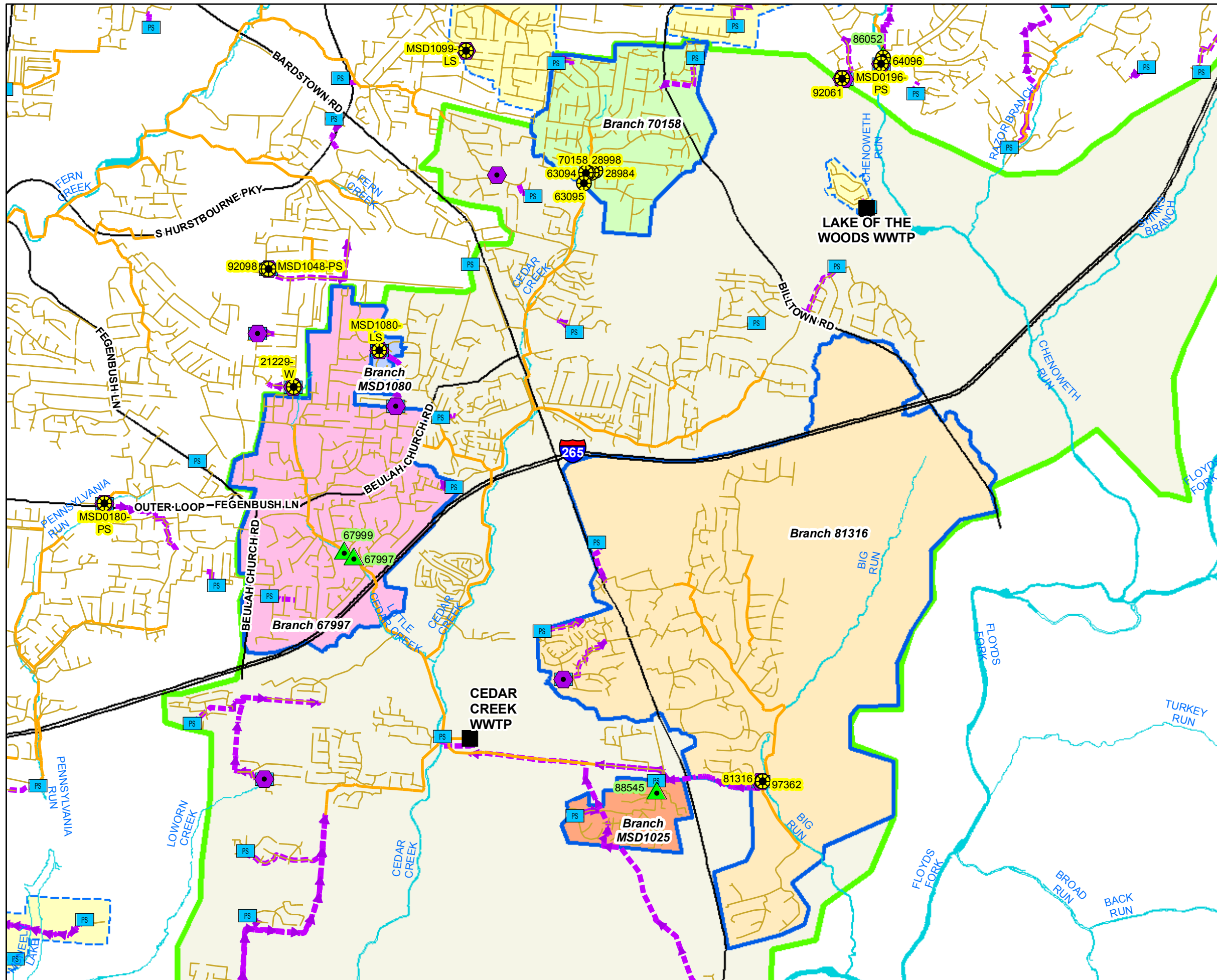


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**Integrated Overflow Abatement Plan  
Vol. 3 Sanitary Sewer Discharge Plan**

**Cedar Creek Sewershed  
Branch Network  
Figure 2.5.3**



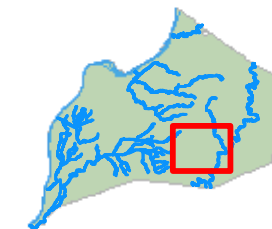
**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- WWTP
- Pump Station
- Force Main
- Collector < 12"
- Interceptor =>12"
- Major Road
- Streams
- CSO Area
- Small WWTP Service Area
- Large WWTP Service Area
- Branch 67997
- Branch 70158
- Branch 81316
- Branch MSD1080
- Branch MSD1025
- County Boundary

1 inch = 2,800 feet  
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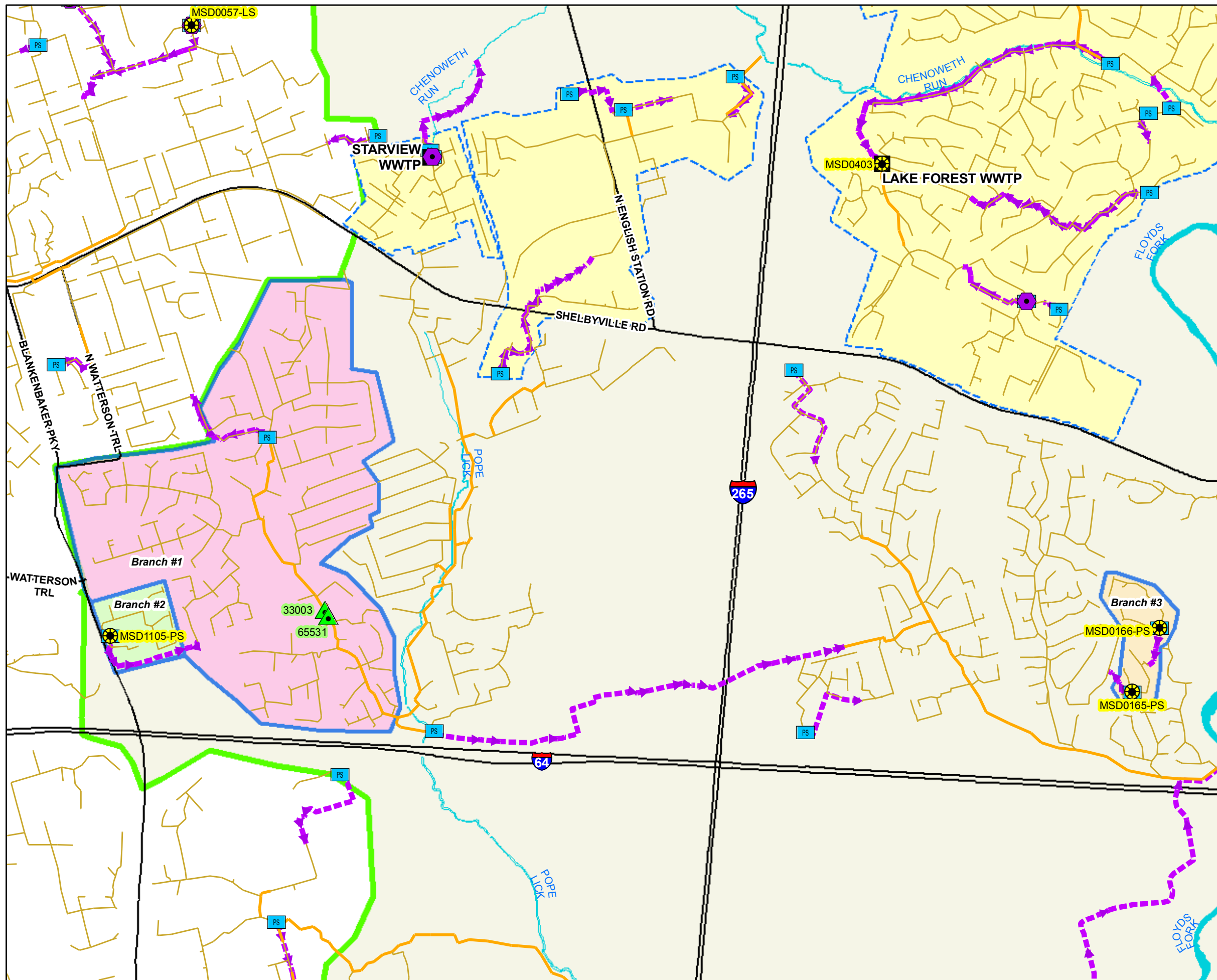
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**Integrated Overflow Abatement Plan**  
**Vol. 3 Sanitary Sewer Discharge Plan**

**Floyds Fork Sewershed**  
**Branch Network**  
**Figure 2.5.4**



- Legend**
- Documented SSO
  - Suspected SSO
  - Haul Operation
  - WWTP
  - Pump Station
  - Force Main
  - Collector < 12"
  - Interceptor =>12"
  - Major Road
  - Streams
  - CSO Area
  - Small WWTP Service Area
  - Large WWTP Service Area
  - Branch #1
  - Branch #2
  - Branch #3
  - County Boundary

1 inch = 1,600 feet  
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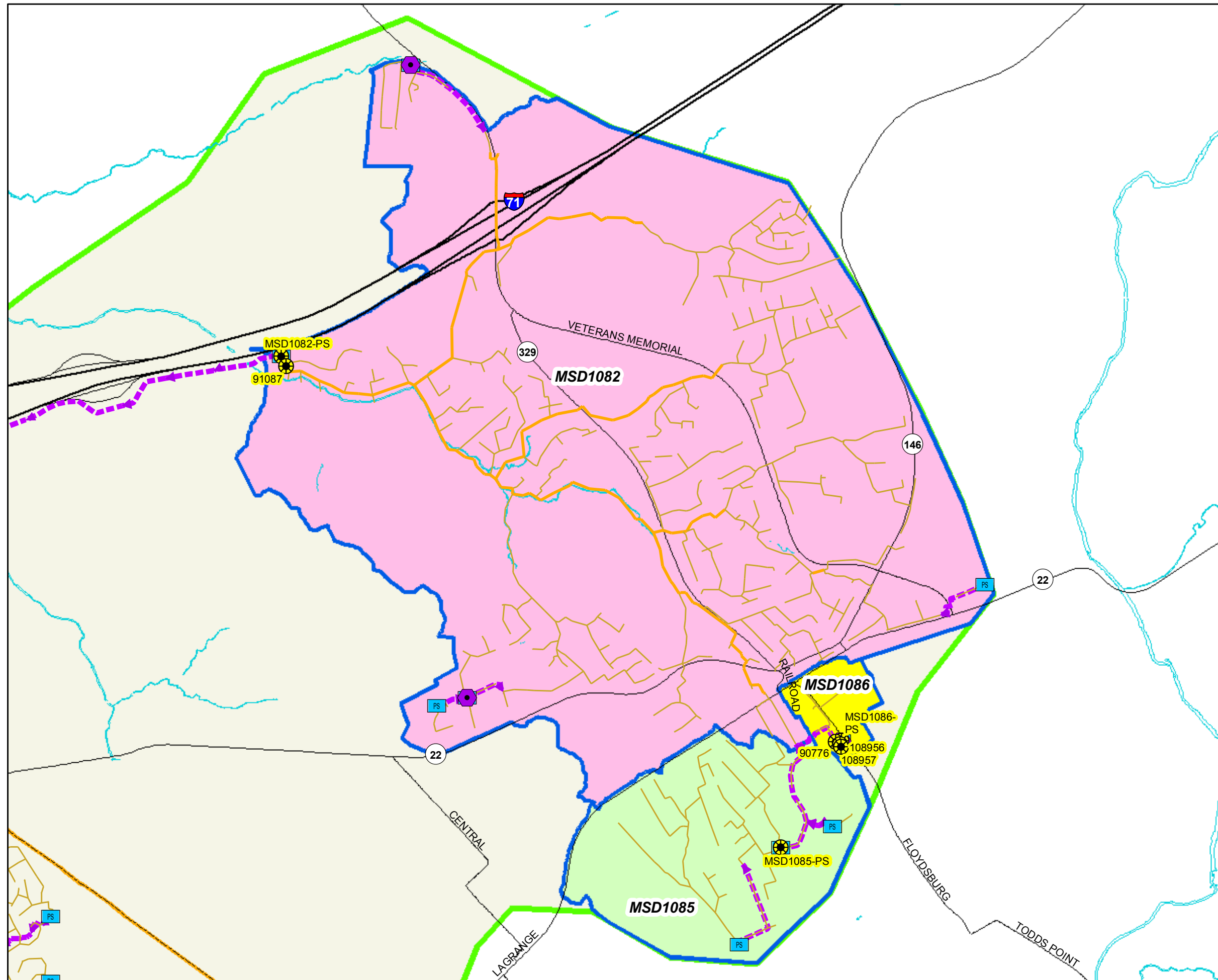
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# Integrated Overflow Abatement Plan

## Vol. 3 Sanitary Sewer Discharge Plan

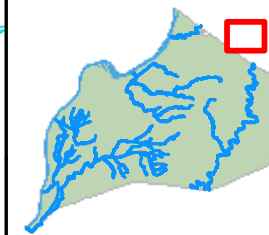
### Hite Creek Sewershed Branch Network Figure 2.5.5



#### Legend

- ☀ Documented SSO
- ▲ Suspected SSO
- ⬡ Haul Operation
- WWTP
- PS
- ➔ Force Main
- Collector < 12"
- Interceptor =>12"
- Major Road
- ~ Streams
- CSO Area
- Small WWTP Service Area
- Large WWTP Service Area
- Branch MSD1085
- Branch MSD1086
- Branch MSD1082
- County Boundary

1 inch = 1,800 feet  
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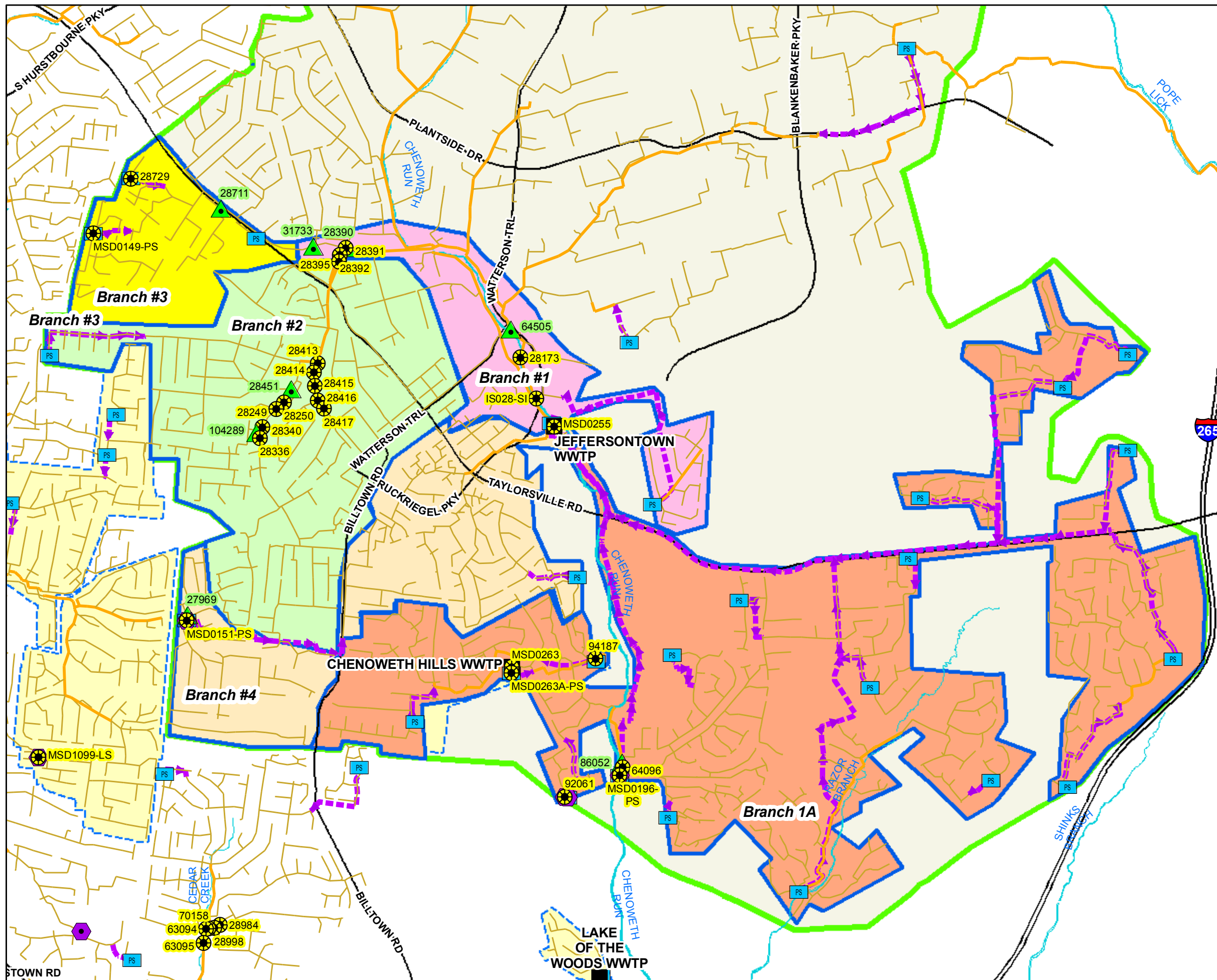


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**Integrated Overflow Abatement Plan  
Vol. 3 Sanitary Sewer Discharge Plan**

**Jeffersontown Sewershed  
Branch Network  
Figure 2.5.6**



**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- WWTP
- Pump Station
- Force Main
- Collector < 12"
- Interceptor =>12"
- Major Road
- Streams
- CSO Area
- Small WWTP Service Area
- Large WWTP Service Area
- Branch #1
- Branch #2
- Branch #3
- Branch #4
- Branch 1A
- County Boundary

1 inch = 2,000 feet  
Scalable when printed on 11" X 17" paper



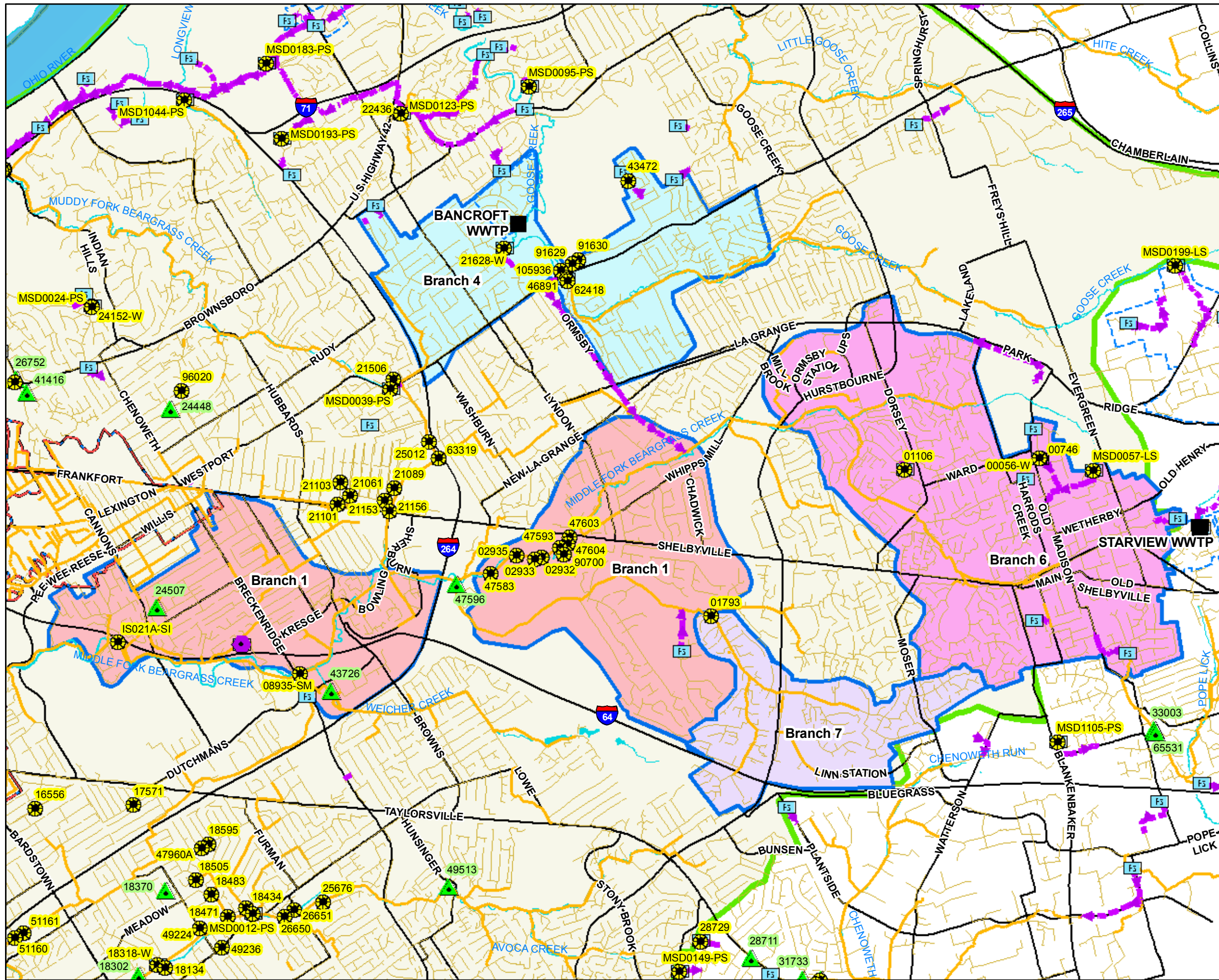
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**Morris Forman Sewershed**  
**Middle Fork**  
**Branch Network**  
**Figure 2.5.7**



**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- WWTP
- Pump Station
- Force Main
- Collector < 12"
- Interceptor =>12"
- Streams
- Interstates
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Branch 1
- Branch 4
- Branch 6
- Branch 7
- County Boundary

1 inch equals 3,600 feet  
 Scalable when printed on 11" X 17" paper



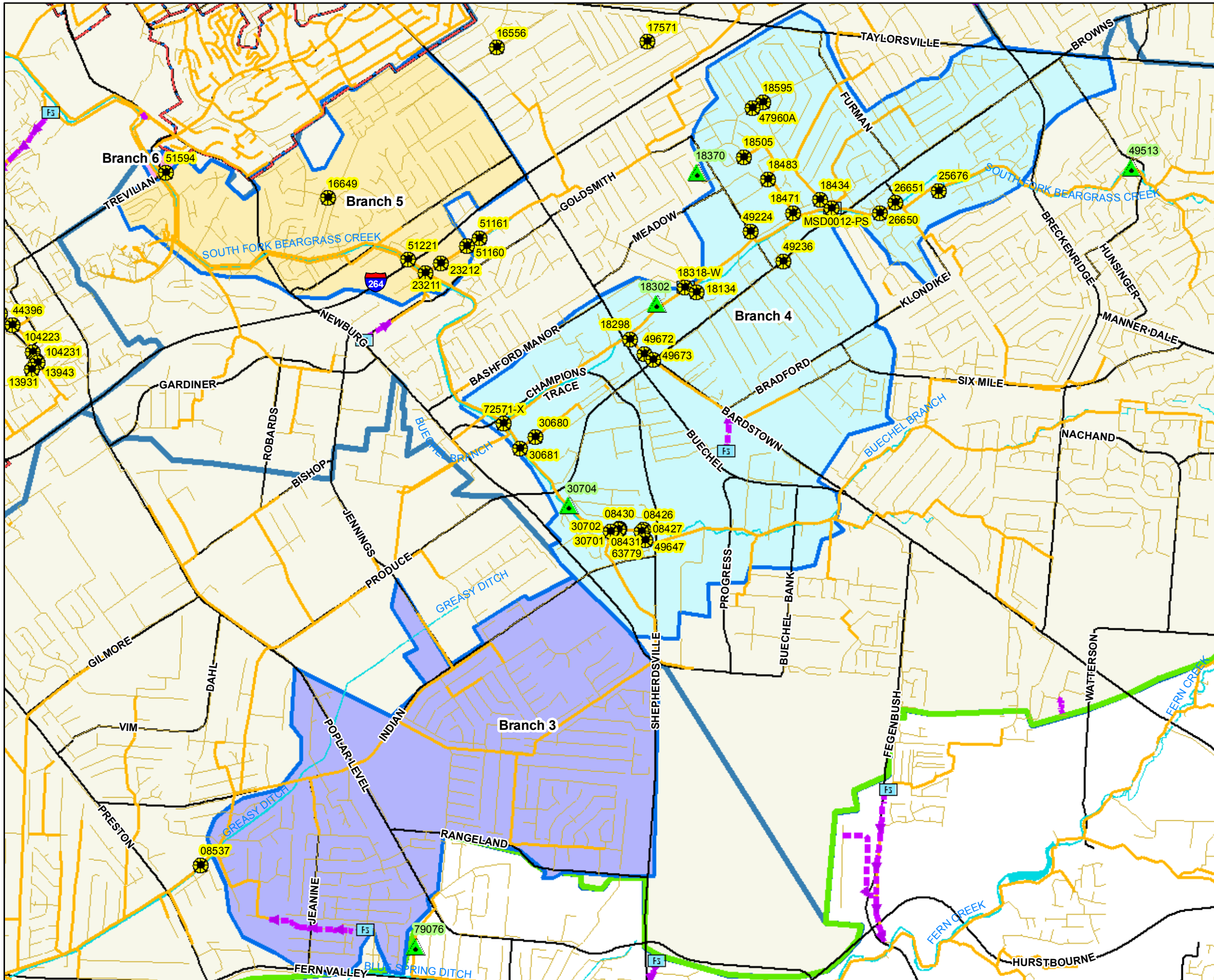
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**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Morris Forman Sewershed  
 Southeast Diversion  
 Branch Network  
 Figure 2.5.8



**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- WWTP
- Pump Station
- Force Main
- Collector < 12"
- Interceptor =>12"
- Streams
- Interstates
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Branch 3
- Branch 4
- Branch 5
- Branch 6
- County Boundary

1 inch equals 2,350 feet  
 Scalable when printed on 11" X 17" paper



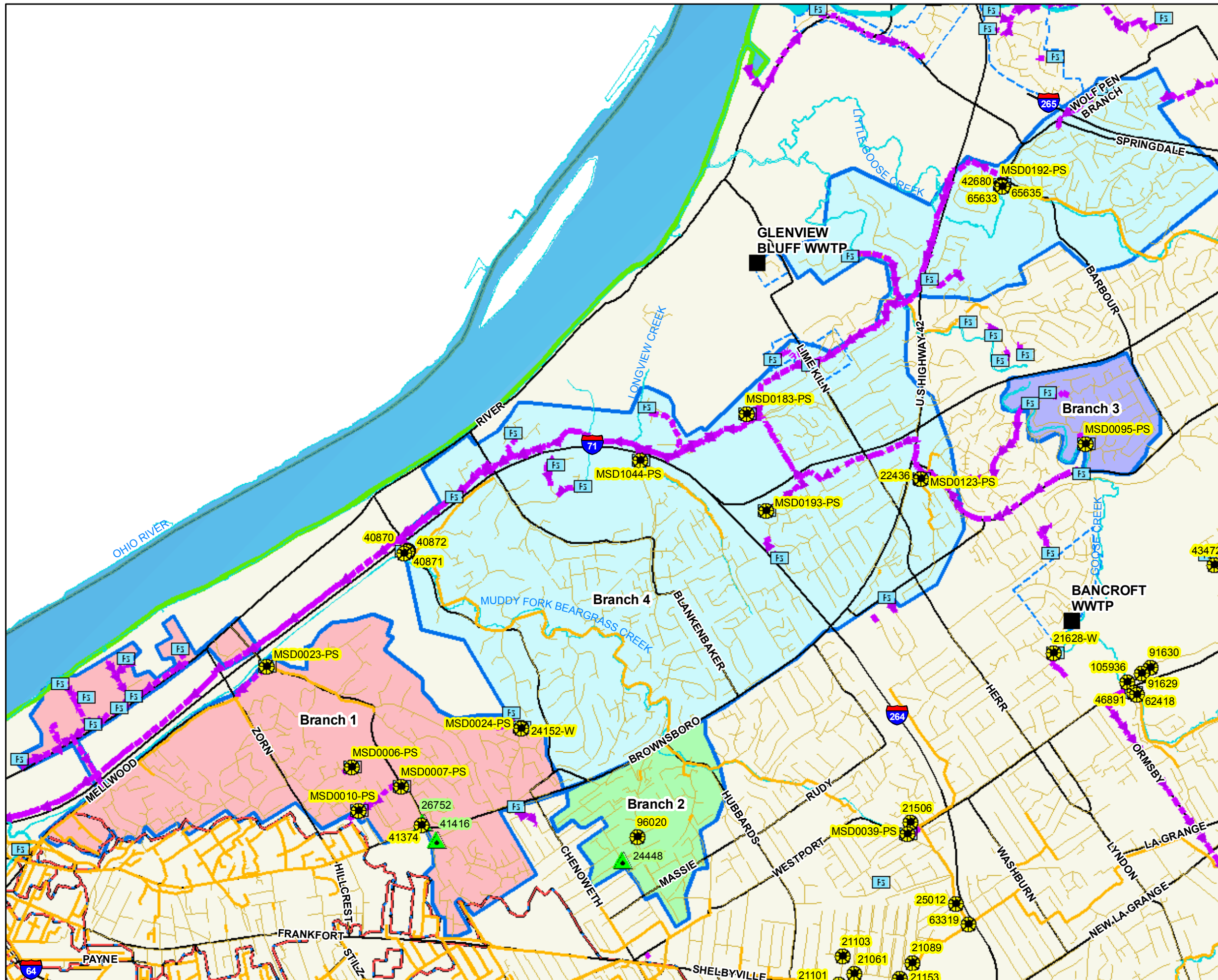
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**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Morris Forman Sewershed**  
**ORFM**  
**Branch Network**  
**Figure 2.5.9**



**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- WWTP
- Pump Station
- Force Main
- Collector < 12"
- Interceptor =>12"
- Streams
- Interstates
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Branch 1
- Branch 2
- Branch 3
- Branch 4
- County Boundary

1 inch equals 2,800 feet  
 Scalable when printed on 11" X 17" paper



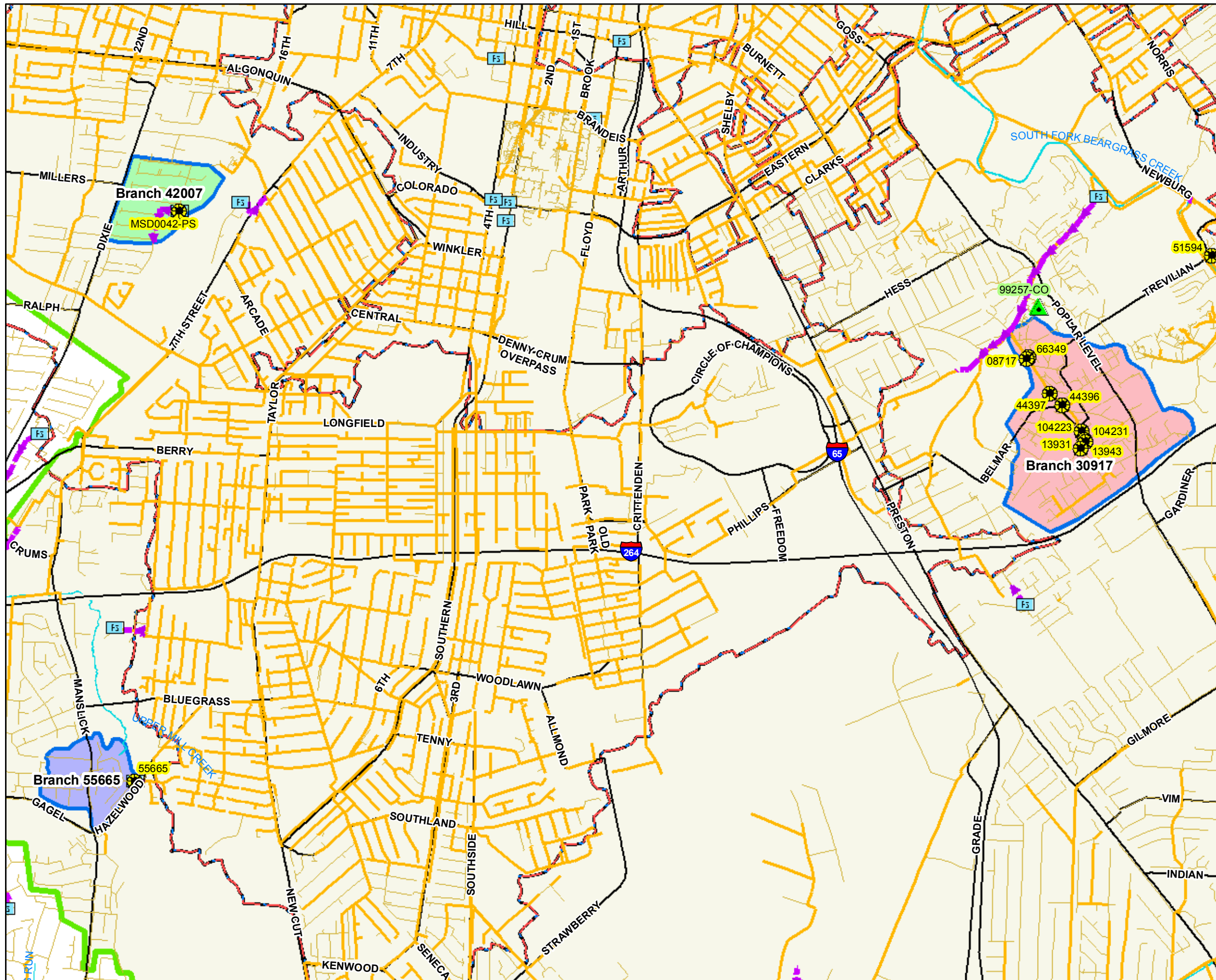
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











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**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Morris Forman Sewershed**  
**CSS Area**  
**Branch Network**  
**Figure 2.5.10**



**Legend**

-  Documented SSO
-  Suspected SSO
-  Haul Operation
-  WWTP
-  Pump Station
-  Force Main
-  Collector < 12"
-  Interceptor =>12"
-  Streams
-  Interstates
-  Small WWTP Service Area
-  Large WWTP Service Area
-  CSO Area
-  Branch 30917
-  Branch 42007
-  Branch 55665
-  County Boundary

1 inch equals 2,400 feet  
 Scalable when printed on 11" X 17" paper



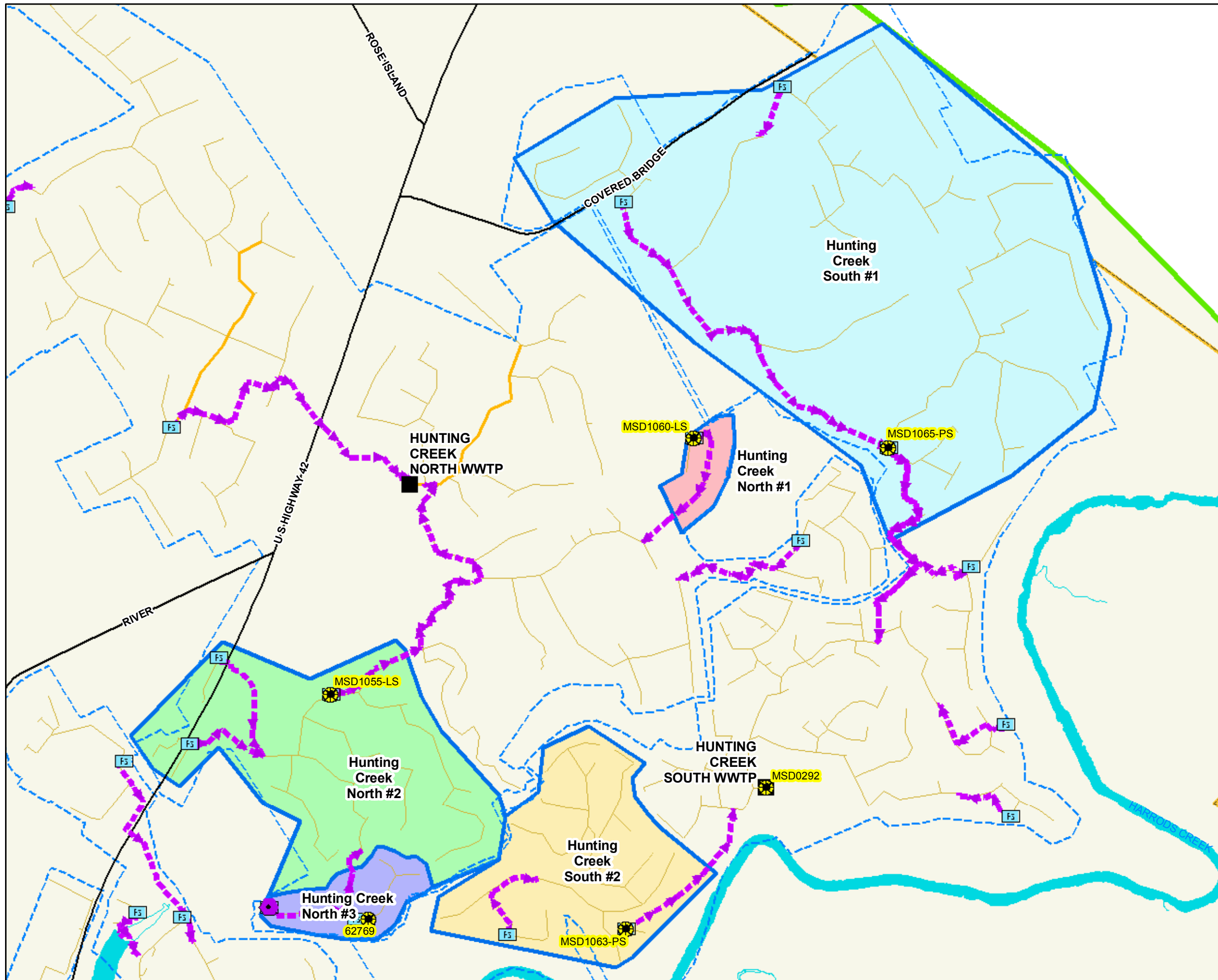
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**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Morris Forman Sewershed**  
**Small WWTP - Hunting Creek Area**  
**Branch Network**  
**Figure 2.5.11**



**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- WWTP
- Pump Station
- Force Main
- Collector < 12"
- Interceptor =>12"
- Streams
- Interstates
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Hunting Creek North #1
- Hunting Creek North #2
- Hunting Creek North #3
- Hunting Creek South #1
- Hunting Creek South #2
- County Boundary

1 inch equals 900 feet  
 Scalable when printed on 11" X 17" paper

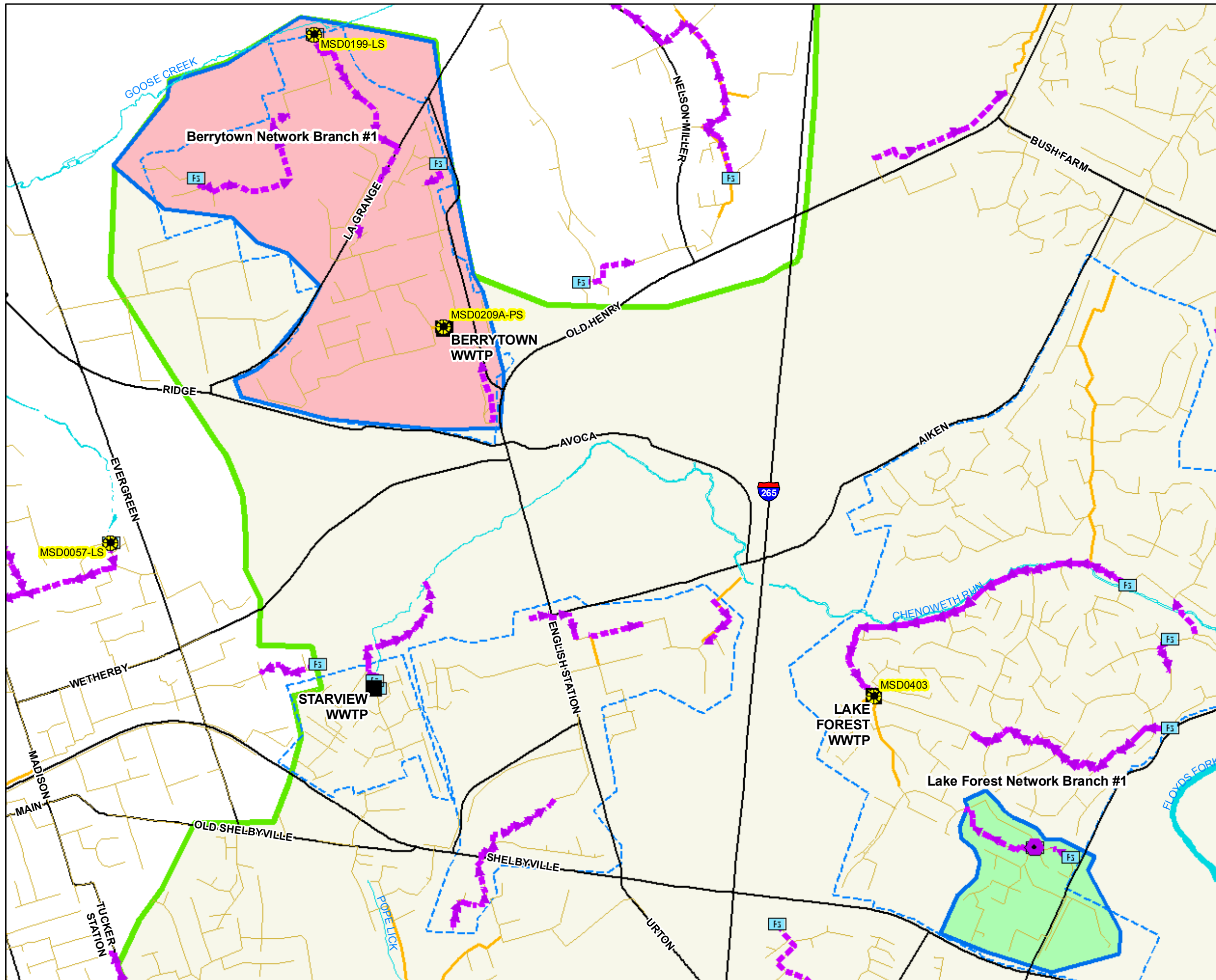


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**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Morris Forman Sewershed**  
**Small WWTP - Berrytown and Lake Forest Area**  
**Branch Network**  
**Figure 2.5.12**



**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- WWTP
- Pump Station
- Force Main
- Collector < 12"
- Interceptor >=12"
- Streams
- Interstates
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Berrytown Network Branch #1
- Lake Forest Network Branch #1
- County Boundary

1 inch equals 1,450 feet  
 Scalable when printed on 11" X 17" paper

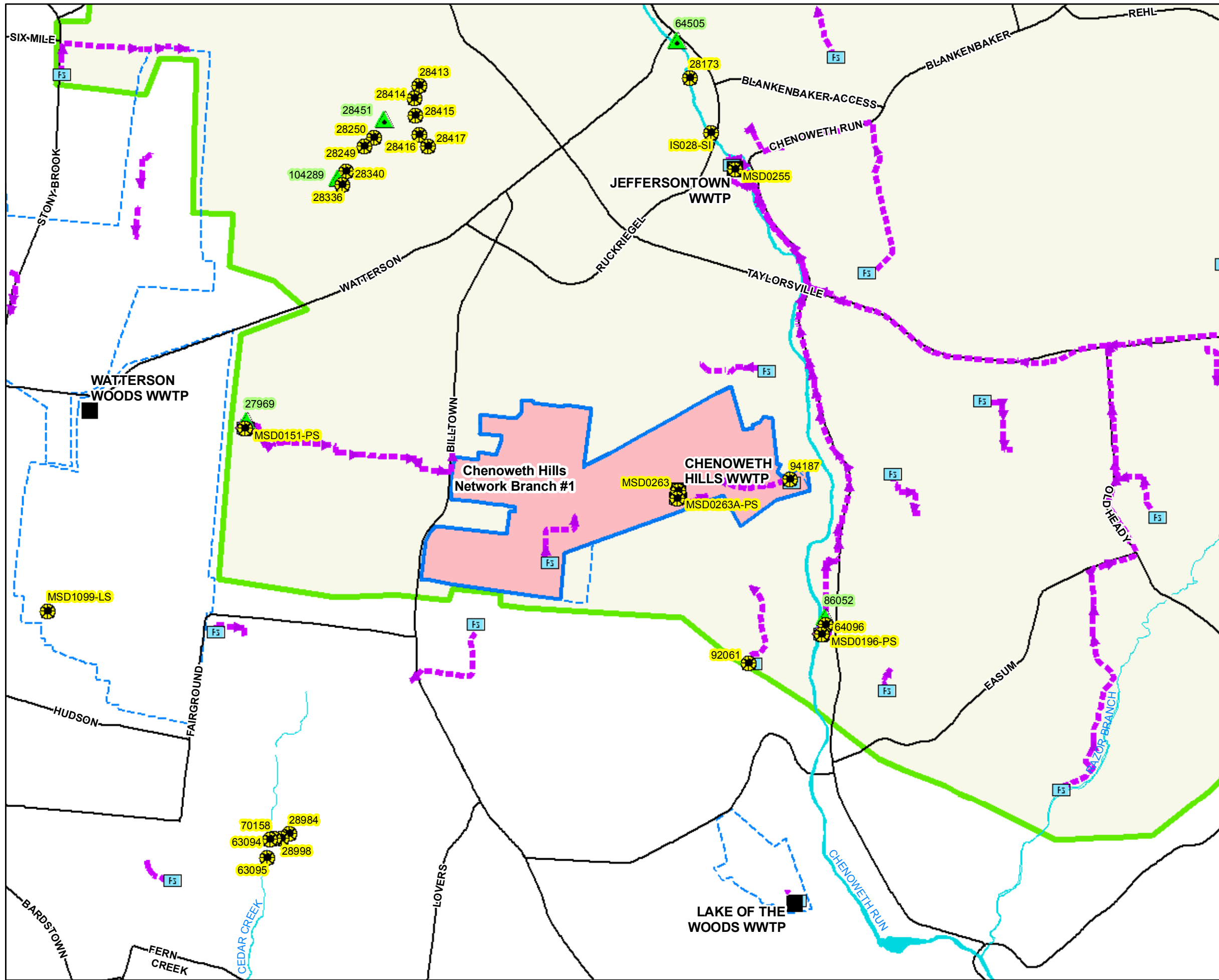


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**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Morris Forman Sewershed**  
**Small WWTP - Chenoweth Hills Area**  
**Branch Network**  
**Figure 2.5.13**



**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- WWTP
- Pump Station
- Force Main
- Collector < 12"
- Interceptor =>12"
- Streams
- Interstates
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Chenoweth Hills Network Branch #1
- County Boundary

1 inch equals 1,500 feet  
 Scalable when printed on 11" X 17" paper



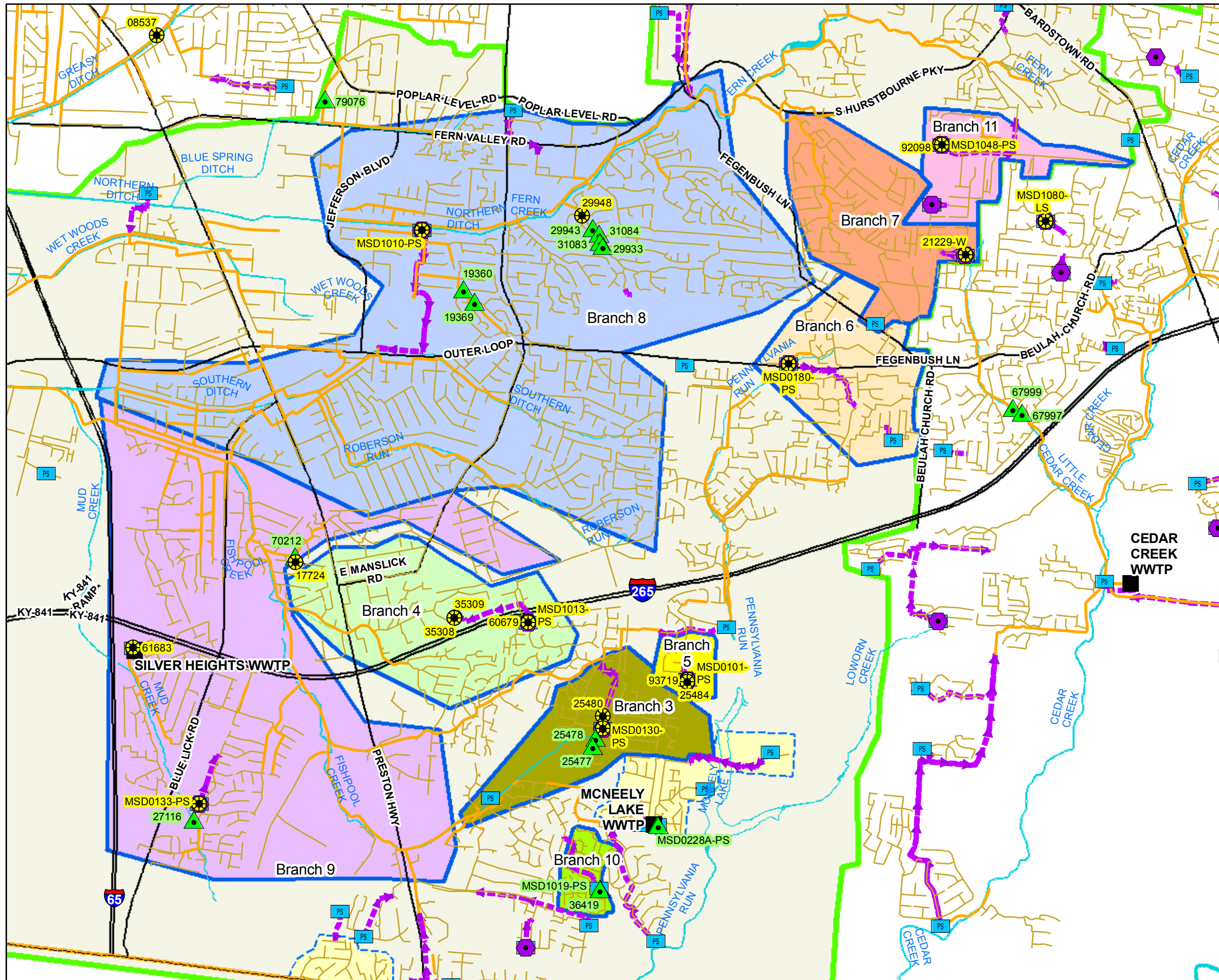
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**Integrated Overflow Abatement Plan**  
**Vol. 3 Sanitary Sewer Discharge Plan**  
**West County Pond**  
**Creek Area Sewershed**  
**Branch Network**  
**Figure 2.5.14**



**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- WWTP
- Pump Station
- Force Main
- Collector < 12"
- Interceptor => 12"
- Streams
- Major Road
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Branch 3
- Branch 4
- Branch 5
- Branch 6
- Branch 7
- Branch 8
- Branch 9
- Branch 10
- Branch 11
- County Boundary

1 inch = 3,000 feet  
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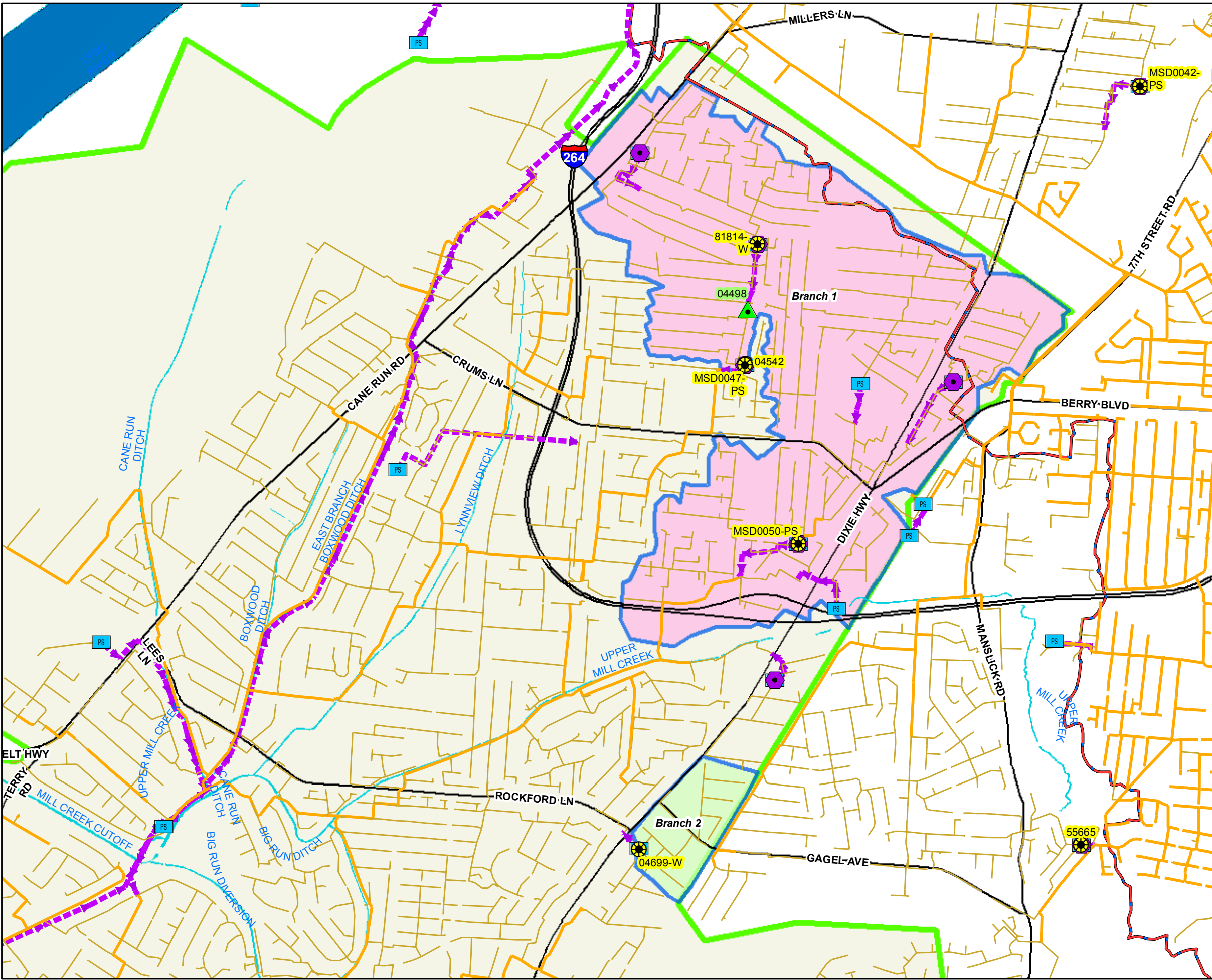
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**Integrated Overflow Abatement Plan**  
**Vol. 3 Sanitary Sewer Discharge Plan**  
**West County Mill**  
**Creek Area Sewershed**  
**Branch Network**  
**Figure 2.5.15**



- Legend**
- Documented SSO
  - Suspected SSO
  - Haul Operation
  - WWTP
  - Pump Station
  - Force Main
  - Collector < 12"
  - Interceptor =>12"
  - Major Road
  - Streams
  - CSO Area
  - Small WWTP Service Area
  - Large WWTP Service Area
  - Branch 1
  - Branch 2
  - County Boundary

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## CHAPTER 3: DEVELOPMENT AND EVALUATION OF ALTERNATIVES FOR SSO ELIMINATION

**Special Note:** This chapter was developed in 2008. The statistical data for the SSO’s reported, specifically related to individual SSO volumes and frequency in a typical rainfall year, were derived from the hydraulic models calibrated in 2007. Since then, a more detailed calibration and validation effort has adjusted the average annual overflow volumes and frequencies in the typical year. This information is provided in Chapter 5. The vast majority of the physical system characterization in this chapter is still accurate.

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Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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## **SUPPORTING INFORMATION**

Appendix 3.1.1 I/I Program Documentation

Appendix 3.1.2 Ground Truthing Documentation

Appendix 3.2.1 Re-evaluation of Preferred Projects Analysis

Appendix 3.3.1 Preferred Solution Cost Tables, Benefit-Cost Tables, Maps, Fact Sheets

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

## **CHAPTER 3: DEVELOPMENT AND EVALUATION OF ALTERNATIVES FOR SSO ELIMINATION**

Once a clear understanding of the root problems of sanitary sewer overflows (SSOs) is obtained through the system characterization process, it is important to develop a comprehensive set of potential solutions that are effective and acceptable by the public.

Chapter 3 presents the methodologies used to evaluate the various SSO elimination solutions. The chapter defines and discusses strategies and technologies available to control and eliminate unauthorized discharges in the separate sanitary sewer system (SSS). The chapter also provides a summary of the evaluation for each SSO elimination alternative. The evaluation criterion includes feasibility screening, computer modeling, quality control, level of protection, cost estimates, and a benefit-cost analysis.

### **3.1 THE FINAL SSDP APPROACH**

Overall, the Final Sanitary Sewer Discharge Plan (SSDP) approach to SSO elimination is to determine the solution that provides the greatest benefit-cost ratio for each watershed branch. Modeling teams used the Louisville and Jefferson County Metropolitan Sewer District (MSD) Project Cost Estimating Tool and the Benefit-Cost Value Model, both developed specifically for the Integrated Overflow Abatement Plan (IOAP). These tools were used to determine benefit scores, capital costs, long-term operation and maintenance (O&M) costs, and the benefit-cost ratio. The process is discussed in more detail in this section.

#### **3.1.1 Solution Development Overview**

The major steps in the solution development process are summarized below:

- Models were calibrated and validated (Volume 3, Chapter 2, Section 2.3).
- Where appropriate, rainfall dependent inflow and infiltration (RDI/I) and build-out was applied to the validated models (Volume 3, Chapter 2, Section 2.3.5.7).
- Where appropriate, capital projects were incorporated into the models (Volume 3, Chapter 2, Section 2.3.5.9).
- Input was gathered from public meetings, as well as guidance from the Wet Weather Team (WWT) Stakeholder Group and ground truthing exercises.
- Initial solutions were developed and presented at WWT Stakeholder Group meetings for review and comments.
- Solutions that addressed SSOs and reduced known surcharging under site-specific design conditions were developed using a diverse set of solution technologies.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

- Benefits, capital costs, and benefit-cost ratios for each solution were developed at the baseline level of protection (1.82-inch cloudburst storm event).
- The solution with the best benefit-cost ratio was selected for development of the preferred level of protection (Volume 3, Chapter 4).

### **3.1.2 SSO Control Measures and Technologies**

A wide range of technology approaches is available for the development of SSO abatement strategies and alternatives. These approaches are summarized in the following sub-sections.

#### **3.1.2.1 Source Control through Infiltration and Inflow (I/I) Reduction**

Source reduction focuses on preventing wet weather flows through various sources from reaching the sewer. Source reduction was considered for each branch solution. The method and degree of source reduction is described in Volume 3, Chapter 2, Section 2.3.5.7. MSD is embarking on programs to address countywide, private-side, and public-side source reduction. As it pertains to the Final SSDP, a 20-year program will be implemented to reduce flows in areas critical to Final SSDP success. The program is outlined in Appendix 3.1.1, I/I Program Documentation.

#### **3.1.2.2 Basement Backups and Sewer Surcharging**

Surcharge reduction focuses on the prevention of basement flooding during wet weather. Basement flooding protection was considered and analyzed for all branch solutions using the System Capacity Assurance Plan criterion discussed in Volume 3, Chapter 2, Section 2.5.1. The surcharge criterion was applied to all areas hydraulically connected to a documented or suspected SSO location (known as the “zone of influence”) and/or downstream of an SSDP solution. Solutions were then sized accordingly to reduce or eliminate surcharging to the Louisville Metro Sewer Capacity Assurance Plan (SCAP) criterion.

Other basement backup complaints or modeled surcharging not within the SSO zone of influence or downstream of an SSDP solution will be addressed by MSD’s Plumbing Modification Program, which is available to all MSD customers, as discussed in Volume 3, Chapter 1, Section 1.3.1.4. To-date, MSD has completed over 8,100 projects totaling approximately \$16 million dollars under the Plumbing Modification Program. Refer to Appendix 1.3.1 for the Plumbing Modifications Program and Downspout Disconnection Program packet available to MSD customers.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 3.1.2.3 Peak Flow Storage Alternatives

A storage solution is an alternative where flow is temporarily stored to eliminate SSOs. This includes inline storage (large diameter pipe(s) built into the sewer system) or offline storage (covered or open storage facilities). Storage alternatives may also include additional pumping capacity, conveyance to and from the storage location, controls, easements, land purchases, odor control, surface treatment, and long-term O&M. Storage solutions developed are then evaluated through a complete “fill-and-empty” cycle in the model, which also includes a secondary storm analysis (as described in Volume 3, Chapter 2, Section 2.3.4).

A significant cost factor in storage is whether the constructed storage facility is open or closed to the environment. Open facilities are generally less expensive, but they present potential problems such as odors and poor aesthetics. Covering the facility, generally by burying, can improve these conditions but significantly increases the cost of the facility.

For any facility, the siting location is critical. Thus, the ground truthing exercises were developed to assist with the siting process. Section 3.1.3.3 describes the ground truthing process in more detail.

### 3.1.2.4 Increased Conveyance Capacity

A conveyance solution increases the sewer capacity to eliminate SSOs. The solution may include: increases in pipe size, additional pumping capacity, parallel sewer conveyance, and elimination of bottlenecks. Pure conveyance solutions will usually result in increased flow downstream. In these cases, the increase in flow must be addressed by downstream branches in the system.

While siting is not as critical as storage alternatives, ground truthing is still required to properly cost the improvements for some conveyance solutions (see Section 3.1.3.3 for more detail on ground truthing).

### 3.1.2.5 Flow Diversion

A diversion solution is an alternative where flow is diverted to other systems or sewersheds to alleviate capacity at the solution location. Generally, a diversion solution will involve gravity solutions, although some pump station improvements may be included.

Diversion alternatives will undoubtedly impact other branches and potentially other watersheds. As a result, solutions will have to account for the additional flows to the impacted branches. Similar to conveyance alternatives, ground truthing is required to properly price diversion alternatives.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### **3.1.2.6 Water Quality Treatment Center (WQTC) Upgrades**

In accordance with the Consent Decree, all WQTCs with the potential to receive additional flow as a result of SSO elimination were evaluated by developing a “Comprehensive Performance Evaluation” (CPE) in accordance with EPA guidance documents called out in the Consent Decree. The CPE process was originally developed to provide a systematic approach to improving the performance of WQTCs that were not in compliance with discharge standards. In this application it was necessary to conduct an evaluation based on the anticipated performance of the plants in treating the modeled peak wet weather flows. Initial evaluations considered the worst case scenario assuming SSO eliminations were accomplished by increasing conveyance capacity, essentially pushing the entire wet weather flow increase to the WQTC. Final evaluations were refined based on modeled wet weather hydrographs considering the actual SSO elimination projects selected in the Final SSDP.

The Consent Decree also required CPEs be conducted on the five plants in the Prospect area, and the Lake Forest WQTC. As a result of both sets of requirements, CPEs were developed for the following WQTCs in accordance with the Consent Decree:

- Berrytown WQTC
- Cedar Creek WQTC
- Chenoweth Hills WQTC
- Hite Creek WQTC
- Hunting Creek South WQTC
- Jeffersontown WQTC
- Ken Carla WQTC
- Lake Forest WQTC
- North Hunting Creek WQTC
- Starview WQTC
- Timberlake WQTC

A more complete description of the CPE process and the resultant Composite Correction Approach WQTC improvement recommendations is contained in Volume 1, Section 4.4. This section in Volume 1 also presents the evaluation of potential collection system modifications compared to WQTC expansions to address wet weather peaks.

CPEs were not developed for the Derek R. Guthrie WQTC (formerly known as the West County Wastewater Treatment Plant) or the Floyds Fork WQTC because both plants are scheduled to undergo significant expansions in the near future. The WQTC expansions will be sized to

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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include any additional wet weather flow peaks anticipated as a result of SSO elimination. In lieu of CPEs, the preliminary design reports for those WQTC expansions are addressed in Volume 1. A CPE was not developed for the Morris Forman WQTC because it serves the combined sewer system and is specifically excluded from the CPE requirement in the Consent Decree.

### **3.1.3 Initial Solutions**

MSD was committed to obtaining WWT Stakeholder Group input throughout the IOAP development. In particular, MSD solicited WWT Stakeholder Group input before modeled solution development began. To “kick off” the potential solution process, the initial solutions were developed for each modeled branch. The initial solution development phase involved desktop evaluation and simple sizing using existing condition model runs and MSD’s historical work order database.

Initial solutions were presented to the WWT Stakeholder Group in a series of meetings where the Group was engaged in discussions about the initial solutions and their comments or concerns were noted. This information was then considered and included in future modeled solution development. The following sections summarize the initial solution phase, from SSO characterization to the ground truthing process, and provide a general overview of the types and number of initial solutions that were a result of this particular stage of solution development.

#### **3.1.3.1 SSO Characterization**

Initially, there were 109 SSOs and more than 200 modeled overflow points (MOPs) used to determine the design of initial solution projects. Refer to Volume 3, Chapter 2, Section 2.4.2 for a discussion of the MOP validation process. Many aspects of each area were reviewed before the initial solutions were developed; for example, the source or cause of the SSO(s) was investigated through a review of discharge work orders and, based on initial evaluation, the overflow volume for various levels of protection was reported.

Site conditions for the entire area surrounding the SSOs and MOPs were also investigated and reported for each initial solution. Surrounding landuse, apparent utility conflicts, and other aspects that could affect a project were reviewed and documented.

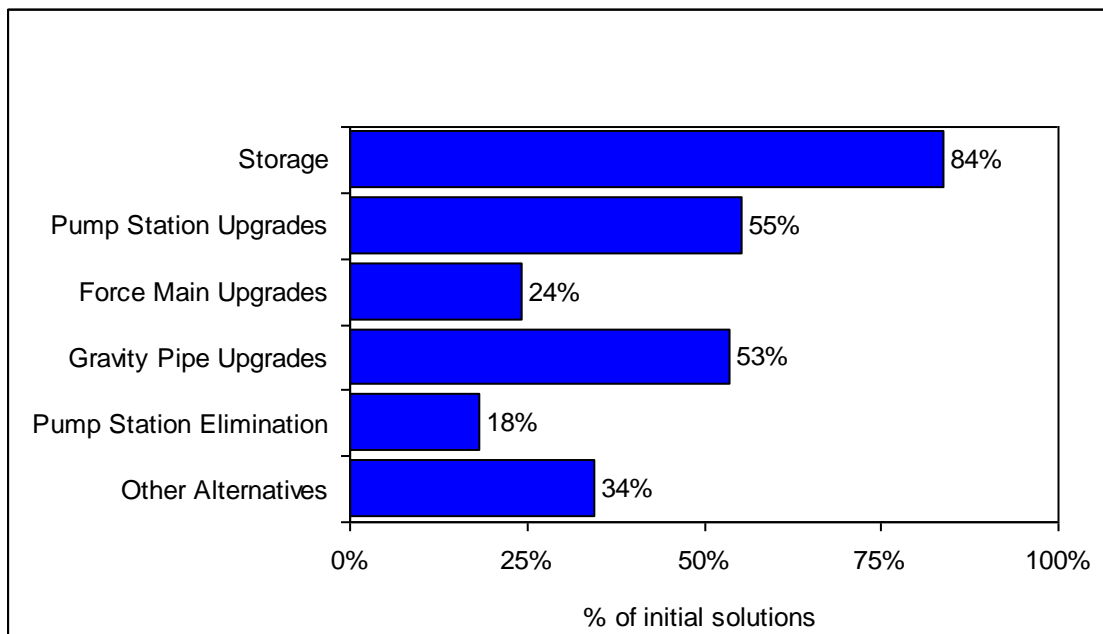
Additionally, capital projects and proposed developments in the area were reviewed and summarized in each initial solution development phase. The initial solutions were developed after investigation of the cause of the SSO, surrounding area landuse, apparent utilities, proposed developments, capital projects, and modeling needs. The research was conducted with the objective of integrating the most important characterizations of each project location into the solution alternatives.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 3.1.3.2 Initial Solution Alternatives

The initial solution alternatives that were considered included one or more of the available technologies as described in Section 3.1.2. Figure 3.1.2 summarizes the developed solutions. Some of the initial locations were identified as having more than one potential solution and the graph shows the percentage of initial solution options by solution type that may be able to eliminate the SSOs. The pump station elimination, sewer upgrades, force main upgrades, and pump station upgrades could be part of either a conveyance solution or a diversion solution.

**FIGURE 3.1.2 SUMMARY OF INITIAL SOLUTION ALTERNATIVES**



#### Storage Alternatives

More than eighty percent of the initial solution locations displayed potential for storage facilities and inline storage pipes. However, some locations were determined to be unsuitable for storage solutions due to maintenance access and land acquisition concerns.

#### Conveyance Alternatives

The conveyance alternatives included pump station, force main, and gravity pipe upgrades, pump station eliminations, and diversions. These alternatives were usually more complex requiring sewer pipe upgrades, newly constructed sewer pipe, and/or pump station upgrades. More than eighty percent of the initial solutions displayed potential for conveyance alternatives.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

## **Other Alternatives**

Other alternatives included capital project solutions, raising manholes and reducing I/I.

### **3.1.3.3 Ground Truthing**

As mentioned earlier, siting is a critical component of project development. Thus, MSD developed a ground truthing process to consistently evaluate storage, conveyance, and diversion alternatives. Ground truthing collects critical information that could affect cost, such as soil conditions and easements, or, in some cases, prevent the site from being further considered, such as future planned development.

Each modeling team was responsible for ground truthing storage, conveyance, and diversion alternatives considered within the respective watersheds. In some cases, the solution involved alignments in existing rights-of-way or easements, such as pipe upsizing, and ground truthing was not necessary. The following list provides examples of features that were investigated during the ground truthing process:

- Rock depth
- 100-Year floodplain location
- Threatened/endangered species assessment
- Potential utility conflicts
- Required Permits, i.e. Kentucky Department of Environmental Protection (KDEP), U.S. Army Corp of Engineers (USACE), Etc.
- Green space initiatives
- National historic registry
- Development conflicts
- Significant topographical features, i.e. steep slope

Once ground truthing was completed, a recommendation was made labeling the site as either suitable or unsuitable for the particular solution type. Specific ground truthing and significant findings are briefly discussed for each individual watershed (see Section 3.3), and full ground truthing documents along with pictures of the sites are available for review in Appendix 3.1.2 Ground Truthing Documentation.

## **3.2 PROJECT SELECTION ANALYSIS**

MSD used a standard benefit-cost ratio process to determine and select the most effective solution for each branch of SSOs for a baseline level of protection. In this case, the 1.82-inch cloudburst storm was utilized as the baseline level of protection. The same process was used to set optimal levels of protection for the selected solutions (described in Volume 3, Chapter 4).

Additionally, several projects were conceptually re-designed using a 2.25-inch cloudburst storm to evaluate if the initial level of control used as the baseline condition created any bias toward a particular technology in selecting a preferred solution from a group of initial competing technologies. The evaluation, detailed in Sections 3.3.5.2, 3.3.9.2, and 3.3.11.2, showed that the initial level of control used as the baseline condition appeared to have no impact on the technology selected. For a full explanation and results of the analysis refer to Appendix 3.2.1, Re-evaluation of Preferred Projects Analysis.

The MSD Project Cost Estimating Tool and the benefit-cost value model were utilized to develop Final SSDP solution costs and benefits, based on input from the WWT. These planning models are fully described in Volume 1, Section 2.5. The individual components are summarized in the following section.

### **3.2.1 Cost Analysis**

A total project capital cost and present worth (including O&M) cost was computed for each solution alternative using the MSD Project Cost Estimating Tool, which uses cost curves based on common parameters obtained from model runs. This includes parameters such as pipe diameters, location (i.e. paved areas versus non-paved) and site conditions (i.e. site dewatering). It also includes costs for easements and land acquisitions, as well as O&M costs for pumping, cleaning and other recurring tasks.

It is important to understand that costs developed at this stage were planning level costs only and included planning level contingencies for the uncertainties at this level. Cost estimates that are more detailed were prepared for selected projects after the optimized solution evaluation stage and are discussed in Volume 3, Chapter 4.

### **3.2.2 Benefit Analysis**

The MSD benefit-cost value model was used to consistently calculate benefits for the solution alternatives. Project-specific values, branching, and benefits based on SSO solutions and locations are discussed in this section.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 3.2.2.1 Project-Specific Values

The WWT identified community values to be considered during SSO abatement planning. The community values identified were asset protection, customer satisfaction, eco-friendly solutions, economic vitality, environmental enhancement, environmental justice and equity, financial equity, financial stewardship, public health enhancement, public education, and regulatory performance. However, not all of these values were specifically analyzed as part of the benefit-cost analysis. Five project specific values were selected to provide a comprehensive and viable benefit-cost analysis.

**Five Project-Specific Core Values**

1. Regulatory Performance
2. Public Health Enhancement
3. Asset Protection
4. Environmental Enhancement
5. Eco-Friendly Solutions

To enhance the benefit-cost ratio process, the WWT assigned weighting factors on a zero to ten scale to each of the five values to reflect the degree of importance to the overall control plan impact to the community. The values and assigned weights that were used to score benefits were as follows:

- Public Health 10
- Regulatory Performance 8
- Environmental Enhancement 8
- Asset Protection 6
- Eco-Friendly Solution 6

One module for each of the five core values exists within the benefit-cost analysis tool in addition to a module that summarizes the resulting scores and costs for up to five alternatives per SSO or branch.

Regulatory Performance and Public Health were scored on a 25-point severity-frequency matrix according to SSO volume and frequency. The baseline characteristics of the SSO were initially scored, followed by scoring the remaining overflow/frequency resulting from the proposed solution. The difference in these values was the benefit score, with a higher score indicating a higher reduction in risk, or higher value of benefit. The Asset Protection value was also scored on a 25 point severity-frequency scale (level of protection versus damage impact) to account for reduction in basement flooding by a proposed SSO solution.

The Environmental Enhancement and Eco-Friendly Solution values were scored using several performance metrics that represent a variety of aspects related to the environment or ecosystems. Each of the aspects were scored on a 10-point negative-to-positive scale (-5 to +5). Environmental Enhancement primarily assesses aquatic impact, while Eco-Friendly Solutions assesses broader land/energy impacts of proposed SSO solution alternatives.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 3.2.2.2 Benefits Based on SSO Locations and SSO Solutions

Two values, Regulatory Performance and Public Health Enhancement, are specific to the frequency and magnitude of each individual SSO location. Therefore, benefits are calculated separately for each SSO for both the existing conditions and proposed conditions, after the solution is in place.

The other three values, Eco-Friendly Solutions, Environmental Enhancement and Asset Protection, are specific to the type of solution. Therefore, benefits are calculated by solution and SSOs in the branch receive the same score for both the existing conditions and proposed conditions, after the solution is in place.

### 3.2.2.3 Branching or Clusters

As described above, benefits are calculated for each SSO individually at the Regulatory Performance and Public Health levels, and then aggregated for a “cluster” (branch) of SSOs to calculate Asset Protection, Environmental Enhancement, and Eco-Friendly Solutions scores.

Consequently, the net benefit is very much dependent on the number of SSOs in each cluster. Accordingly, net benefits cannot be compared directly from branch to branch. Likewise, benefit-cost ratios cannot be directly compared. Within a branch, however, net benefits can be directly compared and resulting benefit-cost ratios will identify the best solutions.

Table 3.2.1 shows an example of the calculations involved in determining a total benefit score for a cluster of SSOs.

TABLE 3.2.1

EXAMPLE BENEFIT CALCULATION

Example Benefit Calculation for One Branch					
SSO ID	Regulatory Performance	Public Health	Asset Protection	Environmental Enhancement	Eco-Friendly Solutions
MSD0023	12	7	4	4	1
MSD0010	5	2	4	4	1
MSD0007	5	2	4	4	1
26752	5	7	4	4	1
41416	5	5	4	4	1
24472	5	5	4	4	1
41374	0	0	4	4	1
MSD0024	0	2	4	4	1
24152-W	0	0	4	4	1
<b>Sum</b>	<b>37</b>	<b>30</b>	<b>36</b>	<b>36</b>	<b>9</b>
<b>Weighting Factor</b>	<b>8</b>	<b>10</b>	<b>6</b>	<b>8</b>	<b>6</b>
<b>Weighted Benefit Score</b>	<b>296</b>	<b>300</b>	<b>216</b>	<b>288</b>	<b>54</b>
<b>Total Benefit Score</b>	<b>1154</b>				

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### **3.2.3 Benefit-Cost Ratio Analysis**

The total weighted benefit-cost ratio can be automatically calculated for alternatives based on the total costs and the weighted benefit scores. Two weighted benefit-cost ratios are calculated; one using capital costs and the other using total present worth costs. Each branch solution has unique benefit-cost ratios for each level of protection. Once the ratios are calculated, the alternatives require further review relative to overall program values and objectives to determine which alternative best fits the overall needs of the community. In addition to the five core values, other values were considered including: Customer Satisfaction, Economic Vitality, Environmental Justice and Equity, Financial Equity, Financial Stewardship, and Public Education.

Benefit-cost Ratio Analysis examples are presented for each individual watershed solution in the following section.

## **3.3 EVALUATION OF SSO ABATEMENT ALTERNATIVES**

The following sections summarize initial solutions considered for each modeled watershed, and the solution feasibility screening that included a thorough investigation of individual properties and sewer alignments in each branch (ground truthing). Additionally, modeled solution analyses including the benefit-cost procedure and the solution technology selected for each branch at the 1.82-inch cloudburst storm level are summarized for each modeled watershed. Appendix 3.1.2 contains the detailed ground truthing documents related to initial solutions. Appendix 3.3.1, Preferred Solution Cost Tables, Benefit-Cost Tables, Maps, Fact Sheets, contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

### **3.3.1 Cedar Creek Alternatives**

Details on branching and SSO descriptions for Cedar Creek can be found in Volume 3, Chapter 2, Section 2.5.1. The initial solution development process is summarized in detail in Sections 3.1.3 and 3.1.3.3 contains information on the ground truthing procedure.

#### **3.3.1.1 Initial Solutions and Feasibility Screening**

Initial solutions were investigated before any baseline conditions (i.e. Capital Projects) or RDI/I reduction were applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated and, therefore, is not summarized below.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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### Branch 70158

This branch includes SSOs caused by a hydraulic bottleneck. The land surrounding the SSOs includes homes that are approximately 100 feet away from the SSO location, which was the former location of the Idlewood WQTC.

The conveyance alternative considered was to build a parallel relief line or increase the existing interceptor size. Initial assessment showed enough room for a construction easement. The first storage alternative considered was to construct a wet weather storage facility near the SSO location. Based on ground truthing, the open land originally considered for the storage facility near the SSO site has development planned. The best location for a storage facility would require additional conveyance downstream approximately 500 feet away. The second storage alternative considered was to construct large pipe in the vicinity of the SSOs to provide inline storage. Ground truthing for inline storage found that 70 percent of the property is in the 100-year floodplain, and the utility conflicts would be minimal.

### Branch 81316

This branch includes SSOs caused by insufficient capacity at the Fairmount Road Pump Station to handle upstream flows. The surrounding area is residential but consists of ample open space.

The conveyance alternative considered upgrading the pump station. The first storage alternative considered was to construct a wet weather storage facility onsite. The second storage alternative considered was to construct large pipe in the vicinity of the SSOs to provide inline storage. Ground truthing for inline storage found that 80 percent of the property is in the 100-year floodplain and there is a potential utility conflict with an overhead electrical line.

### Branch 67997

This branch includes SSOs caused by insufficient capacity of the interceptor to handle upstream flows during wet weather. The conveyance alternative considered was to increase the existing interceptor pipe size. No storage alternatives were considered for this branch due to lack of available open land. Ground truthing for pipe upgrades found that 90 percent of the property is in the 100-year floodplain and potential utility conflicts may occur with electrical and gas line crossings.

### Branch MSD1025

This branch includes an SSO caused by insufficient capacity at the Bardstown Road Pump Station to handle upstream flows. This pump station was not reported as an SSO location until mid-2008; therefore, no initial solutions were developed for this location since it was not known at the time of initial solution development. Solutions, however, were developed later during the solution alternative analysis process discussed below.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Branch MSD1080

This branch includes an SSO caused by insufficient capacity at the Running Fox Pump Station to handle upstream flows. This SSO location was not reported as an SSO until mid-2008; therefore, no initial solutions were developed for the locations since they were not known at the time of initial solution development. Solutions, however, were developed later during the solution alternative analysis process.

**3.3.1.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in Cedar Creek. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and selection process. Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

Branch 70158

Based on the benefit-cost analysis, the chosen solution for Cedar Creek Branch 70158 is Inline Storage. Table 3.3.1 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.1  
 CEDAR CREEK BRANCH 70158 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_CC_CC_70158_M_09A_C	Inline Storage	Inline storage with 250 diameter (84" - 120") pipe to store wet weather peak flow, and upgrade 1,747 LF of (8" - 15") sewer to increase capacity capacity during wet weather peak flows.	24.66	31.36
S_CC_CC_70158_M_01_C	Pipe Upgrades	Upsize 8,218 LF of interceptor pipes.	5.76	7.26

**SSO Data Outdated  
 Refer to Chapter 5**

Branch 81316

The chosen solution for Cedar Creek Branch 81316 (Fairmount Rd. PS) is Pump Station Upgrades. The Pump Station Upgrades solution is a capital project known as the Fairmount Rd. Pump Station Expansion Project (E00303) which is currently planned to install three new pumps at Fairmount Rd. Pump Station. The new pumps are sized to accommodate future development per the Cedar Creek Action Plan. Table 3.3.2 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.2

**CEDAR CREEK BRANCH 81316 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_FF_CC_81316_M_03_C	PS Upgrades	Install (3) 130 HP, 1750 gpm pumps to increase capacity at the Fairmount Rd. Pump Station (Cedar Creek Action Plan)	26.79	26.79
S_FF_CC_81316_M_09A_C	Inline Storage	Offline storage with 283 LF of 72" pipe to store wet weather peak flow.	21.29	27.00

Branch 67997

The chosen solution for Cedar Creek Branch 67997 is Pipe Upgrades. As discussed earlier, the only solution considered for this branch was the conveyance alternative. Table 3.3.3 summarizes the solution and the benefit-cost ratio associated with that solution.

TABLE 3.3.3

**CEDAR CREEK BRANCH 67997 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_CC_CC_67997_M_01_C	Pipe Upgrades	Upsize 3,916 LF with (12" - 21") sewer pipe.	19.06	23.86

Branch MSD1025

Based on the benefit-cost analysis, the chosen solution for Cedar Creek Branch MSD1025 (Bardstown Rd. PS) is Pump Station Upgrades. Table 3.3.4 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.4

**CEDAR CREEK BRANCH MSD1025 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_CC_CC_MSD1025_S_03_C	PS Upgrades	Increase capacity of the Bardstown Rd. PS to handle peak flows of 0.39 mgd	34.40	29.42
S_CC_CC_MSD1025_S_09B_C	Offline Storage	Construct offline covered storage (0.166 MG) of 48" pipe (150' length) upstream of the Bardstown Rd. PS.	28.19	28.52
S_CC_CC_MSD1025_S_09A_C	Inline Storage	Inline storage with 283 LF of 72" pipe to store wet weather peak flow.	12.88	16.50

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Branch MSD1080

Based on the benefit-cost analysis, the chosen solution for Cedar Creek Branch MSD1080 (Running Fox PS) is Diversion. Table 3.3.5 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.5

CEDAR CREEK BRANCH MSD1080 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_CC_CC_MSD1080_S_01_C	Diversion	Construct 75" Force Main to eliminate Running Fox PS.	577.08	659.52
S_CC_CC_MSD1080_S_09A_C	Inline Storage	Inline storage with 400 LF of 60" pipe upstream of Running Fox PS to store wet weather peak flow.	86.72	108.82
S_CC_CC_MSD1080_S_09B_C	Offline Storage	Construct offline covered storage (.015 MG)	44.44	45.57
S_CC_CC_MSD1080_S_03_C	PS Upgrades	Increase the capacity of the Running Fox PS to handle peak flows of 0.4 mgd. Upsize 700 LF of force main to 6".	43.97	38.72

SSO Data Outdated  
 Refer to Chapter 5

**3.3.2 Floyds Fork Alternatives**

Details on branching and SSO descriptions for Floyds Fork can be found in Volume 3, Chapter 2, Section 2.5.2. The initial solution development process summarized in detail in Sections 3.1.3 and 3.1.3.3 contains information on the ground truthing procedure.

**3.3.2.1 Initial Solutions and Feasibility Screening**

Initial solutions were developed before any baseline conditions (i.e. Capital Projects) or RDI/I reduction had been applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated by one of the two and therefore is not summarized below.

Branch 1

This branch includes SSOs due to insufficient conveyance capacity and surcharged pipe during wet-weather events. The surrounding area is residential but includes some small open space.

The conveyance alternative considered was to increase the existing interceptor pipe size upstream of the Pope Lick Pump Station. The diversion alternative considered conveying more flow to the Woodland Hills Pump Station, and then on to the Morris Forman WQTC. The first

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

storage alternative considered was to construct a wet weather storage facility in the residential area. The second storage alternative considered was to construct large pipes in the vicinity of the SSOs to provide inline storage.

### Branch 2

This branch includes an SSO believed to be caused by a blockage at the Eden Care Pump Station that was cleared on March 18, 2006. The pump station is located in a small residential area.

The conveyance alternative considered was to upgrade the pump station and force main. The first storage alternative considered was to construct a wet weather storage facility near the SSO location but available land near the pump station is limited. The best location for a storage facility would require additional conveyance upstream approximately 600 feet. The second storage alternative considered was to construct large pipe in the vicinity of the SSOs to provide inline storage. Ground truthing for inline storage found that a small drainage ditch with riprap runs parallel to the gravity line and would most likely need to be replaced.

### Branch 3

This branch includes SSOs caused by insufficient capacity at both Olde Copper Court and Ashburton Pump Stations to handle upstream flows. The surrounding area is residential with some small wooded areas near the pump stations.

The diversion alternative considered was to divert flow from the Ashburton Pump Station to an alternate gravity system. The first storage alternative considered was to construct a wet weather storage facility near the Olde Copper Court Pump Station. The second storage alternative considered was to construct large pipe in the vicinity of the Olde Copper Court Pump Station to provide inline storage. The third storage alternative considered was to construct large pipe in the woods behind residences near the Ashburton Pump Station to provide inline storage.

Ground truthing identified that a threatened/endangered species assessment is recommended because construction will take place near the wooded area. It also found potential conflicts of force main construction with two electrical lines and one gas main, and gravity sewer construction with an electrical line. Other conflicts with force main construction reveals that it runs along a very steep hill and is located very close to an existing home (would need to be constructed under existing driveway).

### **3.3.2.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in Floyds Fork. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and selection process.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

Branch 1

Based on the benefit-cost analysis, the chosen solution for Floyds Fork Branch 1 is Diversion. Table 3.3.6 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.6

FLOYDS FORK BRANCH 1 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Costs)	Benefit/Cost Ratio (Present Worth Costs)
S_FF_FF_NB01_S_01_C_A	Diversion	Replace the existing gate (to the Woodland Hills PS) with a double barrel overflow that consists of two-15 LF 12" diameter pipes. The invert elevation of the pipes shall be 1" above the upstream invert of the exiting gravity pipe in manhole 82058. This new invert elevation will allow dry weather flow to gravity drain through the interceptor, but anything greater than dry weather flow will be diverted to the PS by an overflow pipe and reduce the surcharge further down the gravity line.	321.41	92.26
S_FF_FF_NB01_S_09A_C_A	Inline Storage	Inline storage with 400 LF and 110 LF of 48" pipes to store wet weather peak flow.	12.83	16.28
S_FF_FF_NB01_S_03_C_A	Pipe Upgrades	Upsize 1,650 LF of 15" sewer pipe with 18" sewer pipe.	10.84	13.60

Branch 2

The chosen solution for Floyds Fork Branch 2 (Eden Care PS) is Monitoring. The only overflow at this Pump Station occurred on March 18, 2006 and was believed to be caused by a blockage at the Eden Care Pump Station that was cleared on that date. Table 3.3.7 summarizes the solution chosen for Floyds Fork Branch 2.

TABLE 3.3.7

FLOYDS FORK BRANCH 2 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Costs)	Benefit/Cost Ratio (Present Worth Costs)
S_FF_FF_NB02_S_13_C	Monitor	Monitor the Eden Care PS during rain events for the next three years according to SORP protocols.	--	--

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**Branch 3**

Based on the benefit-cost analysis, the chosen solution for Floyds Fork Branch 3 (Ashburton PS / Olde Copper PS) is Pipe and Force Main Upgrades (A). Table 3.3.8 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.8**

**FLOYDS FORK BRANCH 3 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Costs)	Benefit/Cost Ratio (Present Worth Costs)
S_FF_FF_NB03_M_01_C_A	Upgrade Force Main & Pipes (A)	Divert flow from Ashburton PS by upgrading 370 LF of force main from 2" to 3" and construct 370 LF of gravity sewer, also eliminates the SSO at Olde Copper Ct PS.	150.66	161.00
S_FF_FF_NB03_M_03_C_B	Force Main Upgrades	Upgrade 200 LF of force main from 2.5" to 4" at Olde Copper Ct PS and 700 LF of force main from 2" to 3" at Ashburton PS.	111.57	106.61
S_FF_FF_NB03_M_HB_C_C	Upgrade Force Main & Pipes (B)	Eliminate Olde Copper Ct PS, construct 370 LF of 8" gravity sewer to divert flow to another part of the system, upgrade 700 LF of force main from 2" to 3" for Ashburton PS.	86.27	91.31
S_FF_FF_NB03_M_HB_C_B	Inline Storage & Upgrade Force Main (A)	Inline storage with 320 LF of 42" pipe at Olde Copper Ct PS, upgrade 700 LF of force main from 2" to 3" at Ashburton PS.	52.51	59.44
S_FF_FF_NB03_M_HB_C_A	Inline Storage & Upgrade Force Main (B)	Inline storage with 150 LF of 60" pipe at Olde Copper Ct PS, upgrade 700 LF of force main from 2" to 3" at Ashburton PS.	51.19	58.40
S_FF_FF_NB03_M_03_C_A	PS & Force Main Upgrades (A)	Upgrade both pumps at Olde Copper Ct PS for a combined 60 gpm to 100 gpm; upgrade 700 LF of force main from 2" to 3" at the Ashburton PS.	47.82	42.51
S_FF_FF_NB03_M_03_C_C	PS & Force Main Upgrades (B)	Upsize existing wet well from 4' to 8' diameter and pumps at Olde Copper Ct PS for a combined 60 gpm to 90 gpm, upgrade 700 LF of force main from 2" to 3" at Ashburton PS.	27.03	27.73

SSO Data Outdated  
Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 3.3.3 Hite Creek Alternatives

Details on branching and SSO descriptions for Hite Creek can be found in Volume 3, Chapter 2, Section 2.5.3. The initial solution development process is summarized in detail in Sections 3.1.3 and 3.1.3.3 contains information on the ground truthing procedure.

#### 3.3.3.1 Initial Solutions and Feasibility Screening

Initial solutions were investigated before any baseline conditions (i.e. Capital Projects) or RDI/I reduction had been applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated by one of the two and, therefore, is not summarized below.

##### Branch MSD1082

This branch includes SSOs caused by insufficient capacity at the Meadow Stream Pump Station to handle upstream flows. The surrounding area is a mix of single-family residential, multi-family residential, and light industrial. There is ample open space in the area.

The conveyance alternative considered either upsizing the force main or adding a wet weather force main and pump. The first storage alternative considered was to construct a wet weather storage facility in an open area near the SSO locations. The second storage alternative considered was to construct a large pipe in the vicinity of the SSOs to provide inline storage. Ground truthing found that a portion of the pump station property is in the 100-year floodplain but construction would take place outside of the floodplain.

##### Branch MSD1085

This branch includes an SSO caused by insufficient capacity at the Kavanaugh Road Pump Station to handle upstream flows. The surrounding area is residential with available open space.

The conveyance alternative considered upgrading the pump station. The first storage alternative considered was to construct a wet weather storage facility on residential property. The best location for a storage facility would require additional conveyance downstream approximately 200 feet. The second storage alternative considered was to construct large pipe in the vicinity of the SSO to provide inline storage. Ground truthing found a potential utility conflict with overhead electrical lines.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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### Branch MSD1086

This branch includes SSOs caused by insufficient capacity at the Floydsburg Road Pump Station to handle upstream flows. The surrounding area is industrial with some residential. There is some open space near the pump station and in a wooded area to the west.

The conveyance alternative considered upgrading the pump station. The storage alternative considered was to construct a wet weather storage facility on developed property. The best location for a storage facility would require additional conveyance downstream approximately 200 feet. Another alternative considered I/I reduction since the area is small (16 properties) and mostly industrial. Ground truthing at the pump station location found that the site is next to an electrical substation and several overhead and underground lines are onsite.

### Branches MSD1085/MSD1086

An alternative that would eliminate SSOs at both Floydsburg Road and Kavanaugh Road Pump Stations was also considered. This alternative consisted of eliminating Floydsburg Road and Kavanaugh Road Pump Stations and constructing interceptors to run south to a new pump station site to serve the whole Crestwood area. A force main would be constructed parallel to the Floydsburg Road Interceptor.

### **3.3.3.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in Hite Creek. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and selection process. Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

### Branch MSD1082

Based on the benefit-cost analysis, the chosen solution for Hite Creek Branch MSD1082 (Meadow Stream PS) is Inline Storage. Table 3.3.9 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.9

HITE CREEK BRANCH MSD1082 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_HC_HC_MSD1082_S_09A_C	Inline Storage	Inline storage with dual 120" parallel pipes to store wet weather peak flow.	10.77	13.77
S_HC_HC_MSD1082_S_09B_C	Overflow Storage	Construct overflow storage vault (0.2 MG).	8.67	8.85
S_HC_HC_MSD1082_S_03_C	PS & Force Main Upgrades	Increase the capacity of the Meadow Stream PS to handle peak flows of approximately 4.5 mgd, upgrade 15,395 LF to 18" force main.	3.14	2.77

**SSO Data Outdated  
Refer to Chapter 5**

Branch MSD1085

Based on the benefit-cost analysis, the chosen solution for Hite Creek Branch MSD1085 (Kavanaugh Rd. PS) is Pump Station and Force Main Upgrades. Table 3.3.10 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.10

HITE CREEK BRANCH MSD1085 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_HC_HC_MSD1085_S_03_C	PS & Force Main Upgrades	Increase the capacity of the Kavanaugh Rd. PS to handle peak flows of 0.674 mgd and upgrade 2,535 LF of force main.	19.46	19.77
S_HC_HC_MSD1085_S_09A_C	Inline Storage	Inline storage with dual 968 LF, 72" influent PS lines. Additional 2,243 LF of upsized sewer is required.	5.25	6.71

**SSO Data Outdated  
Refer to Chapter 5**

Branch MSD1086

The chosen solution for Hite Creek Branch MSD1086 (Floydsburg Rd. PS) is I/I Reduction. This solution was chosen as the recommended alternative since the contributing area is small and the pump station should have enough capacity based on design calculations. If I/I reduction is deemed unsuccessful in eliminating the SSO, then the next best alternative is Pump Station Upgrades. Table 3.3.11 summarizes the solutions considered and the benefit-cost ratios associated with each solution.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.11

HITE CREEK BRANCH MSD1086 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_HC_HC_MSD1086_M_07_C	I/I Reduction	This location is targeted for I/I source control (I/I rehab and private property program).	Cost only for Sanitary Sewer Evaluation Study (SSES) - no benefits calculated	
S_HC_HC_MSD1086_M_03_C	PS & Force Main Upgrades	Upgrade the capacity of the Floydburg Rd. PS to handle peak flows of 0.30 mgd and upgrade 1,183 LF of force main.	19.78	19.80

Branches MSD1085/MSD1086

The Regional Pump Station alternative was not a favorable solution for Hite Creek Branches MSD1085 and MSD1086 based on the benefit-cost analysis; therefore, no further evaluation occurred for this solution. Table 3.3.12 summarizes the solution considered and the associated benefit-cost ratio.

TABLE 3.3.12

HITE CREEK REGIONAL PUMP STATION SOLUTION ALTERNATIVE

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_HC_HC_CrestwoodPS_M_13_C	Regional PS	Eliminate Floydburg Road PS and Kavanaugh Road PS, construct interceptors to a new regional PS to serve the entire area. Construct 6,155 LF of force main parallel to Floydburg Road Interceptor. Additional 6,914 LF of new sewer construction required.	8.14	9.28

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### **3.3.4 Jeffersontown Area Alternatives**

Details on branching and SSO descriptions for Jeffersontown are in Volume 3, Chapter 2, Section 2.5.4. The initial solution development process is summarized in detail in Sections 3.1.3 and 3.1.3.3 contains information on the ground truthing procedure.

#### **3.3.4.1 Initial Solutions and Feasibility Screening**

Initial solutions were investigated before any baseline conditions (i.e. Capital Projects) or RDI/I reduction had been applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated by one of the two and, therefore, is not summarized below.

##### Branch 1

This branch includes SSOs caused by insufficient capacity of the interceptor, siphon and Jeffersontown WQTC to handle wet weather flows. The surrounding area is a mix of commercial, industrial, residential, and athletic facilities.

Numerous storage, conveyance and diversion alternatives were considered. Most alternatives required the replacement of the interceptor from the Grassland area to the Jeffersontown WQTC. Another alternative considered a pump station or storage facility in the Grassland area.

Ground truthing revealed that 10 percent of the gravity interceptor line from the Grassland area to the Jeffersontown WQTC lies within the 100-year floodplain, has significant steep slopes, and an endangered/threatened species assessment is recommended due to the wooded area. The proposed storage site and the pump station at the Jeffersontown WQTC location lie within the 100-year floodplain and very near Chenoweth Run stream.

##### Branch 1A

Branch 1A includes the SSOs at the Chippewa and Chenoweth Run Pump Stations, which had previously been considered in the initial alternatives for Branch 4. Both SSOs are caused by insufficient capacity at the pump stations to handle upstream flows. The surrounding area is residential with lot sizes of approximately one acre or less. There is a large undeveloped area to the south of the Chenoweth Run Pump Station.

The conveyance alternative considered upgrading the pump station and the force main. The storage alternative considered was to construct a wet weather storage facility in the area to the south of the SSO locations.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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## Branch 2

This branch includes SSOs caused by insufficient capacity of the interceptor downstream of Charlane Parkway and Dell Road. The surrounding area is a mix of commercial, single-family, and multi-family residential.

The conveyance alternative considered upsizing the interceptor. The storage alternative considered was to construct a wet weather storage facility in a grassy area east of SSO ID 28391 between the railroad tracks and the sewer. Ground truthing found several utility crossings and a creek located north of the conveyance alternative.

## Branch 3

This branch includes SSOs caused by insufficient capacity at the Raintree and Marian Court Pump Stations to handle upstream flows. The surrounding area is a mix of single-family and multi-family residential.

The conveyance alternative considered upgrading the pump stations. The storage alternative considered was to construct a wet weather storage facility at some undeveloped land to the northeast. An additional storage alternative could be under an existing commercial parking lot on Taylorsville Road. A diversion alternative included construction of new pipe to divert flows to an alternate system and eliminate the pump stations. Ground truthing found several utility crossings for the Marian Court Pump Station and Raintree Pump Station diversion alternative.

## Branch 4

This branch includes an SSO caused by insufficient capacity at the Monticello Place Pump Station to handle upstream flows. As discussed in the Branch 1A description, several SSO locations initially evaluated in the Branch 4 network are now included in the Branch 1 solutions. The Monticello Pump Station is the only SSO location that remains in Branch 4. The surrounding area is a mix of single-family and multi-family residential.

The conveyance alternative considered upgrading the pump station. The storage alternative considered was to construct a wet weather storage facility to the south of the pump station. A diversion alternative included construction of new pipe to divert flows to an alternate system and eliminate the pump station. Ground truthing for the diversion alternative found one underground utility crossing and a creek located near the site.

### **3.3.4.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in Jeffersontown WQTC Branch Network. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

selection process. Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

Branch 1

Based on the benefit-cost analysis, the chosen solution for Jeffersontown Branch 1 is Offline Storage and Pipe Upgrades as well as a new pump station to be constructed at the Jeffersontown WQTC site. This solution will eliminate the Jeffersontown WQTC. The alternative shown in the following table with the highest benefit-cost ratio initially assumed that the Jeffersontown WQTC would be available for upgrading. With the goal being to eliminate the Jeffersontown WQTC this alternative was not evaluated further. Table 3.3.13 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.13**

**JEFFERSONTOWN BRANCH 1 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Costs)	Benefit/ Cost Ratio (Present Worth Costs)
S_JT_JT_NB01_M_01_C_A	Offline Storage, PS Upgrades, WQTC Elimination	Upsize the interceptor (6,200 LF) from Grassland to the WQTC. Storage facility (5.7 MG) at the WQTC site and a PS with capacity of 10 mgd. 32,100 LF of 24" force main constructed to convey flows to the Hikes Lane Interceptor.	4.93	5.23
S_JT_JT_NB01_M_01_C_B	WQTC & Pipe Upgrades	Upsize the interceptor (6,200 LF) from Grassland to the WQTC and increase the capacity of the WQTC to 20 mgd (full plant upgrade).	12.01	11.81
S_JT_JT_NB01_M_01_C_C	WQTC Upgrades, Storage & Pipe Upgrades	Upsize the interceptor (6,200 LF) from Grassland to the WQTC. Storage facility (2.3 MG) at the WQTC site and a new PS with capacity of 10 mgd. 32,100 LF of 24" force main constructed to convey flows to the Hikes Lane Interceptor. Convey Chenoweth Hills WQTC and the pumped zone of Jeffersontown (J'town) to the Billtown Road Interceptor for diversion to Cedar Creek WQTC. Plant upgrades required at Cedar Creek WQTC.	3.29	No Present Worth analysis performed
S_JT_JT_NB01_01_C_D	WQTC Upgrades, Storage, & Pipe Upgrades	Upsize the interceptor (6,200 LF) from Grassland to the WQTC. Storage facility (2.3 MG) at the WQTC site and a new PS with capacity of 10 mgd. 8,000 LF of 24" to 30" force main installed to the Chenoweth Run PS. All J'town flow (including Chenoweth Hills WQTC) is diverted to Cedar Creek WQTC. Plant upgrades required at Cedar Creek WQTC.	2.60	No Present Worth analysis performed

**SSO Data Outdated  
Refer to Chapter 5**

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**Branch 1A**

Based on the benefit-cost analysis, the chosen solution for Jeffersontown Branch 1A is Pump Station and Force Main Upgrades and directs the flow from the Chenoweth Hills WQTC to the Chenoweth Run Pump Station. Each alternative in Branch 1A included the elimination of the Chenoweth Hills WQTC. Table 3.3.14 summarizes the solutions considered and the benefit-cost ratios associated with each solution; however, the costs for Branch 1A are incorporated into Branch 1.

**TABLE 3.3.14**

**JEFFERSONTOWN BRANCH 1A SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Costs)	Benefit/ Cost Ratio (Present Worth Costs)
S_JT_JT_NB01A_M_03_C	PS & Force Main Upgrades, WQTC Elimination	Upgrade Chenoweth Run PS to handle peak flow of 2.7 mgd and upsize 8,030 LF of force main to 12". Chenoweth Hills WQTC elimination. Upgrade Pipe to handle peak flow of 0.15 mgd. Install 1,995 LF of new 15" sewer and replace 600 LF of 8" with 18" sewer pipe for Chenoweth Hills WQTC diversion.	22.47	20.05
S_JT_JT_NB01A_M_09_C	Offline Storage & Pipe Upgrades	Construct offline wet weather storage facility (0.8 MG) at Chenoweth Run PS and Chenoweth Hills WQTC diversion with Chippewa PS upgrades.	11.66	12.24

SSO Data Outdated  
 Refer to Chapter 5

**Branch 2**

Based on the benefit-cost analysis, the chosen solution for Jeffersontown Branch 2 is Pipe Upgrades. Table 3.3.15 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.15**

**JEFFERSONTOWN BRANCH 2 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Costs)	Benefit/ Cost Ratio (Present Worth Costs)
S_JT_JT_NB02_M_01_C	Pipe Upgrades	Upsize interceptor downstream of Charlane and Dell Road SSOs with 4,000 LF of (10"-21") sewer.	25.01	31.35
S_JT_JT_NB02_M_09_C	Offline Storage	Construct and design and install offline storage facility (0.18 MG) near swimming pool site and storage facility (0.03 MG) at manhole 103647.	12.02	12.55

SSO Data Outdated  
 Refer to Chapter 5

**Branch 3**



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Based on the benefit-cost analysis, the chosen solution for Jeffersontown Branch 3 (Raintree PS / Marian Ct. PS) is Diversion and Pipe Upgrades. Table 3.3.16 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.16**

**JEFFERSONTOWN BRANCH 3 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Costs)	Benefit/ Cost Ratio (Present Worth Costs)
S_JT_JT_NB03_M_01_C	Diversion & Pipe Upgrades	Eliminate overflow from Marian Ct. and Raintree PS by installing 455 LF of 8" sewer from Marian Ct. PS and 400 LF of 8" sewer from Raintree PS to divert flows to the Southeast Diversion system, additional 2,000 LF of 8" sewer upgrades is required downstream of the PS diversions.	59.44	72.76
S_JT_JT_NB03_M_09_C	Offline Storage & Pipe Upgrades	Construct underground offline storage facility (0.007 MG) for Marian Ct PS, upgrade 928 LF of force main and pumps for Raintree PS to handle peak flow of 0.63 mgd, additional 2,530 LF of sewer upgrades downstream of the PS is required.	34.31	34.57
S_JT_JT_NB03_M_03_C	PS & Pipe Upgrades	Replace 878 LF of force main at Raintree PS, replace pumps at Marian Ct (to 0.3 mgd) PS and Raintree (to 0.6 mgd) PS, upsize 2,480 LF of gravity sewer downstream of the force main.	33.59	36.94

SSO Data Outdated  
 Refer to Chapter 5

**Branch 4**

Based on the benefit-cost analysis, the chosen solution for Jeffersontown Branch 4 (Monticello PS) is Diversion. Table 3.3.17 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.17**

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**JEFFERSONTOWN BRANCH 4 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Costs)	Benefit/Cost Ratio (Present Worth Costs)
S_JT_JT_NB04_M_01_C_C	Diversion	Eliminate Monticello PS by diverting to Derek R. Guthrie WQTC approximately 5 L to 8" sewer	39.43	48.90
S_JT_JT_NB04_M_03_C_C	PS Upgrades	Upgrade Monticello PS to handle peak flow of 0.75 mgd.	25.16	19.34
S_JT_JT_NB04_M_09_C_C	Offline Storage	Construct offline storage (0.053 MG) at Monticello PS.	8.83	8.59

SSO Data Outdated  
Refer to Chapter 5

**3.3.5 Middle Fork Alternatives**

Details on branching and SSO descriptions for Middle Fork can be found in Volume 3, Chapter 2, Section 2.5.5. The initial solution development process is summarized in detail in Sections 3.1.3 and 3.1.3.3 contains information on the ground truthing procedure.

**3.3.5.1 Initial Solutions and Feasibility Screening**

Initial solutions were investigated before any baseline conditions (i.e. Capital Projects) or RDI/I reduction had been applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated by one of the two and, therefore, is not summarized below.

Branch 1

This branch includes SSOs caused by insufficient capacity in the collection system and the Upper Middle Fork Pump Station to handle upstream flows. The surrounding area is mostly commercial and residential with some industrial areas in the vicinity. This Branch has been evaluated with Southeastern Diversion branches to include the costs of the Buechel Basin for various comparative analyses. Initially, alternatives for this area were developed with the review of the Interim SSDP solutions, namely the Hikes Lane Interceptor and Northern Ditch Interceptor.

Ground truthing was performed at six locations in the area. Three of the locations had property in the 100-year floodplain, and three locations showed potential utility conflicts. Ground truthing identified two sites where a threatened/endangered species assessment was recommended. Four sites contained a protected waterway and another location was identified as a potential wetland (hydric soil was found). Several creeks were noted in the areas near the investigated sites.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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#### Branch 4

This branch includes SSOs caused by insufficient capacity at Devondale, Goose Creek and Saurel Road Pump Stations to handle upstream flows. The surrounding area is primarily residential along with a large tract of farmland to the north, and a school to the east.

The conveyance alternative considered upgrading the Goose Creek, Devondale and Saurel Road Pump Stations and force mains. The storage alternative considered was to construct a wet weather storage facility on an undeveloped property adjacent to the pump station on the north and east. Additional storage sites are also available to the east on school property and to the west on undeveloped property.

Ground truthing was performed at four locations, and all had property in the 100-year floodplain. The Saurel Road force main location showed potential utility conflicts and the project could involve construction between existing homes within the easement.

#### Branch 6

This branch includes SSOs caused by insufficient capacity at Anchor Estates No. 1 and No. 2 Pump Stations, and Vannah Way Pump Station. The surrounding area is single-family residential.

The conveyance alternative considered upgrading the Anchor Estates No. 1, No. 2, and Vannah Way Pump Stations and force mains. The storage alternative considered was to construct large pipe to provide inline storage at Anchor Estates No. 1 and No. 2 Pump Stations. The diversion alternative considered constructing gravity lines to alternate systems to eliminate each of the three pump stations.

Ground truthing was performed at three locations in the area, and a creek was identified at the southern end of the projects. Two locations had property in the 100-year floodplain, and one site had a threatened/endangered species assessment that was recommended. One site identified a protected waterway in the vicinity.

#### Branch 7

This branch includes an SSO caused by insufficient wet weather capacity in the collection system due to excessive I/I. This SSO location was not reported as an SSO until mid-2008; therefore, no initial solutions were developed for the locations since they were not known at the time of initial solution development. Solutions, however, were developed later during the solution alternative analysis process.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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### **3.3.5.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in Middle Fork. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and selection process. Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

#### **Branch 1**

Based on the benefit-cost analysis, the chosen solution for Middle Fork Branch 1 is Offline Storage and Pipe Upgrades (A). This branch is one of the three branches requested to be re-evaluated at the 2.25-inch cloudburst level to ensure the validity of the technology selection approach at the 1.82-inch cloudburst level. Table 3.3.18(A) summarizes the solutions considered for the 1.82-inch cloudburst storm and the benefit-cost ratios associated with each solution. Table 3.3.18(B) summarizes the solutions considered for the 2.25-inch cloudburst storm and the benefit-cost ratios associated with each solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 3.3.18(A)**  
**MIDDLE FORK BRANCH 1 – 1.82-INCH SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_MISF_MF_NB01_M_01_C_A1	Offline Storage & Pipe Upgrades (A)	Construct 30" force main diversion to Hikes Lane Interceptor (10,200 LF), construct Middle Fork Relief Interceptor between Oxmoor Mall and Hikes Lane Middle Fork Lift Station (UMFLS), construct 1.9 MG covered facility near Car Wash Site and 17.3 MG facility at Buechel Site. 11,800 LF total new gravity pipe including Relief Interceptor, storage piping, and relief at manhole 15138.	1.14	1.26
S_MISF_MF_NB01_M_01_C_A2	Offline Storage & Pipe Upgrades (B)	Divert UMFLS to Hikes Lane Interceptor using capacity of existing pumps (no Middle Fork Interceptor required). Construct 17.3 MG storage facility at Buechel Site and 3.0 MG covered storage near Oxmoor Mall. 4,750 LF of additional gravity pipe improvements, 10,200 LF of force main.	1.06	1.15
S_MISF_MF_NB01_M_01_C_A3	Offline Storage & Pipe Upgrades (C)	Construct 30" force main diversion to Hikes Lane Interceptor (10,200 LF), construct Middle Fork Relief Interceptor between Oxmoor Mall and UMFLS, construct 3 MG covered facility at Cannons Lane site and 17.3 MG storage facility at Buechel site, 11,800 LF total new gravity pipe including Relief Interceptor, storage piping, and relief at manhole 15138.	1.05	1.16
S_MISF_MF_NB01_M_01_C_B1	PS & Pipe Upgrades with Offline Storage	Divert all necessary flow through UMFLS to Hikes Lane Interceptor by upgrading pumps to convey peak discharge in diversion, construct 20.5 MG storage at Buechel Site, and construct 36" force main diversion to Hikes Lane Interceptor, 11,800 LF total new gravity pipe including Relief Interceptor, storage piping, and relief at manhole 15138., 10,200 LF of force main.	0.84	0.93

SSO Data Outdated  
 Refer to Chapter 5



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.18(B)

MIDDLE FORK BRANCH 1 – 2.25-INCH SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/Cost Ratio (Capital Cost)	Benefit/Cost Ratio (Present Worth)
S_MISF_MF_NB01_M_01_B_A1	Offline Storage & Pipe Upgrades (A)	Construct 30" force main diversion to Hikes Lane Interceptor (10,200 LF), construct Middle Fork Relief Interceptor between Oxmoor Mall and UMFLS, construct 7.9 MG covered facility near Car Wash Site and 30.1 MG facility at Buechel Site, 16,900 LF total new gravity pipe including Relief Interceptor, storage piping, and relief at manhole 15138.	0.96	1.07
S_MISF_MF_NB01_M_01_B_B1	PS & Pipe Upgrades with Offline Storage	Divert all necessary flow through UMFLS to Hikes Lane Interceptor by upgrading pumps to convey peak discharge in diversion, construct 57.2 MG storage at Buechel Site, and construct 36" force main diversion to Hikes Lane Interceptor, 16,900 LF total new gravity pipe including Relief Interceptor, storage piping, and relief at manhole 15138., 10,200 LF of force main.	0.95	1.06
S_MISF_MF_NB01_M_01_B_A2	Offline Storage & Pipe Upgrades (B)	Divert UMFLS to Hikes Lane Interceptor using capacity of existing pumps (no Middle Fork Interceptor required). Construct 43.1 MG storage facility at Buechel Site and 8.5 MG covered storage near Oxmoor Mall. 5,900 LF of additional gravity pipe improvements, 10,200 LF of force main.	0.95	1.03
S_MISF_MF_NB01_M_01_B_A3	Offline Storage & Pipe Upgrades (C)	Construct 30" force main diversion to Hikes Lane Interceptor (10,200 LF), construct Middle Fork Relief Interceptor between Oxmoor Mall and UMFLS, construct 11.3 MG covered facility at Cannons Lane site and 34 MG storage facility at Buechel site, 25,800 LF total new gravity pipe including Relief Interceptor, storage piping, and relief at manhole 15138.	0.74	0.83

SSO Data Outdated  
Refer to Chapter 5

As indicated in the table, the Offline Storage and Pipe Upgrades (A) alternative had the best benefit-cost ratio, independent of level of control. It can be noted that the Pump Station and Pipe Upgrades with Offline Storage changed from the worst benefit-cost ratio at the 1.82-inch level to the second best benefit-cost ratio at the 2.25-inch level. The other three alternatives used underground, covered storage which increased in cost significantly at the higher storm level. The Pump Station and Pipe Upgrades with Offline Storage assumed an open, earthen facility which has a lower incremental cost to expand. A detailed evaluation of the odor

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

generating potential was not conducted for this technology screening step, but there is a high potential that depending on the final site selected for the storage facility, the larger facility needed to contain the 2.25-inch rain could exceed the criteria established for uncovered facilities, thus increasing the cost considerably for this alternative.

**Branch 4**

Based on the benefit-cost analysis, the chosen solution for Middle Fork Branch 4 (Devondale, Goose Creek, and Saurel Rd. PSs) is Storage and Force Main Upgrades. Table 3.3.19 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.19**

**MIDDLE FORK BRANCH 4 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/Cost Ratio (Capital Cost)	Benefit/Cost Ratio (Present Worth)
S_MI_MF_NB04_M_03_B_A	Offline Storage, PS & Force Main Upgrades	Construct 0.19 MG offline storage facility near Devondale PS. Upsize 16" portion of force main at Goose Creek PS to 20" force main. Upgrade Goose Creek PS to 7.2 mgd. Replace Saurel Rd force main with 6" force main. Upsize a total of 5,300 LF of force main.	10.78	11.00
S_MI_MF_NB04_M_09B_B	Inline and Offline Storage	Construct offline covered storage at Devondale PS (0.48 MG) and Goose Creek PS (0.19 MG). Inline storage with 72" pipe to store wet weather peak flow at Saurel Road PS.	9.04	9.17
S_MI_MF_NB04_M_03_B	Force Main & PS Upgrades	Upgrade the Devondale PS to handle peak flow of 1.5 mgd, upsize the force main to an 8" force main, and upsize downstream gravity pipes to 12" and 15" (5,710 LF). Upsize the 16" portion of Goose Creek force main to a 20" force main, and upgrade the PS to 7.2 mgd. Upsize 4" Saurel Rd force main to a 6" force main.	8.66	8.71

**SSO Data Outdated  
Refer to Chapter 5**

**Branch 6**

The chosen solution for Middle Fork Branch 6 (Anchor Estates No. 1 and 2 Pump Stations / Vannah Way Pump Station) is Diversion. This alternative was chosen because it eliminates three pump stations and has the potential for cost sharing with developers planning for new future connections in a currently un-sewered area. Table 3.3.20 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

September 30, 2009  
2012 Modification: May 2014

TABLE 3.3.20

MIDDLE FORK BRANCH 6 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_MI_MF_NB06_M_01_C_A	Diversion	Construct 9,779 LF of 8" to 10" diversion gravity pipe to eliminate SSES at Anchor Estates No. 1 and No. 2 PSs, and Vannah Way PS. SSES upstream of Anchor Estates No. 2 PS.	20.86	25.39
S_MI_MF_NB06_M_01_C_C	Inline Storage & Diversion (A)	Construct 3,900 LF of diversion gravity pipe to eliminate Vannah Way and Anchor Estates No. 1 PS, and construct 150 LF of 72" pipe at Anchor Estates No. 2 PS to provide inline storage	32.27	39.83
S_MI_MF_NB06_M_09_C	Inline Storage & Diversion (B)	Diversion pipe to eliminate Vannah Way PS, 150 LF of 72" pipe (at Anchor Estates No. 2 PS) and 300 LF of 72" pipe (at Anchor Estates No. 1 PS) to provide inline storage.	27.70	35.43
S_MI_MF_NB06_M_01_C_B	PS Upgrades & Diversion	Construct 3,950 LF of 8" diversion gravity pipes to eliminate Vannah Way and Anchor Estates No. 1 PSs, and Anchor Estates No. 2 PS upgrades with flow diverted to Vannah PS diversion.	20.10	23.05
S_MI_MF_NB06_M_03_C	PS Upgrades	Upgrade all PSs, upsize 2,300 LF of force main, upsize 2,300 LF of downstream collector sewers.	5.34	6.11

Branch 7

The chosen solution for Middle Fork Branch 7 is I/I Reduction. This solution was chosen as the recommended alternative based on modeling results. An overflow did not occur at this manhole in the existing conditions model at the 1.82-inch or 2.25-inch cloudburst storm indicating excessive I/I during heavy rainfall is likely the problem. Table 3.3.21 summarizes the solution considered.

TABLE 3.3.21

MIDDLE FORK BRANCH 7 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_MI_MF_NB07_S_07_C	I/I Reduction	This location is targeted for I/I source control (I/I rehab and private property program)	Cost only for SSES - no benefits calculated.	

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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### **3.3.6 Southeastern Diversion Alternatives**

Details on branching and SSO descriptions for Southeastern Diversion can be found in Volume 3, Chapter 2, Section 2.5.6. The initial solution development process is summarized in detail in Sections 3.1.3 and 3.1.3.3 contains information on the ground truthing procedure.

#### **3.3.6.1 Initial Solutions and Feasibility Screening**

Initial solutions were investigated before any baseline conditions (i.e. Capital Projects) or RDI/I reduction had been applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated by one of the two and, therefore, is not summarized below.

##### Branch 3

This branch includes an SSO caused by insufficient capacity of the interceptor to handle upstream flows during wet weather. The surrounding area is a mix of single-family residential, multi-family residential, and light industrial.

The conveyance alternative considered was to upsize the interceptor. The first storage alternative considered was to construct a wet weather storage facility on land at the upper end of the industrial area or behind the school property. The second storage alternative considered was to construct large pipe in the vicinity of the SSOs to provide inline storage.

Ground truthing at the storage location and along the Rustic Way corridor found hydric soil which may classify the area as a potential wetland site. Additionally, the locations were recommended for a threatened/endangered species assessment.

##### Branch 4

This branch includes an SSO caused by insufficient capacity of the system to handle upstream flows during wet weather. The surrounding area is single-family residential.

The conveyance alternative considered was to construct a relief sewer from the SSO at Alcona Lane to the new Hikes Lane Interceptor. The storage alternative considered was to construct a wet weather storage facility on the school property adjacent to the SSO location.

Ground truthing for the conveyance alternative found the alignment is 100 percent within the 100-year floodplain and a Louisville and Jefferson County Information Consortium (LOJIC) sensitive feature tool identified a protected waterway. A threatened/endangered species assessment was recommended because a portion of the construction would take place adjacent to a stream. Potential utility conflicts identified include water service replacements.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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### Branch 5

This branch includes an SSO caused by insufficient capacity of the interceptor to handle upstream flows during wet weather. The surrounding area is single-family residential.

The conveyance alternative considered was to upsize the interceptor behind homes on Sutherland Drive. The first storage alternative considered was to construct a wet weather storage facility on the school property to the south of the SSO locations. The second storage alternative considered was to construct large pipe in the vicinity of the SSOs to provide inline storage.

Ground truthing for the conveyance alternative found the property is 45 percent within the 100-year floodplain and a LOJIC sensitive feature tool identified a protected waterway. The Beargrass Creek was identified at the south end of the project.

### Branch 6

This branch includes an SSO caused by backwater in the Beargrass Interceptor due to obstructions in the sewer line. No initial solutions were developed for this location. This SSO is targeted for interceptor rehabilitation to remove obstructions in the downstream 42" interceptor.

### **3.3.6.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in the Southeastern Diversion area. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and selection process. Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

### Branch 3

The chosen solution for Southeastern Diversion Branch 3 is I/I Reduction. This solution was chosen as the recommended alternative since the contributing area is small and the interceptor should contain enough capacity based on design calculations. If infiltration reduction is deemed unsuccessful in eliminating the SSO, then the next best alternative is Pipe Upgrades. This solution is more desirable than the storage solution due to the proximity of the nearby school. Table 3.3.22 summarizes the solutions considered and the benefit-cost ratios associated with each solution.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 3.3.22**

**SOUTHEASTERN DIVERSION BRANCH 3 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_SD_MF_NB03_S_07_C	I/I Reduction	This solution is targeted for overflow control (I/I rehab and private property program).	Cost only for SSES - no benefits calculated.	
S_SD_MF_NB03_S_09B_C	Offline Storage	Construct offline storage (0.984 MG) storage capacity adjacent to SSO.	22.76	22.88
S_SD_MF_NB03_S_01_C	Pipe Upgrades	Construct 2,394 LF of 10" relief sewer that parallels the existing sewer along Rustic Way.	17.14	21.23
S_SD_MF_NB03_S_09A_C	Inline Storage	Construct 752 LF of 60" sewer from manhole 19320 to 47252 and 497 LF of 42" sewer from manhole 47252 to 27280 to provide inline storage.	10.62	13.48

SSO Data Outdated  
 Refer to Chapter 5

Branch 4

The solution for the Southeastern Diversion Branch 4 is Pipe Upgrades. This solution involves a 30" gravity interceptor connecting to the Hikes Lane Interceptor where the Jeffersontown Branch 1 24" force main solution connects to the Hikes Lane Interceptor. The Southeastern Diversion Branch 4 solution was priced with a 30" gravity interceptor constructed to the Hikes Lane Interceptor minus the cost of the 24" Jeffersontown force main along the same route. Table 3.3.23 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.23**

**SOUTHEASTERN DIVERSION BRANCH 4 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_SD_MF_NB04_S_01_C_A	Pipe Upgrades	Construct 2,800 LF of 30" gravity interceptor connecting the Jeffersontown Branch 1 24" force main to the Hikes Lane Interceptor.	6.21	9.11
S_SD_MF_NB04_S_01_C_B	Pipe Upgrades	Construct 2,830 LF of 12" relief interceptor.	3.47	4.35
S_SD_MF_NB04_S_09B_C	Offline Storage	Construct a covered 0.12 MG offline storage facility in the school property adjacent to the SSO.	1.21	1.21

SSO Data Outdated  
 Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### Branch 5

Based on the benefit-cost analysis, the chosen solution for Southeastern Diversion Branch 5 is Pipe Upgrades. Table 3.3.24 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.24

SOUTHEASTERN DIVERSION BRANCH 5 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_SD_MF_NB05_M_01_C	Pipe Upgrades	Upsize 1,760 LF of gravity pipe from 10" to 15" along rear yards.	20.54	25.22
S_SD_MF_NB05_M_09B_C	Offline Storage	Construct 620 LF of 60" sewer storage in an open field on school property.	18.10	18.10
S_SD_MF_NB05_M_09A_C	Inline Storage	Construct 620 LF of 60" sewer downstream of manhole ID 16649 to provide inline storage.	16.03	20.34

**SSO Data Outdated  
Refer to Chapter 5**

### Branch 6

The chosen solution for Southeastern Diversion Branch 6 is Pipe Rehab. This is based on findings during the Interceptor Condition Assessment Phase 1. Table 3.3.25 summarizes the solution considered.

TABLE 3.3.25

SOUTHEASTERN DIVERSION BRANCH 6 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_SD_MF_NB06_S_13_C	Pipe Rehab	Heavily clean 2,800 LF of 42" intercepter.	Cost only for Maintenance - no benefits calculated.	

**SSO Data Outdated  
Refer to Chapter 5**

### 3.3.7 Ohio River Force Main (ORFM) Alternatives

Details on branching and SSO descriptions for ORFM can be found in Volume 3, Chapter 2, Section 2.5.7. The initial solution development process is summarized in detail in Sections 3.1.3 and 3.1.3.3 contains information on the ground truthing procedure.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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### **3.3.7.1 Initial Solutions and Feasibility Screening**

Initial solutions were investigated before any baseline conditions (i.e. Capital Projects) or RDI/I reduction had been applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated by one of the two and, therefore, is not summarized below.

#### **Branch 1**

This branch includes SSOs caused by insufficient capacity at pump stations in residential neighborhoods to handle upstream flows. Each pump station location was analyzed separately.

Many of the pump stations had available space for onsite storage alternatives. The conveyance alternatives considered would include pump station upgrades as well as pipe upgrades. The diversion alternatives involved elimination of pump stations by constructing new pipe to alternate systems.

Ground truthing was performed at six locations. Four of the locations include property in the 100-year floodplain. Two locations had a threatened/endangered species assessment recommended and two locations found potential utility conflicts with water lines. One location is located 70 percent in a golf course, and another location is located east of a creek. The Mockingbird Pump Station diversion location has potential steep slope and is in a Floodplain Management Ordinance review zone. The Mellwood Pump Station ground truthing noted a protected waterway. The Mellwood Pump Station force main project has numerous water lines to cross at Zorn Avenue.

#### **Branch 2**

This branch includes an SSO caused by a hydraulic bottleneck of two 8" pipes flowing into one 8" pipe. The surrounding area is single-family residential.

The conveyance alternative considered was to increase the existing pipe size downstream of the SSO. The storage alternative considered was to construct a wet weather storage facility behind residential lots due to lack of available land.

#### **Branch 3**

This branch includes an SSO caused by insufficient capacity at the Derington Court Pump Station to handle upstream flows. The surrounding area is single-family residential.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

The conveyance alternative considered upgrading the pump station. The first storage alternative considered was to construct a wet weather storage facility in an area adjacent to the SSO. The second storage alternative considered was to construct large pipe in the vicinity of the SSO to provide inline storage.

Ground truthing at the pump station property found that 10 percent of the property is in the 100-year floodplain and a sensitive feature was identified as a protected waterway southwest of the pump station. Ground truthing for offline storage found that 100 percent of the property is in the 100-year floodplain. A threatened/endangered species assessment was recommended.

#### Branch 4

This branch includes SSOs caused by insufficient capacity at pump stations in residential neighborhoods to handle upstream flows. Each pump station location was analyzed separately.

The conveyance alternatives considered would include pump station upgrades. The storage alternatives considered offline storage facilities in areas adjacent to the SSOs.

Ground truthing was performed at six locations. Five of the locations had properties in the 100-year floodplain. Two locations had a threatened/endangered species assessment recommended and many stream crossings were found in the area.

#### **3.3.7.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in ORFM. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and selection process. Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

#### Branch 1

Based on the benefit-cost analysis, the chosen solution for ORFM Branch 1 is Pump Station and Pipe Upgrades and Diversion. The Winton Avenue Pump Station and Mockingbird Valley Pump Station will be eliminated by the project. Table 3.3.26 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.26

ORFM BRANCH 1 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/Cost Ratio (Capital Cost)	Benefit/Cost Ratio (Present Worth)
S_OR_MF_NB01_M_01_C	PS Upgrades, Pipe Upgrades, Diversion	Replace 1,760 LF of gravity sewer flowing into Mockingbird Valley PS, upgrade Mellwood Ave PS to handle peak flow of 2.5 mgd and flood-proof PS, upsize approximately 1,240 LF of 6" force main with 12" force main for Mellwood Ave PS, and install 400 LF of 8" pipe for Winton PS diversion and 2,210 LF of 15" pipe for Mockingbird Valley PS diversion to alternate systems.	21.11	25.09
S_OR_MF_NB01_M_03_C	PS Upgrades & Pipe Upgrades	Replace 1,890 LF of gravity sewer flowing into Mockingbird Valley PS, upgrade pumps at Mockingbird Valley PS and Winton PS, total PS upgrade at Mellwood Ave PS, upsize 2,000 LF of force main for Mockingbird Valley PS, and upsize 1,240 LF of force main for Mellwood Ave PS.	19.55	22.90
S_OR_MF_NB01_M_09_C	Pipe Upgrades & Storage	Replace 200 LF of gravity sewer flowing into the storage area for Mockingbird Valley PS, divert Winton PS, construct 0.12 MG pumped storage facility at Mockingbird Valley PS, and construct 0.15 MG covered storage facility at Mellwood Ave PS.	14.27	15.38
S_OR_MF_NB01_M_01_C_A	Diversion, Pipe Upgrades & Storage	Replace 685 LF of 10" gravity sewer, construct 875 LF of 12" relief sewer, and 200 LF of 15" relief sewer for Mockingbird Valley PS. Additional upgrade of storage at Mellwood Ave PS to 1 MG (flood-proofed). Installation of 400 LF of 8" pipe for Winton PS diversion and 2,210 LF of 15" pipe for Mockingbird Valley PS diversion to alternate systems.	8.42	9.31

Branch 2

The chosen solution for ORFM Branch 2 is Condition Assessment. This solution was chosen because cleaning/flushing has occurred twice since March 2006 (the last documented overflow date) at this location and no additional overflows have been reported since that date. Table 3.3.27 the solutions considered and the benefit-cost ratios associated with each solution.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.27

ORFM BRANCH 2 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_OR_MF_NB02_S_13_C	Condition Assessment	Perform periodic condition assessment (I/I and Wet Weather Monitoring) for three years to determine if SSO has been eliminated.	--	--
S_OR_MF_NB02_S_01_B	Pipe Upgrades	Construct 325 LF of 8" relief sewer.	85.67	102.80
S_OR_MF_NB02_S_09_B	Offline Storage	Construct offline covered pumped storage (0.048 MG) along the gravity sewer in the rear of homes on Leland Ave.	12.74	11.45

**SSO Data Outdated  
 Refer to Chapter 5**

Branch 3

The chosen solution for ORFM Branch 3 (Derington Ct. PS) is I/I Reduction. This solution was chosen as the recommended alternative due to the small contributing area and difficult surrounding conditions (steep slopes and lack of available storage sites). If I/I reduction is deemed unsuccessful in eliminating the SSO, the next best solution will be inline storage (based on Present Worth Benefit Cost ratio). Table 3.3.28 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.28

ORFM BRANCH 3 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_OR_MF_NB03_S_07_C	I/I Reduction	The solution targeted for the SSO control (I/I rehab and private property program).	Cost only for SSES - no benefits calculated.	
S_OR_MF_NB03_09_C_B	Offline Storage	Construct offline covered storage facility (0.16 MG) between the sewer pavement of Derington Court and the creek.	43.48	20.75
S_OR_MF_NB03_09_C_A	Inline Storage	Install 285 LF of 60" pipe parallel to the 8" gravity upstream of Derington Court PS to provide inline storage.	16.85	21.49
S_OR_MF_NB03_03_C	PS Upgrades	Upsize pumps at Derington Court PS, upsize 460 LF of force main from 4" to 6".	16.24	13.68

**SSO Data Outdated  
 Refer to Chapter 5**

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Branch 4

Based on the benefit-cost analysis, the chosen solution for ORFM Branch 4 is Pump Station and Pipe Upgrades and WQTC Elimination. This solution includes the elimination of five Prospect WQTCs. These solutions include the cost for a new Harrods Creek Pump Station but do not include the cost for additional treatment at Hite Creek WQTC. Table 3.3.29 summarizes the solutions considered and the benefit-cost ratios associated with each solution. A present worth analysis was not performed for these solutions.

TABLE 3.3.29

ORFM BRANCH 4 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_OR_MF_NB04_M_03_B_B	PS & Pipe Upgrades, WQTC Elimination	Upsize 8,300 LF of interceptor upstream of Muddy Fork PS. Upgrade pumps at Muddy Fork, Winding Falls/Phoenix Hill PS, and New Market PS. Upsize force main from Muddy Fork PS from 14" to a 24". Construct 22,000 LF of 24" force main from Harrods Creek PS and 24,000 LF of 24" force main to pump flow to Hite Creek WQTC. The solution includes the elimination of the 5 Prospect WQTCs: Hunting Creek North, Hunting Creek South, Timberlake, Ken Carla, and Shadow Wood.	2.46	No Present Worth Analysis performed
S_OR_MF_NB04_M_01_B_B	Storage & PS Upgrades (A)	Construct covered storage facilities at Barbour Lane PS. Additional upsizing of interceptor upstream of Muddy Fork PS. Upgrade pumps at New Market PS.	1.94	No Present Worth Analysis performed
S_OR_MF_NB04_M_09_B_B2	PS & Force Main Upgrades	Construct additional 18" barrel for the ORFM from Muddy Fork PS to the outfall of the ORFM. This additional barrel would isolate Muddy Fork flow. Additional upsizing of interceptor required upstream of Muddy Fork PS. Upgrade pumps at Muddy Fork and New Market PSs. Upsize force main from Muddy Fork PS from 14" to an 18".	1.45	No Present Worth Analysis performed
S_OR_MF_NB04_M_09_B_B1	Storage & PS Upgrades (B)	Construct covered storage facilities at Muddy Fork PS and Winding Falls/Phoenix Hill PS. Additional upsizing of interceptor upstream of Muddy Fork PS. Upgrade pumps at New Market PS.	1.19	No Present Worth Analysis performed

SSO Data Outdated  
Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### **3.3.8 CSO Area Alternatives**

Details on branching and SSO descriptions for the CSO area can be found in Volume 3, Chapter 2, Section 2.5.8. The initial solution development process is summarized in detail in Sections 3.1.3 and 3.1.3.3 contain information on the ground truthing procedure.

#### **3.3.8.1 Initial Solutions and Feasibility Screening**

Initial solutions were investigated before any baseline conditions (i.e. Capital Projects) or RDI/I reduction had been applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated by one of the two and therefore is not summarized.

##### Branch 30917

This branch includes SSOs caused by insufficient capacity in the collection system in the Camp Taylor neighborhood. The land surrounding the SSOs consists of single-family and multi-family residential.

The first conveyance alternative considered replacing the entire sewer system with approximately 47,000 LF of new sewer pipe. The second conveyance alternative considered building a relief sewer to convey excess wet weather flow from documented SSOs to the downstream interceptor. The storage alternative considered construction of offline storage facilities to store excess wet weather flow. Due to the age and condition of the system, a storage option alone was not viable. Another alternative considered performing an SSES to better define the problem and target the isolated problem area.

##### Branch 42007

This branch includes an SSO caused most likely by insufficient capacity at the Sonne Avenue Pump Station to handle excess wet weather flow and cross connections in the Sonne Avenue Pump Station area. The surrounding area is residential and industrial and is near electrical utilities.

The conveyance alternative considered upgrading the Sonne Avenue Pump Station to handle excess wet weather flow and convey flow to the downstream combined sewer system. The storage alternative considered construction of an offline storage facility at the adjacent property.

Ground truthing found a potential utility conflict at the pump station location with electrical and gas laterals nearby.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Branch 55665

This branch includes an SSO caused most likely by insufficient capacity at the Hazelwood Pump Station to handle excess wet weather flow. This pump station was not reported as an SSO location until mid-2008; therefore, no initial solutions were developed for this location since it was not known at the time of initial solution development. Solutions, however, were developed later during the solution alternative analysis process.

**3.3.8.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in the CSO area. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and selection process. Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

Branch 30917

Based on the benefit-cost analysis, the chosen solution for CSO Branch 30917 (Camp Taylor Neighborhood) is SSES, Rehabilitation, and Replacement. The chosen solution will include a full SSES to target sewers for replacement. Table 3.3.30 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.30**

**CSO BRANCH 30917 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_SF_MF_30917_M_09_C	SSES, Sewer Rehabilitation/ Replacement, Offline Storage	Replace and rehabilitate targeted sewer pipe after full SSES of the Camp Taylor area. Construct a pump and flow to sewer storage facility to store excess wet weather flows, additional 3,395 LF of 8" pipe required to convey flow to the facility.	69.19	65.12
S_SF_MF_30917_M_12_A_A	System Replacement	Construct approximately 46,786 LF of new sanitary sewer pipe (8" - 15") to replace existing system.	7.18	9.05

SSO Data Outdated  
Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Branch 42007

The chosen solution for CSO Branch 42007 (Sonne PS) is I/I Reduction. This solution was chosen as the recommended alternative due to the small contributing area and the fact that the area is located in the combined sewer system area and likely contains numerous cross connections. If I/I reduction is deemed unsuccessful in eliminating the SSO, the next best alternative is Offline Storage. Table 3.3.31 summarizes the solution and benefit-cost ratio associated with the solution.

TABLE 3.3.31

CSO BRANCH 42007 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_OR_MF_42007_S_07_C	I/I Reduction	This location is targeted for I/I source control (I/I rehab and private property program)	Cost only for SSES - no benefits calculated.	
S_OR_MF_42007_S_09_C	Offline Storage	Construct offline covered pumped storage facility (0.9 MGD) to store excess wet weather flows.	19.53	15.53
S_OR_MF_42007_S_03_C	PS Upgrades	Expand wet well from 6' to 12' diameter at the Sonne PS and upgrade PS to handle peak flow of 1.7 mgd.	9.26	10.12

Branch 55665

The chosen solution for CSO Branch 55665 (Hazelwood PS) is I/I Reduction. This solution was chosen as the recommended alternative due to the small contributing area and the fact that the area is located in the combined sewer system area and most likely contains numerous cross connections. If I/I reduction is deemed unsuccessful in eliminating the SSO, the next best alternative is Offline Storage and Pipe Upgrades. Table 3.3.32 summarizes the solution and the benefit-cost ratio associated with that solution.

TABLE 3.3.32

CSO BRANCH 55665 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_MC_MF_55665_S_07_C	I/I Reduction	This location is targeted for source control (I/I rehab and private property program).	Cost only for SSES - no benefits calculated.	
S_MC_MF_55665_S_13_C_B	Offline Storage & Pipe Upgrades	Construct offline covered storage facility (0.49 MGD) to store excess wet weather flows and upsize 1,858 LF of 8" pipe to (12"-18")	10.98	11.60



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 3.3.9 Small WQTC Area Alternatives

Details on branching and SSO descriptions for the Small WQTC areas can be found in Volume 3, Chapter 2, Section 2.5.9. The initial solution development process is summarized in detail in Sections 3.1.3 and 3.1.3.3 contains information on the ground truthing procedure.

#### 3.3.9.1 Initial Solutions and Feasibility Screening

Initial solutions were investigated before any baseline conditions (i.e. Capital Projects) or RDI/I reduction had been applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated by one of the two and therefore is not summarized.

##### Berrytown Branch 1

This branch includes an SSO caused by insufficient capacity at the Lucas Lane Lift Station (LS) to handle upstream flows. With the exception of a few residences, the area surrounding the SSO is mostly open space and is adjacent to Goose Creek.

The conveyance alternative considered upgrading the wet well, pump station, and force main. The storage alternative considered constructing large pipe in the vicinity of the SSOs to provide inline storage. The diversion alternative considered diverting flow to the Morris Forman WQTC through a force main. However, numerous utility lines would need to be avoided.

Ground truthing found a significant topographical feature identified as a drainage ditch that runs the length of the last two gravity sewer pipes upstream of the Lift Station. There are several trees growing above or very near the existing gravity sewer (sewer is currently scheduled to be replaced) potentially making replacement very difficult, and a resident's retaining wall is within ten feet of the proposed construction. The retaining wall would not impede construction of the proposed storage facility and the offline storage alternative would not require replacement of the entire sewer.

##### Chenoweth Hills Branch 1

This branch initially included an SSO located at the Chenoweth Hills WQTC caused by upstream flows greater than the WQTC capacity. The surrounding area is single-family residential. After initial solutions were investigated, it was found that the Chenoweth Hills WQTC location could be incorporated into the Jeffersontown Branch 1A solution. The SSO addressed by this branch is now the St. Rene Road Pump Station. This pump station was not reported as an SSO location until mid-2008; therefore, no initial solutions were developed for this location since it was not known at the time of initial solution development. Solutions, however, were developed later during the solution alternative analysis process.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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### Hunting Creek North Branch 1

This branch includes an SSO caused by insufficient capacity at the Riding Ridge Pump Station to handle upstream flows. The surrounding area is primarily residential with wooded and green space.

The conveyance alternative considered upgrading the wet well, pump station, and force main. Storage alternatives included constructing storage facilities in wooded areas near the SSO. Another storage alternative considered was to construct a large pipe in the vicinity of the SSO to provide inline storage. Ground truthing found an overhead electrical line runs near the pump station but is not in the potential area for a storage facility.

### Hunting Creek North Branch 2

This branch includes an SSO caused by insufficient capacity at the Gunpowder Pump Station to handle upstream flows. The surrounding area is primarily residential.

The conveyance alternative considered upgrading the wet well, pump station, and force main. The only storage alternative considered was to construct large pipe in the vicinity of the SSO to provide inline storage. Ground truthing at the Gunpowder Pump Station found water and gas mains and an underground electrical line that run parallel to the pump station, but the site was found to be suitable.

### Hunting Creek North Branch 3

This branch includes an SSO caused by insufficient capacity at the Fox Harbor No. 1 and No. 2 Pump Stations to handle upstream flows. These SSO locations were not reported as SSOs until mid-2008; therefore, no initial solutions were developed for the locations since they were not known at the time of initial solution development. Solutions, however, were developed later during the solution alternative analysis process.

### Hunting Creek South Branch 1

This branch includes an SSO caused by insufficient capacity at the Fairway View Pump Station to handle upstream flows. The surrounding area is mostly residential with some open area and a golf course.

The conveyance alternative considered upgrading the wet well, pump station, and force main. The first storage alternative considered was to construct a wet weather storage facility in a small wooded area. The second storage alternative considered was to construct a large pipe in the vicinity of the SSO to provide inline storage. Ground truthing found the pipe upstream of the SSO intersects with three electrical lines and a gas main.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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### Hunting Creek South Branch 2

This branch includes an SSO caused by insufficient capacity at the Deep Creek Pump Station to handle upstream flows. The surrounding area is mostly residential with wooded areas in backyards.

The conveyance alternative considered upgrading the wet well and the pump station, and possibly the force main. The first storage alternative considered was to construct a wet weather storage facility in a small wooded area. The second storage alternative considered was to construct large pipe in the vicinity of the SSO to provide inline storage. Another alternative considered building a storage facility at Deep Creek Trail Pump Station and reducing the pumping rate at Deep Creek Pump Station. Ground truthing identified electrical, water, and gas lines as potential utility conflicts.

### Lake Forest Branch 1

This branch includes an SSO caused by insufficient capacity at the Lake Forest Pump Station to handle upstream flows. The surrounding area is single-family residential.

The conveyance alternative considered upgrading the wet well, pump station, and force main. The first storage alternative considered was to construct a wet weather storage facility; however, there are no locations available to build a storage facility near the pump station. There is an area near the Worthing Pump Station where volume could be stored to delay pumping to the Lake Forest Pump Station. The second storage alternative considered was to construct large pipe in the vicinity of the SSO to provide inline storage.

### **3.3.9.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in Small WQTC areas. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and selection process. Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

### Berrytown Branch 1

Based on the benefit-cost analysis, the chosen solution for Berrytown Branch 1 (Lucas Lane PS) is Inline Storage. The offline and inline storage solution ratios were almost identical, so other values were taken into account such as reduced maintenance costs due to self-flushing pipe (no need to clean). Table 3.3.33 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.33

BERRYTOWN BRANCH 1 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_FF_BT_NB01_S_09A_C_A	Inline Storage	Replace 90 LF of 8" pipe upstream of the Lucas Lane PS with a 54" pipe and install an additional 90 LF of 54" pipe parallel to it to provide inline storage. Also lower the invert of the additional 9" pipe to PS and replace that pipe with a 36" pipe	88.53	112.86
S_FF_BT_NB01_S_09B_C_B	Offline Storage	Construct covered storage facility (0.031 MG)	88.61	90.92
S_FF_BT_NB01_S_03_C_A	PS Upgrades	Upgrade Lucas Lane LS to handle peak flows of 0.23 mgd.	78.51	72.76

**SSO Data Outdated  
Refer to Chapter 5**

Chenoweth Hills Branch 1

Based on the benefit-cost analysis, the chosen solution for Chenoweth Hills Branch 1 (St. Rene Rd. PS) is Inline Storage. Table 3.3.34 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.34

CHENOWETH HILLS BRANCH 1 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_FF_CH_NB01_S_09A_C_A	Inline Storage	Replace 42 LF of 8" pipe with 48" pipe just upstream of the St. Rene Rd. PS to provide inline storage.	163.34	212.00
S_FF_CH_NB01_S_01_C_B	Pipe Upgrades	Divert flow that currently flows to the St. Rene Road PS to a new gravity line that will connect to an existing sewer line that flows to the current location of the Chenoweth Run PS, however, eventually it will be taken offline by the Billtown Road Interceptor. Involves 1,291 LF of new gravity sewer.	72.17	88.66
S_FF_CH_NB01_S_01_C_A	Pipe Upgrades	Divert approximately 60% of the flow that currently flows to the St. Rene Road PS to a new gravity line that will take the flow to the Jeffersontown system. This portion of the Jeffersontown system will eventually be diverted to the Cedar Creek WQTC by the Billtown Road interceptor. Involves 605 LF of new gravity sewer.	44.35	56.16
S_FF_CH_NB01_S_03_C_A	PS Upgrades	Upgrade St. Rene Rd. PS to handle peak flows of 0.44 mgd.	42.87	36.13

**SSO Data Outdated  
Refer to Chapter 5**

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### Hunting Creek North Branch 1

Based on the benefit-cost analysis, the chosen solution for Hunting Creek North Branch 1 (Riding Ridge PS) is Pump Station Upgrades. Table 3.3.35 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.35**

**HUNTING CREEK NORTH BRANCH 1 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_HC_HN_NB01_S_03_C_A	PS Upgrades	Upgrade Riding Ridge PS to handle peak flow of 0.071 cfs.	66.40	52.02
S_HC_HN_NB01_S_09A_C_A	Inline Storage	Upsize 131 LF of existing 8" sewer to 12", and lower its slope via a drop manhole at its upstream end.	29.65	37.96
S_HC_HN_NB01_S_03_C_B	Force Main Upgrades	Upsize 1,464 LF of force main at Riding Ridge PS from 2" to 2.5".	24.95	24.12

### Hunting Creek North Branch 2

Based on the benefit-cost analysis, the chosen solution for Hunting Creek North Branch 2 (Gunpowder PS) is Inline Storage. This branch is one of the three branches requested to be re-evaluated at the 2.25-inch cloudburst level to ensure the validity of the technology selection approach at the 1.82-inch cloudburst level. Table 3.3.36(A) summarizes the solutions considered for the 1.82-inch cloudburst storm and the benefit-cost ratios associated with each solution. Table 3.3.36(B) summarizes the solutions considered for the 2.25-inch cloudburst storm and the benefit-cost ratios associated with each solution.

**TABLE 3.3.36(A)**

**HUNTING CREEK NORTH BRANCH 2 - 1.82-INCH SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_HC_HN_NB02_S_09A_C_B	Inline Storage	Replace 126 LF of 8" with 6" sewer pipe to provide inline storage, 28 LF of additional pipe upgrades required.	61.73	78.71
S_HC_HN_NB02_S_09A_C_A	Inline Storage	Replace 255 LF of 8" with 6" sewer pipe to provide inline storage.	39.75	50.66
S_HC_HN_NB02_S_03_C_A	PS Upgrades	Upgrade both pumps to 155 gpm each, increase wet well to 8 ft diameter, and upsize 3,485 LF of force main to 6" at the Gunpowder PS	8.87	9.09



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 3.3.36(B)**

**HUNTING CREEK NORTH BRANCH 2 - 2.25-INCH SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_HC_HN_NB02_S_09A_B_B	Inline Storage	Replace 120 LF of 8" (east of the lift station) with 60" sewer pipe as well as replace 148 LF of 8" sewer (west of the lift station) with 6" sewer pipe to provide in-line storage.	46.33	59.15
S_HC_HN_NB02_S_03_B_A	PS Upgrades	Upgrade both pumps to 220 gpm each, increase the wet well to 8 feet in diameter and upsize entire force main to 6" at the Gunpowder PS	11.29	11.62

SSO Data Outdated  
 Refer to Chapter 5

As indicated Table 3.3.36(B), Inline Storage is the preferred alternative independent of level of control.

Hunting Creek North Branch 3

Based on the benefit-cost analysis, the chosen solution for Hunting Creek North Branch 3 (Fox Harbor No. 1 and No. 2 PSs) is Inline Storage. It was chosen based on the present worth benefit-cost ratio to avoid moving the problem downstream. Table 3.3.37 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.37**

**HUNTING CREEK NORTH BRANCH 3 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_HC_HN_NB03_M_09A_C_A	Inline Storage	Upgrade 110 LF of 8" pipe east of the Fox Harbor No. 2 PS with 24" pipe. Upsize 110 LF of 8" pipe upstream of the Fox Harbor No. 1 PS with 18" pipe and lower the upstream invert of the pipe, new drop manhole required.	34.11	43.49
S_HC_HN_NB03_M_03_C_B	Inline Storage & Force Main Upgrades	Upgrade 810 LF of force main at Fox Harbor No. 2 PS to 6", upsize 110 LF of gravity sewer upstream of the Fox Harbor No. 1 PS from 8" to 18" to provide inline storage, lower upstream invert, new drop manhole required.	38.30	39.80

SSO Data Outdated  
 Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### Hunting Creek South Branch 1

The chosen solution for Hunting Creek South Branch 1 (Fairway View PS) is Pump Station Upgrades. While Offline Storage had a higher benefit/cost ratio, pump replacement is a lower capital cost and can be accomplished easily with no underground construction that would disrupt the surrounding neighborhood. This is consistent with the community values of customer satisfaction and economic vitality. Table 3.3.38 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.38**

#### **HUNTING CREEK SOUTH BRANCH 1 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_HC_HS_NB01_S_03_C_A	PS Upgrades	Upgrade the three pumps at Fairway View PS to 100, 100, and 120 gpm (previously 88 gpm each).	10.71	10.32
S_HC_HS_NB01_S_09A_C_B	Offline Storage	Construct offline covered storage facility (.0075 MG) upstream of Fairway View PS, upsize additional 175 LF of gravity sewer upstream of the PS.	29.69	33.55
S_HC_HS_NB01_S_13_C_A	PS & Pipe Upgrades	Upgrade the three pumps to 92 gpm (previously 88 gpm each), upsize 152 LF of gravity sewer upstream of PS from 8" to 24", new pipe entrances at a lower elevation drilled into wet well for larger pipe diameters.	10.25	10.20

SSO Data Outdated  
Refer to Chapter 5

### Hunting Creek South Branch 2

The chosen solution for Hunting Creek South Branch 2 (Deep Creek PS) is Diversion. During the solution optimization process (discussed in Volume 3, Chapter 4) it was discovered that this pump station could be eliminated with 130 linear feet of 8" pipe connecting to the new Harrods Creek Interceptor, analyzed in Branch 4 of the ORFM model. Therefore, the solutions initially analyzed for this branch are no longer warranted and the Deep Creek Pump Station will be addressed with ORFM Branch 4 solutions. Table 3.3.39 summarizes the solutions previously considered and the benefit-cost ratios associated with each solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.39

HUNTING CREEK SOUTH BRANCH 2 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
See ORFM Branch 4	Diversion	Construct 130 LF of 8" gravity sewer connecting to the new Hunting Creek Interceptor in ORFM Branch 4 to eliminate Deep Creek PS	--	--
S_HC_HS_NB02_S_09A_C_A	Inline Storage	Replace two 8" gravity sewers immediately upstream of the Deep Creek PS with 150 LF of 42" and 170 LF of 30" sewer pipe respectively to provide inline storage.	64.09	80.83
S_HC_HS_NB02_S_13_C_A	PS Upgrades & Inline Storage	Install two new 138 gpm pumps at PS (previously 122 gpm). Replace 150 LF of 8" sewer directly upstream of the PS with 36" pipe to provide inline storage.	22.45	22.75
S_HC_HS_NB02_S_03_C_A	PS Upgrades	Upgrade the Deep Creek PS by installing a 7' diameter wet well and installing new 156 gpm pumps (previously 122 gpm).	7.89	8.79

Lake Forest Branch 1

The chosen solution for Lake Forest Branch 1 (Lake Forest PS) is Monitoring. The Lake Forest Pump Station was upgraded in June 2008. Two new 144 gpm pumps were installed. Table 3.3.40 summarizes the solution chosen for Lake Forest Branch 1.

TABLE 3.3.40

LAKE FOREST BRANCH 1 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_FF_LF_NB01_S_13_C_A	Monitor	Monitor the Lake Forest PS during rain events for the next three years according to SORP protocols	--	--

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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### **3.3.10 Pond Creek Alternatives**

Details on branching and SSO descriptions for Pond Creek can be found in Volume 3, Chapter 2, Section 2.5.10. The initial solution development process is summarized in detail in Sections 3.1.3 and 3.1.3.3 contains information on the ground truthing procedure.

#### **3.3.10.1 Initial Solutions and Feasibility Screening**

Initial solutions were investigated before any baseline conditions (i.e. Capital Projects) or RDI/I reduction had been applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated by one of the two and therefore is not summarized below.

##### Branch 3

This branch includes SSOs caused by insufficient capacity at the Cooper Chapel Pump Station to handle upstream flows. The surrounding area is single-family residential.

The conveyance alternative considered upgrading the pump station and collection system pipe. The storage alternative considered was to construct an off-site storage facility upstream of the pump station. The diversion alternative considered was to construct a sewer line to an alternate system to eliminate the pump station. Ground truthing at the storage location found that 30 percent of the property is in the 100-year floodplain, and a blue line stream runs through the middle of the open field. This site was not suitable for the project.

##### Branch 4

This branch includes SSOs caused by insufficient capacity at the Cinderella Pump Station to handle upstream flows and limited interceptor capacity downstream. The surrounding area is single-family residential.

The conveyance alternative considered upgrading the pump station and increasing the capacity of the interceptor. The storage alternative considered was to construct a larger wet well at the pump station or a storage facility at the pump station site.

##### Branch 5

This branch includes SSOs caused by insufficient capacity at the Lantana Drive Pump Station to handle upstream flows. The surrounding area is single-family residential.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

The conveyance alternative considered upgrading the pump station. The first storage alternative considered was to construct a larger wet well at the pump station. The second storage alternative considered was to construct large pipe in the vicinity of the SSOs to provide inline storage.

#### Branch 6

This branch includes SSOs caused by insufficient capacity at the Government Center Pump Station to handle upstream flows. The surrounding area is mostly single-family residential with some government-owned property.

The conveyance alternative considered upgrading the pump station. The storage alternative considered was to construct underground storage beneath the parking lot at the Government Center.

#### Branch 7

This branch includes SSOs caused by insufficient capacity at the Avanti Pump Station to handle upstream flows. The surrounding area is primarily residential with some commercial.

The conveyance alternative considered upgrading the pump station and increasing the capacity in the downstream collector sewer. The storage alternative considered was to construct offline storage near the pump station. The diversion alternative considered was to eliminate the pump station and divert all flow to the Cedar Creek WQTC.

#### Branch 8 / Branch 11

This branch includes SSOs caused by insufficient capacity at the Lea Ann Way Pump Station to handle upstream flows and limited collector sewer capacity upstream of the pump station. Initially, this branch included the SSO at the Edsel Pump Station which is now included in Branch 11. This SSO is most likely caused by excessive I/I in the upstream collection system. The surrounding area is primarily single-family residential.

The conveyance alternative considered was to upgrade the pump stations. The first storage alternative considered constructing larger wet wells at the pump stations. The second storage alternative considered was to construct large pipe in the vicinity of the SSOs to provide inline storage.

Ground truthing found 60 percent of one property near Edsel Pump Station (Branch 11) is in the 100-year floodplain and a creek runs through the center of the wooded area. A threatened/endangered species assessment was recommended for this location. The location was found unsuitable for the solution.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### Branch 9

This branch includes SSOs caused by a hydraulic constriction at the I-65 crossing, limited collector sewer capacity, and insufficient capacity at the Caven Avenue Pump Station to handle upstream flows. The surrounding area is mostly single-family residential with some industrial and commercial properties.

The conveyance alternative considered was to upgrade the Caven Avenue Pump Station and upsize the interceptor under I-65 and down the Outer Loop. The storage alternative considered constructing offline storage facilities in open land near the SSO locations.

Ground truthing for one potential storage location found a potential utility conflict with an electrical line. Ground truthing at the Meijer site found 10 percent of the property is in the 100-year floodplain and creeks border the west and north sides of the wooded area. A threatened/endangered species assessment was recommended for this site. A retention basin is located just west of the property. Ground truthing at another site near a nursing home found five percent of the property is in the 100-year floodplain and a threatened/endangered species assessment was recommended for the wooded area. Fishpool Creek and utilities may create conflicts. The site was found unsuitable due to shallow rock and a force main and sewer line located on the property.

### Branch 10

This branch includes an SSO caused by insufficient capacity at the Leven Pump Station to handle upstream flows. This SSO location was not reported as an SSO until mid-2008; therefore, no initial solutions were developed for the locations since they were not known at the time of initial solution development. Solutions, however, were developed later during the solution alternative analysis process.

#### **3.3.10.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in Pond Creek. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and selection process. Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

### Branch 3

The chosen solution for Pond Creek Branch 3 is Pipe Upgrades. The Charleswood Interceptor Capital Improvement Project specifically eliminates the Cooper Chapel Pump Station. This was the only solution considered at this phase because the project is currently under design. The solution listed in the table is an extension to the Capital Improvement Project due to

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

downstream capacity problems caused by the additional flow. Table 3.3.41 summarizes the solution considered and the benefit-cost ratio associated with the solution.

TABLE 3.3.41

POND CREEK BRANCH 3 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_PO_WC_PC03_M_01_C	Pipe Upgrades	Upsize additional 1,846 LF of gravity sewer downstream of the Charleswood Interceptor connection to correct capacity problem.	50.30	62.84

Branch 4

The chosen solution for Pond Creek Branch 4 (Cinderella PS) is Diversion. While this does not appear to have the highest benefit/cost ratio, the cost estimates do not reflect the costs likely needed to keep the pump station in service. This pump station is nearly thirty years old and may require continual servicing and upgrades over time. When these costs are fully considered, it is likely that the diversion solution would have the highest benefit/cost ratio. Table 3.3.42 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.42

POND CREEK BRANCH 4 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_PO_WC_PC04_M_01_C	Diversion	Eliminate Cinderella PS by diverting 2,250 LF of 10" pipe. 208 LF of tunneling under I-265.	17.41	22.14
S_PO_WC_PC04_M_09B_C	Off-line Storage	Construct off-line storage facility at Cinderella PS (0.22 MG).	32.35	32.40
S_PO_WC_PC04_M_0103_C	PS Upgrades	Upgrade pumps at Cinderella PS to 1.5 mgd each (previously 0.5 mgd) and upsize 2,953 LF of force main from 6" to 15". Additional 2,918 LF of sewer improvements required downstream of new force main.	12.94	14.51

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Branch 5

The chosen solution for Pond Creek Branch 5 (Lantana PS) is I/I Reduction. This solution was chosen as the recommended alternative due to the small contributing area. If I/I reduction is deemed unsuccessful in eliminating the SSO, the next best alternative is Offline Storage and Pipe Upgrades. Table 3.3.43 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.43

POND CREEK BRANCH 5 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_PO_WC_PC05_M_07_C	I/I Reduction	This solution will require extensive source control (I/I Rehab and private property program.)	Cost only for SSES - no benefits calculated.	
S_PO_WC_PC05_M_0109B_C	Offline Storage & Pipe Upgrades	Construct offline covered storage facility at Lantana PS (1,200 LF) and install 241 LF of sewer improvements (10" - 15") required upstream of PS.	71.21	72.58
S_PO_WC_PC05_M_0103_C	PS & Pipe Upgrades	Upgrade Lantana PS to handle peak flow of 1.45 mgd, upgrade or replace 1,345 LF of 8" force main, 3,770 LF of additional conveyance improvements (10" - 27") required upstream of the PS and downstream of force main.	12.53	14.48
S_PO_WC_PC05_M_09A_C	Inline Storage	Install 667 LF of 60" pipe upstream of Lantana PS to provide inline storage.	5.05	6.49

SSO Data Outdated  
 Refer to Chapter 5

Branch 6

Based on the benefit-cost analysis, the chosen solution for Pond Creek Branch 6 (Government Center PS) is Diversion. The cost estimates for Offline Storage and Pump Station Upgrades do not reflect the costs likely needed to keep the pump station in service. When these costs are fully considered, it is likely that these solutions would have even lower benefit/cost ratios. Table 3.3.44 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.44

POND CREEK BRANCH 6 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_PO_WC_PC06_M_01_C	Force Main	Eliminate Government Center PS by constructing 1,350 LF of 10" pipe.	35.50	44.91
S_PO_WC_PC06_M_0109B_C	Offline Storage & Pipe Upgrades	Construct offline covered storage facility at Government Center PS (0.11 MG). Additional 3,032 LF of sewer improvements (10" - 12") required upstream of PS.	21.29	22.17
S_PO_WC_PC06_M_0103_C	PS & Pipe Upgrades	Upgrade pumps at Government Center PS to 2.1 mgd each (previously 1 mgd) and upsize 3,107 LF of force main to 10". Additional 3,032 LF of sewer improvements (10" - 12") required downstream of new force main.	15.38	16.70

Branch 7

Based on the benefit-cost analysis, the chosen solution for Pond Creek Branch 7 (Avanti PS) is Diversion. The cost estimates for Offline Storage and Pump Station Upgrades do not reflect the costs likely needed to keep the pump station in service. When these costs are fully considered, it is likely that these solutions would have even lower benefit/cost ratios. Table 3.3.45 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.45

POND CREEK BRANCH 7 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_PO_WC_PC07_M_01_C	Diversion	This alternative eliminates Avanti PS by constructing 150 LF of 8" pipe	900.43	1000.48
S_PO_WC_PC07_M_09B_C	Offline Storage	Construct offline covered storage facility at Avanti PS (0.13 MG)	256.76	263.10
S_PO_WC_PC07_M_0103_C	PS & Pipe Upgrades	Upgrade Avanti PS to handle peak flow of 1.8 mgd. Additional 1,886 LF of sewer improvements (10") required downstream of new force main.	16.80	19.52

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**Branch 8**

The chosen solution for Pond Creek Branch 8 is Pipe Upgrades. This was the only solution considered because the pumps at the Lea Ann Way Pump Station are currently being replaced, which will increase the capacity of the pump station to 22 mgd and eliminate the SSO at the Pump Station. The first pump has been replaced and a developer is installing a fourth pump. The second and third pumps were replaced by MSD Operations in September 2008. The Pipe Upgrades solution addresses insufficient pipe capacity in the collection system upstream of the Lea Ann Way Pump Station. Table 3.3.46 summarizes the solution and the benefit-cost ratio associated with that solution.

**TABLE 3.3.46**

**POND CREEK BRANCH 8 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_PO_WC_PC08_M_01_C	Pipe Upgrades	Upsize 3,255 LF of gravity sewer (12" pipe) upstream of Lea Ann Way PS.	39.74	49.01

**Branch 9**

Based on the benefit-cost analysis, the chosen solution for Pond Creek Branch 9 is Offline Storage and Pipe Upgrades. The storage facility behind the Meijer on Preston Highway is necessary to alleviate future predicted overflows caused by upstream IOAP projects. Table 3.3.47 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

**TABLE 3.3.47**

**POND CREEK BRANCH 9 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_PO_WC_PC09_M_09B_C	Offline Storage & Pipe Upgrades	Construct offline concrete storage facility at Caven Avenue PS (0.21 MG) and offline open storage facility behind the Meijer (1.42 MG) on Preston Hwy. Upsize 1,536 LF of sewer to 36" diameter upstream of Caven Avenue PS.	6.61	7.08
S_PO_WC_PC09_M_0103_C	PS & Pipe Upgrades	Upsize Caven Avenue PS to handle peak flow of 3.9 mgd and upsize 1,715 LF of force main to 8". Additional 18,242 LF of sewer improvements (8" - 48") required in Okolona area.	3.28	4.06



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

Branch 10

Based on the benefit-cost analysis, the chosen solution for Pond Creek Branch 10 is Diversion. The cost estimates for Offline Storage, Inline Storage, and Pump Station Upgrades do not reflect the costs likely needed to keep the pump station in service. When these costs are fully considered, it is likely that these solutions would have even lower benefit/cost ratios. Table 3.3.48 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

TABLE 3.3.48

POND CREEK BRANCH 10 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_PO_WC_PC10_M_01_C	Diversion	Eliminate Leven PS by constructing 890 LF of 10" pipe.	76.88	95.93
S_PO_WC_PC10_M_09B_C	Offline Storage	Construct offline covered storage facility via Leven PS to provide 3.42 mgd.	64.21	65.61
S_PO_WC_PC10_M_03_C	PS Upgrades	Upgrade Leven PS to handle peak flow of 3.42 mgd.	42.87	41.44
S_PO_WC_PC10_M_09A_C	Inline Storage	Install 1,084 LF of 48" pipe upstream of Leven PS to provide inline storage.	14.46	18.51

SSO Data Outdated  
 Refer to Chapter 5

Branch 11

The chosen solution for Pond Creek Branch 11 is I/I Reduction. This solution was chosen as the recommended alternative based on modeling results. An overflow did not occur at this pump station in the existing conditions model at the 1.82-inch, 2.25-inch, or even 2.60-inch cloudburst storm indicating excessive I/I during heavy rain events is likely the problem rather than insufficient capacity at the pump station. If I/I reduction is deemed unsuccessful in eliminating the SSO, the next best alternative is Offline Storage. Table 3.3.49 summarizes the solutions considered and the benefit-cost ratios associated with each solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.49

POND CREEK BRANCH 11 SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_PO_WC_PC11_M_07_C	SSO Reduction	This location is targeted for RDI source control to prevent additional property program).	Cost only for SSES - no benefits calculated.	
S_PO_WC_PC11_M_0109B_C	Offline Storage	Construct offline covered storage facility at Edsel PS (0.4 MG). Additional 57 LF of sewer improvements (10" - 12") required upstream of PS.	58.87	62.63
S_PO_WC_PC11_M_0103_C	PS Upgrades	Upgrade Edsel PS to handle peak flow of 0.7 mgd and upsize 3,468 LF of force main to 10". Additional 925 LF of sewer improvements (10" - 12") required.	9.92	10.49
S_PO_WC_PC11_M_0109A_C	Inline Storage	Install 572 LF of 96" pipe upstream of Edsel PS to provide inline storage. Additional 423 LF of sewer improvements (10" - 12") required.	5.41	6.94

SSO Data Outdated  
 Refer to Chapter 5

**3.3.11 Mill Creek Alternatives**

Details on branching and SSO descriptions for Mill Creek can be found in Volume 3, Chapter 2, Section 2.5.11. The initial solution development process is summarized in detail in Sections 3.1.3 and 3.1.3.3 contain information on the ground truthing procedure.

**3.3.11.1 Initial Solutions and Feasibility Screening**

Initial solutions were investigated before any baseline conditions (i.e. Capital Projects) or RDI/I reduction had been applied; therefore, some preliminary SSOs analyzed in the initial solutions were not considered in the project development phase due to the effects of the baseline conditions or RDI/I reduction. In these cases, the SSO was eliminated by one of the two and therefore is not summarized below.

Branch 1

This branch includes SSOs caused by insufficient capacity at Pioneer, Fern Lea, and Garrs Lane pump stations to handle upstream flow. The landuse in the area is a combination of park, residential, vacant lots, commercial, and industrial. Each pump station location was analyzed separately.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

The conveyance alternatives considered pump station upgrades, pump station replacement, pipe upgrades, and pump station eliminations. The storage alternatives considered off-line storage facilities and expansion of pump station wet wells.

Ground truthing was performed at 22 locations in the Shively area. Twelve of the locations had 15 to 100 percent of the property in the 100-year floodplain. All twenty locations were found to have potential utility conflicts including water lines, gas lines, storm drains, and electrical lines. The pipe upgrade solution could affect many residential properties and landscapes.

### Branch 2

This branch includes an SSO caused most likely by surface flooding in the East Rockford Pump Station area during wet weather. This pump station was not reported as an SSO location until mid-2008; therefore, no initial solutions were developed for this location since it was not known at the time of initial solution development. Solutions, however, were developed later during the solution alternative analysis process.

### **3.3.11.2 Modeled Solutions - Benefit Cost Analysis**

The following section summarizes the solution alternative analysis for each of the branches in Mill Creek. Based on ground truthing findings and judgments made during the modeling process, some initial solutions identified in the previous section may not have been evaluated. Section 3.2 provides detail on the solution alternative development and selection process. Appendix 3.3.1 contains the detailed cost sheets, benefit-cost analyses, solution maps, and fact sheets for all modeled solutions.

### Branch 1

The Shively Interceptor Capital Improvement Project specifically eliminates five pump stations: Jacks Lane Pump Station, Pioneer Pump Station, Fern Lea Pump Station, Garrs Lane Pump Station, and City Park Pump Station, three of which are documented SSOs. This project is currently in the preliminary design stage. The solution listed below includes the benefit-cost ratio for the entire project. This branch is one of the three branches requested to be re-evaluated at the 2.25-inch cloudburst level to ensure the validity of the technology selection approach at the 1.82-inch cloudburst level. Table 3.3.50(A) summarizes the solutions considered for the 1.82-inch cloudburst storm and the benefit-cost ratios associated with each solution. Table 3.3.50(B) summarizes the solutions considered for the 2.25-inch cloudburst storm and the benefit-cost ratios associated with each solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

TABLE 3.3.50(A)

MILL CREEK BRANCH 1 - 1.82-INCH SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_MC_WC_NB01_M_01_C	Pipe Upgrades	Construct 18,830 LF of new gravity sewers (8" – 18") to eliminate the Jacks Lane, Pioneer, Gars Lane, Fern Lea, and City Park ISS. This is the Shively Interceptor capital improvement project.	4.11	5.20
S_MC_WC_NB01_M_0109_C	Offline Storage & Pipe Upgrades	Construct new gravity sewers (2,821 LF). Construct seven small offline storage facilities (0.63 MG total) and 3,214 LF of force main.	1.44	1.70

TABLE 3.3.50(B)

MILL CREEK BRANCH 1 – 2.25-INCH SOLUTION ALTERNATIVES

Project ID	Solution Technology	Project Description	Benefit/ Cost Ratio (Capital Cost)	Benefit/ Cost Ratio (Present Worth)
S_MC_WC_NB01_M_01_B	Pipe Upgrades	Construct 18,830 LF of new gravity sewers (10" – 21") to eliminate the Jacks Lane, Pioneer, Gars Lane, Fern Lea, and City Park ISS.	5.27	6.68
S_MC_WC_NB01_M_0109_B	Offline Storage & Pipe Upgrades	Construct new gravity sewers (2,821 LF). Construct seven small offline storage facilities (0.74 MG total) and 3,214 LF of force main.	1.41	1.66

As indicated in Table 3.3.50(b), the pipe upgrades accomplished by expanding the Shively Interceptor Project has the highest benefit-cost ratio, independent of level of control. Costs are fairly similar for both technologies at each level of evaluation; however, the benefit scores are significantly lower for the Offline Storage solution due to storage facility construction in residential neighborhoods and lower impact in reducing overflow volumes during larger storm events.

Branch 2

The chosen solution for Mill Creek Branch 2 is Pump Station Replacement and Relocation. No modeling was used to identify this solution. It is the only solution considered for this branch because the problem is due to street surface flooding. Table 3.3.51 summarizes the solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 3.3.51**

**MILL CREEK BRANCH 2 SOLUTION ALTERNATIVES**

Project ID	Solution Technology	Project Description
S_MC_WC_NB02_S_03_C	PS replacement and relocation	Relocate the existing Mill Creek Branch 2 PS at 300 gpm. 150 LF of 4" force main will be replaced. Additional 150 LF of 10" gravity improvements required to relocate PS.

SSO Data Outdated  
 Refer to Chapter 5





## CHAPTER 4: SELECTION OF FINAL SANITARY SEWER DISCHARGE PLAN

**Special Note:** This chapter was developed in 2008. The statistical data for the SSO’s reported, specifically related to individual SSO volumes and frequency in a typical rainfall year, were derived from the hydraulic models calibrated in 2007. Since then, a more detailed calibration and validation effort has adjusted the average annual overflow volumes and frequencies in the typical year. This information is provided in Chapter 5. The vast majority of the physical system characterization in this chapter is still accurate.

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Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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## **SUPPORTING INFORMATION**

Appendix 4.1.1 Optimized Solution Cost Estimates and Benefit-Cost Analyses

Appendix 4.1.2 Final SSDP Project Cost Estimates

Appendix 4.1.3 Evaluation of All Levels of Protection Analysis

Appendix 4.5.1 SSO Fact Sheets

## **CHAPTER 4: SELECTION OF FINAL SANITARY SEWER DISCHARGE PLAN**

The Final Sanitary Sewer Discharge Plan (SSDP) approach to sanitary sewer overflow (SSO) elimination is based upon identifying the solution that provides the highest benefit-cost ratio for each modeled watershed branch. As presented in Chapter 3, Louisville and Jefferson County Metropolitan Sewer District (MSD) developed a solution development process. The following is a summary of the Final SSDP solution development process.

- Solutions were developed that eliminated SSOs and known surcharging under site-specific levels of protection using a diverse set of solution technologies.
- Benefits, capital costs, and benefit-cost ratios were developed for each solution at the baseline level of protection (1.82-inch cloudburst storm event).
- The solution with the best benefit-cost ratio was selected for further development and analysis of the preferred level of protection.

Chapter 4 summarizes the final steps in the solution development process. The Chapter discusses the optimized level of protection evaluations and the resulting list of selected projects. Additionally, the chapter reviews the Integrated Overflow Abatement Plan (IOAP) public involvement process. The chapter ends by discussing the process used for tracking and determining success of the Final SSDP projects.

### **4.1 FINAL PROJECT SELECTION**

As detailed in Chapter 3, MSD used a standard benefit-cost ratio process to determine and select the most effective solution (referred to as the preferred solution). The same process was used to set optimal levels of protection for the selected solutions. The following section revisits the preferred solution process.

#### **4.1.1 Preferred Solutions**

During the development of SSO elimination strategies and alternatives, a wide range of technology approaches were considered for the baseline level of protection. The approaches included the following:

- Source control through infiltration and inflow (I/I) reduction
- Reduced surcharging in systems hydraulically connected to SSOs and solutions

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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- A wide variety of conventional constructed facilities commonly referred to as gray infrastructure, including:
  - Peak flow storage (constructed storage tanks, or oversized pipes providing “in-line” storage)
  - Increased conveyance capacity (increased pipe sizes, parallel relief sewers, new or expanded pump stations)
  - Flow diversions to other portions of the system that have available capacity
  - Expanded wastewater treatment capacity (provided at existing regional treatment facilities or provided remotely as high-rate wet weather treatment facilities)

Table 4.1.1 recaps the preferred solution technology list developed for the baseline level of protection. Projects are listed by the eleven model areas.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.1**  
**SUMMARY OF PREFERRED SOLUTIONS**

SSDP Recommended Project Name/Location	Region and Branch ID	SSO(s) Addressed	Technology
<b>Cedar Creek Area</b>			
Idlewood Inline Storage	Cedar Creek - 70158	28998, 28984, 63094, 63095, 70158	Inline Storage
Fairmount Rd. Pump Station Improvements	Cedar Creek - 81316	Fairmount Road Pump Station (PS) (81316 & 97362)	PS Upgrades
Little Cedar Creek Interceptor Improvements	Cedar Creek - 67097	67097, 67098, 67099, 8195, 89197	Pipe Upgrades
Bardstown Rd. PS Improvements	Cedar Creek - MSD1025	88545	PS Upgrades
Running Fox PS Elimination	Cedar Creek - MSD1080	Running Fox PS (MSD1080-LS)	Diversion
<b>Hite Creek Area</b>			
Meadow Stream PS Inline Storage	Hite Creek - MSD1082	Meadow Steam PS (91087 & MSD1082-PS)	Inline Storage
Floydsburg Rd. I/I Investigation & Rehabilitation	Hite Creek - MSD1086	Floydsburg Road (MSD1086-PS, 90776, 108956, 108957, 108958)	I/I Reduction
Kavanaugh Rd. PS Improvements	Hite Creek - MSD1085	Kavanaugh Road (MSD1085-PS)	PS & Force Main Upgrades
<b>Floyds Fork Area</b>			
Woodland Hills PS Diversion	Floyds Fork - NB01	33003, 65531	Diversion
Eden Care PS SSO Investigation	Floyds Fork - NB02	Eden Care PS (MSD1105-PS)	Monitor
Ashburton PS Improvements & Diversion	Floyds Fork - NB03	Olde Copper Court PS (MSD0165-PS), Ashburton PS (MSD0166-PS)	Upgrade Force Main & Pipes
<b>Jeffersontown Area</b>			
Jeffersontown WQTC Elimination	Jeffersontown - NB01	28390, 28391, 28392, 28395, 31733, Jeffersontown WQTC (28173 & 64505 & MSD0255 & IS028-SI)	Offline Storage, Pipe Upgrades, WQTC Eliminations
Chenoweth Hills WQTC Elimination, Chenoweth Run and Chippewa PS Improvements	Jeffersontown - NB01A	Chenoweth Run PS (MSD0196-PS & 86052 & 64096), Chippewa PS (92061), Chenoweth Hills WQTC PS (MSD0263A-PS), Chenoweth Hills WQTC (MSD0263)	PS & Force Main Upgrades, WQTC Eliminations
Dell Rd and Charlane Pkwy Interceptor Improvements	Jeffersontown - NB02	Charlane Pkwy (28250, 28249, 28340, 28336, 104289), Dell Rd. (28413, 28414, 28415, 28416, 28417)	Pipe Upgrades
Raintree & Marian Ct PS Eliminations	Jeffersontown - NB03	28719, 28711, Marian Ct. PS (28729), Raintree PS (MSD0149-PS)	Diversion, Pipe Upgrades
Monticello PS Elimination	Jeffersontown - NB04	Monticello Place PS (MSD0151-PS & 27969)	Diversion

SSO Data Outdated  
 Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.1**  
**SUMMARY OF PREFERRED SOLUTIONS**

SSDP Recommended Project Name/Location	Region and Branch ID	SSO(s) Addressed	Technology
<b>Middle Fork Area</b>			
Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion	Middle Fork - MF01	02932, 02933, 02935, 08537, 23211, 23212, 27005, 45835, 47583, 47593, 47596, 47603, 47604, 51221, 51160, 51161, 90770 (Sullivan) and Middle Fork at Breckenridge (08935-SM)	Offline Storage & Pipe Upgrades
Goose Creek PS Improvements & Wet Weather Storage	Middle Fork - MF04	Devondale PS (21628-W), Goose Creek PS (46891 & 62418 & 91629 & 91630 & 105936), Saurel PS (43472)	Offline Storage, PS & Force Main Upgrades
Anchor Estates Inline Storage & PS Eliminations	Middle Fork - MF06	Anchor Estates #1 PS (00746 & 00056-W), Anchor Estates #2 PS (MSD0057-LS)	Inline Storage & Diversion
Hurstbourne I/I Investigation & Rehabilitation	Middle Fork - MF07	01793	I/I Reduction
<b>Southeastern Diversion Area</b>			
Parkview Estates I/I Investigation & Rehabilitation	Southeastern Diversion - NB03	47250	I/I Reduction
Klondike Interceptor	Southeastern Diversion - NB04	25676 (Alcona), 26650, 26651	Pipe Upgrades
Sutherland Interceptor	Southeastern Diversion - NB05	Sutherland (16649)	Pipe Upgrades
Beargrass Interceptor Rehab Ph. 2	Southeastern Diversion - NB06	51594	Pipe Rehab
<b>Pond Creek Area</b>			
Charleswood Interceptor Extension	Pond Creek - PC03	25477, 25478, Cooper Chapel PS (25480 & MSD0130-PS)	Pipe Upgrades
Cinderella PS Elimination	Pond Creek - PC04	Cinderella PS (60679 & MSD1013-PS), 35309	Diversion
Lantana PS I/I Investigation & Rehabilitation	Pond Creek - PC05	Lantana Drive #1 PS (25484 & 93719 & MSD0101-PS)	I/I Reduction
Government Center PS Elimination	Pond Creek - PC06	Government Center PS (MSD0180-PS)	Diversion
Avanti PS Elimination	Pond Creek - PC07	Avanti PS (21229-W)	Diversion
Lea Ann Way System Improvements	Pond Creek - PC08	19360, 19369, 29933, 29948, 29943, 31083, 31084, 79076, Lea Ann Way PS (MSD1010-PS)	Pipe Upgrades
Outer Loop & Caven Ave Wet Weather Storage	Pond Creek - PC09	27116, 70212, 17724, Caven Ave PS (MSD0133-PS)	Offline Storage & Pipe Upgrades
Leven PS Elimination	Pond Creek - PC10	Leven PS (36419 & MSD1019-PS)	Diversion
Edsel PS I/I Investigation & Rehabilitation	Pond Creek - PC11	Edsel PS (92098 & MSD1048-PS)	I/I Reduction

SSO Data Outdated  
 Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.1**  
**SUMMARY OF PREFERRED SOLUTIONS**

SSDP Recommended Project Name/Location	Region and Branch ID	SSO(s) Addressed	Technology
<b>ORFM Area</b>			
Mellwood System Improvements & PS Eliminations	ORFM - NB01	26752, 41374, 41416, Mockingbird Valley PS (MSD0007-PS), Winton PS (MSD0010-PS), Mellwood Avenue PS (21152-W & 21152-E), Canoe Lane PS (24152-W & MSD0024-PS)	PS Upgrades, Pipe Upgrades & Diversion
Leland Rd. SSO Investigation	ORFM - NB02	96020	Condition Assessment
Derington Ct. PS I/I Investigation & Rehab	ORFM - NB03	Derington Court PS (MSD0095-PS)	I/I Reduction
Prospect WQTC Eliminations, Harrods Creek PS, and ORFM System Improvements	ORFM - NB04 (Prospect)	40870, 40871, 40872, Barbour Lane PS (42680 & 65633 & 65635), West Goose Creek PS (22436 & MSD0123-PS), Phoenix Hill PS (MSD1044-PS), Glenview Hills PS (MSD0183-PS), Barbour Lane PS (MSD0192-PS), New Market PS (MSD0193-PS), Deep Creek PS (MSD1063-PS), Hunting Creek South WQTC (MSD0292)	PS and Pipe Upgrades, Diversion, WQTC eliminations
<b>Mill Creek Area</b>			
Shively Interceptor	Mill Creek - NB01	04498, 04542, Pioneer PS (81814-W), Fern Lea PS (MSD0047-PS), Garr's Lane PS (MSD0050-PS)	Pipe Upgrades
East Rockford PS Relocation	Mill Creek - NB02	East Rockford PS (04699-W)	PS Replacement and Relocation
<b>Small WQTC Area</b>			
Lucas Ln. PS Inline Storage	Berrytown - NB01	Lucas Lane PS (MSD0199-LS)	Inline Storage
Riding Ridge PS Improvements	Hunting Creek North - NB01	Riding Ridge PS (MSD1060-LS)	PS Upgrades
Gunpowder PS Inline Storage	Hunting Creek North - NB02	Gunpowder PS (MSD1055-LS)	Inline Storage
Fox Harbor Inline Storage	Hunting Creek North - NB03	Fox Harbor #1 and #2 PS (62769)	Inline Storage
Fairway View PS Improvements	Hunting Creek South - NB01	Fairway View PS (MSD1065-PS)	PS Upgrades
Lake Forest PS SSO Investigation	Lake Forest - NB01	Lake Forest PS (MSD1169-LS)	Monitor
St. Rene Rd. PS Inline Storage	Chenoweth Hills - CH01	94187	Inline Storage

SSO Data Outdated  
 Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.1**  
**SUMMARY OF PREFERRED SOLUTIONS**

SSDP Recommended Project Name/Location	Region and Branch ID	SSO(s) Addressed	Technology
<b>CSS Area</b>			
Sonne PS I/I Investigation & Rehabilitation	CSO - 42007	Sonne Avenue PS (MSD0042-PS)	I/I Reduction
Camp Taylor System Improvements	CSO - 30917	99717, 33917, 35917, 37763, 44396, 44397, 66349, 104223, 104231	SSES, Sewer Rehabilitation & Replacement, Offline Storage
Hazelwood PS I/I Investigation & Rehabilitation	CSO - 55665	Hazelwood PS (MSD0055665)	I/I Reduction
<p><b>Legend:</b> LS –Lift station, PS – Pump Station, CSO – Combined Sewer Overflow, SSO – Sanitary Sewer Overflow, CSS- Combined Sewer System, WQTC – Water Quality Treatment Center, SSES – Sanitary Sewer Evaluation Study, I/I – Inflow and Infiltration, UMFLS – Upper Middle Fork Lift Station, ORFM – Ohio River Force Main</p>			

SSO Data Outdated  
 Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

#### 4.1.2 Level of Protection Evaluation

The IOAP sets the minimum level of protection at a 1.82-inch cloudburst storm event, and the maximum level of protection evaluated at a 2.60-inch cloudburst storm event. A 1.82-inch cloudburst storm is equivalent to a 3-hour, high-intensity event with a 50 percent probability of occurring in a given year. MSD selected this level of protection to be consistent with the cities of Atlanta, Cincinnati, and Knoxville who also use a 50 percent probability (often referred to as a two-year recurrence interval design storm) as the minimum protection level for SSOs.

For solution optimization, the starting point is the preferred solution and a baseline level of protection set at a 1.82-inch cloudburst storm. The solution is then analyzed at a 2.25-inch cloudburst and 2.60-inch cloudburst (if needed) storm level to compare benefit-cost ratios for the modeled branch. The method implemented involves analyzing the same solution determined at the 1.82-inch cloudburst level and modifying the solution to capture flows and prevent SSOs during the higher-intensity cloudburst storm events.

Costs and benefits are re-evaluated and a new benefit-cost ratio is determined for that solution. The following rules apply to the re-evaluated results:

- If the 2.25-inch cloudburst benefit-cost ratio does not exceed the 1.82-inch cloudburst benefit-cost ratio then the level of protection chosen for that particular solution is the 1.82-inch cloudburst storm level.
- If the 2.25-inch cloudburst benefit-cost ratio does exceed the 1.82-inch cloudburst benefit-cost ratio then the same process is repeated at the 2.60-inch cloudburst storm level.
- If the 2.60-inch cloudburst benefit-cost ratio does not exceed the 2.25-inch cloudburst benefit-cost ratio then the level of protection chosen for that particular solution is the 2.25-inch cloudburst storm level.
- If the 2.60-inch cloudburst benefit-cost ratio does exceed the 2.25-inch cloudburst benefit-cost ratio then the level of protection chosen for that particular solution is the 2.60-inch cloudburst storm level and no further evaluation is performed.

This approach to determine the optimal level of protection means that solutions to address an individual SSO location may be designed to protect against larger storms if that will yield a higher benefit-cost ratio in the analysis of project alternatives.

Additionally, three projects were chosen to examine the above approach by evaluating the 2.60-inch cloudburst event where all three levels of control had not been previously developed. The projects subject to this further evaluation are: Klondike Interceptor, Middle Fork Relief Interceptor, and the Shively Interceptor. The results presented in Table 4.1.2 illustrate that the evaluation rules presented above are appropriate, and identify the level of protection with the



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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highest benefit-cost ratio. Table 4.1.2 sites the modeled area, lists the SSOs that are controlled, summarizes the design level of protection evaluation process for each modeled branch, and highlights the ultimate design level of protection for that particular branch. Projects are listed by modeled area. Level of Protection costs and benefit-cost detailed evaluation tables for each modeled branch are available in Appendix 4.1.1 Optimized Solution Cost Estimates and Benefit-Cost Analyses.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.2**  
**SUMMARY OF LEVEL OF PROTECTION EVALUATION**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio
<b>Cedar Creek Area</b>				
Idlewood Inline Storage	28998, 28984, 62094, 63095, 70155	Inline Storage	1.82-inch	31.36
			2.25-inch	27.11
Fairmount Rd. PS Improvements	Fairmount Road PS (81316 & 97362)	PS Upgrades	1.82-inch	26.79
			2.25-inch	31.33
			2.60-inch	33.29
Little Cedar Creek Interceptor Improvements	67997, 67999, 86423, 89195, 89197	Pipe Upgrades	1.82-inch	23.86
			2.25-inch	17.43
Bardstown Rd. PS Improvements	88545	PS Upgrades	1.82-inch	29.42
			2.25-inch	46.50
			2.60-inch	33.85
Running Fox PS Elimination	MSD1080-LS	Diversion	1.82-inch	659.52
			2.25-inch	118.87
<b>Hite Creek Area</b>				
Meadow Stream PS Inline Storage	Meadow Steam PS (91087 & MSD1082-PS)	Inline Storage	1.82-inch	13.77
			2.25-inch	11.71
Floydsburg Rd. I/I Investigation & Rehabilitation	Floydsburg Road (MSD1086-PS, 90776, 108956, 108957, 108958)	I/I Reduction	Sewer System Evaluation Study (SSES)/Rehab	
Kavanaugh Rd. PS Improvements	Kavanaugh Road (MSD1085-PS)	PS & Force Main Upgrades	1.82-inch	19.77
			2.25-inch	20.23
			2.60-inch	21.09
<b>Floyds Fork Area</b>				
Woodland Hills PS Diversion	33003, 65531	Diversion	1.82-inch	92.26
			2.25-inch	17.75
			2.60-inch	15.45
Eden Care PS SSO Investigation	Eden Care PS (MSD1105-PS)	Monitoring	Monitoring	
Ashburton PS Improvements & Diversion	Olde Copper Court PS (MSD0165-PS), Ashburton PS (MSD0166-PS)	Upgrade Force Main & Pipes	1.82-inch	161.00
			2.25-inch	82.24

SSO Data Outdated  
 Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.2**  
**SUMMARY OF LEVEL OF PROTECTION EVALUATION**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio
<b>Jeffersontown Area</b>				
<b>Jeffersontown WQTC Elimination</b>	28390, 28391, 28392, 28393, 28394, 21737, Jeffersontown WQTC (28175 & 64565 & MSD0255 & 45628-31)	Offline Storage, Pipe Upgrades, WQTC Elimination	1.82-inch	5.23
			2.25-inch	5.09
<b>Chenoweth Hills WQTC Elimination, Chenoweth Run and Chippewa PS Improvements</b>	Chenoweth Run PS (MSD0196-PS & 86052 & 64096), Chippewa PS (92061), Chenoweth Hills WQTC PS (MSD0196-PS & 86052 & 64096), Chenoweth Hills WQTC (28175 & 64565 & MSD0255 & 45628-31)	PS & Force Main Upgrades, WQTC Elimination	1.82-inch	20.05
			2.25-inch	17.94
<b>Dell Rd and Charlane Pkwy Interceptor Improvements</b>	Charlane Pkwy (28250, 28249, 28340, 28336, 104289), Dell Rd. (28413, 28414, 28415, 28416, 28417)	Pipe Upgrades	1.82-inch	31.34
			2.25-inch	26.28
<b>Raintree &amp; Marian Ct. PS Eliminations</b>	28719, 28711, Marian Court PS (28729), Raintree PS (MSD0149-PS)	Diversion, Pipe Upgrades	1.82-inch	72.76
			2.25-inch	51.97
<b>Monticello PS Elimination</b>	Monticello Place PS (MSD0151-PS & 27969)	Diversion	1.82-inch	48.90
			2.25-inch	63.24
			2.60-inch	65.85
<b>Middle Fork Area</b>				
<b>Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion</b>	02932, 02933, 02935, 08537, 23211, 23212, 27005, 45835, 47583, 47593, 47596, 47603, 47604, 51221, 51160, 51161, 90700, IS021A-SI, Middle Fork at Breckenridge (08935-SM)	Offline Storage & Pipe Upgrades	1.82-inch	1.26
			2.25-inch	1.07
			2.60-inch	0.90
<b>Goose Creek PS Improvements &amp; Wet Weather Storage</b>	Devondale PS (21628-W), Goose Creek PS (46891 & 62418 & 91629 & 91630 & 105936), Saurel PS (43472)	Offline Storage, PS & Force Main Upgrades	2.25-inch	11.00
			2.60-inch	6.84
<b>Anchor Estates PS Eliminations</b>	Vannah PS (01106), Anchor Estates #1 PS (00746 & 00056-W), Anchor Estates #2 PS (MSD0057-LS)	Diversion	1.82-inch	25.39
			2.25-inch	29.55
			2.60-inch	31.14
<b>Hurstbourne I/I Investigation &amp; Rehabilitation</b>	01793	I/I Reduction	SSES/Rehab	

SSO Data Outdated  
 Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.2**  
**SUMMARY OF LEVEL OF PROTECTION EVALUATION**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio
<b>Southeastern Diversion Area</b>				
<b>Parkview Estates I/I Investigation &amp; Rehabilitation</b>	47250	I/I Reduction	SSES/Rehab	
<b>Klondike Interceptor</b>	Alcona (25676), 25560, 25561	Pipe Upgrades	1.82-inch	9.11
			2.25-inch	9.11
			2.60-inch	7.02
<b>Sutherland Interceptor</b>	Sutherland (16649)	Pipe Upgrades	1.82-inch	25.22
			2.25-inch	31.98
			2.60-inch	32.71
<b>Beargrass Interceptor Rehab Phase 2</b>	51594	Sewer Rehab	Rehabilitation	
<b>Pond Creek Area</b>				
<b>Charleswood Interceptor Extension</b>	25477, 25478, Cooper Chapel PS (25480 & MSD0130-PS)	Pipe Upgrades	1.82-inch	62.84
			2.25-inch	7.14
<b>Cinderella PS Elimination</b>	Cinderella PS (60679 & MSD1013-PS), 35309	Diversion	1.82-inch	43.86
			2.25-inch	38.20
<b>Lantana PS I/I Investigation &amp; Rehabilitation</b>	Lantana Drive #1 PS (25484 & 93719 & MSD0101-PS)	I/I Reduction	SSES/Rehab	
<b>Government Center PS Elimination</b>	Government Center PS (MSD0180-PS)	Diversion	1.82-inch	50.05
			2.25-inch	48.01
<b>Avanti PS Elimination</b>	Avanti PS (21229-W)	Diversion	1.82-inch	1448.28
			2.25-inch	1448.28
			2.60-inch	1448.28
<b>Lea Ann Way System Improvements</b>	19360, 19369, 29933, 29948, 29943, 31083, 31084, 79076, Lea Ann Way PS (MSD1010-PS)	Pipe Upgrades	1.82-inch	49.01
			2.25-inch	5.63
<b>Outer Loop &amp; Caven Ave Wet Weather Storage</b>	27116, 70212, 17724, Caven Ave PS (MSD0133-PS)	Offline Storage & Pipe Upgrades	1.82-inch	7.08
			2.25-inch	5.38
<b>Leven PS Elimination</b>	Leven PS (36419 & MSD1019-PS)	Diversion	1.82-inch	152.13
			2.25-inch	74.72

SSO Data Outdated  
 Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.2**  
**SUMMARY OF LEVEL OF PROTECTION EVALUATION**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio
<b>Edsel PS I/I Investigation &amp; Rehabilitation</b>	Edsel PS (92098 & MSD1048-PS)	I/I Reduction	SSES/Rehab	
<b>ORFM Area</b>				
<b>Mellwood System Improvements &amp; PS Eliminations</b>	26752, 26754, 40410, Mill Creek Valley PS (MSD0007-PS), Winton PS (MSD0010-PS), Mellwood Avenue PS (24472 & MSD0023-PS), Canoe Lane PS (24152-W & MSD0024-PS)	PS Upgrades, Pipe Upgrades & Diversion	1.82-inch	25.09
			2.25-inch	26.97
			2.60-inch	26.09
<b>Leland Rd. SSO Investigation</b>	96020	Condition Assessment	Condition Assessment	
<b>Derington Ct. PS I/I Investigation &amp; Rehabilitation</b>	Derington Court PS (MSD0095-PS)	I/I Reduction	SSES/Rehab	
<b>Prospect WQTC Eliminations, Harrods Creek PS, and ORFM System Improvements</b>	40870, 40871, 40872, Barbour Lane PS (42680 & 65633 & 65635), West Goose Creek PS (22436 & MSD0123-PS), Phoenix Hill PS (MSD1044-PS), Glenview Hills PS (MSD0183-PS), Barbour Lane PS (MSD0192-PS), New Market PS (MSD0193-PS), Deep Creek PS (MSD1063-PS), Hunting Creek South WQTC (MSD0292)	PS and Pipe Upgrades, Diversion, WQTC eliminations	2.25-inch	1.69
			2.60-inch	0.99
<b>Mill Creek Area</b>				
<b>Shively Interceptor</b>	04498, 04542, Pioneer PS (81814-W), Fern Lea PS (MSD0047-PS), Garr's Lane PS (MSD0050-PS)	Pipe Upgrades	1.82-inch	5.20
			2.25-inch	6.68
			2.60-inch	6.70
<b>East Rockford PS Relocation</b>	East Rockford PS (04699-W)	PS Replacement and Relocation	PS Relocation	
<b>Small WQTC Area</b>				
<b>Lucas Ln. PS Inline Storage</b>	Lucas Lane PS (MSD0199-LS)	Inline Storage	1.82-inch	112.86
			2.25-inch	95.75
<b>Riding Ridge PS Improvements</b>	Riding Ridge PS (MSD1060-LS)	PS Upgrades	1.82-inch	52.02
			2.25-inch	19.61
<b>Gunpowder PS Inline Storage</b>	Gunpowder PS (MSD1055-LS)	Inline Storage	1.82-inch	78.71
			2.25-inch	59.15
<b>Fox Harbor Inline Storage</b>	Fox Harbor #1 and #2 PS (62769)	Inline Storage	1.82-inch	43.49

SSO Data Outdated  
 Refer to Chapter 5



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.2**  
**SUMMARY OF LEVEL OF PROTECTION EVALUATION**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio
			2.25-inch	81.40
			2.60-inch	87.55
Fairway View PS Improvements	Fairway View PS (MSD1251-2)	PS Upgrades	1.82-inch	10.32
			2.25-inch	7.64
Lake Forest PS SSO Investigation	Lake Forest PS (MSD1169-LS)	Monitoring	Monitoring	
St. Rene Rd. PS Inline Storage	94187	Inline Storage	1.82-inch	212.00
			2.25-inch	97.68
<b>CSS Area</b>				
Sonne PS I/I Investigation & Rehabilitation	Sonne Avenue PS (MSD0042-PS)	I/I Reduction	SSES/Rehab	
Camp Taylor System Improvements	08717, 13931, 13943, 36763, 44396, 44397, 66349, 104223, 104231	SSES, Sewer Rehabilitation & Replacement, Offline Storage	1.82-inch	65.12
			2.25-inch	67.63
			2.60-inch	68.47
Hazelwood PS I/I Investigation & Rehabilitation	Hazelwood PS (55665)	I/I Reduction	SSES/Rehab	
<b>Legend:</b> LS –Lift station, PS – Pump Station, CSO – Combined Sewer Overflow, SSO – Sanitary Sewer Overflow, CSS- Combined Sewer System, WQTC – Water Quality Treatment Center, SSES – Sanitary Sewer Evaluation Study, I/I – Inflow and Infiltration, UMFLS – Upper Middle Fork Lift Station, ORFM – Ohio River Force Main				

SSO Data Outdated  
 Refer to Chapter 5

#### 4.1.2.1 Level of Protection Evaluation Results

The level of protection evaluation presented in Table 4.1.2 was assessed by an analysis referred to as the "knee-of-the-curve" analysis. A knee-of-the-curve analysis typically involves estimating costs for a range of design levels, then comparing performance (benefits) versus cost and identifying the point of diminishing returns. For the Final SSDP, the knee-of-the-curve analysis focused on a comparison of total benefits versus total capital costs at various levels of protection.

The Final SSDP optimization process did not calculate the total capital costs and benefits for each preferred technology at all levels of protection. Total capital costs and benefits were calculated for 35 preferred technologies at a level of protection corresponding to the 1.82-inch and 2.25-inch cloudburst storms. Cost and benefits were calculated for several of the preferred technologies at the 1.52-inch and 2.60-inch levels of protection (recall the 2.60-inch level was not calculated if the 1.82-inch benefit-cost ratio was higher than the 2.25-inch benefit-cost ratio). Costs and benefits for all other preferred technologies at the 1.52-inch and 2.60-inch levels were estimated by extrapolation of the 1.82-inch or 2.25-inch level-of-protection values. All costs reflect the more detailed budget-level cost estimates prepared for the preferred alternatives.

Figure 4.1.1 shows a curve of total benefits as a function of total capital cost for each level of protection. This figure also shows a single point above the curve denoting the total benefits (26,800) and total capital cost (\$169 million, 2008 dollars) for the recommended projects (not including Interim SSDP projects). The figure illustrates a typical knee of the curve response, with the point of inflection representing the point of diminishing returns. As depicted, beyond the 1.82-inch level of protection, additional capital expenditures result in a much slower increase in total benefits. The single point corresponding to the recommended projects lies just at the knee of the curve, demonstrating that the program maximizes benefits to the community with a controlled cost.

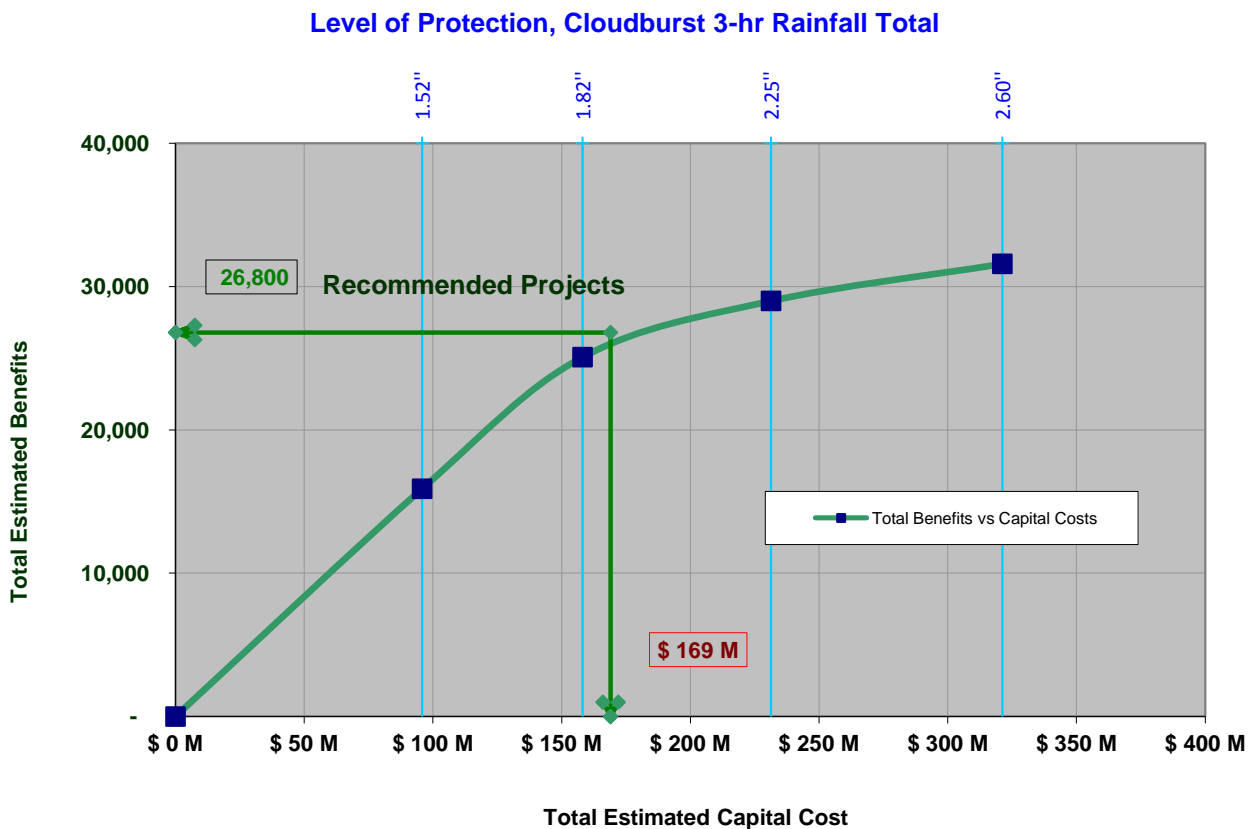
Figure 4.1.2 shows a curve of average project benefit-cost ratio versus total capital cost for each level of protection. There is a single point representing the average benefit-cost ratio (94) and total capital cost (\$169 million, 2008 dollars) for the recommended projects. This curve is plotted in a format to illustrate optimization of the benefit-cost ratio. This figure shows that the maximum average benefit-cost ratio occurs around the 1.82-inch cloudburst storm and benefit-cost ratios decline significantly beyond a 1.82-inch level of protection. The single point shows that the recommended projects are at the highest benefit-cost ratio, again demonstrating that the program maximizes benefits to the community.

Figure 4.1.3 shows a Benefit-Cost curve of three projects (Klondike Interceptor, Middle Fork Relief Interceptor, and Shively Interceptor) at all three levels of evaluation. Based on the evaluation of the three projects selected, the assumptions regarding benefit-cost trends appear to be valid. In two of the three cases, the benefit-cost score for the 2.25-inch cloudburst storm alternative is equal to or less than the score for the 1.82-inch cloudburst storm. In both of these cases the benefit-cost scores for the 2.60-inch cloudburst storm are less than that of the 2.25-

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

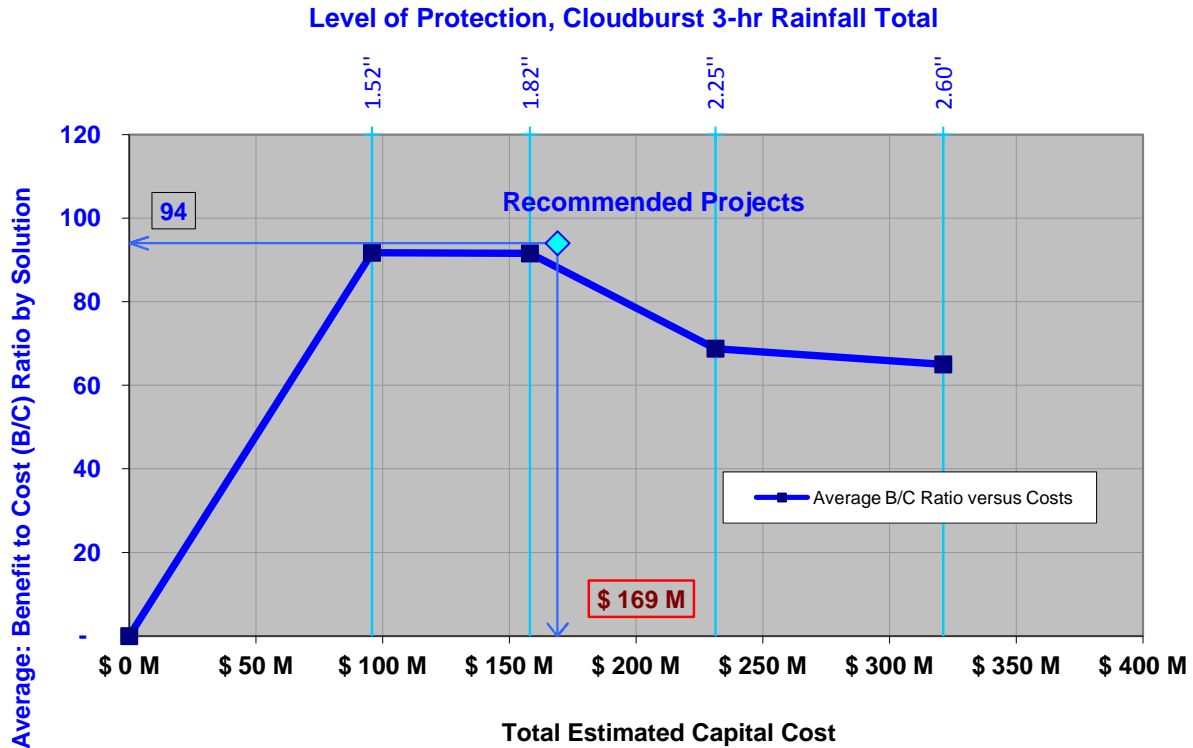
inch cloudburst storm. In one case, the benefit-cost score for the 2.25-inch cloudburst storm is greater than the 1.82-inch cloudburst storm, and in this case the 2.60-inch cloudburst storm benefit/cost score is slightly greater than the 2.25-inch cloudburst storm, and this is the level of protection that was selected. For a full explanation and results of the analysis refer to Appendix 4.1.3 Evaluation of All Levels of Protection Analysis.

**FIGURE 4.1.1 SSDP PROJECT OPTIMIZATION: TOTAL BENEFITS VERSUS TOTAL CAPITAL COST (2008 DOLLARS)**



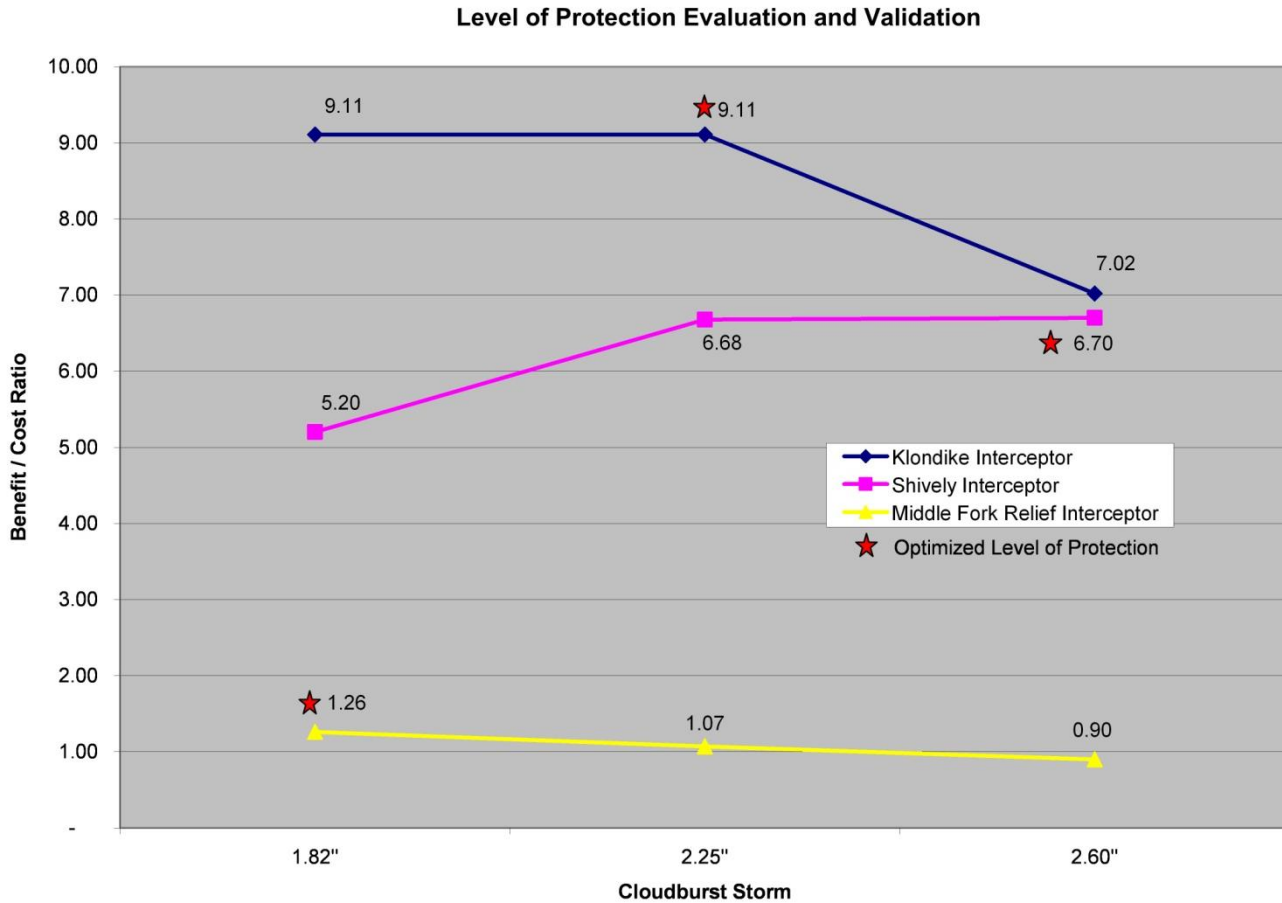
Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 4.1.2 SSDP PROJECT OPTIMIZATION: AVERAGE B/C RATIO VERSUS TOTAL CAPITAL COST (2008 DOLLARS)**



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 4.1.3 SSDP LEVEL OF PROTECTION EVALUATION**





Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 4.1.3 Final SSDP Projects

Driven by the values-based benefit-cost analysis discussed in Chapter 3, the IOAP seeks to present a balanced mix of “green infrastructure” and “gray” solutions to prevent and control SSOs. Since green infrastructure generally is intended to reduce stormwater runoff, it is not directly applicable to flow reduction in a separate sanitary sewer system (SSS). The equivalent to green infrastructure in the Final SSDP includes controlling I/I, using techniques such as disconnecting building laterals, downspouts, sump pumps, and foundation drains that are a direct source of I/I. Gray solutions include options such as storage, diversion, treatment, and conveyance/transport.

The final projects selected for eliminating SSOs also include a mixture of source control (including I/I reduction efforts), wet weather storage, system diversion, conveyance/transport, and basement flooding protection. This mix of control options for SSO locations is a reflection of the benefit-cost analysis and site-specific considerations. Consistent with the Final CSO Long-Term Control Plan (LTCP), the Final SSDP project alternatives are designed to be built around MSD’s existing infrastructure, which may include large diameter pipes and water quality treatment centers (WQTC), and draw on synergistic benefits from other MSD projects.

Overall, the Final SSDP includes 38 gray infrastructure projects, eight I/I reduction projects, and three SSO investigation projects. The Interim SSDP includes six gray infrastructure projects.

The gray infrastructure projects, including the six Interim SSDP projects, are divided into a combination of the following categories, (some projects fall into more than one category):

- 23 conveyance capacity upgrades
- 11 storage projects, inline and offline, many with pipe upgrades as well
- Upgrades or replacements to 12 pump stations
- Elimination of 18 pump stations
- Elimination of 6 small WQTCs, including 5 in the Prospect area
- Expansion of a WQTC

The site-specific level of protection as determined by the value-based benefit-cost analysis resulted in the following for the 38 Final SSDP gray infrastructure projects:

- 24 projects eliminate SSOs up to the 1.82-inch cloudburst storm
- 5 projects eliminate SSOs up to the 2.25-inch cloudburst storm
- 9 projects eliminate SSOs up to the 2.60-inch cloudburst storm

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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Table 4.1.3 represents the final projects chosen for eliminating SSOs at the selected site-specific level of protection. The table includes a list of projects, SSOs controlled by that project, chosen level of protection, capital costs, and scheduled project completion year. In total, there are 214 documented, suspected, and modeled SSOs addressed by the 55 projects (49 Final SSDP and 6 Interim SSDP) listed in Table 4.1.3. This number includes SSOs eliminated by the Interim SSDP projects. Projects are listed by modeled area.

#### **4.1.3.1 Final SSDP Project Fact Sheets and Maps**

Project fact sheets for the Final SSDP projects detailing project specifics are available at the end of this chapter. Each fact sheet includes a project description for the abatement solution, associated capital cost and associated benefit-cost ratio, and lists SSOs addressed by the project solution.

Detailed project maps for each Final SSDP project specify project location and type of solution. Maps also are located at the end of this chapter behind each respective project fact sheet. *Please note: The general representation of the overflow abatement solutions are for preliminary planning purposes only. Alignments and locations may be altered or refined during the design phase.*

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.3**  
**LIST OF FINAL SSDP PROJECTS**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Capital Cost \$ <sup>1</sup>	Annual O&M Dollars	Scheduled Completion Year
<b>Cedar Creek Area</b>							
Idlewood Inline Storage	28998, 28984, 63094, 63095, 70158	Inline Storage	1.82-inch	31.36	\$2,317,000	\$2,800	2023
Fairmount Rd. PS Improvements	Fairmount Road PS (81316 & 07362)	PS Upgrades	2.60-inch	33.29	\$874,000	\$0	2023
Little Cedar Creek Interceptor Improvements	67997, 67999, 86423, 89195, 89197	Pipe Upgrades	1.82-inch	23.86	\$1,875,000	\$21,800	2024
Bardstown Rd. PS Improvements	88545	PS Upgrades	2.25-inch	46.50	\$281,000	\$400	2021
Running Fox PS Elimination	MSD1080-LS	Diversion	1.82-inch	659.52	\$96,000	\$100	2010
<b>Hite Creek Area</b>							
Meadow Stream PS Inline Storage	Meadow Steam PS (91087 & MSD1082-PS)	Inline Storage	1.82-inch	13.77	\$974,000	\$13,000	2016
Floydsburg Rd. I/I Investigation & Rehabilitation	Floydsburg Road (MSD1086-PS, 90776, 108956, 108957, 108958)	I/I Reduction	1.82-inch	--	\$57,000	\$0	2010
Kavanaugh Rd. PS Improvements	Kavanaugh Rd (MSD1085-PS)	PS & Force Main Upgrades	2.60-inch	21.09	\$1,110,000	\$1,400	2024
<b>Floyds Fork Area</b>							
Woodland Hills PS Diversion	33003, 65531	Diversion	1.82-inch	92.26	\$20,000	\$100	2011
Eden Care PS SSO Investigation	Eden Care PS (MSD1105-PS)	Monitor	Monitor	--	--	--	2012
<p><b>SSO Data Outdated</b> <b>Refer to Chapter 5</b></p>							
<p><sup>1</sup> Detailed cost evaluations are included in Appendix 4.1.2 Final SSDP Project Cost Estimates</p>							

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.3**  
**LIST OF FINAL SSDP PROJECTS**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Capital Cost \$ <sup>1</sup>	Annual O&M Dollars	Scheduled Completion Year
Ashburton PS Improvements & Diversion	Olde Copper Court PS (MSD0165-PS), Ashburton PS (MSD0166-PS)	Upgrade Force Main & Pipe	1.82-inch	161.00	\$118,000	\$100	2021
<b>Jeffersontown Area</b>							
Jeffersontown WQTC Elimination	28390, 28391, 28392, 28395, 31733, Jeffersontown WQTC (28173 & 64505 & MSD0255 & IS028-91)	Offline Storage, Pipe Upgrades, WQTC Elimination	1.82-inch	5.23	\$23,737,000	\$28,500	2015
Chenoweth Hills WQTC Elimination, Chenoweth Run and Chippewa PS Improvements	Chenoweth Run PS (MSD0196-PS & 86052 & 64096), Chippewa PS (92061), Chenoweth Hills WQTC PS (MSD0263A-PS), Chenoweth Hills WQTC (MSD0263)	PS & Force Main Upgrades, WQTC Elimination	1.82-inch	20.05	\$3,140,000	\$43,800	2015
Dell Rd and Charlane Pkwy Interceptor Improvements	Charlane Pkwy (28250, 28249, 28340, 28336, 104289), Dell Rd. (28413, 28414, 28415, 28416, 28417)	Pipe Upgrades	1.82-inch	31.34	\$917,000 <sup>1</sup>	\$1,900	2022
Raintree & Marian Ct PS Eliminations	28719, 28711, Marian Court PS (28729), Raintree PS (MSD0149-PS)	Diversion, Pipe Upgrades	1.82-inch	72.76	\$1,005,000	\$1,000	2021
Monticello PS Elimination	Monticello Place PS (MSD0151-PS & 27969)	Diversion	2.60-inch	65.85	\$207,000	\$300	2022
<b>Middle Fork Area</b>							
<p><b>SSO Data Outdated</b></p> <p><b>Refer to Chapter 5</b></p>							
<p><sup>1</sup> Detailed cost evaluations are included in Appendix 4.1.2</p>							

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.3**  
**LIST OF FINAL SSDP PROJECTS**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Capital Cost \$ <sup>1</sup>	Annual O&M Dollars	Scheduled Completion Year
Middle Fork Relief Interceptor, Wet Weather Storage, and Upper Middle Fork LS Diversion	02932, 02933, 02935, 08537, 23211, 23212, 27005, 51221, 51160, 51161, 45835, 47583, 47593, 47596, 47603, 47604, 90700, IS021A-SI, Middle Fork at Breckenridge (08935-SM)	Offline Storage & Pipe Upgrades	1.82-inch	1.26	\$26,627,000	\$18,700	2013, 2023
Goose Creek PS Improvements & Wet Weather Storage	Devondale PS (21628-W), Goose Creek PS (46891 & 62418 & 91629 & 91630 & 105936), Saurel PS (43472)	Offline Storage, PS & Force Main Upgrades	2.25-inch	11.00	\$2,844,000	\$2,100	2024
Anchor Estates PS Eliminations	Vannah PS (01106), Anchor Estates #1 PS (00746 & 00056-W), Anchor Estates #2 PS (MSD0057-LS)	Diversion	2.60-inch	31.14	\$1,909,000	\$51,200	2013, 2016
Hurstbourne I/I Investigation & Rehabilitation	01793	I/I Reduction	1.82-inch	--	\$536,000	\$0	2011
<b>Southeastern Diversion Area</b>							
Parkview Estates I/I Investigation & Rehabilitation	47250	I/I Reduction	1.82-inch	--	\$285,000	\$0	2011
Klondike Interceptor	25676 (Alcona), 26650, 26651	Pipe Upgrades	2.25-inch	9.11	\$558,000	\$2,200	2015
Sutherland Interceptor	Sutherland (16649)	Pipe Upgrades	2.60-inch	32.71	\$412,000	\$900	2023
Beargrass Interceptor Rehab Ph. 2	51594	Pipe Rehab	1.82-inch	--	\$57,000	\$0	2010
<b>Pond Creek Area</b>							
Charleswood Interceptor Extension	25477, 25478, Cooper Chapel PS (25480 & MSD0130-PS)	Pipe Upgrades	1.82-inch	62.84	\$603,000	\$900	2022

**SSO Data Outdated**  
**Refer to Chapter 5**



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**TABLE 4.1.3**  
**LIST OF FINAL SSDP PROJECTS**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Capital Cost \$ <sup>1</sup>	Annual O&M Dollars	Scheduled Completion Year
Cinderella PS Elimination	Cinderella PS (60679 & MSD1013-PS), 35309	Diversion	1.82-inch	22.14	\$2,205,000 <sup>1</sup>	\$100	2023
Lantana PS I/I Investigation & Rehabilitation	Lantana Drive #1 PS (25484 & 93719 & MSD0101-PS)	I/I Reduction	1.82-inch	--	\$20,000	\$100	2011
Government Center PS Elimination	Government Center PS (MSD0180-PS)	Diversion	1.82-inch	44.91	\$1,225,000	\$100	2024
Avanti PS Elimination	Avanti PS (21229-W)	Diversion	2.60-inch	1000.48	\$31,000	\$200	2010
Lea Ann Way System Improvements	19360, 19369, 29933, 29948, 29943, 31083, 31084, 79076, Lea Ann Way PS (MSD1010-PS)	Pipe Upgrades	1.82-inch	49.01	\$827,000	\$1,600	2015
Outer Loop & Caven Ave Wet Weather Storage	27116, 70212, 17724, Caven Ave PS (MSD0133-PS)	Offline Storage & Pipe Upgrades	1.82-inch	7.08	\$6,084,000	\$100	2016, 2024
Leven PS Elimination	Leven PS (36419 & MSD1019-PS)	Diversion	1.82-inch	95.93	\$376,000	\$100	2022
Edsel PS I/I Investigation & Rehabilitation	Edsel PS (92098 & MSD1048-PS)	I/I Reduction	1.82-inch	--	\$367,000	\$0	2011
<b>ORFM Area</b>							
Mellwood System Improvements & PS Eliminations	26752, 41374, 41416, Mockingbird Valley PS (MSD0007-PS), Winton PS (MSD0010-PS), Mellwood Avenue PS (24472 & MSD0023-PS), Canoe Lane PS (24152-W & MSD0024-PS)	PS Upgrades, Pipe Upgrades & Diversion	2.25-inch	26.97	\$3,055,000 <sup>2</sup>	\$2,100	2012, 2024
<p><sup>1</sup> Detailed cost evaluations are included in Appendix 4.1.2</p> <p><sup>2</sup> Detailed cost evaluations are included in Appendix 4.1.2</p>							

SSO Data Outdated  
 Refer to Chapter 5

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.3  
LIST OF FINAL SSDP PROJECTS**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Capital Cost \$ <sup>1</sup>	Annual O&M Dollars	Scheduled Completion Year
Leland Rd. SSO Investigation	96020	Condition Assessment	Monitor	--	--	--	2012
Derington Ct. PS I/I Investigation & Rehabilitation	Derington Court PS (MSD0093-PS)	I/I Reduction	1.82-inch	--	\$265,000	\$700	2012
Prospect WQTC Eliminations, Harrods Creek PS, and ORFM System Improvements	40870, 40871, 40872, Barbour Lane PS (42680 & 65633 & 65635), West Goose Creek PS (22436 & MSD0112-PS), Phoenix Hill PS (MSD1044-PS), Glenview Hills PS (MSD0183-PS), Barbour Lane PS (MSD0192-PS), New Market PS (MSD0193-PS), Deep Creek PS (MSD1063-PS), Hunting Creek South WQTC (MSD0292)	PS and Pipe Upgrades, Diversion, WQTC eliminations	2.25-inch	1.69	\$34,062,000	\$78,300	2015, 2016
<b>Mill Creek Area</b>							
Shively Interceptor	04498, 04542, Pioneer PS (81814-W), Fern Lea PS (MSD0047-PS), Garr's Lane PS (MSD0050-PS)	Pipe Upgrades	2.60-inch	6.70	\$16,419,000	\$11,400	2014
East Rockford PS Relocation	East Rockford PS (04699-W)	PS Replacement and Relocation	1.82-inch	----	\$1,044,000	\$9,300	2021
<b>Small WQTC Area</b>							
Lucas Ln. PS Inline Storage	Lucas Lane PS (MSD0199-LS)	Inline Storage	1.82-inch	112.86	\$183,000	\$400	2021
Riding Ridge PS Improvements	Riding Ridge PS (MSD1060-LS)	PS Upgrades	1.82-inch	52.02	\$27,000	\$100	2014
Gunpowder PS Inline Storage	Gunpowder PS (MSD1055-LS)	Inline Storage	1.82-inch	78.71	\$176,000	\$9,700	2021
Fox Harbor Inline Storage	Fox Harbor #1 and #2 PS (62769)	Inline Storage	2.60-inch	87.55	\$328,000	\$8,000	2021
Fairway View PS Improvements	Fairway View PS (MSD1065-PS)	PS Upgrades	1.82-inch	10.32	\$87,000	\$300	2014

**SSO Data Outdated  
Refer to Chapter 5**

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.3**  
**LIST OF FINAL SSDP PROJECTS**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Capital Cost \$ <sup>1</sup>	Annual O&M Dollars	Scheduled Completion Year
Lake Forest PS SSO Investigation	Lake Forest PS (MSD1169-I/S)	Monitor	Monitor	--	--	--	2012
St. Rene Rd. PS Inline Storage	94187	Inline Storage	1.82-inch	212.00	\$30,000	\$400	2021
<b>CSS Area</b>							
Sonne PS I/I Investigation & Rehabilitation	Sonne Avenue PS (MSD0042-PS)	I/I Reduction	1.82-inch	--	\$265,000	\$11,600	2011
Camp Taylor System Improvements	08717, 13931, 13943, 36763, 44396, 44397, 66349, 104223, 104231	SSES, Sewer Rehabilitation & Replacement, Offline Storage	2.60-inch	68.47	\$28,279,000	\$0	2011, 2013, 2017, 2023
Hazelwood PS I/I Investigation & Rehabilitation	Hazelwood PS (55665)	I/I Reduction	1.82-inch	--	\$173,000	\$1,400	2011

SSO Data Outdated  
Refer to Chapter 5

<sup>1</sup>Detailed cost evaluations are included in Appendix 4.1.2, Final SSDP Project Cost Estimates

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.1.3**  
**LIST OF FINAL SSDP PROJECTS**

SSDP Recommended Project Name/Location	SSO(s) Addressed	Technology	Level of Protection	Capital Cost \$ <sup>1</sup>	Scheduled Completion Year
<b>Interim SSDP Projects</b>					
Beechwood Village Sanitary Sewer Replacement	21061, 21081, 21101, 21153, 21170	Sewer Replacement	--	\$11,800,000	2011
Hikes Lane Interceptor and Highgate Springs PS	17571, 18134, 18298, 18302, 18318-W, 18434, 18471, 18483, 18505, 18595, 49236, 49672, 49673, 49237, 49238, 49239, 49240, 49241, 49242, 49243, 49244, 49245, 49246, 49247, 49248, 49249, 49250, 49251, 49252, 49253, 49254, 49255, 49256, 49257, 49258, 49259, 49260, 49261, 49262, 49263, 49264, 49265, 49266, 49267, 49268, 49269, 49270, 49271, 49272, 49273, 49274, 49275, 49276, 49277, 49278, 49279, 49280, 49281, 49282, 49283, 49284, 49285, 49286, 49287, 49288, 49289, 49290, 49291, 49292, 49293, 49294, 49295, 49296, 49297, 49298, 49299, 49300, 49301, 49302, 49303, 49304, 49305, 49306, 49307, 49308, 49309, 49310, 49311, 49312, 49313, 49314, 49315, 49316, 49317, 49318, 49319, 49320, 49321, 49322, 49323, 49324, 49325, 49326, 49327, 49328, 49329, 49330, 49331, 49332, 49333, 49334, 49335, 49336, 49337, 49338, 49339, 49340, 49341, 49342, 49343, 49344, 49345, 49346, 49347, 49348, 49349, 49350, 49351, 49352, 49353, 49354, 49355, 49356, 49357, 49358, 49359, 49360, 49361, 49362, 49363, 49364, 49365, 49366, 49367, 49368, 49369, 49370, 49371, 49372, 49373, 49374, 49375, 49376, 49377, 49378, 49379, 49380, 49381, 49382, 49383, 49384, 49385, 49386, 49387, 49388, 49389, 49390, 49391, 49392, 49393, 49394, 49395, 49396, 49397, 49398, 49399, 49400, 49401, 49402, 49403, 49404, 49405, 49406, 49407, 49408, 49409, 49410, 49411, 49412, 49413, 49414, 49415, 49416, 49417, 49418, 49419, 49420, 49421, 49422, 49423, 49424, 49425, 49426, 49427, 49428, 49429, 49430, 49431, 49432, 49433, 49434, 49435, 49436, 49437, 49438, 49439, 49440, 49441, 49442, 49443, 49444, 49445, 49446, 49447, 49448, 49449, 49450, 49451, 49452, 49453, 49454, 49455, 49456, 49457, 49458, 49459, 49460, 49461, 49462, 49463, 49464, 49465, 49466, 49467, 49468, 49469, 49470, 49471, 49472, 49473, 49474, 49475, 49476, 49477, 49478, 49479, 49480, 49481, 49482, 49483, 49484, 49485, 49486, 49487, 49488, 49489, 49490, 49491, 49492, 49493, 49494, 49495, 49496, 49497, 49498, 49499, 49500, 49501, 49502, 49503, 49504, 49505, 49506, 49507, 49508, 49509, 49510, 49511, 49512, 49513, 49514, 49515, 49516, 49517, 49518, 49519, 49520, 49521, 49522, 49523, 49524, 49525, 49526, 49527, 49528, 49529, 49530, 49531, 49532, 49533, 49534, 49535, 49536, 49537, 49538, 49539, 49540, 49541, 49542, 49543, 49544, 49545, 49546, 49547, 49548, 49549, 49550, 49551, 49552, 49553, 49554, 49555, 49556, 49557, 49558, 49559, 49560, 49561, 49562, 49563, 49564, 49565, 49566, 49567, 49568, 49569, 49570, 49571, 49572, 49573, 49574, 49575, 49576, 49577, 49578, 49579, 49580, 49581, 49582, 49583, 49584, 49585, 49586, 49587, 49588, 49589, 49590, 49591, 49592, 49593, 49594, 49595, 49596, 49597, 49598, 49599, 49600, 49601, 49602, 49603, 49604, 49605, 49606, 49607, 49608, 49609, 49610, 49611, 49612, 49613, 49614, 49615, 49616, 49617, 49618, 49619, 49620, 49621, 49622, 49623, 49624, 49625, 49626, 49627, 49628, 49629, 49630, 49631, 49632, 49633, 49634, 49635, 49636, 49637, 49638, 49639, 49640, 49641, 49642, 49643, 49644, 49645, 49646, 49647, 49648, 49649, 49650, 49651, 49652, 49653, 49654, 49655, 49656, 49657, 49658, 49659, 49660, 49661, 49662, 49663, 49664, 49665, 49666, 49667, 49668, 49669, 49670, 49671, 49672, 49673, 49674, 49675, 49676, 49677, 49678, 49679, 49680, 49681, 49682, 49683, 49684, 49685, 49686, 49687, 49688, 49689, 49690, 49691, 49692, 49693, 49694, 49695, 49696, 49697, 49698, 49699, 49700, 49701, 49702, 49703, 49704, 49705, 49706, 49707, 49708, 49709, 49710, 49711, 49712, 49713, 49714, 49715, 49716, 49717, 49718, 49719, 49720, 49721, 49722, 49723, 49724, 49725, 49726, 49727, 49728, 49729, 49730, 49731, 49732, 49733, 49734, 49735, 49736, 49737, 49738, 49739, 49740, 49741, 49742, 49743, 49744, 49745, 49746, 49747, 49748, 49749, 49750, 49751, 49752, 49753, 49754, 49755, 49756, 49757, 49758, 49759, 49760, 49761, 49762, 49763, 49764, 49765, 49766, 49767, 49768, 49769, 49770, 49771, 49772, 49773, 49774, 49775, 49776, 49777, 49778, 49779, 49780, 49781, 49782, 49783, 49784, 49785, 49786, 49787, 49788, 49789, 49790, 49791, 49792, 49793, 49794, 49795, 49796, 49797, 49798, 49799, 49800, 49801, 49802, 49803, 49804, 49805, 49806, 49807, 49808, 49809, 49810, 49811, 49812, 49813, 49814, 49815, 49816, 49817, 49818, 49819, 49820, 49821, 49822, 49823, 49824, 49825, 49826, 49827, 49828, 49829, 49830, 49831, 49832, 49833, 49834, 49835, 49836, 49837, 49838, 49839, 49840, 49841, 49842, 49843, 49844, 49845, 49846, 49847, 49848, 49849, 49850, 49851, 49852, 49853, 49854, 49855, 49856, 49857, 49858, 49859, 49860, 49861, 49862, 49863, 49864, 49865, 49866, 49867, 49868, 49869, 49870, 49871, 49872, 49873, 49874, 49875, 49876, 49877, 49878, 49879, 49880, 49881, 49882, 49883, 49884, 49885, 49886, 49887, 49888, 49889, 49890, 49891, 49892, 49893, 49894, 49895, 49896, 49897, 49898, 49899, 49900, 49901, 49902, 49903, 49904, 49905, 49906, 49907, 49908, 49909, 49910, 49911, 49912, 49913, 49914, 49915, 49916, 49917, 49918, 49919, 49920, 49921, 49922, 49923, 49924, 49925, 49926, 49927, 49928, 49929, 49930, 49931, 49932, 49933, 49934, 49935, 49936, 49937, 49938, 49939, 49940, 49941, 49942, 49943, 49944, 49945, 49946, 49947, 49948, 49949, 49950, 49951, 49952, 49953, 49954, 49955, 49956, 49957, 49958, 49959, 49960, 49961, 49962, 49963, 49964, 49965, 49966, 49967, 49968, 49969, 49970, 49971, 49972, 49973, 49974, 49975, 49976, 49977, 49978, 49979, 49980, 49981, 49982, 49983, 49984, 49985, 49986, 49987, 49988, 49989, 49990, 49991, 49992, 49993, 49994, 49995, 49996, 49997, 49998, 49999, 50000	PS Elimination and New Interceptor	--	\$21,216,000	2012
Northern Ditch Diversion Interceptor	MSD0271	New Interceptor / WQTC Elimination	--	\$20,397,000	2011
Sinking Fork Relief Sewer	21103, 25012, 63319	New Relief Sewer	--	\$1,690,000	2010
Southeastern Diversion Structure and Interceptor	08426, 08427, 08430, 08431, 30701, 30702, 49647, 63779, 30680, 30681, 72571-X	New Relief Sewer and Flow Control Modifications	4.50-inch	\$1,744,000	2012
Derek R. Guthrie WQTC	22370, 22385, 32682, 32688, 59169, MSD0277	WQTC Upgrade	4.50-inch	\$102,700,000	2011

SSO Data Outdated  
 Refer to Chapter 5

<sup>1</sup> Detailed cost evaluations are included in Appendix 4.1.2 Final SSDP Project Cost Estimates



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

## **4.2 DEVELOPMENT OF RECOMMENDED PLAN**

### **4.2.1 Prioritization of Projects**

As a guiding principle, MSD's IOAP is being developed based on front-end consideration of source control and green infrastructure. Overall, this means that traditional gray infrastructure in the IOAP are sized after considering both the anticipated flow-reduction benefits of programmatic and site-specific green infrastructure solutions (in the Final LTCP), and source control including reduction of private sources of I/I (in the Final SSDP). Prior to the final design of gray solutions, the actual flow reduction performance will be documented and compared against the estimated targets. The final sizing of the gray solutions will then be based on documented performance of the green infrastructure or other source control solutions previously implemented.

Several green infrastructure and source control solutions in the IOAP will be implemented early in the program to allow data to be gathered on the flow reduction benefits. The following list represents the general order of priority that was used to set the implementation schedule for the Final SSDP projects, in descending order:

- Interim SSDP projects and milestones from previously approved submittals
- "Enabling projects" required to implement Consent Decree or milestone projects
- Source control solutions (especially targeted I/I reduction locations)
- Downstream projects that need to be constructed to capture additional flow when smaller upstream projects are constructed (for example, the Buechel Basin is required prior to constructing the Upper Middle Fork Relief Sewer)
- Capital Improvement Projects already under design that address SSOs, as discussed in Chapter 2, Section 2.3.5.9 (i.e., Shively Interceptor)
- Remaining projects rank-ordered based on benefit-cost ratio and scheduled to assist with cash flow leveling

### **4.2.2 Implementation Schedule to Achieve Consent Decree Requirements**

The Final SSDP project implementation schedule is represented in Figure 4.2.1 at the end of this chapter, prior to the project fact sheets and maps. Eight Final SSDP projects have been divided into multiple construction phases and are reflected in multiple fact sheets and maps at the end of the chapter. Multiple cost estimates representing these projects are also in Appendix 4.1.2.

This phasing approach was implemented to accommodate various construction schedules occurring in one project or to allow for components of one project (if vastly different) to be constructed at different times.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

The eight Final SSDP projects that are divided into multiple phases are:

- Middle Fork Relief Interceptor, Wet Weather Storage, and Upper Middle Fork Lift Station Diversion
- Camp Taylor System Improvements
- Prospect WQTC Eliminations, Harrods Creek Pump Station, and Ohio River Force Main System Improvements
- Mellwood System Improvements and Pump Station Eliminations
- Anchor Estates Pump Station Eliminations
- Outer Loop and Caven Avenue Wet Weather Storage
- Raintree and Marian Court Pump Station Eliminations
- Goose Creek Pump Station Improvements and Wet Weather Storage

#### **4.3 PUBLIC INVOLVEMENT**

As stated in the Consent Decree, one requirement for public involvement is for the Wet Weather Team (WWT) to assist in developing the plan to involve the public in planning, prioritization and selection of projects. This section recaps the public involvement process throughout the development of the Final SSDP projects.

Early in the IOAP development stage, the WWT, including the WWT Stakeholder Group and the technical team, developed a risk-management approach to evaluating and prioritizing alternative approaches to SSO control. This process was based on managing the risks to a set of community values identified by the WWT Stakeholder Group. The process of identifying, evaluating, and prioritizing projects was a highly interactive process involving all members of the WWT. The interactive process, with the essential engagement of the WWT Stakeholder Group, was critical to the success of the Final SSDP because it created a well-documented and transparent process to consider a wide range of community concerns. This process used a benefit-cost approach with performance measures that had complete buy-in from the WWT Stakeholder Group.

A review of the steps of the values-based decision making process is as follows:

- WWT Stakeholder Group defined values and relative weights for the values;
- The technical team developed draft performance measures and scales based on the “focus areas” or objectives WWT Stakeholder Group identified for the values;
- WWT Stakeholder Group reviewed and helped refine the performance measurement scales;

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

- The technical team used the performance scales to evaluate alternatives; and
- WWT Stakeholder Group reviewed the results and refined scoring considerations.

During the course of 22 WWT Stakeholder Group meetings, numerous ideas for specific education programs and potential SSO abatement solutions were identified. Records of the ideas were distributed to the technical team for consideration as the potential solutions were identified and evaluated.

The work of the WWT was essential to define the goals and objectives of the IOAP and the public involvement program. With the goals and objectives in hand, the technical team of consultants and MSD staff conceptualized and prepared approaches for the broader public to review and provide comment at public meetings. MSD and the WWT believed it would be valuable to have frequent contact with the public to validate the guidance provided by the WWT Stakeholder Group. As a result, there were four rounds of public meetings; each at a specific phase of the planning process when decisions and selection of priorities were needed.

The first two rounds of public meetings, held in Spring 2007 and Fall 2007 respectively, focused on defining the Project WIN purpose and preparing the public for what was to come in the future related to infrastructure improvements and associated sewer rate increases. The third round of public meetings, in Spring 2008, was specifically designed to give the public and impacted neighborhoods information on the types, locations, and size of facilities that were being considered. The public meetings provided public notice that the facilities were under serious consideration for mitigation; engaged the public in discussion about these facilities and the proposed schedule for construction; and informed the public of the remaining steps of the process.

The fourth round of public meetings to receive public comment on the IOAP was held in November 2008. These public meetings were specifically designed to present the IOAP program in an informal forum that encouraged questions and answers with the public. The presentations included an overview of the program, including project lists, budgets, schedules, and potential rate impacts. To reach as many customers as possible, a presentation was also videotaped for viewing by the public.

In addition to the public meetings, a public hearing was held on December 2, 2008. The purpose of the public hearing was to receive formal comments from the public about the content of the IOAP. The draft IOAP was distributed for public review 30 days before the public hearing. The public notice was published in *The Courier-Journal* announcing the availability of the draft plan, the public hearing date, time and location, and the deadline for the acceptance of comments on the plan. The deadline for accepting comments on the plan was 30 days after the notice of the plan availability.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

#### **4.4 ENVIRONMENTAL BENEFITS OF RECOMMENDED PROGRAM**

Environmental benefits, in addition to the public health benefits of SSO reduction, are a critical measure for selecting and optimizing solutions to eliminate SSOs and basement backups. This section describes the environmental benefits of SSO elimination.

##### **4.4.1 Determining Environmental Benefits**

Through the stakeholder process, a list of values most vital to the community, as well as the means to measure them, was identified and refined. The WWT Stakeholder Group ultimately identified five project-specific values and associated performance criteria that were selected to be evaluated during the benefit-cost analysis. All of the criteria included environmental benefit.

The benefit-cost analysis tool was important because it provided the means to track and rate the diverse environmental benefits of each solution. It also included cost contingencies for properly designing, installing, and maintaining the environmental benefits inherent to the proposed solutions. The benefit-cost analysis tool also provided standards through a list of criteria that could not be violated (fatal flaws) regardless of any cost advantage.

- Five Project-Specific Values with Required Environmental Benefits**
- 1 Regulatory Performance
  - 2 Public Health Enhancement
  - 3 Asset Protection
  - 4 Environmental Enhancement
  - 5 Eco-Friendly Solutions

Table 4.4.1 provides an overview of how the Final SSDP performs with respect to these five values. Under some values, such as Regulatory Performance, the Final SSDP will provide complete compliance for all rainfall events at or less than the defined level of protection.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.4.1**  
**SSDP PROJECT-SPECIFIC VALUES WITH ENVIRONMENTAL BENEFITS**

Criteria		SSDP Distinguishing Attribute
<b>Regulatory Performance</b>	Eliminating Overflows	No overflows at or below the defined level of protection at known or suspected SSO locations.
	Eliminating or Reducing Overflow Volume	No overflows at or below defined level of protection at known or suspected SSO locations. Overflow volumes may be reduced above the defined level of protection at known and suspected SSOs.
<b>Asset Protection</b>	Eliminating or reducing surcharging and basement back-ups	No basement back-ups at or below the defined level of protection within zone of influence of known or suspected SSO locations. Surcharging reduced above the defined level of protection within zone of influence of known or suspected SSO locations.
	Aquatic and Terrestrial Habitat Protection	No solution will, in any way, impact the aquatic and terrestrial habitat of endangered species.
<b>Environmental Enhancement</b>	Aesthetics - Solids and Floatables	All solutions will reduce floatables by 1) eliminating overflows, and thus floatables, at or below the defined level of protections and 2) reducing overflow volumes above the defined level of protections, in particular first-flush floatables.
	Aesthetics - Odor and Air Emissions	No solution will create odors occasionally affecting more than 20 customers. All storage solutions near customers will be required to install and maintain odor-control equipment.
	Dissolved Oxygen Impacts	All solutions will provide intermittent improvement of in-stream dissolved oxygen.
	Downstream Impacts	All solutions will provide intermittent improvement of in-stream BOD and nutrient loads.
	Stream Flow Impacts (Peak flows)	All solutions will provide intermittent reduction of stream peak flows.
	Stream Flow Impacts (Dry Weather Flow)	No solution will impact dry weather flow.
	<b>Eco-Friendly Solutions</b>	Non-Renewable Energy Consumption
	Use of Natural Systems	No solutions will permanently displace more than 5 acres of wetlands or 50% of locally available green space. Most conveyance solutions will replace existing features and will have no permanent displacement of wetlands or green areas.
	Multiple-Use Facilities	No Solution will impact recreational opportunities. In fact, many solutions will provide new recreational opportunities.
	Source Control of sub watershed pollutant loads	By elimination of overflows at known, suspected and new SSOs, there will be complete source control at or below the defined level of protection. There will be some source control above the defined level of protection, particularly of the first-flush contaminants.
	Non-Obtrusive Construction Techniques	All RDII reduction will be done with the latest non-obtrusive techniques such as in-situ lining and repairs. There will also be opportunities for non-obtrusive pipe work such as directional drilling. Given the nature of the solutions, there will be limited opportunities for non-obtrusive construction techniques for gray projects such as storage sites. BMPs will be required for all construction projects.
	Consistent Land Use	All features will be consistent with neighborhood or adjacent land use. Most conveyance solutions will be underground using existing right of ways.
	Impermeable Surfaces	Most conveyance solutions and many storage solutions, especially underground storage, will result in no change in impervious areas. All other solutions will include stormwater management features.
	LEEDS Performance	Most systems use gravity for energy. There will be opportunities for LEEDS in pumps, controls and lighting.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

#### **4.4.2 Measuring and Modeling Environmental Benefits**

Elimination of SSOs and basement backups clearly provide environmental benefits as a whole. Based on water quality data from 2005-2007 normalized by rainfall annually, over 290 million gallons (MG) of overflows could potentially be removed by implementing the Final SSDP. On average, this would annually remove 100 tons of biochemical oxygen demand (BOD)<sub>5</sub> and 200 tons of suspended solids from local waterways. In addition, the improvements to the Jeffersontown WQTC and elimination of the Prospect WQTCs would reduce nutrient loads in the respective watersheds.

Under the Final SSDP, there is no specific program to measure and model the benefits of SSO reduction on the environment. In the next section, the elimination of SSOs and basement backups as the key measurement of success are discussed. Moreover, other programs will capture the benefits and evaluate the overall improvements of modeled areas. For example, the Beargrass Creek Total Maximum Daily Load (TMDL) program will use reduced SSO events and volumes as well as positive impacts from the Final CSO LTCP to predict in-stream improvements.

#### **4.5 MEASURES OF SUCCESS**

This section provides an overview of known, documented SSO locations and the associated project that addresses the SSO, as well as a detailed discussion of the performance goals that will be used to measure the success of each Final SSDP project. The measures of success are a means to demonstrate compliance with the Consent Decree requirements and to quantify the benefits achieved from SSO elimination projects. Each project's performance goals should be tailored to site-specific situations. A review of the Final SSDP projects after completion will evaluate how well the project accomplished the performance goals that were established before the project began.

Table 4.5.1 at the end of this chapter, following the implementation schedule, lists the known, documented SSOs, SSO characteristics, the associated project that addresses the SSO (including Final SSDP, Interim SSDP, and Capital Improvement Projects), levels of protection, overflow volumes, and project start/complete dates. The table is sorted by Project Name followed by SSO ID. Detailed fact sheets for each documented SSO are available for review in Appendix 4.5.1 SSO Fact Sheets. The SSO fact sheets provide additional information such as a map of the SSO location, a background and history of the SSO location, downstream landuse, receiving stream, and the overflow volume summary for the past five years.

The four performance goals to be tracked under the Final SSDP include:

1. No Wet Weather, Capacity-Related SSOs under the Selected Level of Protection
2. No Wet Weather, Capacity-Related Basement Backups under the Selected Level of Protection



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

3. Sufficient Treatment Capacity under the Selected Level of Protection
4. Project Flow Monitoring Performed and Documented

It is worth noting that Goal One is the only goal specifically required by the Consent Decree. Goals Two through Four are in response to WWT Stakeholder Group requests and/or Kentucky Department of Environmental Protection (KDEP) Permit and regulatory requirements. Additionally, an overriding success measure and initial goal identified by MSD already met is that the plan is cost-effective for MSD ratepayers as presented in Figure 4.1.2. The next section provides an overview of the measure of success for each performance goal.

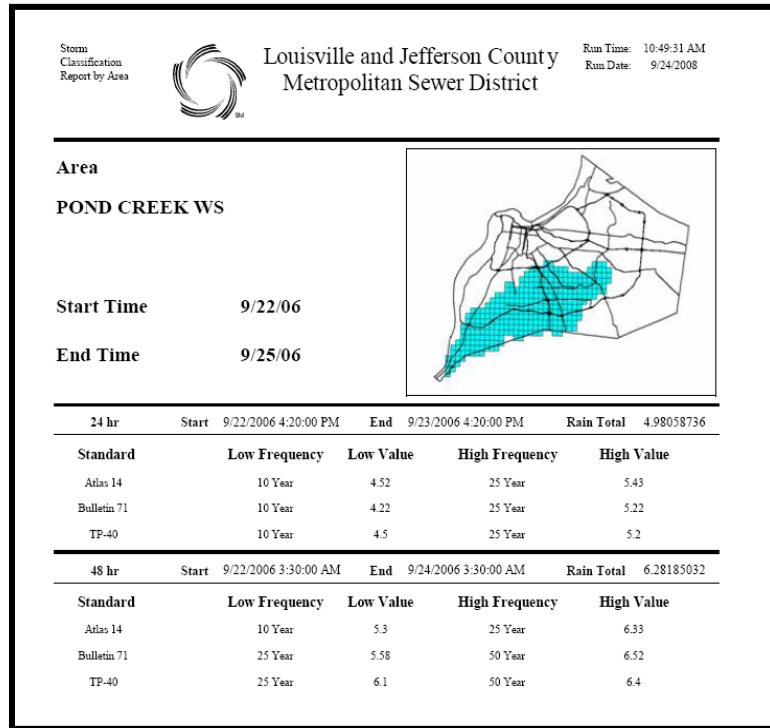
#### **4.5.1 Goal One: No Wet Weather, Capacity-Related SSOs under the Selected Level of Protection**

Since the main premise of the Consent Decree is to prevent unauthorized discharges, the goal of the Final SSDP is to eliminate capacity-related SSOs under the site-specific levels of protection. To demonstrate the success of the Consent Decree premise, monitoring of the SSOs will be implemented. MSD will follow Sewer Overflow Response Protocol (SORP) guidelines to monitor SSOs.

Key to the monitoring is determining the magnitude of the rainfall, how significant the rainfall event was, and did the event exceed the level of protection for the appropriate area. MSD developed a rain-tracking tool called *MSD-NET RainTrack* that utilizes MSD's rain gauge network, radar data, and various software to determine the rainfall frequency for any area within the MSD collection system. Figure 4.5.1 is an example of the tool output displaying the rainfall frequency for various durations and rainfall distributions for a significant September 2006 storm in the Pond Creek watershed.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 4.5.1 EXAMPLE OF OUTPUT FROM MSD RAIN-TRACKING TOOL**



In addition to the rain-tracking tool, the hydraulic models can provide insight into the magnitude of the storm. The Post Construction Compliance Monitoring Plan, (Volume 1, Section 6.5) discusses how the hydraulic models will be maintained. The models will be re-calibrated on a regular basis and will be modified to reflect changes in collection systems, Final SSDP improvements, and rainfall-derived infiltration and inflow (RDI/I) reduction measures. Additionally, calibrated models can be used to determine if specific significant storms created watershed conditions that exceed the levels of protection.

Once a solution has been constructed and a significant storm has been monitored, MSD can measure the success of that solution. If the measure is successful for two consecutive significant storm events, then the solution is deemed successful relative to Goal One.

If the measure is unsuccessful under one significant (defined level of protection) storm event, MSD will utilize its adaptive management process to improve the project. For example, these improvements could include additional storage or targeted RDI/I-reduction measures upstream of the solution.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

#### **4.5.2 Goal Two: No Wet Weather, Capacity-Related Basement Backups under the Selected Design Level**

A second goal for measuring the success of Final SSDP projects is to ensure basement flooding does not occur in the pre-remediated surcharge zone of influence under the level of protection and after the projects are complete. This is not a Consent Decree requirement, but rather a priority identified by the Wet Weather Stakeholder Group.

Success will be measured in the same manner as Goal One, except that the measurement will be for basement flooding in the zone of influence of known or suspected SSOs. If no basement backups due to capacity are reported for two consecutive significant storm events (defined level of protection or greater), then the solution is deemed to be successful relative to Goal Two.

If the measure is unsuccessful under one significant (defined level of protection) storm event, MSD will utilize their adaptive management process to improve the project. For example, these improvements could include additional storage or targeted RDI/I-reduction measures upstream of the solution.

#### **4.5.3 Goal Three: Sufficient Treatment Capacity under the Selected Level of Protection**

A third goal for measuring success of Final SSDP projects is to prevent WQTCs from exceeding wet weather capacity, which could potentially cause basement backups and SSOs in the upstream system and at the WQTC. The System Capacity Assurance Plan (SCAP) provides standards and details how the capacity of a WQTC is established, updated, and used for project evaluations. The SCAP is available on MSD's website under the Project WIN public repository at <http://www.msdlouky.org/projectwin/docs.htm>.

Success will be measured in the same manner as Goal One and Goal Two, except that the measurement will be for bypasses or violations at the WQTC. If no capacity related bypasses or violations are reported for two consecutive significant storm events (defined level of protection or greater), then WQTC improvements are deemed to be successful relative to Goal Three.

If the measure is unsuccessful under one significant (defined level of protection) storm event, MSD will utilize its adaptive management process to improve the project. For example, these improvements could include additional storage or targeted RDI/I-reduction measures upstream of the WQTC or additional WQTC improvements.

#### **4.5.4 Goal Four: Project Flow Monitoring Performed and Documented**

Flow monitoring related to the Final SSDP will build upon the pre-established Post Construction Compliance Monitoring program. Pre-construction data will be compared to the post-construction data to evaluate the effectiveness of improvements. Success will be measured in two ways. First, the flow monitoring will be used to determine if projected RDI/I reduction efforts

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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(refer to Appendix 2.3.4 RDI/I Method and Modeling Techniques Technical Paper) utilized in solution development has been achieved. Second, downstream solutions must be successful, as measured by Goal One. Ultimately, data provided by flow monitoring will dictate success of the project.

Table 4.5.2 provides an overview of the specific requirements for each goal, type, the characteristics of success, and the specific feature that is successful.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 4.5.2**  
**FINAL SSDP MEASURES OF SUCCESS**

Goal	Measurement	Location of Measurement	Event Triggering Measurement	Program Responsible for Measurement	Agency Requiring Measurement	Characteristics of Success	Successful Feature	
1	<b>No Capacity Related Overflows under the Level of Protection</b>	Overflow, or lack thereof, at known, suspected or new SSO location	By solution (branch)	Large rainfall event near or above level of protection for solution area (branch)	SORP	Consent Decree	Two or more periods with rainfall at or above design conditions with NO overflows at known, suspected or new SSO locations within branch	Solution
2	<b>No Capacity Related Basement Back-ups under the Level of Protection</b>	Basement back-ups, or lack thereof, in zone of influence upstream of known, suspected or new SSOs	By solution (branch)		SORP	WWT Stakeholder Group	Two or more periods with rainfall at or above design conditions with NO basement back-ups within zone of influence of overflows at known, suspected or new SSO locations	Downstream Solution
3	<b>Sufficient Treatment Capacity under the Level of Protection</b>	Bypass or inadequate treatment, or lack thereof, at WQTCs in separate sewer system	By WQTC	Large rainfall event near or above cloudburst conditions for collection-system area	SCAP/CMOM	KDEP	Two or more periods with rainfall at or above 2-year cloudburst design conditions with NO bypasses or WQTC violations	WQTC
4	<b>Project Flow Monitoring Performed and Documented</b>	Reduction of projected RDI/I used in Hydraulic Modeling (1)	By any solution requiring RDI/I reduction as part of technology (2)	Any large storm (comparison based on control basin)	Post Construction Compliance Monitoring Plan, (See Volume 1, Section 6.5)	WWT Stakeholder Group requirement for RDI/I reduction as first part of any solution	Two or more periods with rainfall where RDI/I is reduced at or above requirement listed in RDI/I reduction memorandum	Downstream Solutions success eliminates the need for additional monitoring
		Overflow, or lack thereof, at downstream known, suspected or new SSO locations	By solution (branch)	Large rainfall event near or above level of protection for solution area (branch)	SORP		Two or more periods with rainfall at or above level of protection with NO overflows at downstream known, suspected or new SSO locations	

**Legend:** CMOM - Capacity, Management, Operations, and Maintenance  
**Notes:** 1. These RDI/I reduction rates are listed in RDI/I-reduction memorandum (Appendix 2.3.4).  
2. These solutions are listed in I/I program memorandum (Appendix 3.1.1)



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

#### **4.5.5 Benefits of the Measures of Success**

The measures of success are a means to show compliance and benefits achieved from projects undertaken. Meeting these performance goals has many potential benefits including: improved water quality, reducing negative impacts on public health, fewer impacts on receiving waters, and legal compliance. These measures are also a means to provide documented project results and verification that the benefit-cost analyses and risk management approach used to choose targeted deficiencies, levels of protection, and project scheduling were effective. The success measures encompass a flexibility to consider site-specific and project-specific values in an effort to find cost-effective means to reduce SSOs. Communication, collaboration, data tracking, documentation, and trend monitoring will be instrumental in achieving these success measures. Operational data from the Capacity, Management, Operations, and Maintenance (CMOM) and SORP may also be useful to incorporate into projects.

#### **4.5.6 Additional Performance Goals**

In addition to the performance goals described in the previous section, projects will follow standard MSD business practices. Performance goals for sewer construction and acceptance testing will be based on MSD standard specifications and the Inspector Guidance Manual. The Flow Monitoring Field Operations Program (CMOM Section 2.2.6) provides data to support specific project needs such as watershed hydraulic modeling and calibration. The Water Quality Monitoring Program (CMOM Section 2.1.11) is a well-established program that uses a watershed management approach with routine water quality monitoring, investigative water quality monitoring, and water quality monitoring for spill impact. The Contingency Plan for Sewer and Treatment Systems Programs (CMOM Section 2.1.12) has its own performance goals for emergency response, public notification, agency notification, planning and water quality monitoring. Documentation and policies for emergency issues that could result in unauthorized discharges are detailed in the SORP section of the contingency plan. Additional green solution benefits and detailed monitoring procedures are found in Volume 1 of the IOAP.

#### **4.5.7 New SSO Locations**

It is anticipated that new SSO locations will be found over time. As a result, existing solutions will be modified to address new SSO locations. New SSOs could be a result of the following:

- Structural deficiencies that cause a loss of downstream capacity over time which may result in an overflow upstream of the structural deficiency. These structural deficiencies could include sewer collapses, the loss of efficiency at pump stations, blockages, or root intrusions.
- Increases in RDI/I due to long-term deterioration of the sewer system.
- Increases in flow through private property connections, such as illicitly-connected sump pumps. During wet weather, the increased flow could result in an overflow in the area adjacent or downstream of the connections.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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These new locations will be addressed on a case-by-case basis through MSD's adaptive management process (e.g., new SSOs will be added to the SORP investigation list and monitored. If necessary, hydraulic models will be validated to the new SSOs and used to develop solutions). SSOs that are not capacity-related will be addressed through the Gravity Preventative Maintenance and Continuing Sanitary Sewer Assessment (CSSA) Programs.

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Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**Chapter 5 is new to Volume 3 for the 2012 Modification.**

## **CHAPTER 5: 2012 SANITARY SEWER DISCHARGE PLAN MODIFICATION**

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### **SUPPORTING INFORMATION**

Appendix 5.3.1 2012 Project Modification Justification  
 Appendix 5.3.2 2012 Revised Benefit Cost Analyses

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

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## **CHAPTER 5: 2012 SANITARY SEWER DISCHARGE PLAN MODIFICATION**

### **5.1 SSDP IMPLEMENTATION UPDATE**

As of May 2013, Louisville and Jefferson County Metropolitan Sewer District (MSD) has completed and certified 28 SSDP projects, including significant inflow and infiltration reduction projects. The 'Big Four' SSO elimination projects at Beechwood Village, Southeast Diversion, Hikes Point and the Highgate Springs Pump Station have been completed, reducing SSO volume by approximately 70 percent. Various projects related to the elimination of the five package treatment projects in the Prospect area and the elimination of the Jeffersontown WQTC are either in design or under construction. Completed SSDP projects are listed in Table 5.1.1.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 5.1.1**  
**COMPLETED SSDP PROJECTS AS OF MAY 2013**

CERTIFICATION DATES FOR SSDP PROJECTS			
(Sorted By ACD Date, 5/31/13)			
ACD Project Number	Project Name	Date Completed	ACD Date
S_PO_WC_PC07_M_01_A	AVANTI PS ELIMINATION	10-Jul-09	28-Jul-09
SINKING FORK RELIEF SEWER	SINKING FORK RELIEF SEWER	30-Nov-09	23-Dec-09
S_CC_CC_MSD1080_S_01_C	RUNNING FOX PS ELIMINATION	10-Mar-10	31-Dec-10
S_SD_MF_NB06_S_13_C	BEARGRASS INTERCEPTOR REHABILITATION PH 2	14-Dec-10	31-Dec-10
S_HC_HC_MSD1086_M_07_C_A	FLOYDSBURG RD I/I INVESTIGATION & REHABILITATION	17-Dec-10	31-Dec-10
BEECHWOOD VILLAGE SANITARY SEWER REPLACEMENT	BEECHWOOD VILLAGE SANITARY SEWER REPLACEMENT	29-Sep-10	27-Apr-11
S_FF_FF_NB01_S_01_C_A	WOODLAND HILL PS DIVERSION	4-Mar-10	30-Jun-11
S_SD_MF_NB03_S_07_C	PARKVIEW ESTATES I/I INVESTIGATION & REHABILITATION	28-Jun-11	30-Jun-11
S_MC_MF_55665_S_07_C	HAZELWOOD PS I&I INVESTIGATION & REHABILITATION	30-Jun-11	30-Jun-11
S_OR_MF_42007_S_07_C	SONNE PUMP STATION I&I INVESTIGATION & REHABILITATION	30-Jun-11	30-Jun-11
NORTHERN DITCH DIVERSION INTERCEPTOR	NORTHERN DITCH DIVERSION INTERCEPTOR	16-Feb-11	31-Jul-11
S_PO_WC_PC11_M_07_C	EDSEL PS I/I INVESTIGATION & REHABILITATION	27-Sep-11	30-Sep-11
S_SF_MF_30917_M_09_A	CAMP TAYLOR #1 - SSES	8-Jul-11	31-Dec-11
CPE/CCP MODIFICATIONS TO WQTC	CPE/CCP MODIFICATIONS TO WQTC	19-Dec-11	31-Dec-11
S_MI_MF_NB07_S_07_C	HURSTBOURNE I&I INVESTIGATION & REHABILITATION	27-Dec-11	31-Dec-11
S_PO_WC_PC05_M_07_C	LANTANA PS I/I INVESTIGATION & REHABILITATION	29-Dec-11	31-Dec-11
S_OR_MF_NB03_S_07_C	DERINGTON CT PS I/I INVESTIGATION & REHABILITATION	30-Mar-12	31-Mar-12

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 5.1.1**  
**COMPLETED SSDP PROJECTS AS OF MAY 2013**

<b>CERTIFICATION DATES FOR SSDP PROJECTS</b>			
(Sorted By ACD Date, 5/31/13)			
ACD Project Number	Project Name	Date Completed	ACD Date
SOUTHEASTERN DIVERSION STRUCTURE & INTERCEPTOR	SOUTHEAST DIVERSION STRUCTURE & INTERCEPTOR	19-Apr-12	12-May-12
HIKES LANE INTERCEPTOR /HIGHGATE SPRINGS PS	HIKE LANE INTERCEPTOR & HIGHGATE SPRINGS PS	2-Nov-12	27-Nov-12
S_FF_LF_NB01_S_13_C_A	LAKE FOREST PS SSO INVESTIGATION	18-Dec-12	31-Dec-12
S_HC_HC_MSD1082_S_09A_C	MEADOW STREAM PS INLINE STORAGE	18-Dec-12	31-Dec-12
S_OR_MF_NB01_M_01_B	MELLWOOD SYS 1 - MELLWOOD PS & FORCE MAIN	19-Dec-12	31-Dec-12
S_MI_MF_NB06_M_01_A_A - 2	ANCHOR ESTATES- VANNAH PS ELIMINATION	15-Oct-11	31-Dec-13
S_MC_WC_NB01_M_01_A	SHIVELY INTERCEPTOR	13-Apr-12	31-Dec-14
S_FF_FF_NB03_M_01_C_A	ASHBURTON PS IMPROVEMENTS AND DIVERSION	30-Dec-09	31-Dec-21
S_MC_WC_NB02_S_03_C	EAST ROCKFORD LANE PS RELOCATION	30-Mar-12	31-Dec-21
S_FF_CC_81316_M_03_C_A	FAIRMOUNT RD PS IMPROVEMENTS	24-Apr-12	31-Dec-23
S_PO_WC_PC06_M_01_C	GOVERNMENT CENTER PS ELIMINATION	1-Apr-11	31-Dec-24

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

## **5.2 2012 SANITARY SEWER DISCHARGE PLAN MODIFICATION**

As part of the adaptive management approach outlined in the approved 2009 Integrated Overflow Abatement Plan (IOAP), the MSD has been expanding the monitoring network throughout its sewer system.

MSD has been utilizing data from this network to recalibrate the hydrologic and hydraulic models used to size overflow abatement projects and refine individual project approaches and sizes based on an improved understanding of the sewer system operation and the relationship of certain overflows to one another. This chapter outlines the project modifications resulting from this effort along with program updates for the green infrastructure program. A detailed description of the project modification process is outlined in Volume 1, Chapter 6.5.3.7.

## **5.3 FINAL SELECTION OF THE 2012 RECOMMENDED PLAN**

The tables at the end of this chapter summarize the level of control results for each project within the 2012 project suite, both those proposed for modification and those remaining the same as proposed in the 2009 plan. The level of control analysis for all projects in the 2012 suite, both those modified and those remaining the same, are provided in Table 5.3.1. In addition, the final 2012 project suite and revised project schedule are provided in Table 5.3.2 along with the revised project schedule.

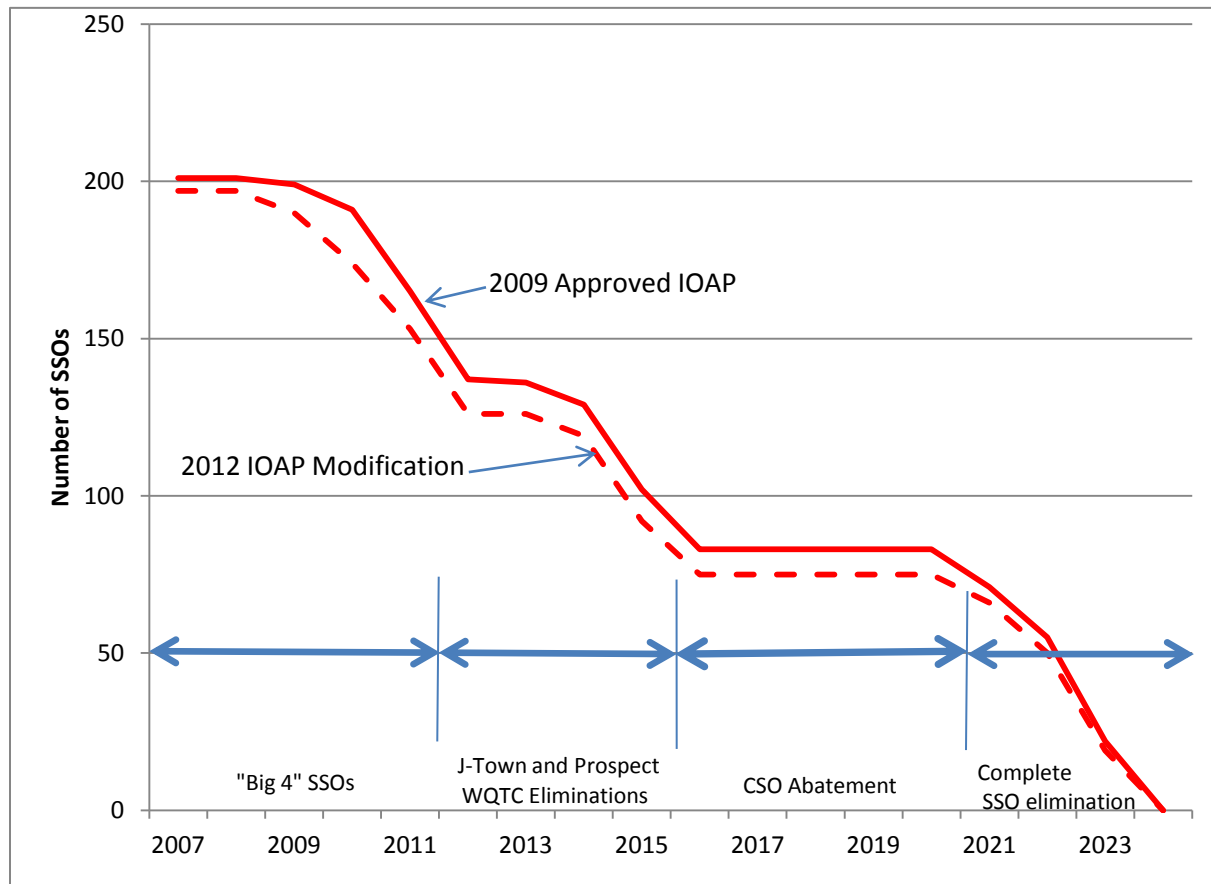
Justification for individual project modifications can be found in Appendix 5.3.1 along with a countywide project map. All benefit and cost analyses can be found in Appendix 5.3.2.

Figure 5.3.1 on the next page demonstrates that the proposed changes result in a more effective overflow abatement program with higher community benefit and more expeditious overflow reduction as a program.

A revised SSDP project schedule is attached at the end of this chapter, titled MSD Integrated Overflow Abatement Plan Implementation Schedule (SSDP) (01 Jan 2009- 31 Dec 2024).

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 5.3.1 - SSO REDUCTIONS THRU 2024**



**5.4 INFLOW AND INFILTRATION REDUCTION UPDATE**

MSD’s 2009 IOAP outlined the District’s initial approach to reduce inflow and infiltration (I/I) and the justification of project sizing based on projected modeled I/I reductions. The chief objectives of the I/I Reduction Program for SSO Abatement include:

- Removing sufficient rainfall-derived inflow and infiltration (RDI/I) to reflect removal assumed in SSO Abatement modeling efforts,
- Complementing and coordinating with other sewer rehabilitation objectives, namely efforts associated with the Continuous Sewer System Assessment (CSSA) and Blockage Abatement Program, the Capacity, Management, Operations, and Maintenance (CMOM) Program, and the Sewer Capacity Assurance Plan (SCAP),

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

- Removing I/I from the sanitary sewer system to effectively manage operational, maintenance and treatment costs, thus maintaining lower sewer rates.
- Committing to an “I/I Reduction First” approach to SSO abatement, before constructing new infrastructure.
- Complying with all regulatory guidelines to protect the environment and best serve MSD ratepayers.

The following section provides an update on the green program following approximately three years of implementation.

#### **5.4.1 Inflow/Infiltration (I/I) Reduction Program Background**

The terms of this Consent Decree require elimination of SSOs and minimization of CSOs to specific levels of control. As guided by the Wet Weather Team (WWT) Stakeholder Group (see Volume 1 of the IOAP for details of the stakeholder process), MSD has committed to use I/I removal as the first approach to abate SSOs.

To meet this commitment, MSD has developed several programs to address I/I removal.

##### **5.4.1.1 I/I Reduction Program Overview**

Sanitary sewers are pipes designed to transport wastewater from sanitary plumbing fixtures, such as toilets, sinks, bathtubs, showers, and lavatories. The term I/I is an abbreviation for Inflow/Infiltration and is used to describe the sources of stormwater (rain and groundwater) that enter into the dedicated sanitary sewer system through structural sewer defects and illicit connections. The I/I Reduction Program has been implemented to identify and remove I/I sources from the sanitary sewer system. These sources can overload the sanitary sewer system and cause sanitary sewer backups into homes and businesses, as well as sanitary sewer overflows (SSOs) to nearby communities and sensitive environmental resources such as rivers and creeks.

Inflow sources are those that flow directly into the sanitary sewer via a defined route (pipe, etc.). Infiltration sources are those that inadvertently enter into the sanitary sewer via cracks, holes, faulty connections, or other openings. Inflow sources within the public right-of-way can include sanitary manhole covers and stormwater catch basins that are inadvertently tied into the sanitary sewer. Private property inflow sources include roof downspout connections, yard and driveway drains, broken or missing sanitary lateral cleanout caps, and sump pump connections to the sanitary sewer system. These connections are illegal and can add thousands of gallons of stormwater into the sanitary sewer system per household during large rain events. Inflow sources are usually the easiest to remediate. Infiltration sources within the sewers can include broken or cracked sanitary pipes, deteriorated manholes, and misaligned or faulty pipe joints. Private infiltration sources can include broken lateral sewers, faulty lateral connections, tree root



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

penetration, and broken cleanouts. Infiltration sources can be more difficult to identify as sewer are underground. Figure 5.4.1 demonstrates typical I/I sources.

### 5.4.2 Continuing Sewer System Assessment (CSSA) Program

MSD is conducting an intensive sewer condition evaluation to comply with its federal Consent Decree as well as the Capacity, Management, Operations and Maintenance (CMOM) and Nine Minimum Control (NMC) programs. Through the Continuing Sewer System Assessment (CSSA) Program, sewer infrastructure conditions are being assessed using a variety of desktop and field inspection techniques which include, but are not limited to, closed circuit television (CCTV), smoke testing, dye testing, visual manhole inspection, private property inspection and wet weather inspection.

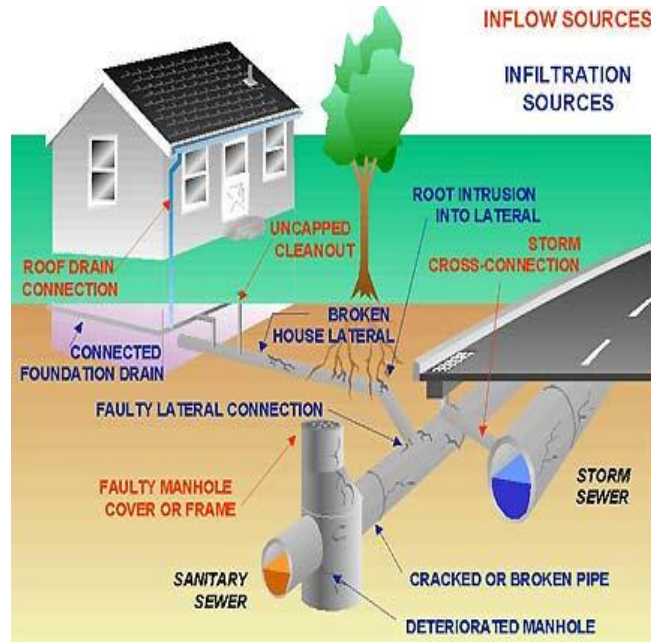


FIGURE 5.4.1 TYPICAL INFLOW AND INFILTRATION SOURCES

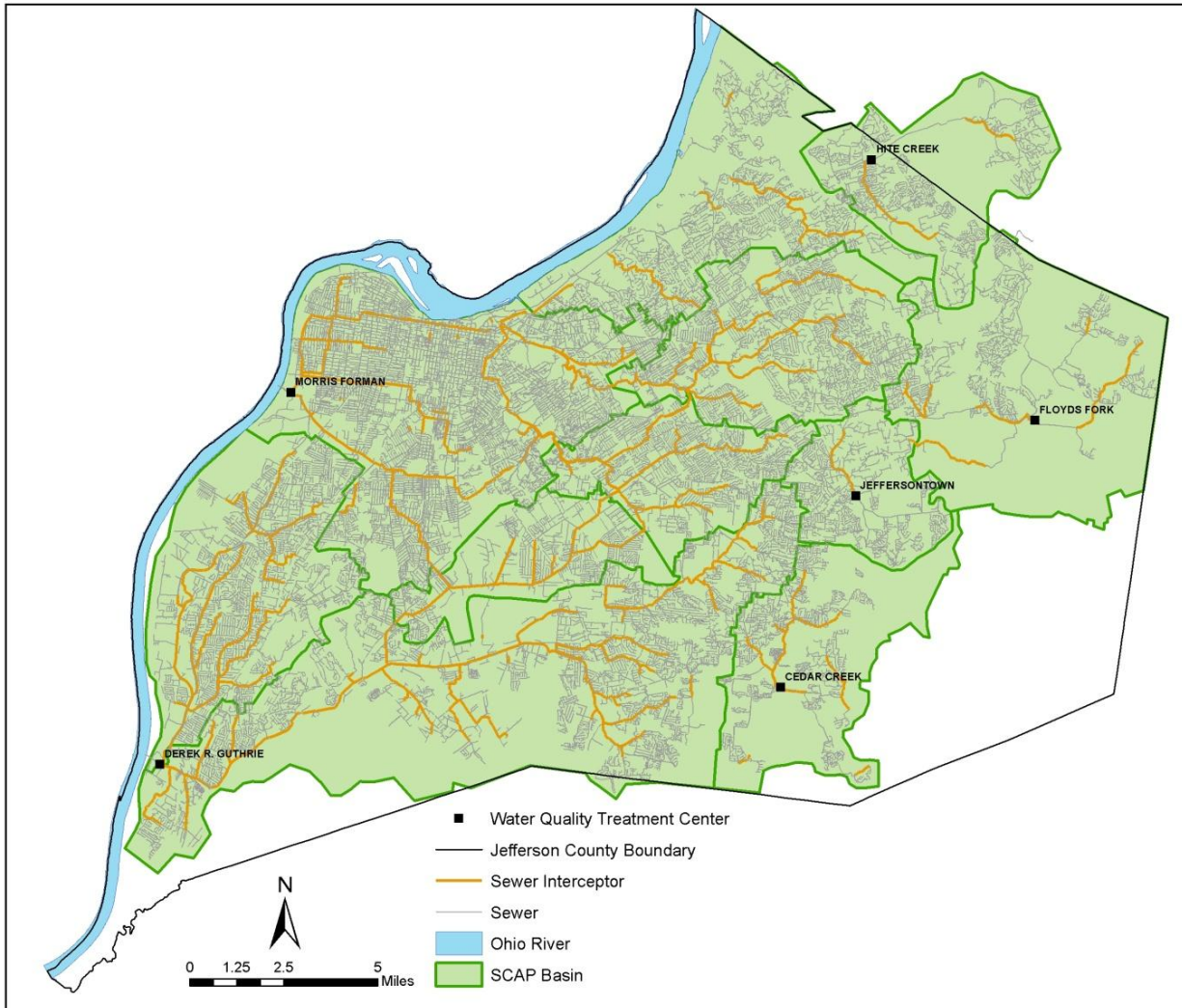
Once inspection of a study area is complete, inspection data are evaluated through a pipe condition assessment process. A primary goal of evaluating infrastructure assets is to develop and implement maintenance and rehabilitation recommendations that reduce sewer overflows and improve the capacity, structural integrity and functionality of existing assets. The inspection and rehabilitation activities are carried out under MSD's CSSA program, while recurring maintenance activities are handled in the Blockage Abatement Program (BAP).

#### 5.4.2.1 CSSA Program Background

MSD is responsible for the operation and maintenance of the sewer system within the public right-of-way and dedicated easements in Jefferson County, Kentucky, in addition to small areas in several of the surrounding counties. The sanitary sewer collection system includes over 3,200 miles sewers ranging from 6 inches to 27.5 feet in diameter that was built between the late 1800's and present day. The construction materials consist of brick, clay, polyvinyl chloride (PVC), clay pipe, vitrified clay pipe (VCP) and reinforced concrete pipe (RCP). There are over 64,000 manholes in the system constructed of reinforced concrete and brick materials. Figure 5.4.2 displays the MSD sewer system.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 5.4.2 MAP OF MSD SEWER SYSTEM**



The CSSA and Blockage Abatement Program focus on maintaining the conveyance capacities and integrity of these main line sewers, interceptors, and manholes in this collection system by addressing structural and operational defects, respectively. Stemming from CMOM M-E-9 Infrastructure Rehabilitation and S-C-1 Gravity Line Preventive Maintenance components, the CSSA and Blockage Abatement Program programs require a defined approach to prioritize, perform, and track the inspection, cleaning, rehabilitation, replacement, and maintenance of sewer assets on a consistent and prioritized cycle. The two programs are also intended to achieve compliance with Nine Minimum Controls (NMC) 1 and 2, which require the proper operation, regular maintenance, and maximum use of MSD's combined sewer system.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

The CSSA program is an asset management program with the purpose of determining the functional and structural state of MSD's existing sewer assets, both combined and separate, and taking action to maintain or restore sewer capacity. Under this effort, all sewer mains will be inspected based on risk and other programmatic obligations. The inspection data is captured in a normalized format allowing for the comparison of various segment conditions, which facilitates remedial action prioritization.

The BAP, a subsidiary program to the CSSA, encompasses sewer lines identified through the CSSA inspection as having recurring maintenance needs due to root blockages, sedimentation, or oil and grease deposits. This program tracks the segments with operational defects, sets up recurring work orders, assigns work to available resources, tracks progress and documents the work performed.

The program objectives of the CSSA Program include:

- Maintain the functional and structural integrity of the combined and separate sewer system.
- Prioritize annual inspection of at least 10 percent, on a 10 year cycle, of sewer system infrastructure balancing various regulatory and operational program needs until the entire system has been inspected.
- Inspect sewer lines based on the CSSA priority using standard Pipeline Assessment Certification Program (PACP) defect coding criteria.
- Capture inspection and rehabilitation data in a manner that facilitates prioritization of assets and defines inspection interval per asset.
- Address system defects that require immediate attention through in-house efforts or capital contract.
- Build a historical inspection and sewer video library to facilitate access and maintain a condition record of assets.
- Analyze sewer condition data consistently to identify segments and areas with actionable structural deficiencies, I/I sources, and maintenance issues.
- Develop consistent recommendation packages that facilitate bidding of rehabilitation and maintenance work and the internal assignment of appropriate activities.
- Prioritize and perform sewer repairs, rehabilitation, or replacement through in-house means or through capital projects.
- Document completed work in MSD's asset management system (Hansen).
- Periodically quantify the work completed and evaluate the various benefits realized from the program.
- Develop and apply inspection cycle schedules based on inspected sewer condition and criticality. Assign anticipated inspection cycles to sewer segments based on results.

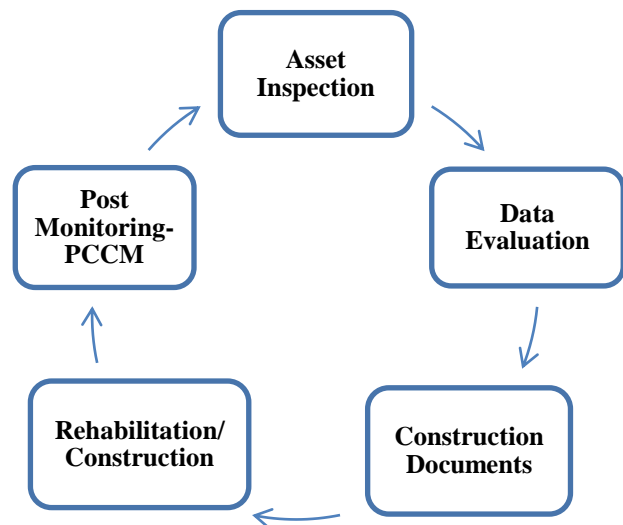
Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

- Paired with preventive maintenance, abate sewer overflows and service interruptions caused by structural failures while also removing I/I entering the system through manhole and pipe defects.

### 5.4.2.2 The CSSA Implementation Process

In the Louisville Metro area, the sewer infrastructure dates back to the 1800's. As with any infrastructure, age has impacts on the functionality. Current MSD sewer infrastructure conditions range from functioning-as-intended to structurally-degraded. The challenge is to identify, assess, and prioritize the sewer infrastructure assets to minimize the risk of failure. To proactively address current and upcoming infrastructure issues, a detailed decision framework has been developed. The decision framework steps are to inspect, evaluate, develop construction documents, complete rehabilitation and perform post-construction monitoring, as illustrated to the right. Asset inspection includes conducting field condition inspections to document existing conditions. The field data is evaluated and utilized in developing corrective rehabilitation activities. The implementation steps continue with the creation of cost estimates and construction documents for remediation efforts.

FIGURE 5.4.2 – SEWER ASSESSMENT CYCLE



The assessment process does not conclude once rehabilitation is complete, but with defining an inspection cycle to continue to monitor success of the infrastructure improvements. Thus, the cycle continues.

### 5.4.3 Sewer Asset Inspection Approach

MSD developed a 3-pronged approach to gather sewer asset inspection data: Sanitary Sewer Evaluation Studies (SSES), Interceptor Condition Assessments (ICA) and in-house data assessment and evaluations. The inspections include all MSD assets in easements and public right-of-ways, such as sewer pipes, manholes and lateral line connections. Areas to be inspected are prioritized using system historical data and various programmatic drivers. Some operational data examples include confirmed SSO locations, pump station condition assessments and sewer line segments that are frequently repaired under the BAP program. Programmatic drivers include areas located in an IOAP project or sewer lines selected for assessment, identified during SCAP, CMOM or NMC activities.



Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

### 5.4.3.1 Sanitary Sewer Assessment Studies (SSES)

MSD staff identified specific areas for in-depth SSES projects. SSES projects are completed under professional engineering contracts. The project areas are typically larger, associated with specific IOAP project areas. SSES projects are also utilized to complete smoke testing, private property and manhole inspections. These are activities MSD does not have the resources to complete in-house on a large scale. Since SSES activities utilize significant internal and external resources, project scopes include a full assessment of the targeted area.

The area's sewer line segments are video inspected and smoke tested along with a visual inspection area manholes. Depending on the severity of the SSOs in the area, a targeted goal for private property inspections is ten to twenty-five percent. This includes visual inspections and dye testing of both commercial and residential properties, looking for unwanted sources of I/I such as sump pumps, area yard drains and down spouts. SSES activities also include wet weather inspections. During a ½-inch or greater rain event in a six hour window, inspections occur to check manhole surcharge conditions and surface flooding of sewer assets. The picture on the right shows a roadside ditch over topping the road and flooding a manhole.

The assessed data is analyzed and rehabilitation recommendations are presented in mapping and report form. To-date, SSES costs are averaging about \$2.50 per linear foot of sewer pipe assessed. The following Table 5.4.1 lists both the SSES projects completed as of October 30, 2012, and the assets inspected during each project.





Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 5.4.1**  
**SSSES PROJECTS COMPLETED, JULY 1, 2009 TO MAY 31, 2013**

SSSES PROJECT	Sewer (LF)	Sewer (Miles)	Manholes (EA)	Private Property
Camp Taylor	169,483	32.1	661	524
Lea Ann Way East	390,803	74	1,892	75
Lea Ann Way West	290,028	54.9	1,273	299
Lantana PS	3,655	54.9	15	32
Prospect	121,816	23	588	325
Meadow Stream	195,054	36.9	952	129
Berrytown WQTC	30,563	5.8	147	24
Lake Forest WQTC	118,246	22.4	616	126
Starview WQTC	12,243	2.3	70	23
Eden Care PS	4,628	0.9	25	8
Little Cedar Creek	114,577	21	577	97
Edsel PS	28,909	5.5	107	54
Cherokee Park Area	12,714	2.4	60	0
East Rockford PS	8,361	1.6	34	0
Sonne PS	13,076	2.5	56	12
Hazelwood PS	11,461	2.1	60	12
Cedar Creek Phase 2	272,000	51.5	1406	250
Prospect Phase 2	94,700	17.9	475	81
Caven Ave Pump Station	11,300	2.1	28	0
Shively	641,600	121.5	2642	617
<b>TOTALS</b>	<b>2,545,217</b>	<b>535</b>	<b>11,684</b>	<b>2,688</b>

Interceptor Condition Assessment (ICA) projects concentrate on larger diameter sewers, typically greater than 48-inches in diameter, and sewers with significant flow with surcharged conditions. Standard CCTV equipment cannot operate under these conditions needing significant flow diversions or pump around activities for visual pipe assessment. ICA projects utilize technologies that allow full pipe assessment under these conditions. Sonar instrumentation is used in full surcharged sewer conditions where visual inspection is impossible. The sonar instrument is sent through the sewer to produce a cross section view every second in real time. A sonar image is used to determine the location and severity of any structural or hydraulic problems or defects found in the sewer. Totally Integrated CCTV and Sonar (TISCIT) is used for those lines that are flowing partially full. It is a combination of the above two methods with the CCTV above the water line and the sonar below resulting in a 360 degree inspection of the pipe. Due to the expense and specialized nature of the equipment needed for ICA activities, these assessments are completed under professional engineering

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

contracts. ICA project locations can vary from easily accessible city streets to isolated farmland. Depending on the location, accessibility and flow conditions, ICA projects range from four to six dollars per linear foot assessed. The assessed data is analyzed and rehabilitation recommendations are presented in mapping and report form.

#### 5.4.3.2 In-house Data Assessment and Evaluations

Supplementing the SSES and ICA assessment activities are the daily programmatic activities completed by multiple divisions at MSD. Examples of these activities include the BAP, the CMOM Program, NMC and the SCAP. MSD's I&FP Division coordinates CCTV inspections for both the CSSA and BAP programs. CCTV data is assessed and rehabilitation efforts are planned and completed with in-house resources as needed. Typically, in-house resources can complete sewer repairs or rehabilitation under the following conditions:

- Sewer depth eight feet or less
- Pipe diameter 12-inches or less
- Repair or replacement lengths up to 120 feet

Once it is determined that repair or rehabilitation efforts exceed these conditions, I&FP staff coordinates with MSD's Engineering and Regulatory Services Divisions for planning capital construction projects. I&FP also coordinates MSD's root control program. This proactive program uses a chemical treatment for root removal and control. Areas are prioritized based on severity of roots found, blockage abatement work orders and SSOs. Post inspections are performed on a routine schedule to confirm efficacy of the chemical treatment.

**TISCIT – Video above  
Water and Sonar Below**



#### 5.4.3.3 Data Evaluation

Getting successful results when planning and completing rehabilitation efforts is challenging, it demands a consistency of thought, purpose and action over a long period of time. To insure a consistency in coding sewer defects, MSD adopted the PACP defect coding standards. Staff involved in planning sewer assessment and rehabilitation activities are required to be PACP certified. This gives staff a consistency in thought and an understanding of remediation needs based on asset conditions. Once an understanding was in place, a single thought was created to give purpose to rehabilitation efforts. The single goal for the rehabilitation program was to correct all assessed sources of I/I. If a leak or evidence of a leak is confirmed, the purpose and actions of the program will be to correct the leak.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

#### 5.4.4 Project SEAL (Seal Every Assessed Leak)

Project SEAL is an assessment tool to prioritize I/I rehabilitation projects in a consistent manner. The tool was created in-house to give staff a method to filter defect data to create rehabilitation recommendations. Project Seal is an ArcGIS application which utilizes MSD’s extensive mapped sewer system attributes and Hansen data management information. The tool uses rule based condition assessment for prioritization and geospatial recognition of asset attributes. For example, if a manhole is located in a flood plain and the asset attribute is coded with a standard manhole frame and lid, Project Seal will recommend replacing the lid with a water tight frame and lid. The tool gives staff a consistent method to process inspection data, identify the major I/I sources and prioritize rehabilitation needs. Recommended defect activities are mapped through the ArcGIS application for review. Once final, the mapped recommendations are used to create construction drawings and quantify final construction quantities. Also built into the tool are the SCAP flow reduction estimates which are used to quantify flow reductions to the system.

#### 5.4.1 Defining the Rules

Part of defining the rules to be used to evaluate asset defects, MSD defined the scope of work to be performed during rehabilitation projects. There are multiple construction methods and technologies used to complete rehabilitation actives. Deciding what method to fix a defective pipe can be challenging. Early in the process, MSD decided to narrow the rehabilitation alternatives to keep things simple and to help staff become more proficient. The following Table 5.4.2 lists selected rehabilitation alternatives selected per sewer pipe and manhole assets.

**TABLE 5.4.2**

**REHABILITATION ALTERNATIVES**

PIPE REHABILITATION	MANHOLE REHABILITATION
CIPP	EPOXY COATING
POINT REPAIRS	CHIMNEY SEALS
CLEANING	REALIGN FRAME AND LID
LATERAL REPAIRS	RAISE FRAME AND LID TO GRADE
REPLACEMENT	REPLACEMENT

Once the alternatives were selected, the rules governing the rehabilitation methods could be defined. PACP severity ratings vary from one to five, the later being the worst defect condition. The rule based all defect ratings of four and five would automatically be rehabilitated. Defect ratings of one through three would be further reviewed and prioritized based on geographical location and asset historical knowledge. Typical defects coded three or less or coded to be addressed under CMOM and NMC programmatic activities. Root defects coded three or less, for example, are resolved under MSD’s CMOM root control program. Some additional considerations that help to define the rules and quantify rehabilitation activities and costs include:

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

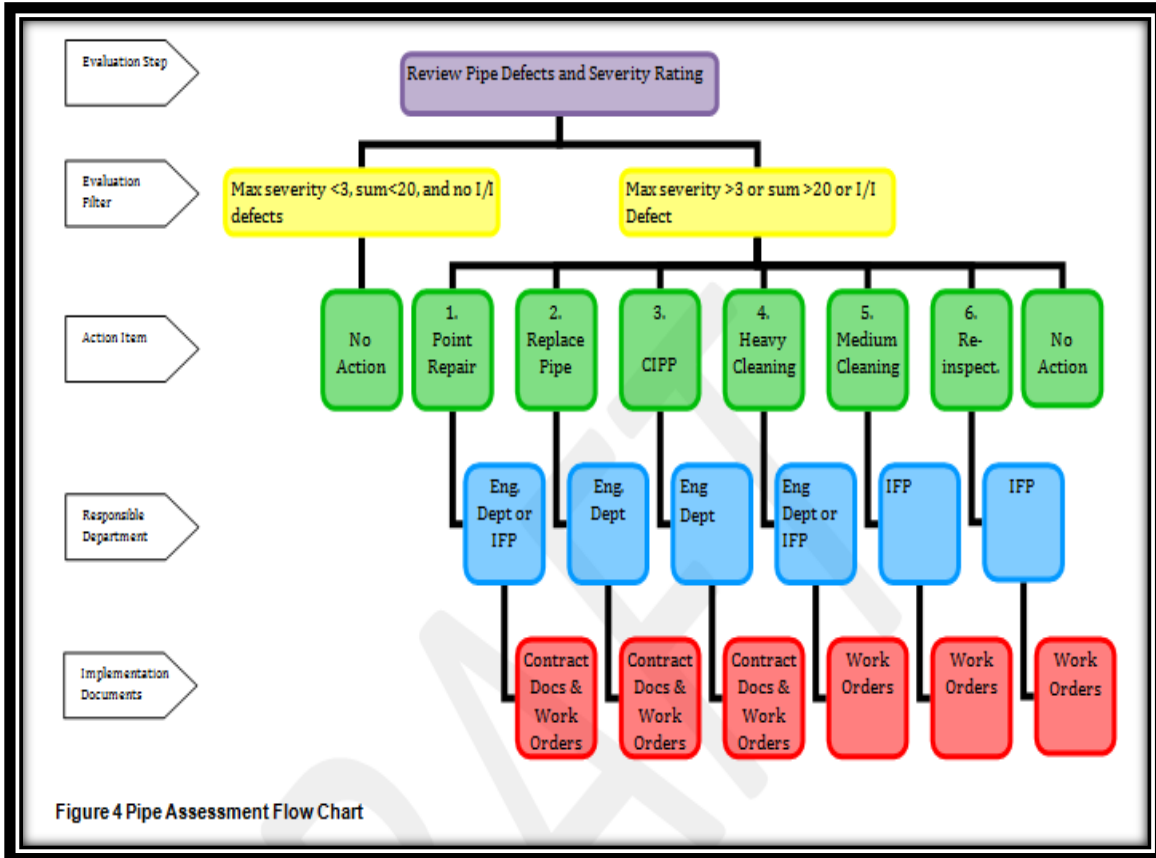
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- Right-of-way vs. Easement
- Accessibility
- Grass vs. Pavement
- Diameter of Pipe
- Pipe Material
- Date of installation
- Inundated Areas (Ex. Streams, floodplains)
- Environmentally Sensitive Features

Project Seal is a tool to quantify and narrow in on recommended rehabilitation activities. The tool also includes assessment process flow charts to define the rehabilitation process and who will be responsible for the work for sewer pipe and manhole assets. The following two figures define the rehabilitation solution matrix for pipe and manhole assets.

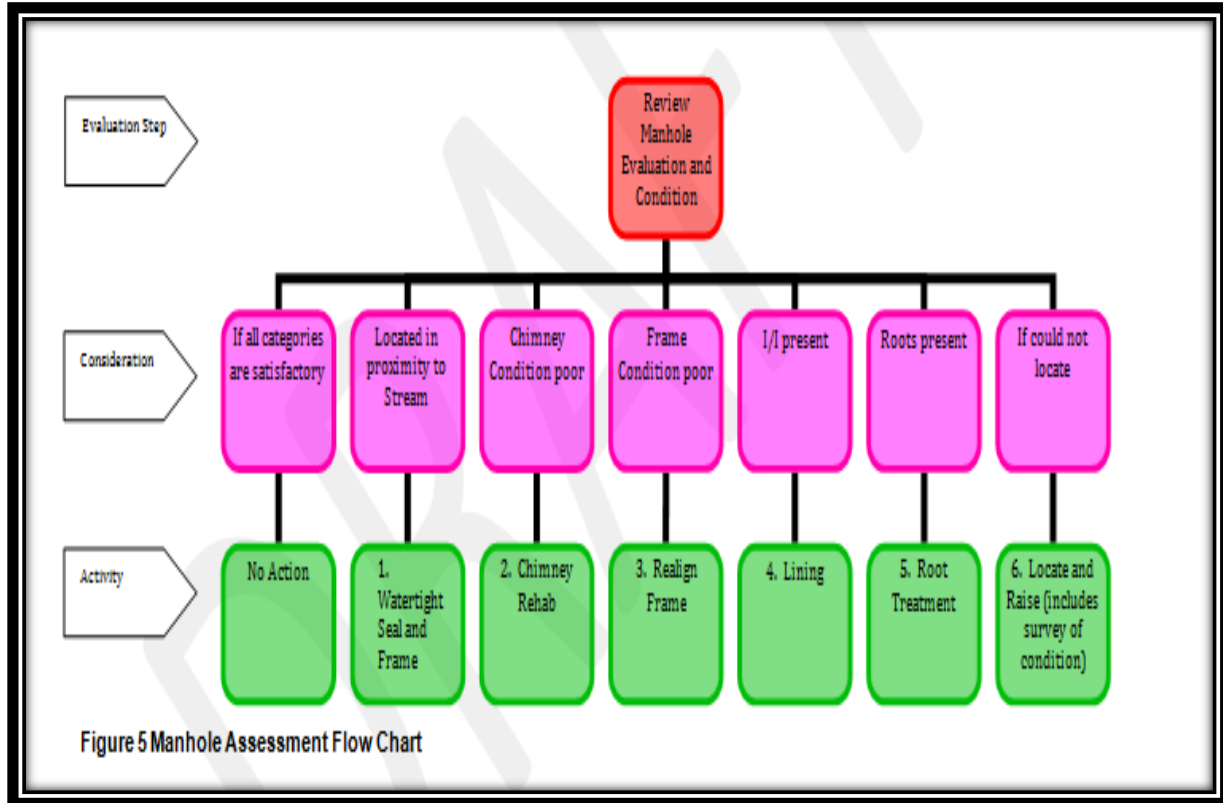
The process still requires hands on review to confirm the recommendations meet the intent of the I/I reduction program, constructability and the scope is within available budget.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information





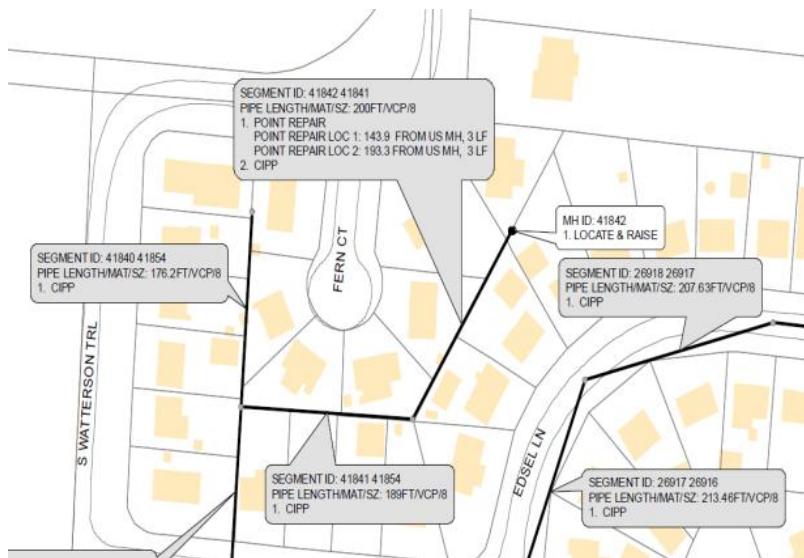
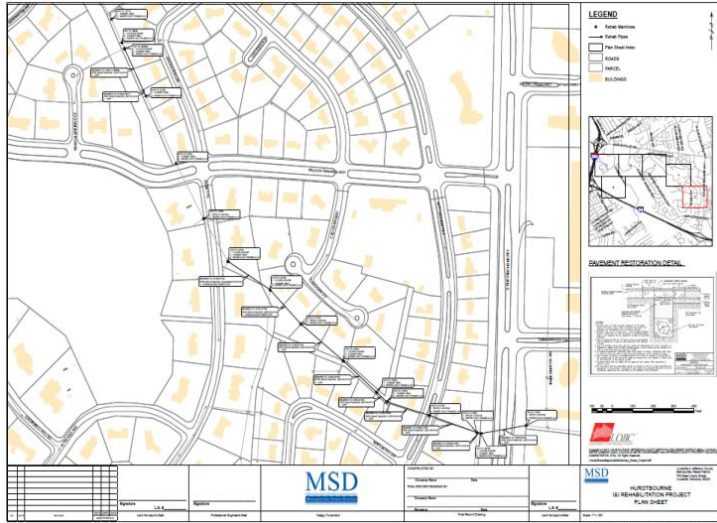
Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information



## 5.5 Construction Documents

Once all the data has been processed, construction drawings are created. The drawings quantify work to be completed listing specific recommendation alternatives, as shown in examples below.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information



In addition, detailed bid quantities and construction estimates are created. The construction estimate is created using a cost database containing historical bids since June 2009.

The contraction drawings, bid quantities and estimate are used to start the bidding process to start each rehabilitation project. The following Table 5.5.1 provides a list of rehabilitation projects that have been completed since May 2013, including specific activities completed.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**BID PROPOSAL**

Computerized Proposal for: **HURSTBOURNE I&I REHABILITATION PROJECT**  
 Contract No. 15572 Bid Date: July 26, 2011

Item	Description	Qty.	Unit	Unit \$	Total \$
<b>Pipe</b>					
1	Cured-in-Place Pipe, 15-inch Pipe	485	LF		
2	Cured-in-Place Pipe, 18-inch Pipe	1,223	LF		
2	Cured-in-Place Pipe, 21-inch Pipe	1,494	LF		
3	Cured-in-Place Pipe, 24-inch Pipe	651	LF		
4	Cured-in-Place Pipe, 27-inch Pipe	2,122	LF		
5	Open Cut Point Repair, Grass	21	LF		
6	Cleaning and Inspection	705	LF		
<b>Manhole</b>					
7	Manhole Rehabilitation Epoxy Coating (approx. 138 VF)	13	EA		
8	Mechanically Locking Chimney Seal	58	EA		
9	Manhole Chimney Seal Extensions	58	EA		
10	Locate & Raise to Grade, Grass	38	EA		
11	Water Tight Frame and Lid, grass	69	EA		
12	Water Tight Frame and Lid, pavement	1	EA		
13	Clean and Inspection	1	EA		
<b>General</b>					
14	Preconstruction Photographs	1	LS		
15	Asbuilt Drawing Coordination	1	LS		
16	Project Sign	2	EA		
					SUBTOTAL
17	Mobilization/Demobilization (MAX 1.0% of SUBTOTAL)	1	LS		
18	Bonds (MAX 1.5% of SUBTOTAL)	1	LS		
					BID TOTAL

Legal Entity Bidder: \_\_\_\_\_

(Sign here) By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: \_\_\_\_\_

Address: \_\_\_\_\_

Telephone No. \_\_\_\_\_

Note: Bidder is responsible for verifying calculations ascertained by the electronic spreadsheet computation of all bid amounts, subtotals, totals, etc. prior to submitting their bid.

Cost Estimates  
Hurstbourne I/I

**Hurstbourne I/I Rehabilitation Cost Estimates**

Date: Jul-11  
 IOAP Drainage Basin: Middle Fork  
 Line Analyzed: 744 LF  
 Manholes Analyzed: 70 MH

Manhole Rehabilitation	Quantity	Unit Cost	Unit	Price
locate & raise, yard	38	\$400.00	EA	\$15,200.00
chimney seal	58	\$400.00	EA	\$23,200.00
chimney seal extensions	58	\$200.00	EA	\$11,600.00
cleaning and inspection	1	\$250.00	EA	\$250.00
lining	13	\$400.00	EA	\$5,200.00
water-tight frame & lid, asphalt	1	\$1,200.00	EA	\$1,200.00
water-tight frame & lid, yard	69	\$800.00	EA	\$55,200.00

Pipe Rehabilitation	Quantity	Unit Cost	Unit	Price
cipp, 15 in.	485	\$50.00	LF	\$24,237.50
cipp, 18 in.	1,223	\$50.00	LF	\$61,155.50
cipp, 21 in.	1,493	\$50.00	LF	\$74,668.50
cipp, 24 in.	651	\$400.00	LF	\$260,500.00
cipp, 27 in.	2,122	\$400.00	LF	\$848,880.02
cleaning and inspection	705	\$2.20	LF	\$1,550.69
point repair, yard	21	\$1,000.00	LF	\$21,000.00

Subtotal \$1,403,842.21  
 Contingency\* (25%) \$350,960.55  
**TOTAL \$1,754,802.77**  
 SCAP Credits\*\*  
 Cost/Credit Ratio

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**TABLE 5.5.1**  
**REHABILITATION PROJECTS COMPLETED, JULY 1, 2009 TO MAY 31, 2013**

Project	Completed	Sewer (LF)	Manholes (EA)	Total Cost	Flow Reduction (GPD)
BGI Phase 2	12/31/2010		13	\$18,260.00	19,008
Floydsburg	12/31/2010	8	32	\$46,620.00	28,437
Parkview	6/30/2011		0	\$25,669.58	36
Hazelwood	6/30/2011	2,121	72	\$393,200.00	38,700
Sonne	6/30/2011	7,770	67	\$838,500.00	120,800
Edsel	9/30/2011	14,569	46	\$1,377,132.00	106,700
Shadow Wood		3	11	\$29,000.00	5,600
Lantana	12/31/2011	1,529	4	\$207,500.00	5,000
Hurstbourne	12/31/2011	5,996	180	\$1,400,000.00	1,408,279
Saint Matthews Interceptor	6/1/2012	7,011	40	\$1,143,000.00	20,841
Lea Ann Way Interceptor	6/1/2012	2,126	178	\$950,000.00	1,017,423
FY 12 Annual I/I	11/1/2012	17,952	235	\$1,640,899.75	1,200,000
Fern Creek	Active	19,437	550	\$2,057,089.00	195,012
Fegenbush	Active	4,356	281	\$490,801.15	63,358
Stoney Brook/Piccadilly	Active	19,255	233	\$741,634.73	253,855
Lake Forest	Active	1,821	547	\$669,000.00	355,476
<b>TOTALS</b>		<b>103,954</b>	<b>2,489</b>	<b>\$ 12,028,306.21</b>	<b>4,838,525</b>

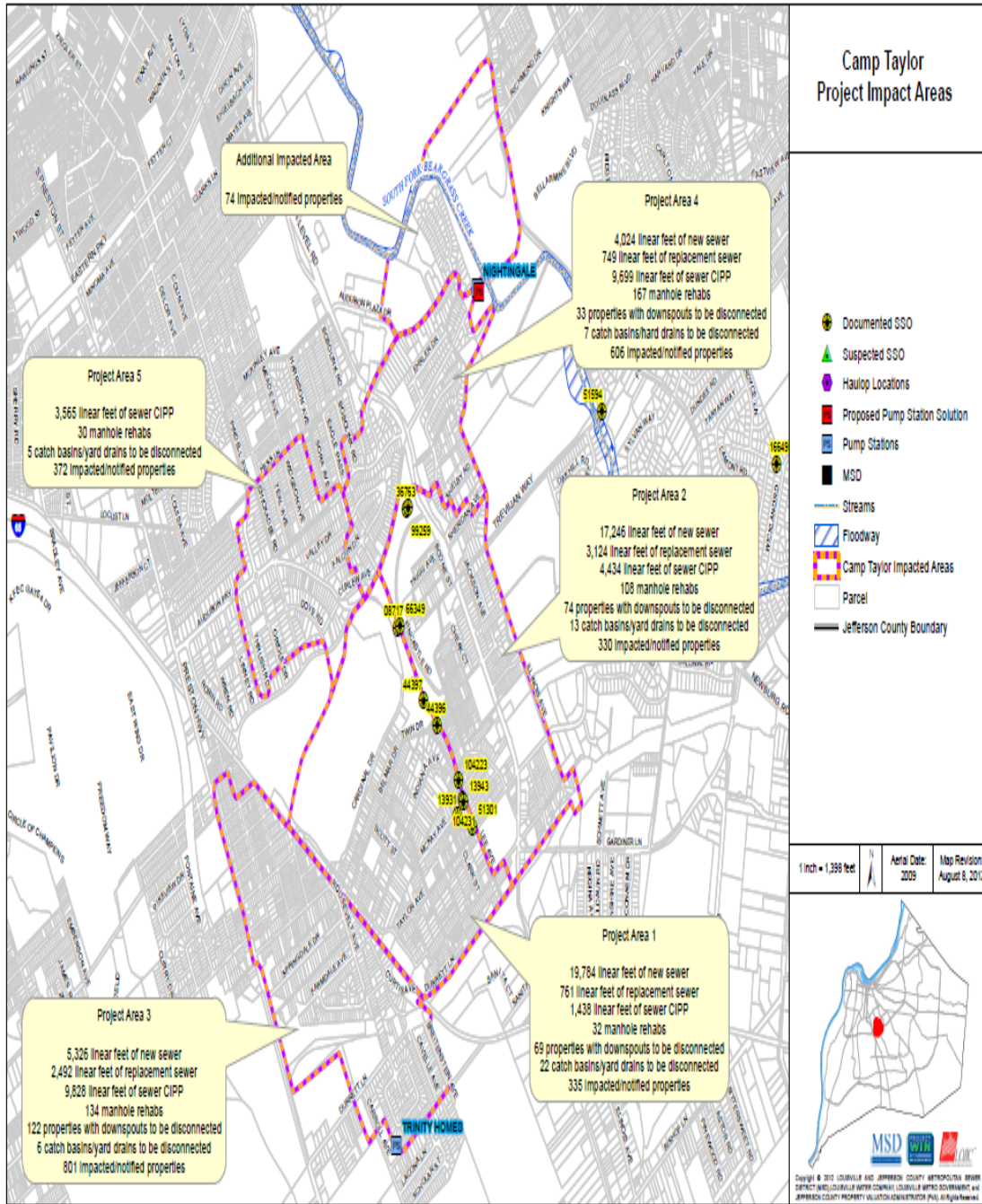
## 5.6 Private Property Inflow Reduction Program

MSD is proactively inspecting private properties for source of inflow such as sump pumps and downspouts. During SSES activities, homes are visually inspected on both the inside and outside of the property. Depending on the severity of the SSOs in the area, inspections will target 10 to 25 percent of the properties in the study area. The selected percentage is low do to historical knowledge of past SSES projects and the lack of public participation. Currently, MSD has no legal authority to inspect homes for illicit connections, all private property inspections are solicited on a volunteer basis. Once a private illicit I/I source is found, MSD will work with the property owner to develop a plan to remove the source from the sewer system.

Early inspections show private sources of I/I are worse than originally anticipated. In the Camp Taylor SSES area for example, 260 of the 624 (or 42%) homes inspected had illicit connections. If you assume the same percentage for the 2,444 properties in the project area, 1,026 homes would have illicit connections. The Lantana Pump Station SSES found suspected sump pump connections in 20 of the 56 homes inspected. The Camp Taylor SSES area and depicted in Figure 5.6.1.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

**FIGURE 5.6.1 CAMP TAYLOR PROJECT IMPACT AREAS**





Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information

## 5.7 Inflow and Infiltration Program Summary

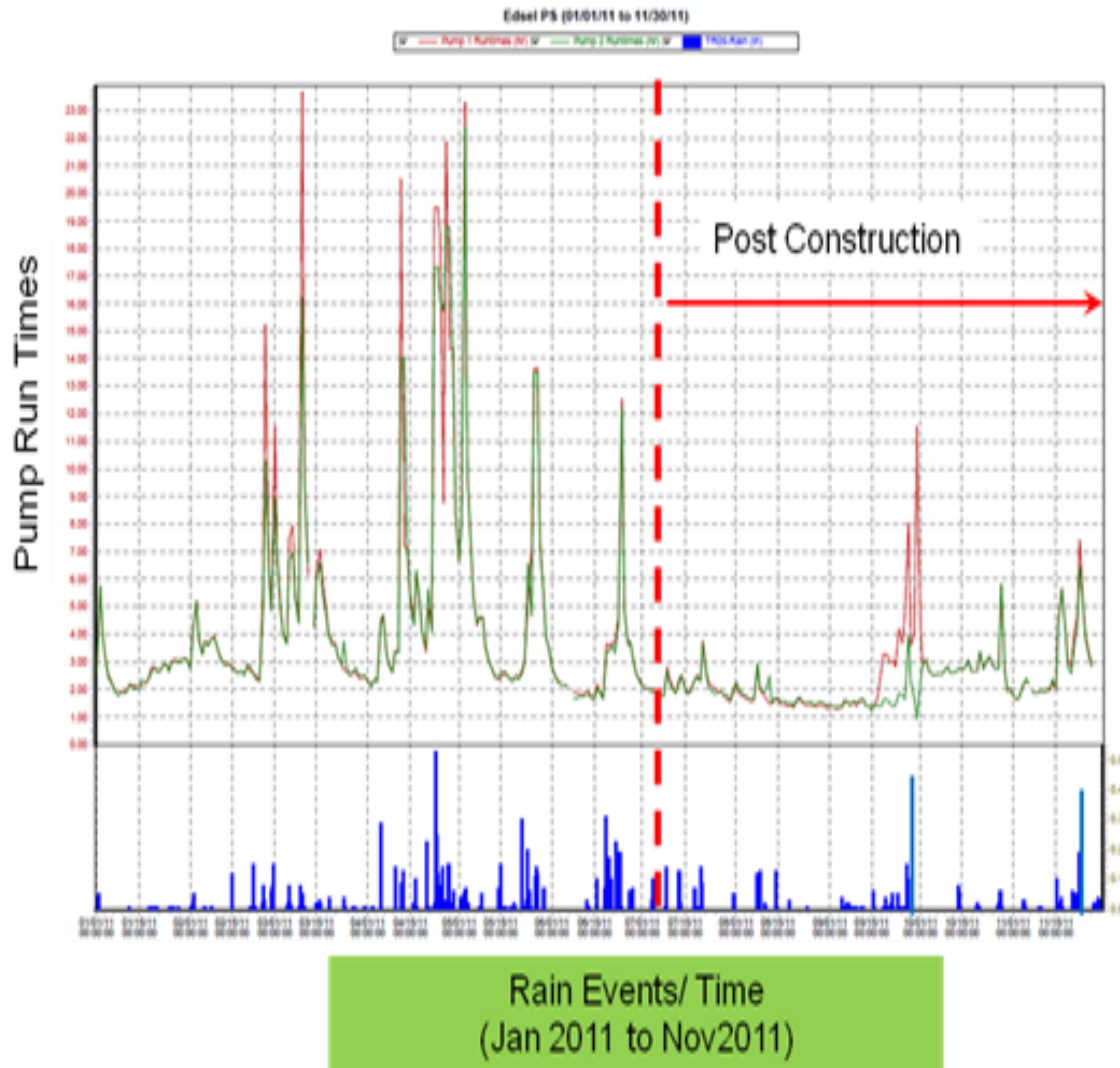
As of May 2013, MSD has lined over 19 miles of sewer and rehabilitated 2,292 manholes. The Table 5.7.1 to the right quantifies all rehabilitation activities completed as of May 2013. The Project Seal Assessment tool allows staff to consistently assess sewer assets and successfully develop and communicate corrective recommendations. Over \$12 million dollars have been spent with a rehabilitative cost to credit ratio of 2.49, spending approximately \$2.49 for every gallon removed from the system. There has been only 0.08 percent spent on construction changes orders further validating the effectiveness of the program to accurately communicate through the construction drawings. A significant lesson learned is that the older, clay pipe is typically the source of I/I related defects in the system. Another lesson is more obvious but not always followed. Rehabilitation activities get more back for your buck following the water table. Areas along waterways, wetlands and drainage facilities are more likely to cause I/I issues in the system. These will be used to improve prioritization and selection of rehab activities in the future.

**TABLE 5.7.1**

Activity	Total	Units
CIPP	77,519	LF
CIPP Tophats	1,180	EA
Point Repairs	1,003	LF
Clean and Inspect	33,323	LF
Chimney Seals	374	EA
Epoxy Coating	256	EA
Frame and Lid	105	EA
Water Tight Frame and Lid	254	EA
Realign Frame and Lid	79	EA
Locate and Raise	163	EA
Clean and Inspect	197	EA

The project directive to “fix every assessed leak” is proving to be effective. PCCM activities have shown that not only have SSOs been reduced, both operation and maintenance improvements have been achieved. In the Edsel Pump Station, post pump run times during rain events greater than 1-inch have been reduced 46 percent with reductions greater than 52 percent for events greater than 2-inches. The Hurstbourne Interceptor rehabilitation project has seen post rehabilitation flow reductions of 20 MGD wet weather flow and 4 MGD dry weather flow.

Refer to Volume 2, Chapter 5, and Volume 3 Chapter 5 for detailed overflow volume, frequency and project information



**TABLE 5.3.1  
2012 SSDP LEVEL OF CONTROL EVALUATION**

SSDP Recommended Project Name/Location	IOAP Number	Budget ID	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Comments
<b>2012 Project Modifications</b>							
Meadow Stream PS & Force Main Upgrade	S_HC_HC_MSD1082_S_09A_C	H09174	Meadow Steam PS (91087 & MSD1082-PS)	PS Upgrade	2.60-inch	--	Project changed from a small storage basin to a pump station upgrade and new force main due to the capacity needs of Crestwood. The City paid the additional costs beyond MSD's overflow control commitment, therefore Level of Protection raised to 10-year.
Camp Taylor System Improvements	S_SF_MF_30917_M_09_A	H09201, H09220, H09218, H1004	08717, 13931, 13943, 36763, 44396, 44397, 66349, 104223, 104231	Sewer Rehabilitation & Replacement	2.60-inch	--	Project approach is similar to 2009, but the project area targeted for inspection and rehabilitation is larger. B/C analysis unavailable at this time.
Caven Avenue Pump Station Elimination	S_PO_WC_PC09_M_09B_C	H12022	27116, Caven Ave PS (MSD0133-PS)	PS Elimination	1.82-inch	139.48	Recent new pipeline constructed to eliminate a nearby package treatment plant makes the elimination of the pump station the most cost effective overflow solution.
					2.25-inch	155.40	
					2.60-inch	158.27	
Outer Loop Storage Basin	S_PO_WC_PC09_M_09B_C	H10046	70212, 17724	Project Eliminated	--	--	Due to improvements in the Pond Creek hydraulic model calibration, this storage basin is no longer necessary.
Eden Care PS SSO Investigation	S_FF_FF_NB02_S_13_C	H09170	Eden Care PS (MSD1105-PS)	Project Eliminated	--	--	Only one overflow had been documented at this location. MSD cleaned the sewers in the vicinity and has not documented an overflow in over 3 years. No further action is deemed necessary.
Fairmount Rd. PS Off-line Storage	S_FF_CC_81316_M_03_C_A	H09167	Fairmount Road PS (81316 & 97362)	Offline Storage	1.82-inch		Project needed to accommodate flows from eliminated Jeffersontown WQTC and acknowledge capacity at Cedar Creek WQTC.
					2.25-inch		
					2.60-inch		
Lea Ann Way System Improvements	S_PO_WC_PC08_M_01_C	C08433	19360, 19369, 29933, 29948, 29943, 31083, 31084, 79076, Lea Ann Way PS (MSD1010-PS)	Pipe Upgrades & I/I Reduction	Rehabilitation & Monitoring		Additional overflows have been occurring in recent years. Therefore, additional sewer inspection and rehabilitation are underway. Contingency plans have been developed and are dependent upon the efficacy of rehabilitation of wet weather flows.
Leland Rd. SSO Investigation	S_OR_MF_NB02_S_13_C	H09189	96020	Project Eliminated	--	--	Only one overflow had been documented at this location. MSD cleaned the sewers in the vicinity and has not documented an overflow in over 3 years. No further action is deemed necessary.

**TABLE 5.3.1  
2012 SSDP LEVEL OF CONTROL EVALUATION**

SSDP Recommended Project Name/Location	IOAP Number	Budget ID	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Comments
<b>Cedar Creek Area</b>							
Idlewood Inline Storage	S_CC_CC_70158_M_09A_C	H09164	28998, 28984, 63094, 63095, 70158	Inline Storage	1.82-inch	31.36	
					2.25-inch	27.11	
Little Cedar Creek Interceptor Improvements	S_CC_CC_67997_M_01_C	H09163	67997, 67999, 86423, 86424, 89195, 89196, 89197	Pipe Upgrades	1.82-inch	23.86	
					2.25-inch	17.43	
Bardstown Rd. PS Improvements	S_CC_CC_MSD1025_S_03_B	H09165	88545	PS Upgrades	1.82-inch	29.42	
					2.25-inch	46.5	
					2.60-inch	33.85	
Running Fox PS Elimination	S_CC_CC_MSD1080_S_01_C	H09178	MSD1080-LS	Diversion	1.82-inch	659.52	Project Completed
					2.25-inch	118.87	
<b>Hite Creek Area</b>							
Floydsburg Rd. I/I Investigation & Rehabilitation	S_HC_HC_MSD1086_M_07_C_A	H09172	Floydsburg Road (MSD1086-PS, 90776, 108956, 108957, 108958)	I/I Reduction	Sewer System Evaluation Study (SSES)/Rehab		Project Completed - Monitoring Ongoing
Kavanaugh Rd. PS Improvements	S_HC_HC_MSD1085_S_03_A	H09171	Kavanaugh Road (MSD1085-PS)	PS & Force Main Upgrades	1.82-inch	19.77	
					2.25-inch	20.23	
					2.60-inch	21.09	
<b>Floyds Fork Area</b>							
Woodland Hills PS Diversion	S_FF_FF_NB01_S_01_C_A	H09169	33003, 65531	Diversion	1.82-inch	92.26	Project Completed
					2.25-inch	17.75	
					2.60-inch	15.45	
Ashburton PS Improvements & Diversion	S_FF_FF_NB03_M_01_C_A	A09092	Olde Copper Court PS (MSD0165-PS), Ashburton PS (MSD0166-PS)	Upgrade Force Main & Pipes	1.82-inch	161	Project Completed
					2.25-inch	82.24	

**TABLE 5.3.1  
2012 SSDP LEVEL OF CONTROL EVALUATION**

SSDP Recommended Project Name/Location	IOAP Number	Budget ID	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Comments
<b>Jeffersontown Area</b>							
Jeffersontown WQTC Elimination	S_JT_JT_NB01_M_01_C_A	H07293	28390, 28391, 28392, 28395, 28551, 31733, Jeffersontown WQTC (28173 & 64505 & MSD0255 & IS028-SI)	Offline Storage, Pipe Upgrades, WQTC Elimination	1.82-inch	5.23	
					2.25-inch	5.09	
Chenoweth Hills WQTC Elimination, Chenoweth Run and Chippewa PS Improvements	S_JT_JT_NB01A_M_03_C	H09238	Chenoweth Run PS (MSD0196-PS & 86052 & 64096), Chippewa PS (92061), Chenoweth Hills WQTC PS (MSD0263A-PS), Chenoweth Hills WQTC (MSD0263)	PS & Force Main Upgrades, WQTC Elimination	1.82-inch	20.05	
					2.25-inch	17.94	
Dell Rd and Charlane Pkwy Interceptor Improvements	S_JT_JT_NB02_M_01_C	H09179	Charlane Pkwy (28250, 28249, 28340, 28336, 104289), Dell Rd. (28413, 28414, 28415, 28416, 28417)	Pipe Upgrades	1.82-inch	31.34	
					2.25-inch	26.28	
Raintree & Marian Ct. PS Eliminations	S_JT_JT_NB03_M_01_C	H09180, H10043	28719, 28711, Marian Court PS (28729), Raintree PS (MSD0149-PS)	Diversion, Pipe Upgrades	1.82-inch	72.76	
					2.25-inch	51.97	
Monticello PS Elimination	S_JT_JT_NB04_M_01_A	H09182	Monticello Place PS (MSD0151-PS & 27969)	Diversion	1.82-inch	48.9	
					2.25-inch	63.24	
					2.60-inch	65.85	
<b>Middle Fork Area</b>							
Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion	S_MISF_MF_NB01_M_01_C_A1	H04276, H07288, H09186	02932, 02933, 02935, 08537, 23211, 23212, 27005, 45835, 47583, 47593, 47596, 47603, 47604, 51180, 51221, 51160, 51161, 90700, IS021A-SI, Middle Fork at Breckenridge (08935-SM)	Offline Storage & Pipe Upgrades	1.82-inch	1.26	
					2.25-inch	1.07	
					2.60-inch	0.9	
Goose Creek PS Improvements & Wet Weather Storage	S_MI_MF_NB04_M_03_B	H09183, H10044	Devondale PS (21628-W), Goose Creek PS (46891, 62418, 62420, 91629, 91630, 105936), Saurel PS (43472)	Offline Storage, PS & Force Main Upgrades	2.25-inch	11	
					2.60-inch	6.84	
Anchor Estates PS Eliminations	S_MI_MF_NB06_M_01_A_A - 1, S_MI_MF_NB06_M_01_A_A - 2	H10045, H09184	Vannah PS (01106), Anchor Estates #1 PS (00746 & 00056-W), Anchor Estates #2 PS (MSD0057-LS)	Diversion	1.82-inch	25.39	
					2.25-inch	29.55	
					2.60-inch	31.14	
Hurstbourne I/I Investigation & Rehabilitation	S_MI_MF_NB07_S_07_C	H09219	01793	I/I Reduction	SSES/Rehab		Project Completed - Monitoring Ongoing
<b>Southeastern Diversion Area</b>							
Parkview Estates I/I Investigation & Rehabilitation	S_SD_MF_NB03_S_07_C	H09198	47250	I/I Reduction	SSES/Rehab		Project Completed - Monitoring Ongoing
Klondike Interceptor	S_SD_MF_NB04_S_01_B_A	H09199	Alcona (25676), 25560, 25561	Pipe Upgrades	1.82-inch	9.11	
					2.25-inch	9.11	
					2.60-inch	7.02	
Sutherland Interceptor	S_SD_MF_NB05_M_01_A	H09200	Sutherland (16649)	Pipe Upgrades	1.82-inch	25.22	
					2.25-inch	31.98	
					2.60-inch	32.71	
Beargrass Interceptor Rehab Phase 2	S_SD_MF_NB06_S_13_C	H09239	51594	Sewer Rehab	Rehabilitation		Project Completed - Monitoring Ongoing



**TABLE 5.3.1  
2012 SSDP LEVEL OF CONTROL EVALUATION**

SSDP Recommended Project Name/Location	IOAP Number	Budget ID	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Comments
<b>Pond Creek Area</b>							
Charleswood Interceptor Extension	S_PO_WC_PC03_M_01_C	C94103	25477, 25478, Cooper Chapel PS (25480 & MSD0130-PS)	Pipe Upgrades	1.82-inch	62.84	
					2.25-inch	7.14	
Cinderella PS Elimination	S_PO_WC_PC04_M_01_C	H09192	Cinderella PS (60679 & MSD1013-PS), 35309	Diversion	1.82-inch	43.86	
					2.25-inch	38.2	
Lantana PS I/I Investigation & Rehabilitation	S_PO_WC_PC05_M_07_C	H09193	Lantana Drive #1 PS (25484 & 93719 & MSD0101-PS)	I/I Reduction	SSES/Rehab		Project Completed - Monitoring Ongoing
Government Center PS Elimination	S_PO_WC_PC06_M_01_C	H09194	Government Center PS (MSD0180-PS)	Diversion	1.82-inch	50.05	Project Completed
					2.25-inch	48.01	
Avanti PS Elimination	S_PO_WC_PC07_M_01_A	A09090	Avanti PS (21229-W)	Diversion	1.82-inch	1448.28	Project Completed
					2.25-inch	1448.28	
					2.60-inch	1448.28	
Leven PS Elimination	S_PO_WC_PC10_M_01_C	H09196	Leven PS (36419 & MSD1019-PS)	Diversion	1.82-inch	152.13	
					2.25-inch	74.72	
Edsel PS I/I Investigation & Rehabilitation	S_PO_WC_PC11_M_07_C	H09197	Edsel PS (92098 & MSD1048-PS)	I/I Reduction	SSES/Rehab		Project Completed - Monitoring Ongoing
<b>ORFM Area</b>							
Mellwood System Improvements & PS Eliminations	S_OR_MF_NB01_M_01_B	A09556, H09188	26752, 41374, 41416, Mockingbird Valley PS (MSD0007-PS), Winton PS (MSD0010-PS), Mellwood Avenue PS (24472 & MSD0023-PS), Canoe Lane PS (24152-W & MSD0024-PS)	PS Upgrades, Pipe Upgrades & Diversion	1.82-inch	25.09	
					2.25-inch	26.97	
					2.60-inch	26.09	
Derington Ct. PS I/I Investigation & Rehabilitation	S_OR_MF_NB03_S_07_C	H09190	Derington Court PS (MSD0095-PS)	I/I Reduction	SSES/Rehab		
Prospect WQTC Eliminations, Harrods Creek PS, and ORFM System Improvements	S_OR_MF_NB04_M_03_B_B	D94206, A12023, A12179	40870, 40871, 40872, 89646, Barbour Lane PS (42680, 65633, 65635, MSD0192-PS), West Goose Creek PS (22436 & MSD0123-PS), Phoenix Hill PS (MSD1044-PS), Glenview Hills PS (MSD0183-PS), New Market PS (MSD0193-PS), Deep Creek PS (MSD1063-PS), Hunting Creek South WQTC (MSD0292)	PS and Pipe Upgrades, Diversion, WQTC eliminations	2.25-inch	1.69	
					2.60-inch	0.99	

**TABLE 5.3.1  
2012 SSDP LEVEL OF CONTROL EVALUATION**

SSDP Recommended Project Name/Location	IOAP Number	Budget ID	SSO(s) Addressed	Technology	Level of Protection	Present Worth Benefit-Cost Ratio	Comments
<b>Mill Creek Area</b>							
Shively Interceptor	S_MC_WC_NB01_M_01_A	B06208	04498, 04542, Pioneer PS (81814-W), Fern Lea PS (MSD0047-PS), Garr's Lane PS (MSD0050-PS)	Pipe Upgrades	1.82-inch	5.2	
					2.25-inch	6.68	
					2.60-inch	6.7	
East Rockford PS Relocation	S_MC_WC_NB02_S_03_C	A09091	East Rockford PS (04699-W)	PS Replacement and Relocation	PS Relocation		Project Completed
<b>Small WQTC Area</b>							
Lucas Ln. PS Inline Storage	S_FF_BT_NB01_S_09A_C_A	H09166	Lucas Lane PS (MSD0199-LS)	Inline Storage	1.82-inch	112.86	
					2.25-inch	95.75	
Riding Ridge PS Improvements	S_HC_HN_NB01_S_03_C_A	H09175	Riding Ridge PS (MSD1060-LS)	PS Upgrades	1.82-inch	52.02	
					2.25-inch	19.61	
Gunpowder PS Inline Storage	S_HC_HN_NB02_S_09A_C_B	H09242	Gunpowder PS (MSD1055-LS)	Inline Storage	1.82-inch	78.71	
					2.25-inch	59.15	
Fox Harbor Inline Storage	S_HC_HN_NB03_S_09A_A_A	H09176	Fox Harbor #1 and #2 PS (62769)	Inline Storage	1.82-inch	43.49	
					2.25-inch	81.4	
					2.60-inch	87.55	
Fairway View PS Improvements	S_HC_HS_NB01_S_03_C_A	H09177	Fairway View PS (MSD1065-PS)	PS Upgrades	1.82-inch	10.32	
					2.25-inch	7.64	
Lake Forest PS SSO Investigation	S_FF_LF_NB01_S_13_C_A	H09173	Lake Forest PS (MSD1169-LS)	Monitoring	Monitoring		Monitoring Ongoing
St. Rene Rd. PS Inline Storage	S_FF_CH_NB01_S_09A_C_A	H09168	94187	Inline Storage	1.82-inch	212	
					2.25-inch	97.68	
<b>CSS Area</b>							
Sonne PS I/I Investigation & Rehabilitation	S_OR_MF_42007_S_07_C	H09187	Sonne Avenue PS (MSD0042-PS)	I/I Reduction	SSES/Rehab		Project Completed - Monitoring Ongoing
Hazelwood PS I/I Investigation & Rehabilitation	S_MC_MF_55665_S_07_C	H09181	Hazelwood PS (55665)	I/I Reduction	SSES/Rehab		Project Completed - Monitoring Ongoing

**Legend:** LS –Lift station, PS – Pump Station, CSO – Combined Sewer Overflow, SSO – Sanitary Sewer Overflow, CSS- Combined Sewer System, WQTC – Water Quality Treatment Center, SSES – Sanitary Sewer Evaluation Study, I/I – Inflow and Infiltration, UMFLS – Upper Middle Fork Lift Station, ORFM – Ohio River Force Main

Table 5.3.2 2012 SSDP Final Project Suite and Revised Project Schedule

ACD Project Number	Project Name	Receiving Stream	Overflows Controlled	2009 Level of Control Depth (in)	2009 Level of Control Storm	2009 Size (MG)	2009 Cost	2012 Level of Control Depth (in)	2012 Level of Control Storm	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
<b>CEDAR CREEK AREA</b>														
S_CC_CC_70158_M_09A_C	Idlewood Inline Storage	CEDAR CREEK	28998, 28984, 63094, 63095, 70158	1.82	2-Year, 3-Hour	N/A	\$2,317,000	1.82	2-Year, 3-Hour	N/A	\$2,317,000	12/31/2023	12/31/2023	
S_FF_CC_81316_M_03_C_A	Fairmount Road Pump Station Off-Line Storage	BIG RUN	Fairmount Road PS (81316 & 97362)	N/A	N/A (New Project)	N/A	N/A	1.82	2-Year, 3-Hour	3.4 MG	\$13,439,000	N/A	12/31/2015	Project needed to accommodate flows from eliminated Jeffersontown WQTC and acknowledge capacity at Cedar Creek WQTC.
S_CC_CC_67997_M_01_C	Little Cedar Creek Interceptor Improvements	LITTLE CEDAR CREEK	67997, 67999, 86423, 86424, 89195, 89196, 89197	1.82	2-Year, 3-Hour	Pipe Upgrades	\$1,875,000	1.82	2-Year, 3-Hour	N/A	\$1,875,000	12/31/2024	12/31/2024	
S_CC_CC_MSD1025_S_03_B	Bardstown Rd. PS Improvements	BIG RUN	88545	2.25	5-Year, 3-Hour	N/A	\$281,000	2.25	5-Year, 3-Hour	N/A	\$281,000	12/31/2021	12/31/2021	
S_CC_CC_MSD1080_S_01_C	Running Fox PS Elimination	LITTLE CEDAR CREEK	MSD1080-LS	1.82	2-Year, 3-Hour	N/A	\$96,000	1.82	2-Year, 3-Hour	N/A	\$77,000	12/31/2010	12/31/2010	Project Completed
<b>HITE CREEK AREA</b>														
S_HC_HC_MSD1082_S_09A_C	Meadow Stream Pump Station & Force Main Upgrade	FLOYDS FORK, SOUTH FORK HARRODS CREEK	Meadow Steam PS (91087, MSD1082-PS)	1.82	2-Year, 3-Hour	0.5	\$974,000	2.60	10-Year, 3-Hour	3.89 MGD PS & New 18" Force Main	\$974,000	12/31/2016	12/31/2012	Project changed from a small storage basin to a pump station upgrade and new force main due to the capacity needs of Crestwood. The City paid the additional costs beyond MSD's overflow control commitment. Project Completed - Monitoring Ongoing
S_HC_HC_MSD1086_M_07_C_A	Floydsburg Rd. SSES, Rehabilitation and Pump Station Upgrade	FLOYDS FORK	Floydsburg Road (MSD1086-PS, 90776, 108956, 108957, 108958)	1.82	2-Year, 3-Hour	N/A	\$57,000	1.82	2-Year, 3-Hour	N/A	\$57,000	12/31/2010	12/31/2010	Project Completed - Monitoring Ongoing
S_HC_HC_MSD1085_S_03_A	Kavanaugh Rd. PS Improvements	HITE CREEK	Kavanaugh Rd (MSD1085-PS)	2.60	10-Year, 3-Hour	N/A	\$1,110,000	2.60	10-Year, 3-Hour	N/A	\$1,110,000	12/31/2024	12/31/2024	
<b>FLOYDS FORK AREA</b>														
S_FF_FF_NB01_S_01_C_A	Woodland Hills PS Diversion	POPE LICK	33003, 65531	1.82	2-Year, 3-Hour	N/A	\$20,000	1.82	2-Year, 3-Hour	N/A	\$20,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing
S_FF_FF_NB02_S_13_C	Eden Care PS SSO Investigation	FLOYDS FORK	Eden Care PS (MSD1105-PS)	N/A	N/A (Monitor)	N/A	N/A	N/A	N/A	N/A	\$0	N/A	Eliminated	Only one overflow had been documented at this location. MSD cleaned the sewers in the vicinity and has not documented an overflow in over 3 years. No further action is deemed necessary.
S_FF_FF_NB03_M_01_C_A	Ashburton PS Improvements & Diversion	FLOYDS FORK	Olde Copper Court PS (MSD0165-PS), Ashburton PS (MSD0166-PS)	1.82	2-Year, 3-Hour	N/A	\$118,000	1.82	2-Year, 3-Hour	N/A	\$118,000	12/31/2021	12/31/2021	Project Completed
<b>JEFFERSONTOWN AREA</b>														
S_JT_JT_NB01_M_01_C_A	Jeffersontown WQTC Elimination	CHENOWETH RUN	28390, 28391, 28392, 28395, 28551, 31733, Jeffersontown WQTC (28173 & 64505 & MSD0255 & IS028-SI)	1.82	2-Year, 3-Hour	N/A	\$23,737,000	1.82	2-Year, 3-Hour	N/A	\$23,737,000	12/31/2015	12/31/2015	
S_JT_JT_NB01A_M_03_C	Chenoweth Hills WQTC Elimination & PS Improvements	CHENOWETH RUN	Chenoweth Run PS (MSD0196-PS & 86052 & 64096), Chippewa PS (92061), Chenoweth Hills WQTC PS (MSD0263A-PS), Chenoweth Hills WQTC (MSD0263)	1.82	2-Year, 3-Hour	N/A	\$3,140,000	1.82	2-Year, 3-Hour	N/A	\$3,140,000	12/31/2015	12/31/2015	
S_JT_JT_NB02_M_01_C	Dell Rd & Charlane Project Pkwy Interceptor	BEATTY BROOK	Charlane Pkwy (28250, 28249, 28340, 28336, 104289), Dell Rd. (28413, 28414, 28415, 28416, 28417)	1.82	2-Year, 3-Hour	Pipe Upgrades	\$917,000	1.82	2-Year, 3-Hour	N/A	\$917,000	12/31/2022	12/31/2022	
S_JT_JT_NB03_M_01_C	Raintree & Marian Ct PS Eliminations and Pipe Upgrades (2 Phases)	BEATTY BROOK	28719, 28711, Marian Court PS (28729), Raintree PS (MSD0149-PS)	1.82	2-Year, 3-Hour	N/A	\$1,005,000	1.82	2-Year, 3-Hour	N/A	\$1,005,000	12/31/2021	12/31/2021	
S_JT_JT_NB04_M_01_A	Monticello PS Elimination	FERN CREEK	Monticello Place PS (MSD0151-PS & 27969)	2.60	10-Year, 3-Hour	N/A	\$207,000	2.60	10-Year, 3-Hour	N/A	\$207,000	12/31/2022	12/31/2022	

Table 5.3.2 2012 SSDP Final Project Suite and Revised Project Schedule

ACD Project Number	Project Name	Receiving Stream	Overflows Controlled	2009 Level of Control Depth (in)	2009 Level of Control Storm	2009 Size (MG)	2009 Cost	2012 Level of Control Depth (in)	2012 Level of Control Storm	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
<b>MIDDLE FORK AREA</b>														
S_MISF_MF_NB01_M_01_C_A1	Middle Fork Relief Interceptor, Wet Weather Storage, and Upper Middle Fork LS Diversion (2 Phases)	MIDDLE FORK BEARGRASS CREEK	02932, 02933, 02935, 08537, 23211, 23212, 27005, 51180, 51221, 51160, 51161, 45835, 47583, 47593, 47596, 47603, 47604, 90700, IS021A-SI, Middle Fork at Breckenridge (08935-SM)	1.82	2-Year, 3-Hour	1.6	\$26,333,500	1.82	N/A	N/A	\$26,333,500	12/31/2013, 12/31/2023	12/31/2013, 12/31/2023	
S_MI_MF_NB04_M_03_B	Goose Creek PS Improvements & Wet Weather Storage (2 Phases)	GOOSE CREEK	Devondale PS (21628-W), Goose Creek PS (46891, 62418, 62420, 91629, 91630, 105936), Saurel PS (43472)	2.25	5-Year, 3-Hour	0.5	\$7,558,000	2.25	5-Year, 3-Hour	N/A	\$7,558,000	12/31/2024	12/31/2024	
S_MI_MF_NB06_M_01_A_A - 1, S_MI_MF_NB06_M_01_A_A - 2	Anchor Estates PS Eliminations (2 Phases)	MIDDLE FORK BEARGRASS CREEK	Vannah PS (01106), Anchor Estates #1 PS (00746 & 00056-W), Anchor Estates #2 PS (MSD0057-LS)	2.60	10-Year, 3-Hour	N/A	\$1,909,000	2.6	10-Year, 3-Hour	N/A	\$1,909,000	12/31/2013, 12/31/2016	12/31/2013, 12/31/2016	Phase 1 Completed - Vannah PS Eliminated
S_MI_MF_NB07_S_07_C	Hurstbourne I/I Investigation & Rehabilitation	HURSTBOURNE CREEK	01793	1.82	2-Year, 3-Hour	N/A	\$536,000	1.82	2-Year, 3-Hour	N/A	\$536,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing
<b>SOUTHEAST DIVERSION AREA</b>														
S_SD_MF_NB03_S_07_C	Parkview Estates I/I Investigation & Rehabilitation	SOUTH FORK BEARGRASS CREEK	47250	1.82	2-Year, 3-Hour	N/A	\$285,000	1.82	2-Year, 3-Hour	N/A	\$285,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing
S_SD_MF_NB04_S_01_B_A	Klondike Interceptor	SOUTH FORK BEARGRASS CREEK	25676 (Alcona), 26650, 26651	2.25	5-Year, 3-Hour	Pipe Upgrades	\$558,000	2.25	5-Year, 3-Hour	N/A	\$558,000	12/31/2015	12/31/2015	
S_SD_MF_NB05_M_01_A	Sutherland Interceptor	SOUTH FORK BEARGRASS CREEK	Sutherland (16649)	2.60	10-Year, 3-Hour	Pipe Upgrades	\$412,000	2.60	10-Year, 3-Hour	N/A	\$412,000	12/31/2023	12/31/2023	
S_SD_MF_NB06_S_13_C	Beargrass Interceptor Rehab Ph. 2	SOUTH FORK BEARGRASS CREEK	51594	1.82	2-Year, 3-Hour	N/A	\$57,000	1.82	2-Year, 3-Hour	N/A	\$57,000	12/31/2010	12/31/2010	Monitoring Ongoing
<b>POND CREEK AREA</b>														
S_PO_WC_PC03_M_01_C	Charleswood Interceptor Extension	FISHPOOL CREEK	25477, 25478, Cooper Chapel PS (25480 & MSD0130-PS)	1.82	2-Year, 3-Hour	Pipe Upgrades	\$603,000	1.82	2-Year, 3-Hour	N/A	\$1,600,000	12/31/2022	12/31/2022	
S_PO_WC_PC04_M_01_C	Cinderella PS Elimination	FISHPOOL CREEK	Cinderella PS (60679 & MSD1013-PS), 35309	1.82	2-Year, 3-Hour	N/A	\$2,205,000	1.82	2-Year, 3-Hour	N/A	\$2,205,000	12/31/2023	12/31/2023	
S_PO_WC_PC05_M_07_C	Lantana PS I/I Investigation & Rehabilitation	PENNSYLVANIA RUN	Lantana Drive #1 PS (25484 & 93719 & MSD0101-PS)	1.82	2-Year, 3-Hour	N/A	\$20,000	N/A (SSES/Rehab)	N/A (SSES/Rehab)	N/A	\$20,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing
S_PO_WC_PC06_M_01_C	Government Center PS Elimination	PENNSYLVANIA RUN	Government Center PS (MSD0180-PS)	1.82	2-Year, 3-Hour	N/A	\$1,225,000	1.82	2-Year, 3-Hour	N/A	\$1,225,000	12/31/2024	12/31/2024	Project Completed - Monitoring Ongoing
S_PO_WC_PC07_M_01_A	Avanti PS Elimination	LITTLE CEDAR CREEK	Avanti PS (21229-W)	2.60	10-Year, 3-Hour	N/A	\$31,000	2.6	10-Year, 3-Hour	N/A	\$31,000	12/31/2010	12/31/2010	Project Completed - Monitoring Ongoing
S_PO_WC_PC08_M_01_C	Lea Ann Way System Improvements	FERN CREEK	19360, 19369, 29933, 29948, 29943, 31083, 31084, 79076, Lea Ann Way PS (MSD1010-PS)	1.82	2-Year, 3-Hour	Pipe Upgrades	\$827,000	1.82	2-Year, 3-Hour	Additional Pipe Upgrades	\$827,000	12/31/2015	12/31/2015	Additional overflows have been occurring in recent years. Therefore, additional sewer inspection and rehabilitation are underway. Contingency plans have been developed and are dependent upon the efficacy of rehabilitation of wet weather flows.
S_PO_WC_PC09_M_09B_C	Outer Loop Wet Weather Storage	FISHPOOL CREEK	70212, 17724	1.82	2-Year, 3-Hour	1.42	\$4,280,000	2.60	10-Year, 3-Hour		\$0	12/31/2024	Eliminated	Due to improvements in the Pond Creek hydraulic model calibration, this storage basin is no longer necessary.
S_PO_WC_PC09_M_09B_C	Caven Ave Pump Station Elimination	FISHPOOL CREEK	27116, Caven Ave PS (MSD0133-PS)	1.82	2-Year, 3-Hour	0.21	\$731,000	2.60	10-Year, 3-Hour	PS Elimination	\$1,800,000	12/31/2024	12/31/2016	Recent new pipeline constructed to eliminate a nearby package treatment plant makes the elimination of the pump station the most cost effective overflow solution.
S_PO_WC_PC10_M_01_C	Leven PS Elimination	PENNSYLVANIA RUN	Leven PS (36419 & MSD1019-PS)	1.82	2-Year, 3-Hour	N/A	\$376,000	1.82	2-Year, 3-Hour	N/A	\$376,000	12/31/2022	12/31/2022	
S_PO_WC_PC11_M_07_C	Edsel PS I/I Investigation & Rehabilitation	FERN CREEK	Edsel PS (92098 & MSD1048-PS)	1.82	2-Year, 3-Hour	N/A	\$367,000	1.82	2-Year, 3-Hour	N/A	\$367,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing

Table 5.3.2 2012 SSDP Final Project Suite and Revised Project Schedule

ACD Project Number	Project Name	Receiving Stream	Overflows Controlled	2009 Level of Control Depth (in)	2009 Level of Control Storm	2009 Size (MG)	2009 Cost	2012 Level of Control Depth (in)	2012 Level of Control Storm	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
<b>ORFM AREA</b>														
S_OR_MF_NB01_M_01_B	Mellwood PS and Forcemain Improvements, System Improvements & PS Eliminations (2 Phases)	MUDDY FORK BEARGRASS CREEK	26752, 41374, 41416, Mockingbird Valley PS (MSD0007-PS), Winton PS (MSD0010-PS), Mellwood Avenue PS (24472 & MSD0023-PS), Canoe Lane PS (24152-W & MSD0024-PS)	2.25	5-Year, 3-Hour	N/A	\$3,055,000	2.25	5-Year, 3-Hour	N/A	\$3,055,000	12/31/2012, 12/31/2024	12/31/2012, 12/31/2024	Phase 1 Project Completed - Monitoring Ongoing
S_OR_MF_NB02_S_13_C	Leland Road SSO Investigation	CHERRYWOOD CREEK	96020	N/A	N/A	N/A	N/A	N/A (Rehab & Monitoring)	N/A (Rehab & Monitoring)	N/A	\$0	N/A	Eliminated	Only one overflow had been documented at this location. MSD cleaned the sewers in the vicinity and has not documented an overflow in over 3 years. No further action is deemed necessary.
S_OR_MF_NB03_S_07_C	Derington Ct. PS I/I Investigation & Rehabilitation	GOOSE CREEK	Derington Court PS (MSD0095-PS)	1.82	2-Year, 3-Hour	N/A	\$265,000	1.82	2-Year, 3-Hour	N/A	\$265,000	12/31/2012	12/31/2012	Project Completed - Monitoring Ongoing
S_OR_MF_NB04_M_03_B_B	Prospect WQTC Eliminations, Harrods Creek PS, and ORFM System Improvements (3 Phases)	LITTLE GOOSE CREEK	40870, 40871, 40872, 89646, Barbour Lane PS (42680, 65633, 65635, MSD0192-PS), West Goose Creek PS (22436 & MSD0123-PS), Phoenix Hill PS (MSD1044-PS), Glenview Hills PS (MSD0183-PS), New Market PS (MSD0193-PS), Deep Creek PS (MSD1063-PS), Hunting Creek South WQTC (MSD0292)	2.25	5-Year, 3-Hour	N/A	\$31,368,000	2.25	5-Year, 3-Hour	N/A	\$31,368,000	12/31/2015, 12/31/2016	12/31/2015, 12/31/2016	
<b>MILL CREEK AREA</b>														
S_MC_WC_NB01_M_01_A	Shively Interceptor	LYNNVIEW DITCH	04498, 04542, Pioneer PS (81814-W), Fern Lea PS (MSD0047-PS), Garr's Lane PS (MSD0050-PS)	2.60	10-Year, 3-Hour	Pipe Upgrades	\$16,419,000	2.6	10-Year, 3-Hour	N/A	\$16,419,000	12/31/2014	12/31/2014	Project Completed - Monitoring Ongoing
S_MC_WC_NB02_S_03_C	East Rockford PS Relocation	MILL CREEK	East Rockford PS (04699-W)	1.82	2-Year, 3-Hour	N/A	\$1,044,000	1.82	2-Year, 3-Hour	N/A	\$1,044,000	12/31/2021	12/31/2021	Project Completed
<b>SMALL WQTC AREA</b>														
S_FF_BT_NB01_S_09A_C_A	Lucas Ln. PS Inline Storage	GOOSE CREEK	Lucas Lane PS (MSD0199-LS)	1.82	2-Year, 3-Hour	N/A	\$183,000	1.82	2-Year, 3-Hour	N/A	\$183,000	12/31/2021	12/31/2021	
S_HC_HN_NB01_S_03_C_A	Riding Ridge PS Improvements	HARRODS CREEK	Riding Ridge PS (MSD1060-LS)	1.82	2-Year, 3-Hour	N/A	\$27,000	1.82	2-Year, 3-Hour	N/A	\$27,000	12/31/2014	12/31/2014	
S_HC_HN_NB02_S_09A_C_B	Gunpowder PS Inline Storage	HARRODS CREEK	Gunpowder PS (MSD1055-LS)	1.82	2-Year, 3-Hour	N/A	\$176,000	1.82	2-Year, 3-Hour	N/A	\$176,000	12/31/2021	12/31/2021	
S_HC_HN_NB03_S_09A_A_A	Fox Harbor Inline Storage	HARRODS CREEK	Fox Harbor #1 and #2 PS (62769)	2.60	10-Year, 3-Hour	N/A	\$328,000	2.60	10-Year, 3-Hour	N/A	\$328,000	12/31/2021	12/31/2021	
S_HC_HS_NB01_S_03_C_A	Fairway View PS Improvements	HARRODS CREEK	Fairway View PS (MSD1065-PS)	1.82	2-Year, 3-Hour	N/A	\$87,000	1.82	2-Year, 3-Hour	N/A	\$167,000	12/31/2014	12/31/2014	
S_FF_LF_NB01_S_13_C_A	Lake Forest PS SSO Investigation	CHENOWETH RUN	Lake Forest PS (MSD1169-LS)	N/A	N/A	N/A	N/A	N/A (Monitoring)	N/A (Monitoring)	N/A	\$77,000	12/31/2012	12/31/2012	Monitoring Ongoing
S_FF_CH_NB01_S_09A_C_A	St. Rene Rd. PS Inline Storage	CHENOWETH RUN	94187	1.82	2-Year, 3-Hour	N/A	\$30,000	1.82	2-Year, 3-Hour	N/A	\$30,000	12/31/2021	12/31/2021	
<b>CSS AREA</b>														
S_OR_MF_42007_S_07_C	Sonne PS I/I Investigation	PADDY RUN	Sonne Avenue PS (MSD0042-PS)	1.82	2-Year, 3-Hour	N/A	\$265,000	1.82	2-Year, 3-Hour	N/A	\$265,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing
S_SF_MF_30917_M_09_A	Camp Taylor System Improvements (Four Phases)	MUDDY FORK BEARGRASS CREEK	08717, 13931, 13943, 36763, 44396, 44397, 66349, 104223, 104231	2.60	10-Year, 3-Hour	Pipe Upgrades	\$28,279,000	2.60	10-Year, 3-Hour	Pipe Upgrades	\$28,279,000	Dec 31, 2012, 2013, 2017 & 2024	Multiple (Same as 2009)	Project approach is similar to 2009, but the project area targeted for inspection and rehabilitation is larger.
S_MC_MF_55665_S_07_C	Hazelwood PS I/I Investigation & Rehabilitation	MANSLICK BRANCH	Hazelwood PS (55665)	1.82	2-Year, 3-Hour	N/A	\$173,000	1.82	2-Year, 3-Hour	N/A	\$173,000	12/31/2011	12/31/2011	Project Completed - Monitoring Ongoing



Table 5.3.2 2012 SSDP Final Project Suite and Revised Project Schedule

ACD Project Number	Project Name	Receiving Stream	Overflows Controlled	2009 Level of Control Depth (in)	2009 Level of Control Storm	2009 Size (MG)	2009 Cost	2012 Level of Control Depth (in)	2012 Level of Control Storm	2012 Revised Size (MG)	2012 Revised Cost (in 2008 dollars)	2009 Completion Date	Proposed Completion Date	Explanation for Proposed Revisions or Comments
INTERIM SSDP														
HIKES LANE INTERCEPTOR /HIGHGATE SPRINGS PS	Hikes Lane Interceptor and Highgate Springs	SOUTH FORK BEARGRASS CREEK AND WEDGEWOOD DITCH	18134, 18298, 18302, 18434, 18471, 18483, 18505, 18595, 49224, 49236, 49672, 49673, MSD0012-PS								\$21,216,000		11/27/2012	This project includes improvements to the Hikes Point Sewer System and eliminates the Highgate Springs Pump Station. In the general Hikes Point area includes improvements of 3,500 LF of new or replacement sewers, and decommissioning the Highgate Springs Pump Station. The new Hikes Lane Interceptor consists of 10,000 LF of 72-inch sewer that connects to Southeastern Interceptor. Project Completed - Monitoring Ongoing
SOUTHEASTERN DIVERSION STRUCTURE & INTERCEPTOR	Southeastern Diversion Structure and Interceptor	SOUTH FORK BEARGRASS CREEK	08426, 08427, 08430, 08431, 30680, 30681, 49647								\$1,744,000		5/12/2012	This project includes improvements to the Southeast Diversion Structure for increased flows due to the Hikes Lane Interceptor and other Final SSDP projects. The project consists of a new parallel Southeastern Interceptor relief sewer, two flow control junction boxes, and modifications to the existing Southeastern Diversion Structure (including removing control weirs and reprogramming Real Time Control gates). Project Completed - Monitoring Ongoing
NORTHERN DITCH DIVERSION INTERCEPTOR	Northern Ditch Diversion Interceptor	NORTHERN DITCH	MSD0271 (Yorktown)								\$20,397,000		7/31/2011	This project includes construction of a new Northern Ditch Diversion Interceptor which will allow flow from upstream projects to reach the Derek R. Guthrie WQTC. The project consists of 13,000 LF of 84-inch pipe constructed long Greasy Ditch. Project Completed - Monitoring Ongoing
SINKING FORK RELIEF SEWER	Sinking Fork Relief Sewer	MIDDLE FORK BEARGRASS CREEK AND UPPER SINKING FORK	21103, 25012, 63319								\$1,690,000		12/23/2009	This project includes conveying flow from some of the new Beechwood Village sewers and providing additional wet weather capacity downstream of the Beechwood Village East area to accommodate upstream SSDP projects. The project includes installing 2,800 LF of 24-inch relief sewer. Project Completed
BEECHWOOD VILLAGE SANITARY SEWER REPLACEMENT	Beechwood Village Sanitary Sewer Replacement	UPPER SINKING FORK	21061, 21089, 21101, 21153, 21156								\$11,800,000		4/27/2011	This project includes replacing or rehabilitating the entire local system, including 23,700 LF of sewer pipe and 580 homeowner's service connections. The project will be completed in two phases, East and West. Project Completed
DEREK R GUTHRIE WATER QUALITY TREATMENT CENTER	Derek R. Guthrie WQTC	OHIO RIVER, BLACK POND CREEK, ALVEY DITCH, MENDORA BRANCH, MILL CREEK	Wet Weather SSOs	4.50	10-Year, 24-Hour	100 MGD HRT	\$102,700,000	4.50	10-Year, 24-Hour	100 MGD HRT	\$102,700,000	12/31/2011	11/27/2012	Full high rate treatment capacity not yet available for flows to be seen by 2024 due to extreme wet weather in 2011, but current flows and overflow eliminations can be accommodated with current treatment capacity. Project Completed - Monitoring Ongoing

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**Cedar Creek  
Area**

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**Project Name**     **Bardstown Rd. PS Improvements**

**Project Number**     **S\_CC\_CC\_MSD1025\_S\_03\_B**

**Modeled Area**             Cedar Creek

**Branch or SSO ID**             MSD1025

**Project Type**             PS Upgrades

**Receiving Stream**             Big Run

**Project Description**             This alternative includes increasing the capacity of the pump station with an additional 70% of hydraulic capacity to 0.53 MGD so that overflows do not occur upstream.

**Reason for Overflow**             Capacity

**Design Parameters**             This solution is based on a 2.25 inch cloudburst rain event.

**Project Constraints**             N/A

**Estimated Capital Cost**             \$281,000

**Weighted Benefit/Cost Ratio**             46.50

Asset ID	SSO Start Date	Volume (Gal)
88545	5/12/2008	1



# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Cedar Creek Sewershed

Solution ID # S\_CC\_CC\_MS1025\_S\_03\_B

Bardstown Rd. PS Improvements

**Preliminary - For Budget Development Only**

### Legend

- Documented SSO
- Suspected SSO
- Haul Operation
- Proposed Pump Station Solution
- Pump Station
- WWTP
- Proposed Pipe Solution
- Force Main
- Collector < 12"
- Interceptor => 12"
- Combined Sewer Pipe
- Proposed Off-line Storage
- Road
- Streams
- Floodway
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Metro Parks

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

1 inch = 100 feet  
Scalable when printed on 11" X 17" paper



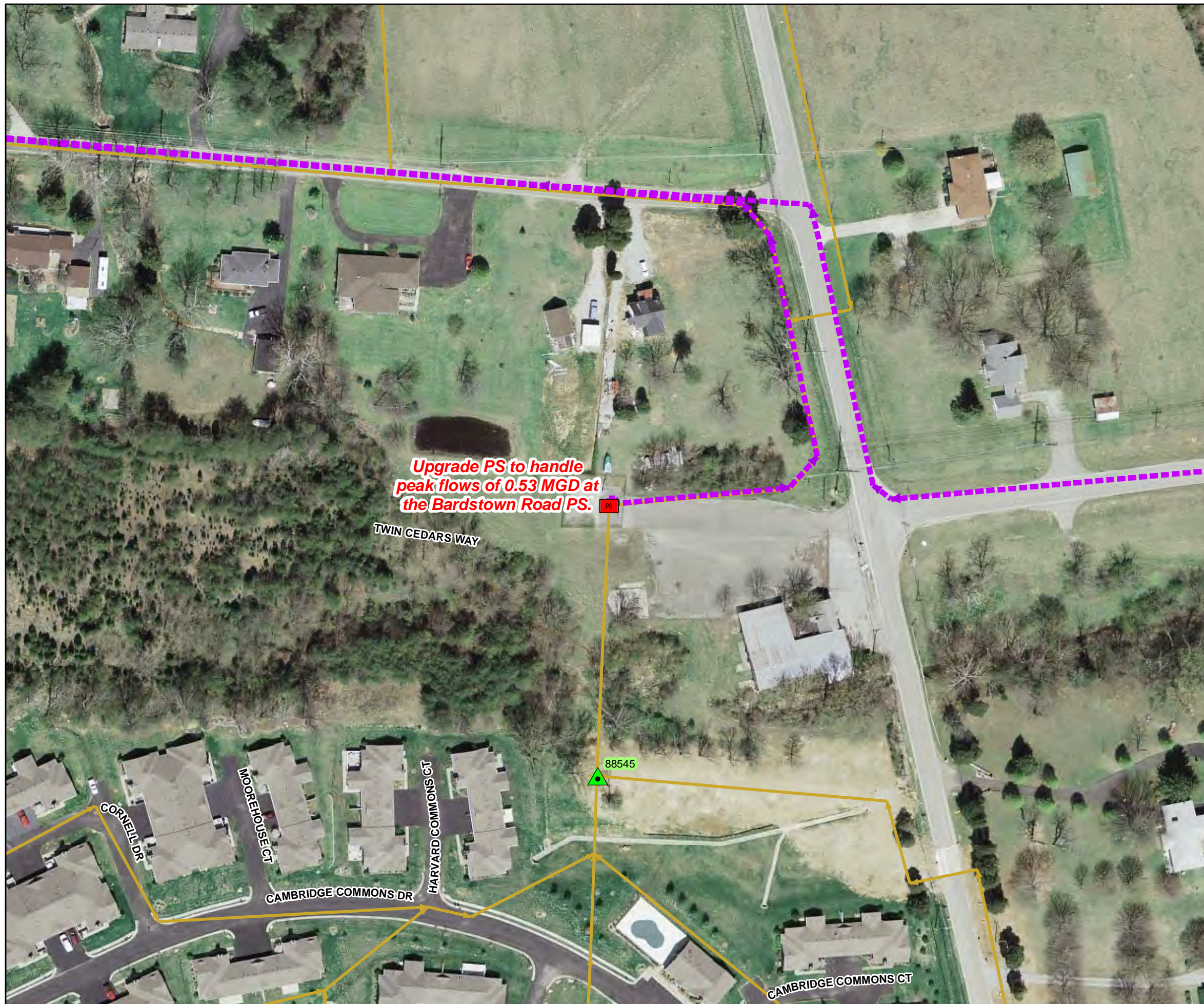
Some boundaries are uniquely symbolized within the map.

Map Revision  
May 08, 2009

Aerial Date: 2006



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**Project Name** Fairmount Road Pump Station Off-Line Storage

**Project Number** S\_FF\_CC\_81316\_M\_03\_C\_A

**Modeled Area** Cedar Creek

**Branch or SSO ID** 81316

**Project Type** Offline Storage

**Receiving Stream** Big Run

**Project Description** This project includes a 3.4 MG Underground Off-line Storage Basin and a 4.2 MGD firm capacity pump station to empty the basin.

**Reason for Overflow** Pump station capacity

**Design Parameters** JTWQTC will be eliminated and a portion of its flow diverted to this project. The new 4.2 MGD Fairmont Rd PS in the proposed storage basin will pump wet/dry weather flow to CCWQTC. This solution eliminates SSOs up to the 1.82-inch cloudburst event.

**Project Constraints** Project is located in Glenmary Subdivision Section 1, but work will occur in MSD easements or land

**Estimated Capital Cost** \$13,439,000

**Weighted Benefit/Cost Ratio** 10.17

Asset ID	SSO Start Date	Volume (Gal)
97362	4/23/2004	26400
81316	4/23/2004	500


















**Integrated Overflow Abatement Plan**

**Vol. 3 - Sanitary Sewer Discharge Plan**

Cedar Creek Sewershed

Fairmount Rd. PS Off-line Storage Basin

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Proposed Pump Station Solution
-  Pump Stations
-  MSD
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Proposed Off-line Storage
-  Streams
-  Floodway
-  Jefferson County Boundary

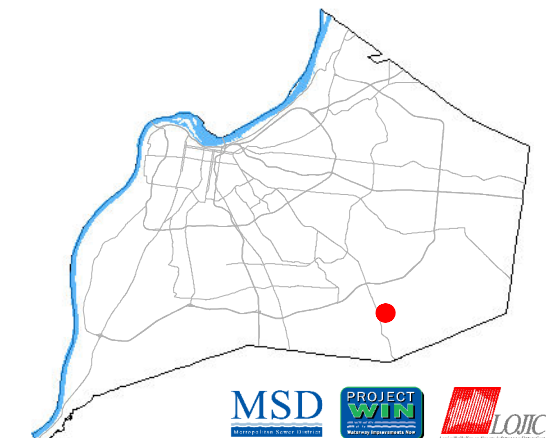
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1 inch = 100 feet



Aerial Date: 2012

Map Revision: April 15, 2014



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<b>Project Name</b>	Idlewood Inline Storage
<b>Project Number</b>	S_CC_CC_70158_M_09A_C
<b>Modeled Area</b>	Cedar Creek
<b>Branch or SSO ID</b>	70158
<b>Project Type</b>	Inline Storage
<b>Receiving Stream</b>	Cedar Creek
<b>Project Description</b>	This alternative includes in-line storage with 995 LF of (84" to 120") pipe to store wet weather peak flows. Also included are pipe upgrades for 1,747 LF of open cut (8" to 15") sewer to increase hydraulic capacity during wet weather peak flows.
<b>Reason for Overflow</b>	Hydraulic Bottleneck
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	Homes are ~100' from the SSO locations. Depth to rock is ~3'
<b>Estimated Capital Cost</b>	\$2,317,000
<b>Weighted Benefit/Cost Ratio</b>	31.36

Asset ID	SSO Start Date	Volume (Gal)
63094	1/13/2013	1500
63095	1/13/2013	1500
28998	1/24/2002	288000
70158	1/24/2002	72000
28984	1/24/2002	14400
70158	1/3/2005	803000
70158	10/19/2004	91000
63095	12/5/2011	10375
63094	12/5/2011	5300
28984	2/1/2002	21600
63094	2/6/2012	1
63094	4/12/2011	2750
70158	4/12/2011	2250
28984	4/12/2011	7150
28998	4/12/2011	9750
63095	4/12/2011	9500
63094	4/27/2011	90000
63094	4/27/2011	5
28998	4/27/2011	22500
28984	4/27/2011	22500
63095	4/27/2011	15000
63094	5/13/2012	2000
63094	5/2/2010	1475
70158	5/2/2010	1500
63095	5/2/2010	4575
63094	5/3/2011	30000
70158	5/30/2004	241000
28998	9/23/2006	21600

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**Project Name** Idlewood Inline Storage

**Project Number** S\_CC\_CC\_70158\_M\_09A\_C

28984

9/23/2006

21600

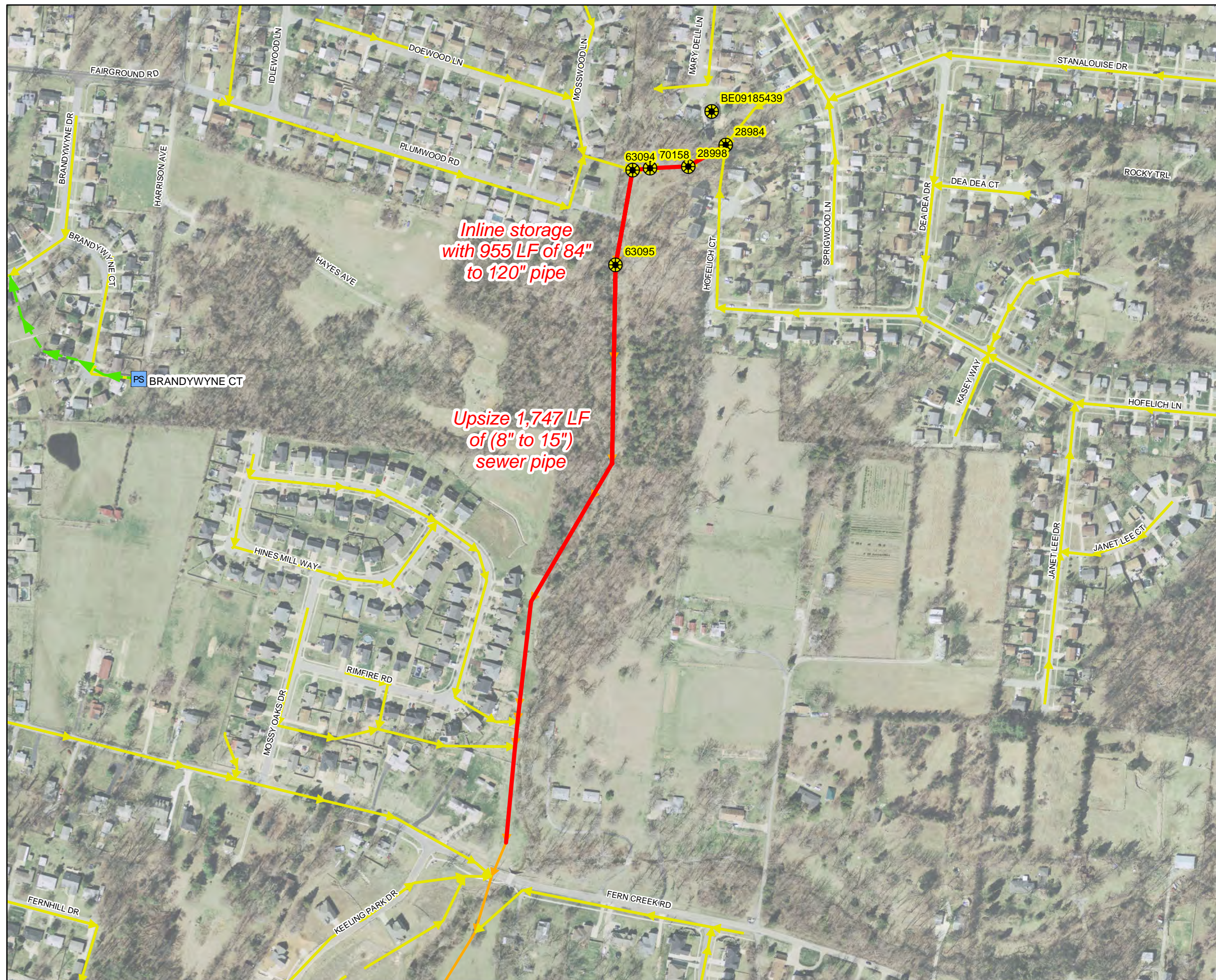


**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

**Cedar Creek Sewershed**

**Idlewood Inline Storage**

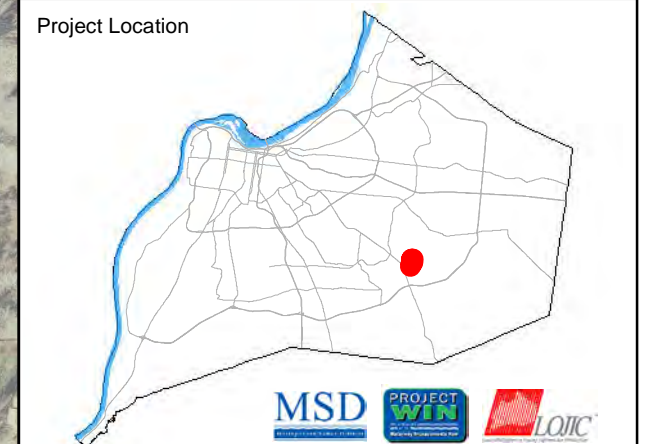
Preliminary - For Budget Development Only



- Documented SSO
- Suspected SSO
- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- WQTC
- Proposed Pipe Solution
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 300 feet		Aerial Date: 2009	Map Revision: April 9, 2012
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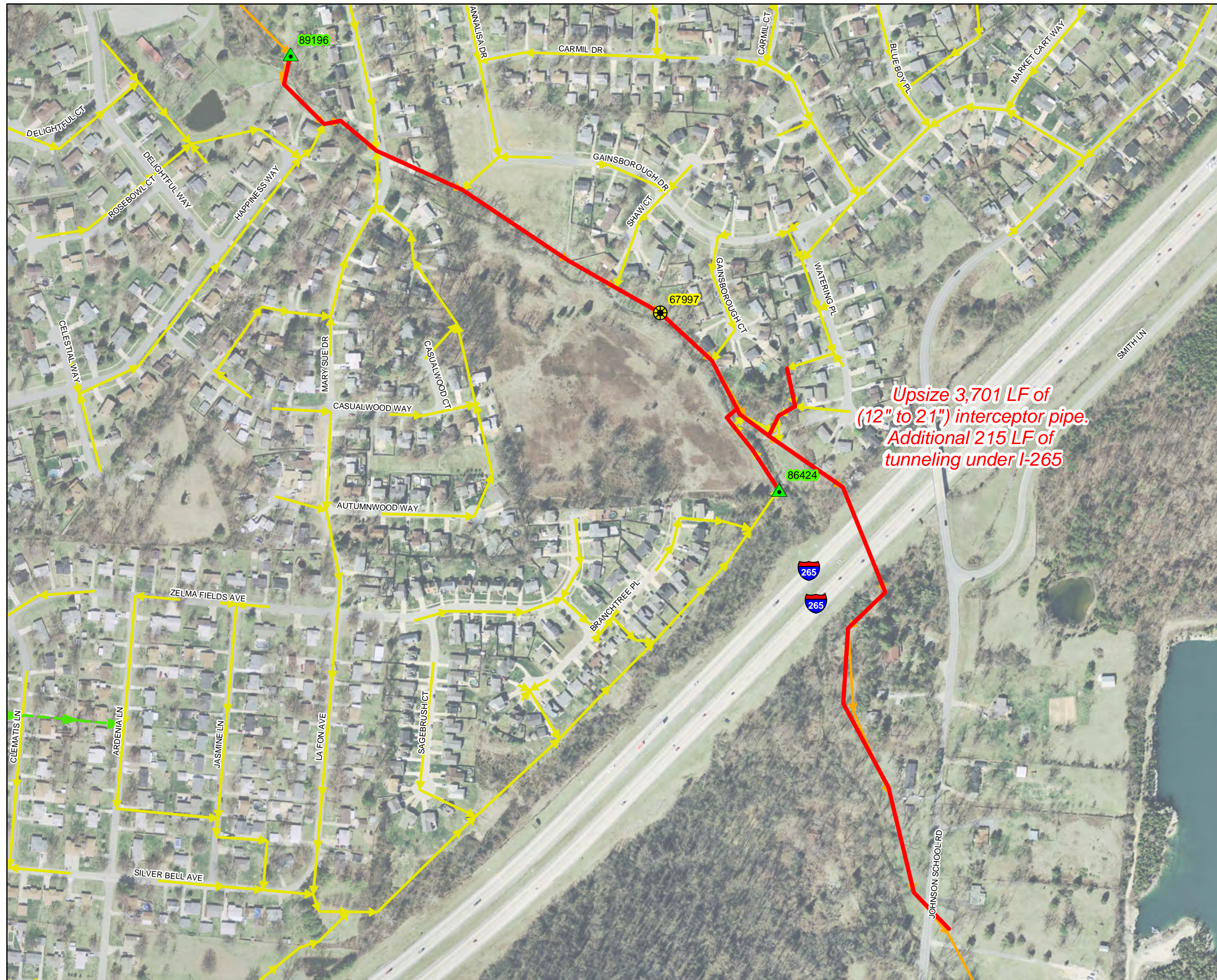
<b>Project Name</b>	Little Cedar Creek Interceptor Improvements
<b>Project Number</b>	S_CC_CC_67997_M_01_C
<b>Modeled Area</b>	Cedar Creek
<b>Branch or SSO ID</b>	67997
<b>Project Type</b>	Pipe Upgrades
<b>Receiving Stream</b>	Little Cedar Creek
<b>Project Description</b>	This alternative includes upsizing 3,701 LF of open cut sewer and 215 LF of 21" tunneling interceptor pipe in the area to increase hydraulic capacity during wet weather peak flows.
<b>Reason for Overflow</b>	System capacity
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	Project will occur primarily in existing MSD easements.
<b>Estimated Capital Cost</b>	\$1,875,000
<b>Weighted Benefit/Cost Ratio</b>	23.86

Asset ID	SSO Start Date	Volume (Gal)
67997	5/2/2010	40300
86424	5/3/2010	1
89196	5/3/2010	1



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Cedar Creek Sewershed**  
**Little Cedar Creek Interceptor Improvements**

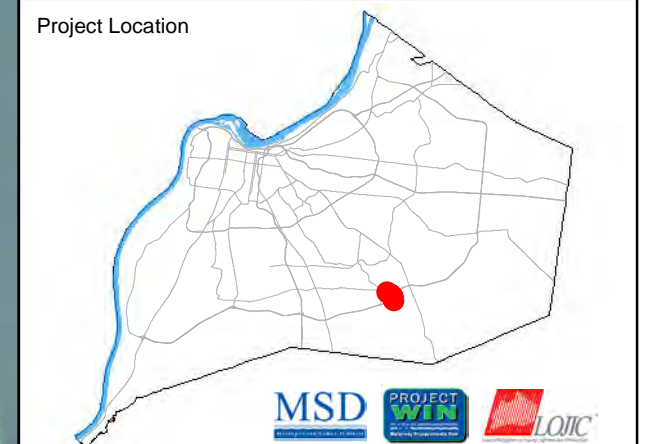
Preliminary - For Budget Development Only



- Documented SSO
- Suspected SSO
- Haulop Locations
- Pump Stations
- WQTC
- Proposed Pipe Solution
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Proposed Storage Solution
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 300 feet		Aerial Date: 2009	Map Revision: April 9, 2012
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MSD PROJECT WIN LOIC  
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**Project Name**     Running Fox PS Elimination

**Project Number**     S\_CC\_CC\_MSD1080\_S\_01\_C

**Modeled Area**             Cedar Creek

**Branch or SSO ID**         MSD1080

**Project Type**                Diversion

**Receiving Stream**         Little Cedar Creek

**Project Description**       Construct 375 LF of 8" gravity sewer to eliminate Running Fox PS.

**Reason for Overflow**       Pump station capacity

**Design Parameters**        This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**        N/A

**Estimated Capital Cost**     \$77,000

**Weighted Benefit/Cost Ratio**     536.23

Asset ID	SSO Start Date	Volume (Gal)
MSD1080-LS	3/19/2008	48000
MSD1080-LS	4/4/2008	25875



# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Cedar Creek Sewershed

Solution ID # S\_CC\_CC\_MSD1080\_S\_01\_C

Running Fox PS Elimination

**Preliminary - For Budget Development Only**

### Legend

- Documented SSO
- Suspected SSO
- Haul Operation
- Proposed Pump Station Solution
- Pump Station
- WWTP
- Proposed Pipe Solution
- Force Main
- Collector < 12"
- Interceptor => 12"
- Combined Sewer Pipe
- Proposed Off-line Storage
- Road
- Streams
- Floodway
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Metro Parks

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

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Some boundaries are uniquely symbolized within the map.

Map Revision  
May 07, 2009

Aerial Date: 2006



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**Construct 375 LF of 8" gravity sewer to eliminate Running Fox PS. Existing PS and force main will remain functional, but dormant, to allow for monitoring downstream impacts of the new diversion. If no impacts are noted, station will be eliminated.**



**Hite Creek  
Area**

**Project Name**     **Floydsburg Rd. I/I Investigation & Rehabilitation**

**Project Number**   **S\_HC\_HC\_MSD1086\_M\_07\_C\_A**

**Modeled Area**             Hite Creek

**Branch or SSO ID**             MSD1086

**Project Type**                     I/I Reduction

**Receiving Stream**             Floyds Fork

**Project Description**             The sewer service area draining to Floydsburg Road Pump Station was investigated using tele-inspection equipment and significant defects were rehabilitated. The reduction of inflow and infiltration was significant; however, post-construction data indicates that the 2-year cloudburst level of overflow control has not been met.

**Reason for Overflow**             Pump station capacity

**Design Parameters**             This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**             Project may need to include lateral work on private property

**Estimated Capital Cost**             \$57,000

**Weighted Benefit/Cost Ratio**     --

Asset ID	SSO Start Date	Volume (Gal)
90776	1/13/2005	3800
108957	1/13/2013	10950
MSD1086-PS	1/22/2006	200
90776	1/3/2005	10000
90776	1/4/2005	100000
MSD1086-PS	11/15/2005	5000
108957	11/28/2011	7875
108953	11/28/2011	7875
108956	12/12/2007	75
90776	12/15/2007	43500
108953	12/22/2013	205
108957	12/22/2013	205
108953	12/22/2013	205
108958	12/22/2013	205
MSD1086-PS	12/24/2008	3600
108957	12/5/2011	19600
90776	2/13/2007	300
108958	2/25/2011	8175
MSD1086-PS	2/5/2008	50
MSD1086-PS	3/10/2008	1200
MSD1086-PS	3/13/2006	300
90776	3/18/2008	48000
90776	3/28/2005	30000
MSD1086-PS	3/4/2008	2000
90776	3/9/2011	4100
90776	3/9/2011	540
108957	3/9/2011	525



**Project Name**    **Floydsburg Rd. I/I Investigation & Rehabilitation**














**Project Number**    **S\_HC\_HC\_MSD1086\_M\_07\_C\_A**

108953	3/9/2011	480
MSD1086-PS	4/11/2008	250
108958	4/12/2011	29750
MSD1086-PS	4/2/2006	200
108953	4/23/2011	53500
108958	4/23/2011	107000
MSD1086-PS	4/27/2011	4350
90776	4/30/2005	10000
108957	4/4/2008	85500
MSD1086-PS	5/15/2008	1500
108958	5/26/2011	140
108957	5/26/2011	140
108953	5/26/2011	140
90776	5/26/2011	140
108953	5/3/2011	4250
108958	5/3/2011	10625
MSD1086-PS	5/8/2008	325
108958	5/8/2009	15900
MSD1086-PS	6/2/2006	500
MSD1086-PS	7/14/2006	4000
108958	7/29/2009	7750
108958	7/31/2008	13000
MSD1086-PS	8/27/2006	6000
MSD1086-PS	8/30/2005	10000
MSD1086-PS	9/23/2006	6000



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Hite Creek Sewershed**  
**Floydsburg Rd I&I investigation**  
**and Rehabilitation**

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  Proposed Pipe Solution
-  WQTC
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

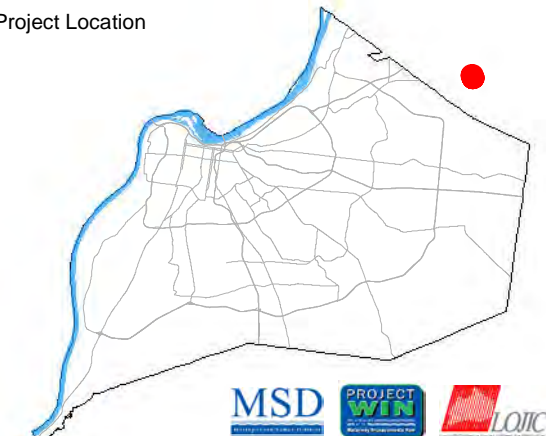
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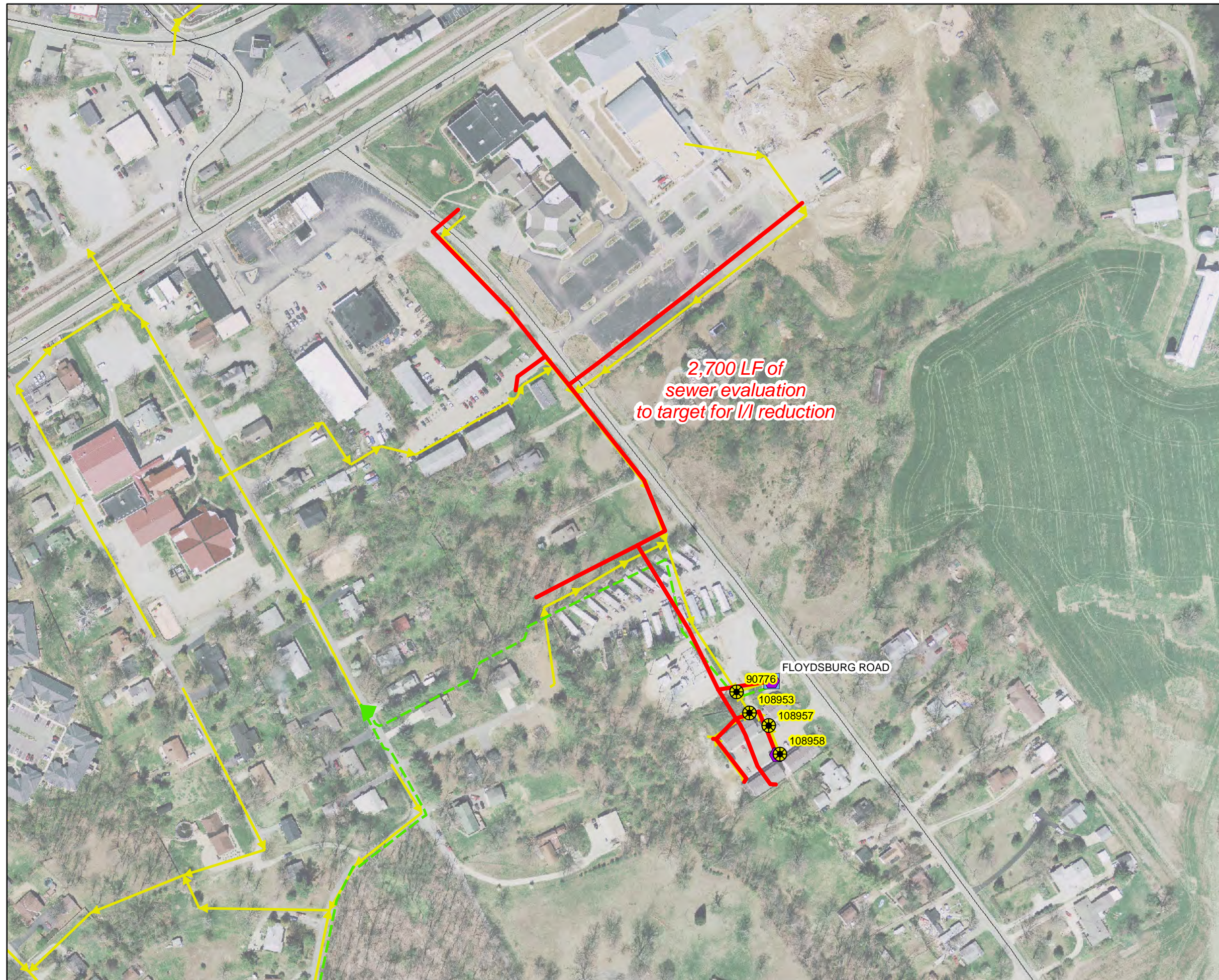
Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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<b>Project Name</b>	Kavanaugh Rd. PS Improvements
<b>Project Number</b>	S_HC_HC_MSD1085_S_03_A
<b>Modeled Area</b>	Hite Creek
<b>Branch or SSO ID</b>	MSD1085
<b>Project Type</b>	PS Upgrades
<b>Receiving Stream</b>	Hite Creek
<b>Project Description</b>	This alternative includes upgrading the Kavanaugh Road pump station to handle peak flows of 0.84 MGD and upsize 2,458 LF of force main to 8".
<b>Reason for Overflow</b>	Pump station capacity
<b>Design Parameters</b>	This solution is based on a 2.60 inch cloudburst rain event.
<b>Project Constraints</b>	Project will occur in MSD easements or land
<b>Estimated Capital Cost</b>	\$1,110,000
<b>Weighted Benefit/Cost Ratio</b>	21.09
















Asset ID	SSO Start Date	Volume (Gal)
MSD1085-PS	4/4/2008	176000
MSD1085-PS	5/11/2003	800



**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

**Hite Creek Sewershed  
Kavanaugh Rd PS Improvement**

*Preliminary - For Budget Development Only*

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Proposed Pump Station Solution
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Proposed Storage Solution
-  Streams
-  Floodway
-  Jefferson County Boundary

*General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.*

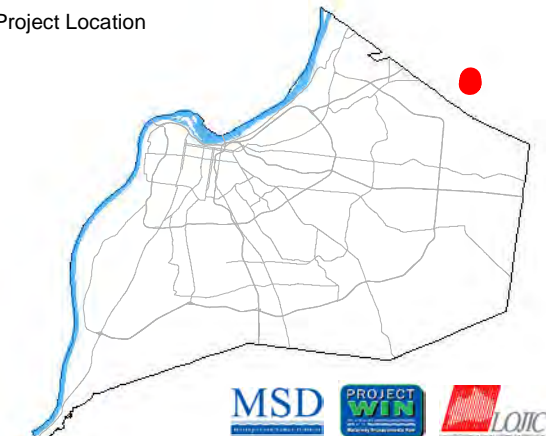
1 inch = 200 feet



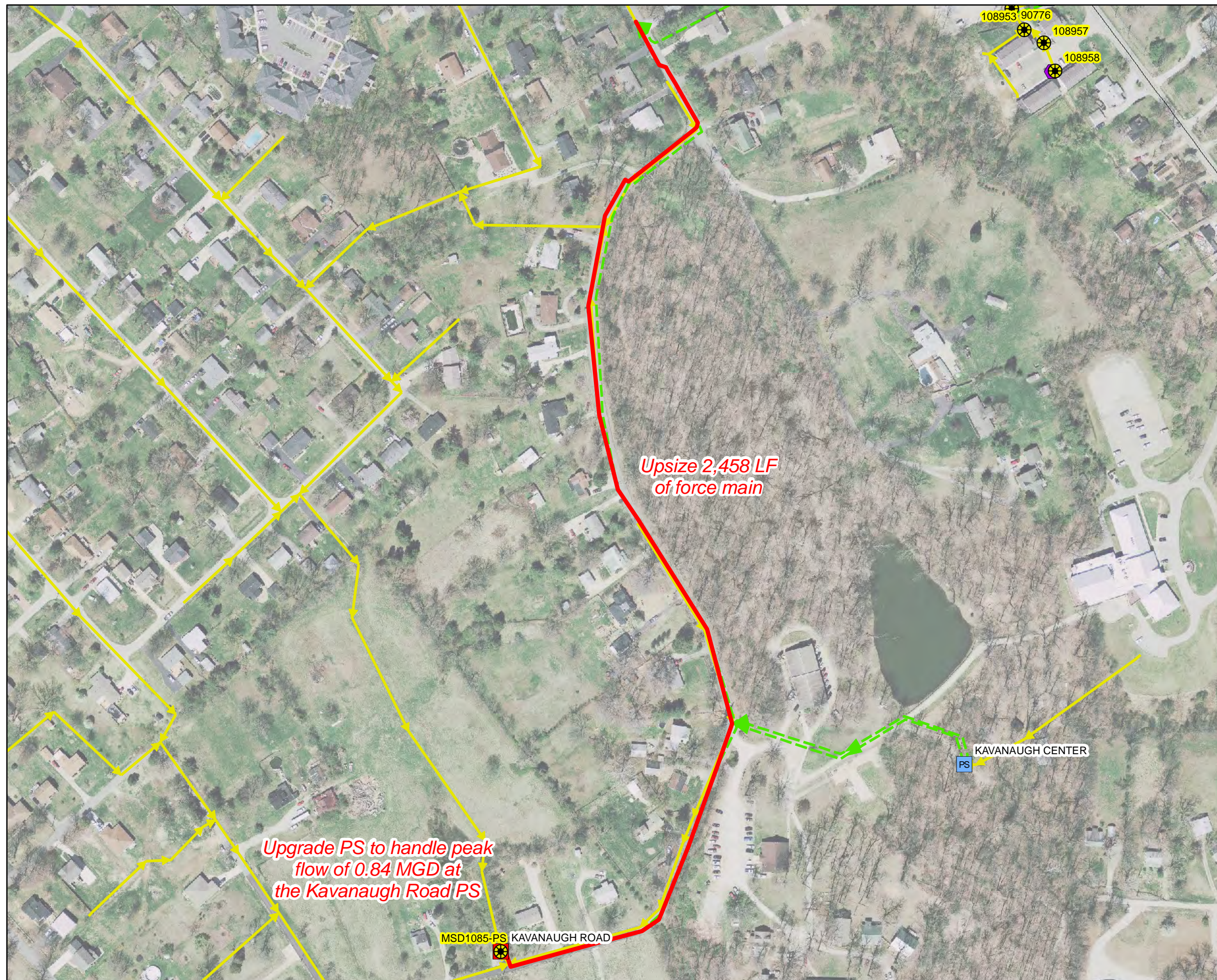
Aerial Date:  
2009

Map Revision:  
April 9, 2012

Project Location



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**Project Name** Meadow Stream Pump Station & Force Main Upgrade

**Project Number** S\_HC\_HC\_MSD1082\_S\_09A\_C

**Modeled Area** Hite Creek

**Branch or SSO ID** MSD1082

**Project Type** PS Upgrade

**Receiving Stream** Floyds Fork and South Fork Harrods Creek

**Project Description** This project involves the upgrade of Meadow Stream Pump Station to 3.89 MGD including a new wet well that mirrors the existing well and the construction of a new 18-inch force main parallel to the existing main. The project is to be constructed with funding from MSD and the City of Crestwood. The City's interest in the upgrade is to enable additional development within its boundaries. Sizing of the project was to mitigate existing wet weather issues and to accommodate this new development. As such, the IOAP benefit/cost methodology did not apply.

**Reason for Overflow** Pump station capacity

**Design Parameters** This solution is based on a 2.6 inch cloudburst rain event.

**Project Constraints** Project will occur in MSD easements or land

**Estimated Capital Cost** \$974,000

**Weighted Benefit/Cost Ratio** Not Applicable

Asset ID	SSO Start Date	Volume (Gal)
MSD1082-PS	1/27/2012	159750
MSD1082-PS	1/3/2005	97000
91087	10/9/2009	56250
91087	11/28/2011	6400
91087	12/5/2011	78500
MSD1082-PS	2/25/2011	6600
91087	3/18/2008	1440000
91087	3/9/2011	20600
91087	4/11/2011	335250
91087	4/23/2011	652500
MSD1082-PS	4/27/2011	348125
91087	4/4/2008	180000
91087	5/13/2012	14875
91087	5/2/2010	21000
91087	5/3/2011	112500
91087	7/29/2009	10
91087	9/21/2009	12700


















# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Hite creek Sewershed

Meadow Stream PS Expansion

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Proposed Pump Station Solution
-  Pump Stations
-  MSD
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Proposed Off-line Storage
-  Streams
-  Floodway
-  Jefferson County Boundary

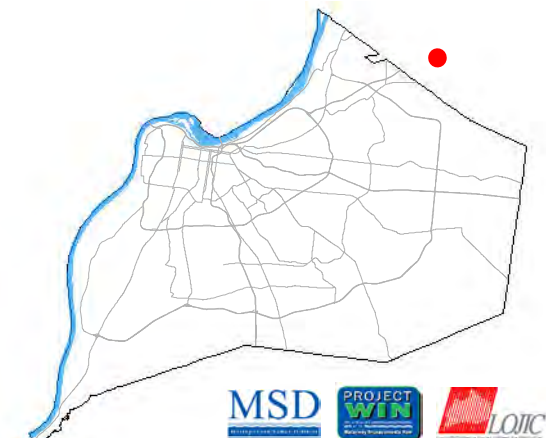
General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 100 feet

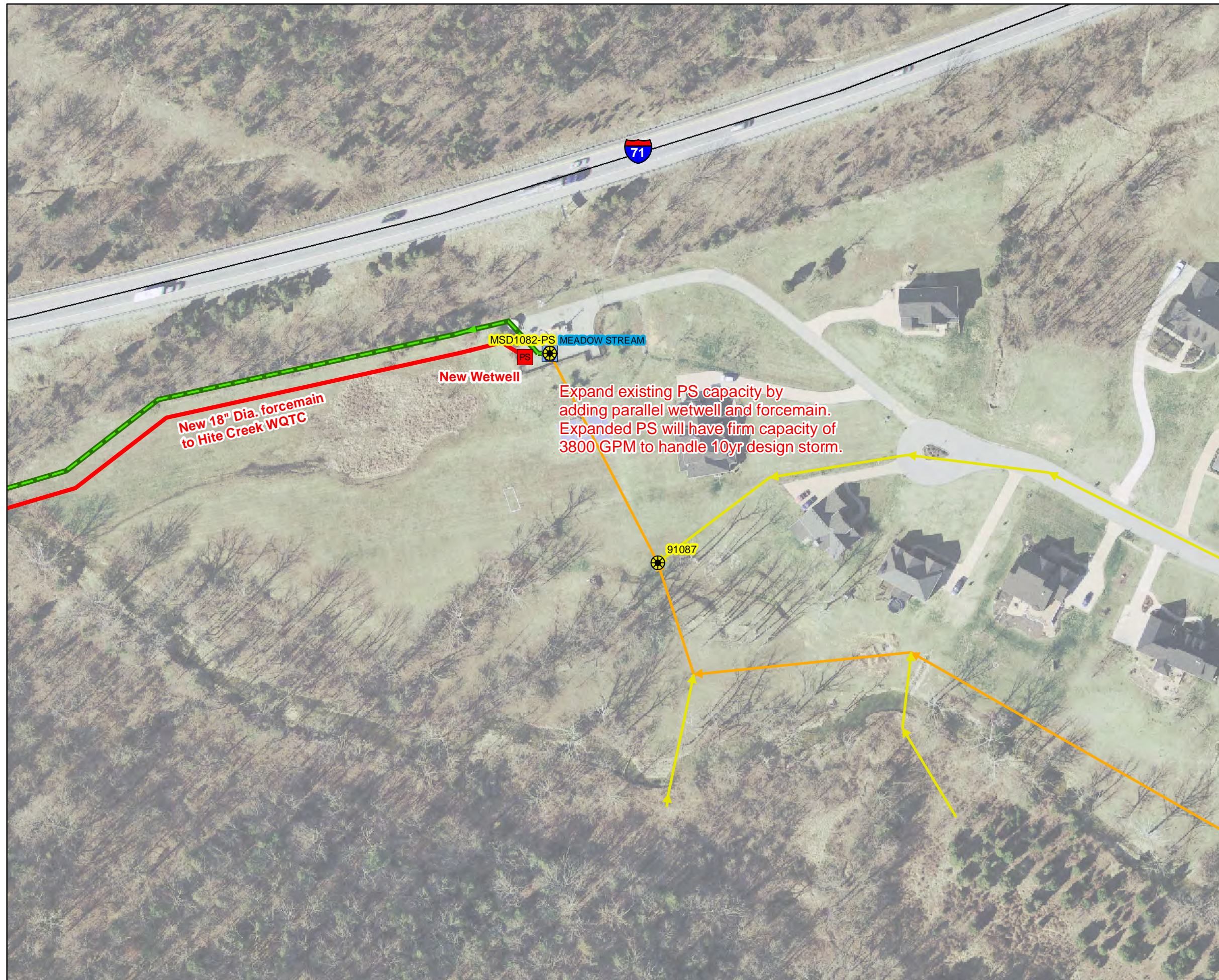


Aerial Date: 2009

Map Revision: April 9, 2012



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New Wetwell

Expand existing PS capacity by adding parallel wetwell and forcemain. Expanded PS will have firm capacity of 3800 GPM to handle 10yr design storm.

New 18" Dia. forcemain to Hite Creek WQTC

MSD1082-PS MEADOW STREAM

91087



**Floyd's Fork  
Area**

<b>Project Name</b>	Ashburton PS Improvements & Diversion
<b>Project Number</b>	S_FF_FF_NB03_M_01_C_A
<b>Modeled Area</b>	Floyds Fork
<b>Branch or SSO ID</b>	NB03
<b>Project Type</b>	Upgrade Force Main & Pipes
<b>Receiving Stream</b>	Floyds Fork
<b>Project Description</b>	This alternative includes diverting flow from Ashburton PS by upgrading 370 LF of FM (from 2" to 6") and adding 115 LF of 8" gravity sewer. It also eliminates the overflow at Olde Copper Ct PS.
<b>Reason for Overflow</b>	Pump station capacity
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$118,000
<b>Weighted Benefit/Cost Ratio</b>	161.00

Asset ID	SSO Start Date	Volume (Gal)
MSD0165-PS	1/2/2004	6000
MSD0165-PS	1/4/2004	1000
MSD0165-PS	11/12/2003	500
MSD0165-PS	11/18/2003	200
MSD0165-PS	11/27/2003	5000
MSD0165-PS	12/10/2003	3000
MSD0165-PS	12/16/2000	0
MSD0165-PS	12/17/2001	200
MSD0165-PS	12/19/2002	6600
MSD0165-PS	12/29/2003	300
MSD0165-PS	12/30/2002	1800
MSD0165-PS	12/31/2002	6000
MSD0165-PS	3/20/2002	800
MSD0165-PS	4/17/2003	1000
MSD0165-PS	4/17/2003	500
MSD0165-PS	4/25/2003	2000
MSD0165-PS	5/13/2002	8000
MSD0165-PS	5/13/2012	3650
MSD0165-PS	5/5/2003	3000
MSD0165-PS	9/2/2003	8000
MSD0165-PS	9/22/2006	4000
MSD0165-PS	9/27/2002	3000
















# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Floyds Fork Sewershed

Ashburton PS Improvement & Diversion

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  Proposed Pipe Solution
-  WQTC
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

*Upsize 370 LF of FM pipe from 2" to 6" and construct 115 LF of 8" pipe to divert flow from Ashburton PS.*

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

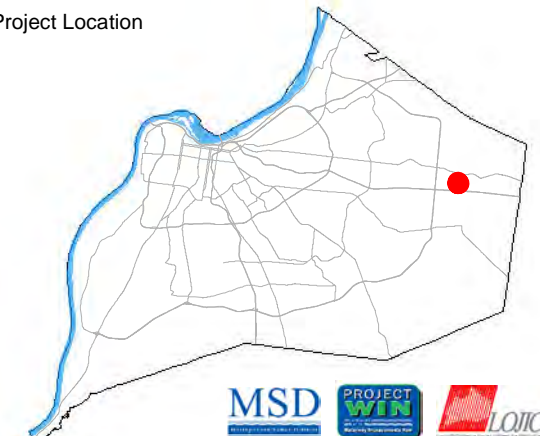
1 inch = 100 feet



Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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**Project Name**    [Eden Care PS SSO Investigation](#)

**Project Number**    [S\\_FF\\_FF\\_NB02\\_S\\_13\\_C](#)

**Modeled Area**                      Floyds Fork

**Branch or SSO ID**                      NB02

**Project Type**                              Inline Storage

**Receiving Stream**                      Floyds Fork

**Project Description**                      The overflow at Eden Care PS had only been documented to overflow once. The overflow location was monitored for three years and no additional overflows were witnessed. As such, no further action for overflow mitigation will be undertaken.

**Reason for Overflow**                      Pump station capacity

**Design Parameters**                      Project Eliminated.

**Project Constraints**                      Project Eliminated

**Estimated Capital Cost**                      Project Eliminated

**Weighted Benefit/Cost Ratio**                      Project Eliminated




















<b>Asset ID</b>	<b>SSO Start Date</b>	<b>Volume (Gal)</b>
MSD1105-PS	3/18/2006	200



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Floyds Fork Sewershed  
 Solution ID # S\_FF\_FF\_NB02\_S\_13\_C  
 Eden Care PS SSO Investigation

**Preliminary - For Budget Development Only**

**Legend**

-  Documented SSO
-  Suspected SSO
-  Haul Operation
-  Proposed Pump Station Solution
-  Pump Station
-  WWTP
-  Proposed Pipe Solution
-  Force Main
-  Collector < 12"
-  Interceptor => 12"
-  Combined Sewer Pipe
-  Proposed Off-line Storage
-  Road
-  Streams
-  Floodway
-  Small WWTP Service Area
-  Large WWTP Service Area
-  CSO Area
-  Metro Parks

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

1 inch = 100 feet  
 Scalable when printed on 11" X 17" paper



Some boundaries are uniquely symbolized within the map.

Map Revision  
 May 07, 2009

Aerial Date: 2006



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**Project Name**      Woodland Hills PS Diversion

**Project Number**    S\_FF\_FF\_NB01\_S\_01\_C\_A

**Modeled Area**                Floyds Fork

**Branch or SSO ID**            NB01

**Project Type**                 Pipe Upgrades

**Receiving Stream**            Pope Lick

**Project Description**        This alternative consists of replacing the existing overflow and automated gate (to the Woodland Hills PS) with a double barrel overflow that consists of 30 LF for two 12" diameter pipes. The upstream invert of these pipes needs to be 2 inches above the upstream invert of the exiting gravity pipe in MH 82058. This new invert elevation will allow dry weather flow to gravity drain down the interceptor, but anything greater than DWF will be diverted to the PS via the overflow pipes thus reducing the surcharge further down the gravity line. 15 LF of open cut sewer required.

**Reason for Overflow**        Hydraulic Bottleneck

**Design Parameters**         This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**         Capacity of other system

**Estimated Capital Cost**     \$20,000

**Weighted Benefit/Cost Ratio** 92.26

Asset ID	SSO Start Date	Volume (Gal)
33003	10/6/2013	5250
33003	12/5/2011	20300
33003	3/9/2011	20000
33003	4/12/2011	7650
33003	4/23/2011	12825
33003	4/23/2011	2250
33003	4/27/2011	15000
33003	5/3/2011	7800
















**Integrated Overflow Abatement Plan**

**Vol. 3 - Sanitary Sewer Discharge Plan**


Floyds Fork Sewershed

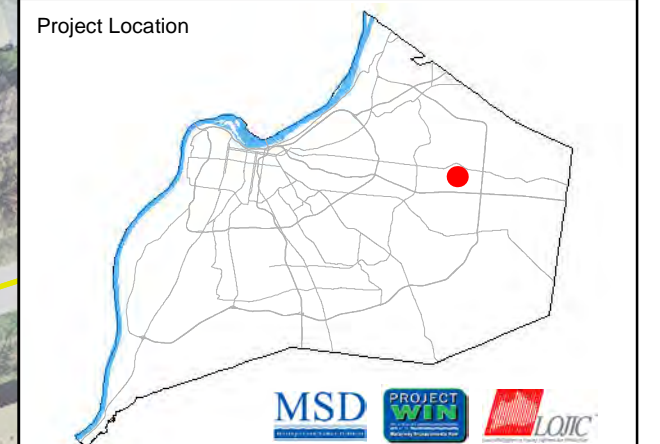
Woodland Hills PS Diversion

Preliminary - For Budget Development Only

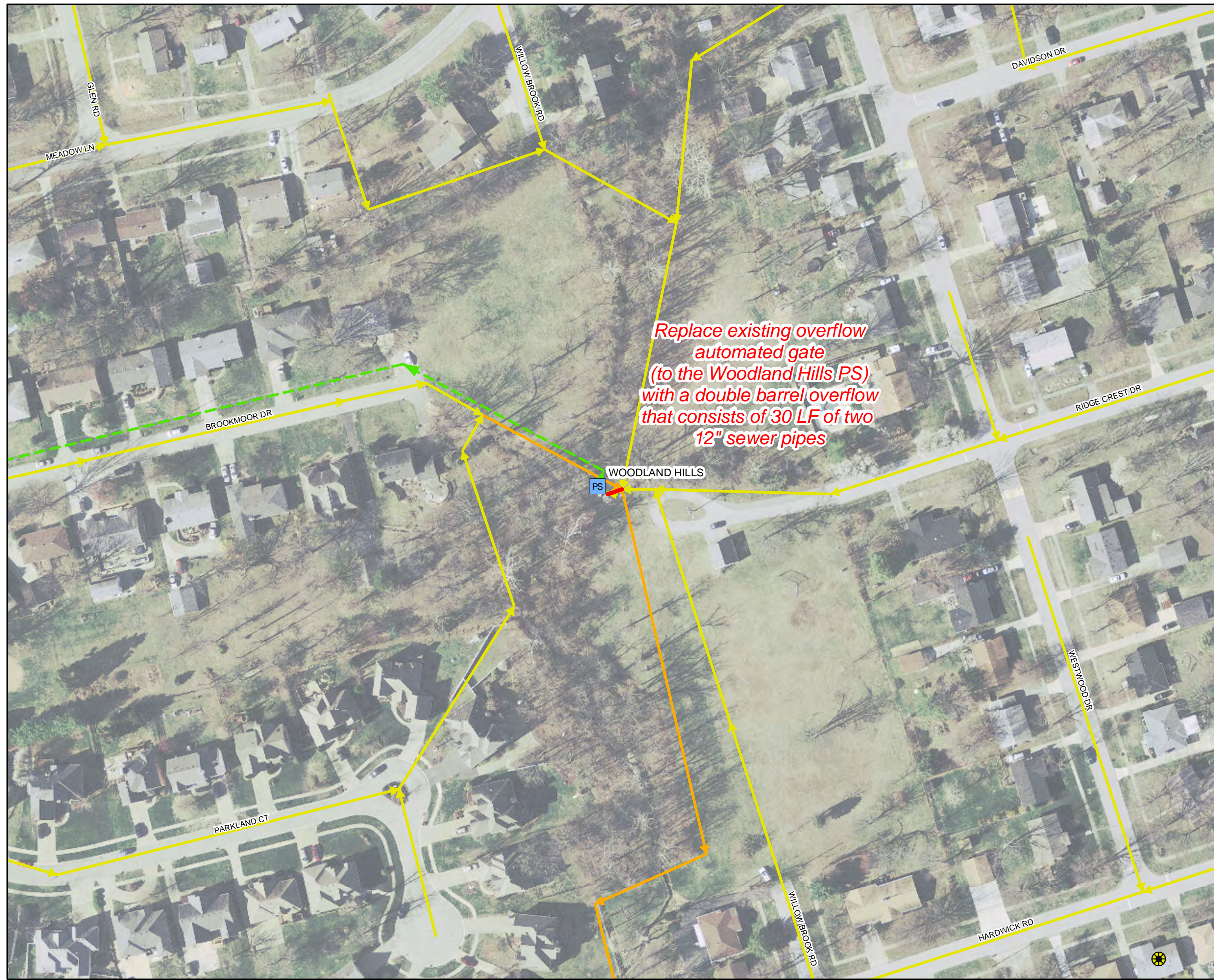
-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

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1 inch = 100 feet		Aerial Date: 2009	Map Revision: April 9, 2012
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**Project Name** Chenoweth Hills WQTC Elimination & PS Improvements

**Project Number** S\_JT\_JT\_NB01A\_M\_03\_C

**Modeled Area** Jeffersontown

**Branch or SSO ID** NB01A

**Project Type** Pump Station & Force Main Upgrades

**Receiving Stream** Chenoweth Run

**Project Description** This alternative includes upgrading pumps at Chenoweth Run PS to pump 2.7 MGD and upsizing the entire 8,030 LF of force main to 12". Chenoweth Hills WQTC will be eliminated. Pumps at Chippewa PS upgraded to 0.15 MGD. Install 1,995 LF of new 15" sewer and replace 600 LF of 8" with 18" sewer pipe for Chenoweth Hills WQTC diversion.

**Reason for Overflow** System capacity, siphon, and WQTC

**Design Parameters** This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints** N/A

**Estimated Capital Cost** \$3,140,000

**Weighted Benefit/Cost Ratio** 20.05

Asset ID	SSO Start Date	Volume (Gal)
MSD0263	1/13/2013	26700
MSD0263	1/13/2013	45000
92061	1/13/2013	1300
MSD0263	1/13/2013	600625
MSD0263A-PS	10/23/2007	20000
MSD0263	10/6/2013	596
MSD0263	11/25/2010	77800
64096	11/26/2010	2600
MSD0263	12/1/2008	35333
64096	12/24/2008	6575
92061	12/5/2011	680
MSD0263	12/5/2011	1200
MSD0263	12/5/2011	12000
MSD0263	12/8/2009	67535
MSD0263	2/11/2009	8143
92061	2/15/2001	500
92061	2/25/2011	45
64096	3/19/2008	250
MSD0196-PS	3/19/2008	55350
64096	3/9/2011	31250
MSD1043-PS	3/9/2011	4500
MSD0196-PS	4/12/2011	5
92061	4/12/2011	20300
64096	4/23/2011	182550
64096	4/27/2011	137000
MSD0263A-PS	4/4/2008	306000
MSD0196-PS	4/4/2008	81000

**Project Name** Chenoweth Hills WQTC Elimination & PS Improvements

**Project Number** S\_JT\_JT\_NB01A\_M\_03\_C

MSD0263	5/1/2010	41944
92061	5/13/2012	16750
92061	5/16/2008	5450
92061	5/2/2010	90750
MSD0263	5/2/2010	97700
MSD0263	5/2/2010	9770
64096	5/3/2011	235000
MSD0263	5/8/2009	21454
64096	6/23/2011	70000
64096	7/29/2009	37500
92061	7/4/2008	6000
92061	8/30/2005	300
MSD1043-PS	9/23/2006	5000
64096	9/25/2006	0
MSD0263	9/27/2002	5000



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Jeffersontown Sewershed**  
**Chenoweth Hills WQTC Elimination, Chenoweth Run and Chippewa PS Improvements**

Preliminary - For Budget Development Only

- Documented SSO
- Suspected SSO
- Haulop Locations
- Pump Stations
- Proposed Pipe Solution
- WQTC
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

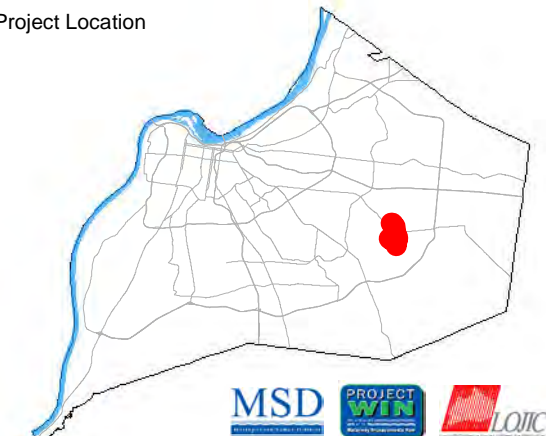
1 inch = 800 feet



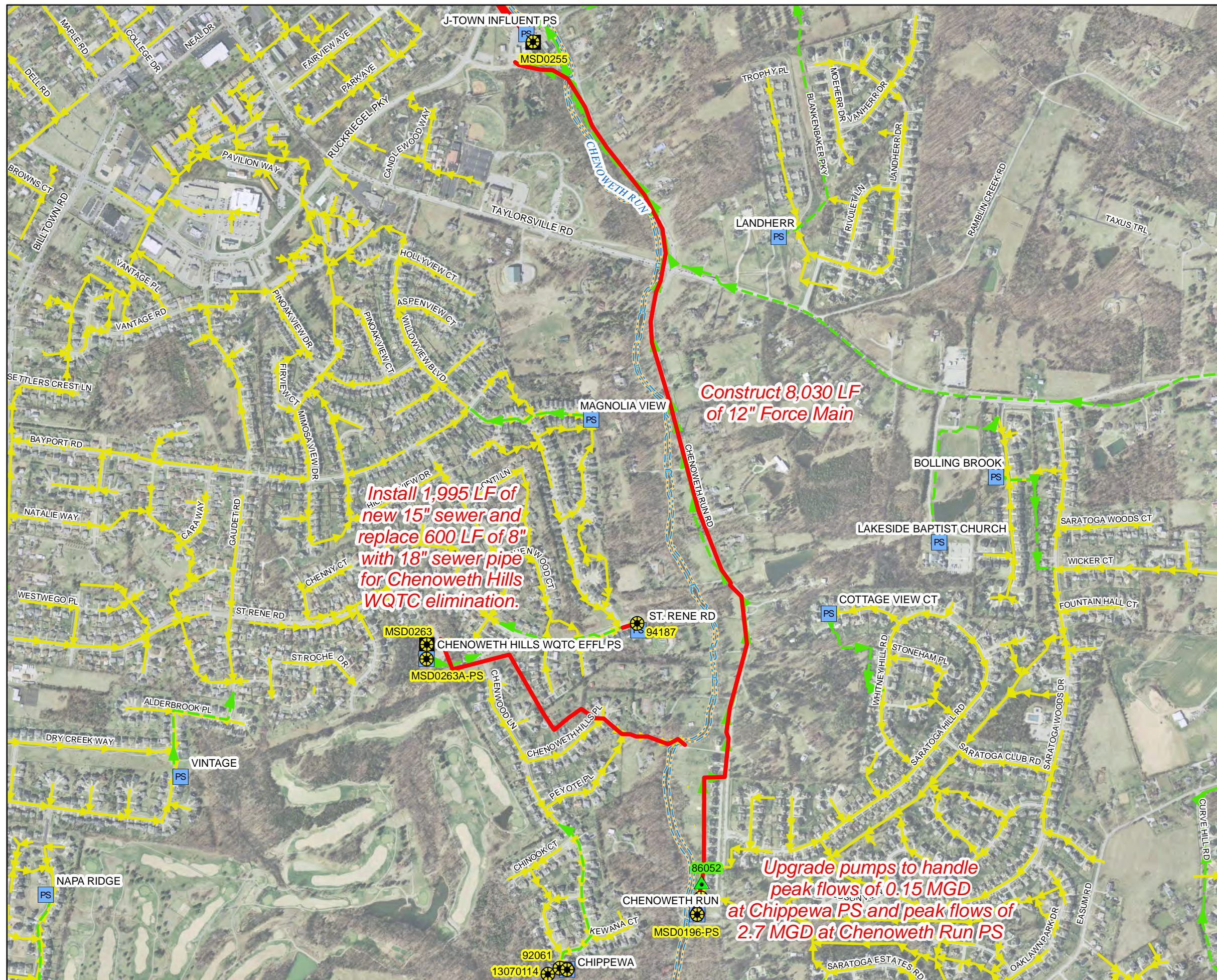
Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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*Construct 8,030 LF of 12" Force Main*

*Install 1,995 LF of new 15" sewer and replace 600 LF of 8" with 18" sewer pipe for Chenoweth Hills WQTC elimination.*

*Upgrade pumps to handle peak flows of 0.15 MGD at Chippewa PS and peak flows of 2.7 MGD at Chenoweth Run PS*



<b>Project Name</b>	Dell Rd and Charlane Pkwy Interceptor Improvements
<b>Project Number</b>	S_JT_JT_NB02_M_01_C
<b>Modeled Area</b>	Jeffersontown
<b>Branch or SSO ID</b>	NB02
<b>Project Type</b>	Pipe Upgrades
<b>Receiving Stream</b>	Chenoweth Run
<b>Project Description</b>	Upsize interceptor downstream of Charlane and Dell Road overflows with 3,788 LF of (10"-21") sewer.
<b>Reason for Overflow</b>	System capacity
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$917,000
<b>Weighted Benefit/Cost Ratio</b>	31.34

Asset ID	SSO Start Date	Volume (Gal)
28336	1/13/2013	57000
28340	1/13/2013	15600
28414	1/13/2013	45000
28340	1/26/2012	31500
28415	1/26/2012	6000
28336	1/26/2012	12000
28250	1/3/2005	165600
28340	1/3/2005	165600
28415	1/3/2005	165600
28414	1/3/2005	165600
28336	10/23/2007	351360
28340	10/23/2007	12960
28250	10/23/2007	4320
28249	10/24/2007	2160
28340	10/5/2013	67000
28415	10/5/2013	81000
28250	10/5/2013	52000
28336	10/6/2013	89000
28416	10/6/2013	29000
28417	10/6/2013	33000
28336	11/17/2013	30500
28250	11/17/2013	19500
28340	11/17/2013	75000
28414	11/22/2011	4100
28336	11/22/2011	6100
28336	11/28/2011	33000
28414	11/28/2011	3000
28415	12/15/2007	360
28250	12/15/2007	4185



**Project Name** Dell Rd and Charlane Pkwy Interceptor Improvements

**Project Number** S\_JT\_JT\_NB02\_M\_01\_C

28249	12/15/2007	4320
28340	12/15/2007	12960
28336	12/15/2007	351360
28415	12/19/2002	132000
28414	12/24/2008	150
28336	12/5/2011	64000
28340	12/5/2011	30000
28416	12/5/2011	36000
28249	12/5/2011	21500
28417	12/5/2011	22500
28415	12/5/2011	48000
28416	2/25/2011	170
28414	2/25/2011	150
28340	3/11/2013	1450
28336	3/11/2013	950
28340	3/12/2006	52900
28249	3/12/2006	52900
28414	3/12/2006	50600
28336	3/12/2006	52900
28415	3/12/2006	59400
28250	3/12/2006	52900
28336	3/18/2013	10500
28340	3/18/2013	18000
28414	3/19/2008	12960
28249	3/19/2008	12960
28415	3/19/2008	351360
28336	3/19/2008	351360
28250	3/19/2008	12960
28340	3/19/2008	12960
28413	3/20/2002	25000
28249	3/4/2008	24000
28415	3/4/2008	78000
28336	3/4/2008	84240
28340	3/4/2008	39000
28250	3/4/2008	39000
28414	3/4/2008	42120
28415	3/9/2011	14000
28415	4/12/2011	227000
28416	4/12/2011	215000
28417	4/12/2011	117000
28336	4/12/2011	8500
28415	4/23/2011	232000
28416	4/23/2011	197000

**Project Name** Dell Rd and Charlane Pkwy Interceptor Improvements

**Project Number** S\_JT\_JT\_NB02\_M\_01\_C

28249	4/23/2011	113500
28417	4/23/2011	126500
28414	4/27/2011	97500
28415	4/27/2011	77250
28416	4/27/2011	84500
28250	4/27/2011	94500
28249	4/27/2011	126000
28250	4/4/2008	17442
28417	4/4/2008	15000
28416	4/4/2008	78000
28249	4/4/2008	17280
28414	4/4/2008	3780
28340	4/4/2008	17280
28415	4/4/2008	474500
28336	4/4/2008	468480
28336	5/10/2013	18000
28340	5/10/2013	16500
28336	5/13/2012	19500
28340	5/13/2012	9750
28415	5/15/2008	2700
28417	5/2/2010	9500
28250	5/2/2010	17742
28416	5/2/2010	10000
28340	5/2/2010	21000
28415	5/2/2010	3100
28249	5/2/2010	27000
28336	5/2/2010	49000
28414	5/3/2011	67500
28415	6/23/2011	56000
28336	6/26/2013	36000
28340	6/26/2013	72000
28415	6/26/2013	40500
28415	7/14/2006	19440
28250	8/30/2005	13800
28336	8/30/2005	13800
28340	8/30/2005	13800
28340	8/4/2009	1500
28250	8/4/2009	11500
28336	9/21/2013	24500
28250	9/21/2013	3000
28340	9/23/2006	3780
28336	9/23/2006	307440
28249	9/23/2006	3780

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**Project Name** Dell Rd and Charlane Pkwy Interceptor Improvements

**Project Number** S\_JT\_JT\_NB02\_M\_01\_C

28250














9/23/2006

3780



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Jeffersontown Sewershed**  
**Dell Rd and Charlane Pkwy Interceptor Improvements**

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

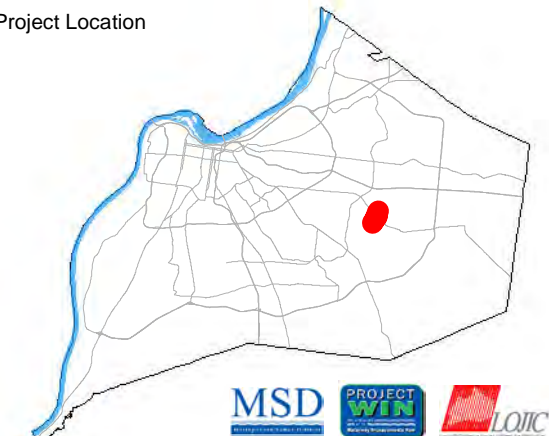
1 inch = 400 feet



Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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*Upsize 3,788 LF of sewer pipe  
(ranging from 10" - 21")*



<b>Project Name</b>	Jeffersontown WQTC Elimination
<b>Project Number</b>	S_JT_JT_NB01_M_01_C_A
<b>Modeled Area</b>	Jeffersontown
<b>Branch or SSO ID</b>	NB01
<b>Project Type</b>	Off-line Storage & Pipe Upgrades
<b>Receiving Stream</b>	Chenoweth Run
<b>Project Description</b>	Upsize the interceptor (6,200 LF) from Grassland to the WQTC. Storage basin (5.7 MG) at the WQTC site and a new PS with capacity of 10 MGD. 32,100 LF of 24" force main constructed to convey flows to the Hikes Lane Interceptor (HLI).
<b>Reason for Overflow</b>	System capacity, siphon, and WQTC
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$23,737,000
<b>Weighted Benefit/Cost Ratio</b>	5.23

Asset ID	SSO Start Date	Volume (Gal)
MSD0255	1/1/2011	839840
MSD0255	1/11/2014	1684349
MSD0255	1/13/2013	7177246
28551	1/13/2013	160000
31733	1/13/2013	42000
28395	1/13/2013	90000
28173	1/13/2013	72000
64505	1/13/2013	24000
MSD0255	1/14/2007	600
MSD0255	1/21/2010	2208502
MSD0255	1/24/2010	855454
28173	1/26/2012	48000
MSD0255	1/26/2012	4044173
28551	1/26/2012	24000
64505	1/26/2012	7500
MSD0255	1/28/2009	547071
28391	1/3/2005	418000
MSD0255	1/30/2013	1712000
28551	1/30/2013	100
MSD0255	10/1/2012	62687
28391	10/19/2004	91000
MSD0255	10/2/2009	34812
IS028-SI	10/23/2007	500
MSD0255	10/27/2009	47448
MSD0255	10/30/2013	37242
MSD0255	10/31/2009	966634
MSD0255	10/31/2013	434117
64505	10/5/2013	77000

Project Name	Jeffersontown WQTC Elimination	
Project Number	S_JT_JT_NB01_M_01_C_A	
28173	10/5/2013	106000
28551	10/5/2013	74000
28395	10/5/2013	101000
MSD0255	10/5/2013	6345803
31733	10/6/2013	105000
MSD0255	10/9/2009	1650306
28173	11/1/2013	2100
MSD0255	11/15/2011	177661
MSD0255	11/16/2011	385858
28173	11/17/2013	60000
MSD0255	11/17/2013	1825854
64505	11/17/2013	45000
28551	11/17/2013	41000
28173	11/22/2011	6500
MSD0255	11/22/2011	1459476
28551	11/22/2011	12500
28173	11/25/2010	2550
MSD0255	11/25/2010	2838171
MSD0255	11/27/2011	8900996
28551	11/28/2011	65000
28173	11/28/2011	94500
28392	11/29/2001	2000000
MSD0255	11/30/2010	1067355
28551	12/10/2012	52500
MSD0255	12/13/2007	100000
28395	12/15/2007	144000
MSD0255	12/15/2007	250
MSD0255	12/21/2013	2381265
MSD0255	12/22/2011	372989
28551	12/22/2013	55000
28173	12/22/2013	29500
MSD0255	12/24/2008	3442891
MSD0255	12/26/2012	592914
MSD0255	12/27/2011	683551
28395	12/5/2011	33000
MSD0255	12/5/2011	6060240
31733	12/5/2011	66000
28551	12/5/2011	157000
64505	12/5/2011	31500
28173	12/5/2011	142000
64505	12/7/2012	64500
MSD0255	12/7/2012	3920379
28173	12/7/2012	64500

<b>Project Name</b>	<b>Jeffersontown WQTC Elimination</b>	
<b>Project Number</b>	<b>S_JT_JT_NB01_M_01_C_A</b>	
MSD0255	12/8/2009	378642
MSD0255	2/1/2011	132886
MSD0255	2/10/2009	440
MSD0255	2/11/2009	51664
MSD0255	2/12/2008	2894355
MSD0255	2/22/2008	1056000
64505	2/24/2011	12200
28173	2/24/2011	11500
MSD0255	2/24/2011	5206733
28395	2/25/2011	7200
28173	2/28/2011	47500
MSD0255	2/28/2011	3061868
MSD0255	2/5/2010	516697
MSD0255	3/10/2008	101450
28173	3/11/2013	2300
28551	3/11/2013	1500
MSD0255	3/11/2013	2821225
MSD0255	3/16/2012	1058730
MSD0255	3/17/2012	238197
MSD0255	3/17/2013	4500
MSD0255	3/17/2013	5348765
28551	3/17/2013	21500
MSD0255	3/17/2013	10000
MSD0255	3/18/2008	10457592
28173	3/18/2013	31500
28395	3/19/2008	322080
28173	3/19/2008	1350
IS028-SI	3/19/2008	240
IS028-SI	3/20/2002	25000
MSD0255	3/27/2008	4859194
28551	3/3/2011	400
28395	3/4/2008	52812
MSD0255	3/4/2008	10733700
28173	3/4/2008	2340
IS028-SI	3/4/2008	480
MSD0255	3/5/2011	36132
MSD0255	3/8/2012	559144
MSD0255	3/9/2011	9733803
28173	3/9/2011	246000
28551	3/9/2011	78500
31733	3/9/2011	46000
28395	3/9/2011	115000
MSD0255	4/1/2008	29177

Project Name	Jeffersontown WQTC Elimination	
Project Number	S_JT_JT_NB01_M_01_C_A	
28551	4/1/2012	7500
64505	4/1/2012	9000
28173	4/1/2012	31500
MSD0255	4/1/2012	1345076
28551	4/11/2011	456500
28173	4/11/2011	1255250
28395	4/11/2011	262250
MSD0255	4/11/2011	10253354
31733	4/12/2011	126500
64505	4/12/2011	356000
MSD0255	4/19/2009	679890
MSD0255	4/19/2013	958564
MSD0255	4/20/2009	57951
MSD0255	4/23/2011	16950522
28395	4/23/2011	124000
31733	4/23/2011	145000
28173	4/23/2011	257500
28551	4/23/2011	412500
MSD0255	4/24/2013	10794
MSD0255	4/3/2008	12277926
MSD0255	4/3/2009	219479
28173	4/4/2008	180000
IS028-SI	4/4/2008	2100
28395	4/4/2008	198000
MSD0255	4/4/2011	251808
MSD0255	5/1/2010	1000
MSD0255	5/1/2010	7661762
MSD0255	5/1/2011	87413
64505	5/10/2013	16200
28395	5/10/2013	32000
28173	5/10/2013	44000
31733	5/10/2013	19500
MSD0255	5/10/2013	3507926
28551	5/10/2013	64000
64505	5/13/2012	10500
28173	5/13/2012	36000
MSD0255	5/13/2012	4152668
28551	5/13/2012	7500
MSD0255	5/14/2008	20000
MSD0255	5/14/2008	28943
28173	5/15/2008	420
MSD0255	5/15/2008	5066000
64505	5/2/2010	64000



Project Name	Jeffersontown WQTC Elimination	
Project Number	S_JT_JT_NB01_M_01_C_A	
28173	5/2/2010	24000
28395	5/2/2010	49000
28391	5/2/2010	19000
28173	5/2/2011	207000
28551	5/2/2011	247000
MSD0255	5/2/2011	7136760
31733	5/2/2011	94500
MSD0255	5/21/2010	253859
28173	5/21/2010	50
MSD0255	5/23/2011	243550
28173	5/26/2011	4500
MSD0255	5/26/2011	3247272
MSD0255	5/29/2012	839349
28551	5/29/2012	27000
28173	5/29/2012	16910
64505	5/29/2012	47000
MSD0255	5/3/2008	1660000
28395	5/3/2011	41000
28391	5/30/2004	652000
MSD0255	5/31/2012	899028
MSD0255	5/5/2013	775331
28173	5/5/2013	50
MSD0255	5/8/2008	398086
MSD0255	5/8/2009	1934989
MSD0255	6/10/2009	387
MSD0255	6/11/2009	3289
MSD0255	6/17/2013	203626
MSD0255	6/18/2009	377559
28173	6/18/2009	375
MSD0255	6/18/2009	1048935
MSD0255	6/22/2011	3181344
31733	6/23/2011	67500
28395	6/26/2013	27000
28173	6/26/2013	72000
28551	6/26/2013	144000
MSD0255	6/26/2013	2520260
64505	6/26/2013	54000
MSD0255	6/9/2010	786248
MSD0255	7/22/2009	402
MSD0255	7/29/2009	548114
MSD0255	7/4/2008	500
MSD0255	7/4/2008	707000
MSD0255	7/6/2013	1318047

Project Name	Jeffersontown WQTC Elimination	
Project Number	S_JT_JT_NB01_M_01_C_A	
MSD0255	8/13/2013	82844
MSD0255	8/14/2010	275497
MSD0255	8/31/2013	227989
MSD0255	8/4/2009	1932553
MSD0255	9/20/2009	312827
64505	9/21/2013	9000
28173	9/21/2013	1000
MSD0255	9/21/2013	1778728
28551	9/21/2013	31000
MSD0255	9/22/2006	0
28392	9/23/2006	2160000
MSD0255	9/23/2006	0
28395	9/23/2006	540000
MSD0255	9/26/2009	254916
MSD0255	9/26/2011	349988
MSD0255	9/27/2009	100
MSD0255	9/8/2012	2000
MSD0255	9/8/2012	1500
MSD0255	9/8/2012	49387



**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

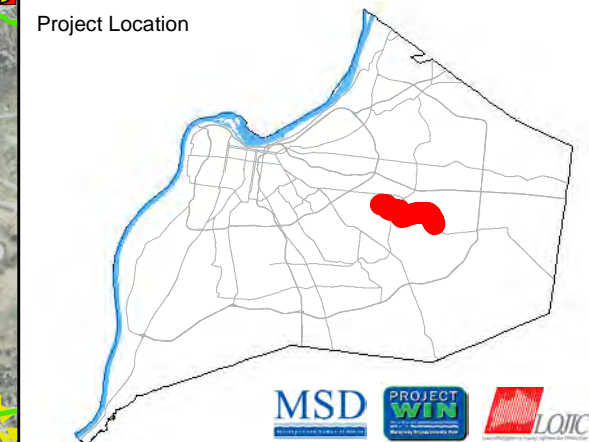
**Jeffersontown Sewershed  
Jeffersontown WQTC Elimination**

Preliminary - For Budget Development Only

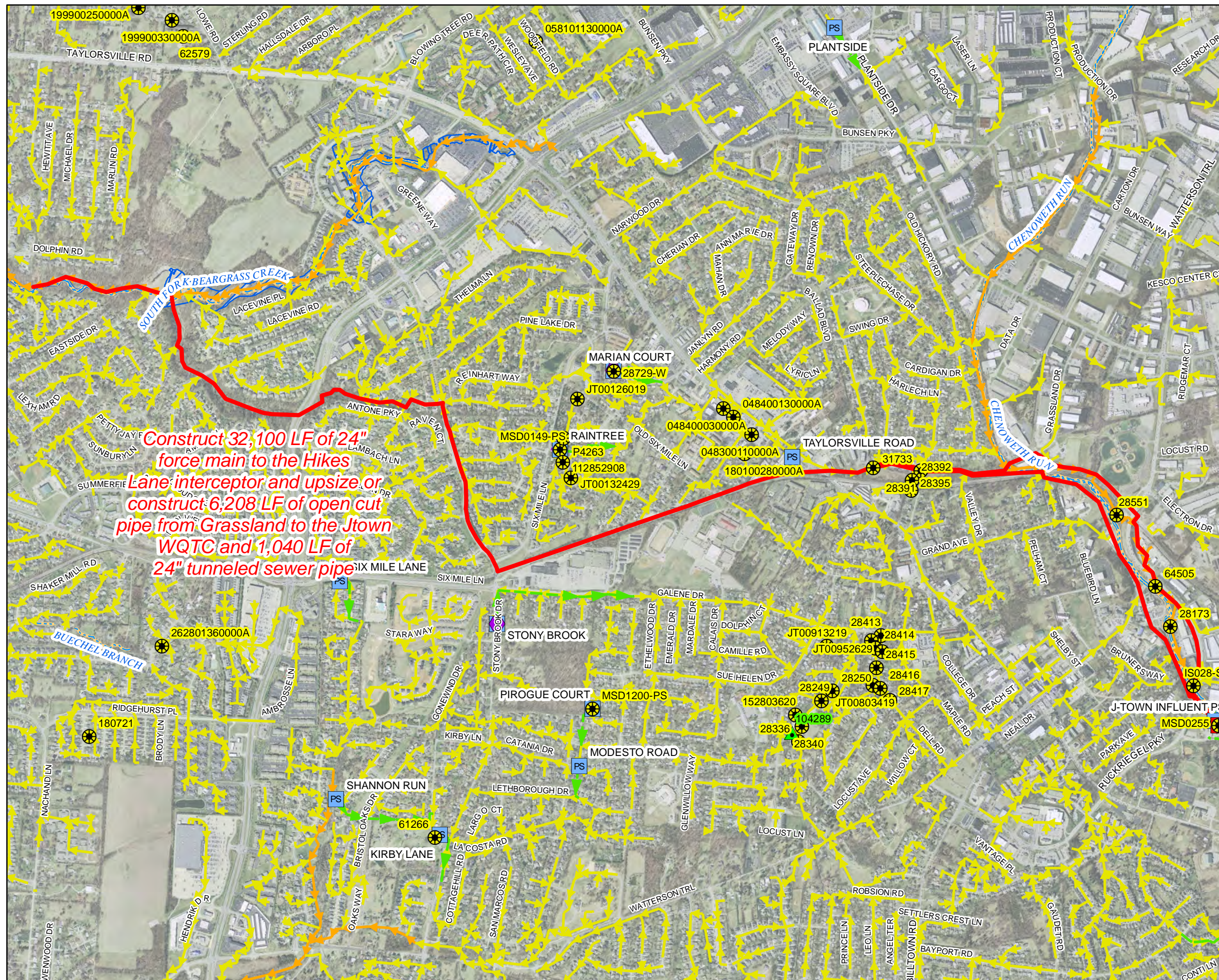
- Documented SSO
- Suspected SSO
- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- WQTC
- Proposed Pipe Solution
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,402 feet       Aerial Date: 2009    Map Revision: April 9, 2012



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**Project Name**     **Monticello PS Elimination**

**Project Number**   **S\_JT\_JT\_NB04\_M\_01\_A**

**Modeled Area**             Jeffersontown

**Branch or SSO ID**         NB04

**Project Type**             Diversion & PS Elimination

**Receiving Stream**         Chenoweth Run and Fern Creek

**Project Description**       This alternative includes eliminating Monticello PS by diverting to West County with 625 LF of 8" sewer.

**Reason for Overflow**       Pump station capacity

**Design Parameters**        This solution is based on a 2.60 inch cloudburst rain event.

**Project Constraints**        N/A

**Estimated Capital Cost**     \$207,000

**Weighted Benefit/Cost Ratio**   65.85

<b>Asset ID</b>	<b>SSO Start Date</b>	<b>Volume (Gal)</b>
MSD0151-PS	3/19/2008	10000
















**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**


Jeffersontown Sewershed

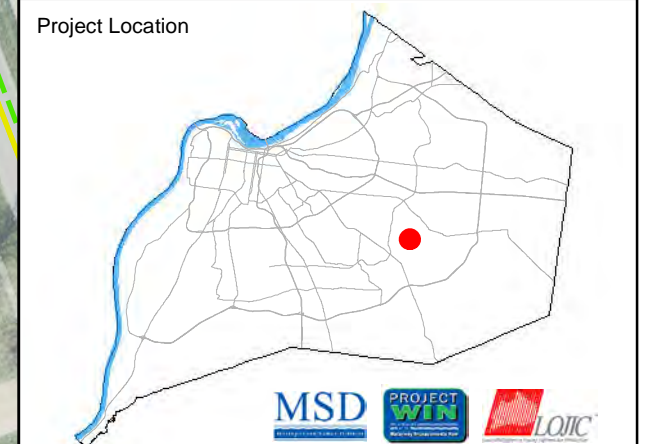
Monticello PS Elimination

Preliminary - For Budget Development Only

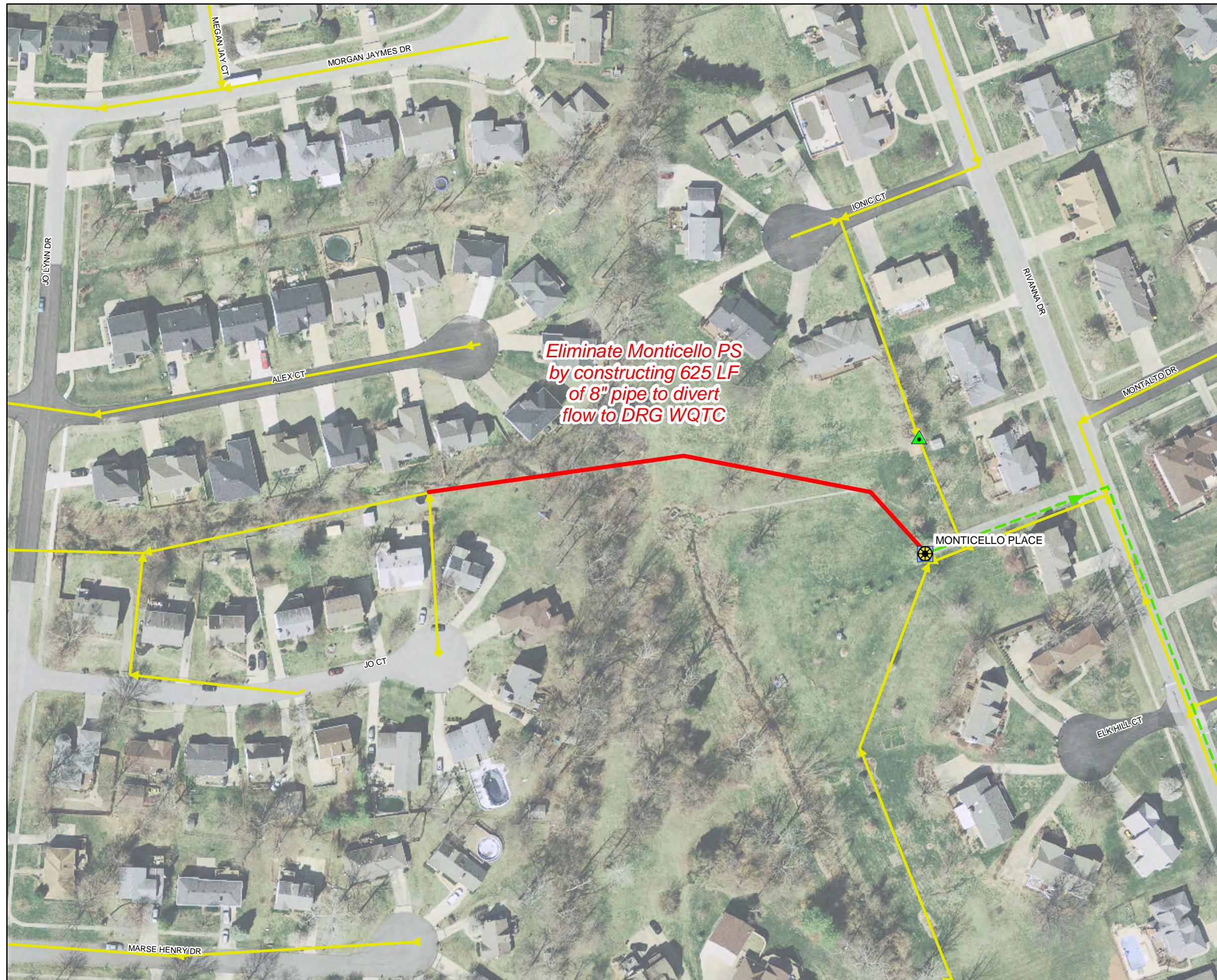
-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

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1 inch = 100 feet  Aerial Date: 2009 Map Revision: April 9, 2012



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**Project Name**     **Raintree and Marian Ct 1 - PS Elimination**

**Project Number**     **S\_JT\_JT\_NB03\_M\_01\_C**

**Modeled Area**                     Jeffersontown

**Branch or SSO ID**                     NB03

**Project Type**                     Pipe Upgrades

**Receiving Stream**                     Avoca Creek

**Project Description**                     This alternative includes installing 455 LF of 8" open cut sewer from Marion PS and 400 LF of 8" from Raintree PS to divert flows to the SED.

**Reason for Overflow**                     System & pump station capacity

**Design Parameters**                     This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**                     N/A

**Estimated Capital Cost**                     \$260,000














**Weighted Benefit/Cost Ratio**                     72.76

<b>Asset ID</b>	<b>SSO Start Date</b>	<b>Volume (Gal)</b>
MSD0149-PS	4/27/2011	8905
MSD0149-PS	5/2/2011	385500



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Jeffersontown Sewershed**  
**Raintree & Marian Ct PS Elimination - 1**  
**PS Eliminations**

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

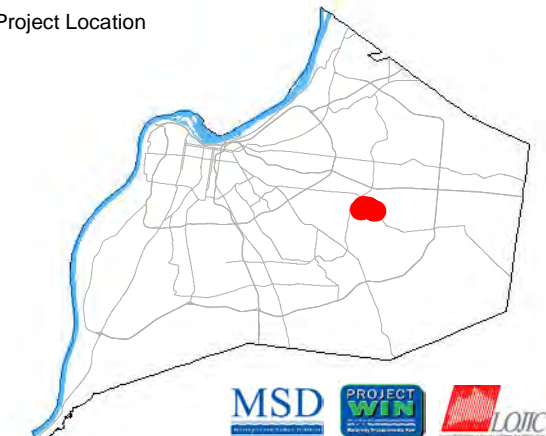
1 inch = 200 feet



Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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**Project Name**     Raintree and Marian Ct 2 - Pipe Upgrades

**Project Number**     S\_JT\_JT\_NB03\_M\_01\_C

**Modeled Area**                     Jeffersontown

**Branch or SSO ID**                 NB03

**Project Type**                         Pipe Upgrades

**Receiving Stream**                 Avoca Creek

**Project Description**                This alternative includes 2,675 LF of 15" conveyance upgrades from Marion PS and Raintree PS to divert flows to the SED.

**Reason for Overflow**               System & pump station capacity

**Design Parameters**                This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**                 N/A

**Estimated Capital Cost**             \$745,000














**Weighted Benefit/Cost Ratio**        72.76

Asset ID	SSO Start Date	Volume (Gal)
MSD0149-PS	4/27/2011	8905
MSD0149-PS	5/2/2011	385500




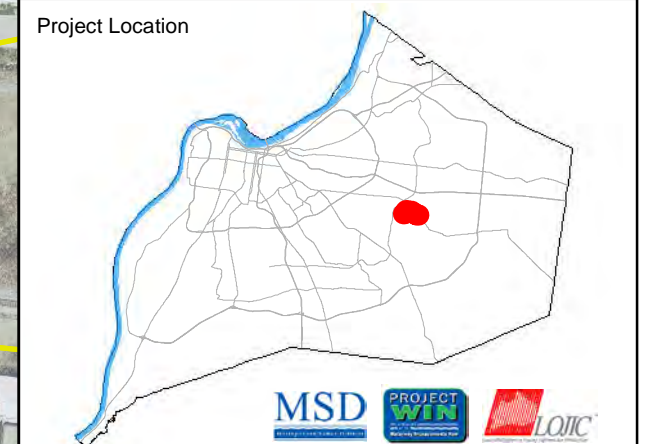
**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Jeffersontown Sewershed**  
**Raintree & Marian Ct PS Elimination - 2**  
**Pipe Upgrades**

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 200 feet		Aerial Date: 2009	Map Revision: April 9, 2012
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**Beargrass Creek  
Middle Fork Area**

---

1

<b>Project Name</b>	Anchor Estates PS Elimination 1 - Vannah PS Elimination
<b>Project Number</b>	S_MI_MF_NB06_M_01_A_A - 2
<b>Modeled Area</b>	Middle Fork Beargrass Creek
<b>Branch or SSO ID</b>	MF06
<b>Project Type</b>	Diversion
<b>Receiving Stream</b>	Middle Fork Beargrass Creek
<b>Project Description</b>	This alternative includes 350 LF of 8" pipe at Vannah PS to eliminate the pump station.
<b>Reason for Overflow</b>	Bypass Pipe at Vannah Way, Undersized Pumps at Anchor Estates #1 and #2.
<b>Design Parameters</b>	This solution is based on a 2.60 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$59,000
<b>Weighted Benefit/Cost Ratio</b>	31.14

Asset ID	SSO Start Date	Volume (Gal)
MSD0057-LS	1/1/2005	5000
00056-W	1/11/2014	25250
00056-W	1/13/2013	35650
0057-W	1/13/2013	59400
MSD0057-LS	1/2/2004	5000
MSD0057-LS	1/22/2006	1300
MSD0057-LS	1/24/2002	5000
MSD0057-LS	1/3/2005	90000
MSD0057-LS	1/30/2002	1500
MSD0057-LS	1/4/2005	3000
MSD0057-LS	1/5/2004	3000
MSD0057-LS	1/6/2005	14000
MSD0057-LS	10/11/2002	3000
MSD0057-LS	10/14/2001	800
MSD0057-LS	10/19/2004	5000
00056-W	10/6/2013	4020
0057-W	10/6/2013	2700
00056-W	11/10/2013	8750
MSD0057-LS	11/11/2004	5800
MSD0057-LS	11/19/2004	2000
MSD0057-LS	11/2/2004	10000
00056-W	11/22/2011	2750
MSD0057-LS	11/27/2001	200
MSD0057-LS	11/27/2003	2000
MSD0057-LS	11/28/2001	5000
MSD0057-LS	11/28/2003	6000
00056-W	11/28/2011	5840
MSD0057-LS	11/28/2011	9945
MSD0057-LS	11/29/2001	2500

**Project Name**     **Anchor Estates PS Elimination 1 - Vannah PS Elimination**

**Project Number**     **S\_MI\_MF\_NB06\_M\_01\_A\_A - 2**

MSD0057-LS	12/10/2003	2500
00056-W	12/15/2007	7200
MSD0057-LS	12/15/2007	128250
MSD0057-LS	12/16/2000	0
MSD0057-LS	12/16/2001	5000
MSD0057-LS	12/19/2002	19000
00056-W	12/22/2013	500
MSD0057-LS	12/30/2002	1400
MSD0057-LS	12/30/2004	10000
MSD0057-LS	12/31/2002	10000
00056-W	12/5/2011	37500
MSD0057-LS	12/8/2012	250
MSD0057-LS	2/15/2003	2000
00056-W	2/28/2011	10
MSD0057-LS	3/11/2013	25
MSD0057-LS	3/12/2006	700
00056-W	3/18/2013	14600
MSD0057-LS	3/18/2013	2530
MSD0057-LS	3/19/2002	1000
00056-W	3/19/2008	16500
MSD0057-LS	3/19/2008	57000
MSD0057-LS	3/26/2002	5000
MSD0057-LS	3/27/2008	97800
00056-W	3/27/2008	21825
MSD0057-LS	3/28/2005	12000
MSD0057-LS	3/4/2004	1500
MSD0057-LS	3/4/2004	3000
MSD0057-LS	3/4/2008	3000
00056-W	3/4/2008	500
00056-W	3/9/2011	53500
0057-W	3/9/2011	110175
MSD0057-LS	4/1/2006	50
00056-W	4/12/2011	45500
MSD0057-LS	4/17/2003	500
0057-W	4/23/2011	383625
MSD0057-LS	4/25/2003	2000
MSD0057-LS	4/30/2005	15000
00056-W	4/4/2008	25350
MSD0057-LS	4/4/2008	23850
0057-W	5/10/2013	23500
MSD0057-LS	5/11/2008	1000
00056-W	5/13/2012	12925
MSD0057-LS	5/17/2002	20000



**Project Name** Anchor Estates PS Elimination 1 - Vannah PS Elimination

**Project Number** S\_MI\_MF\_NB06\_M\_01\_A\_A - 2

MSD0057-LS	5/17/2003	8000
00056-W	5/2/2010	43500
00056-W	5/2/2011	375
MSD0057-LS	5/2/2011	25
MSD0057-LS	5/25/2004	5000
MSD0057-LS	5/27/2004	1200
MSD0057-LS	5/28/2004	10000
0057-W	5/3/2011	25
MSD0057-LS	5/5/2003	5000
MSD0057-LS	6/2/2006	800
00056-W	6/23/2011	6975
0057-W	6/23/2011	10
00056-W	6/26/2013	21500
0057-W	6/27/2013	5125
MSD0057-LS	7/17/2004	10000
MSD0057-LS	7/29/2009	250
00056-W	7/29/2009	1075
MSD0057-LS	8/30/2005	50
00056-W	8/4/2009	600
MSD0057-LS	9/2/2003	20000
MSD0057-LS	9/22/2006	3000
MSD0057-LS	9/27/2002	100000



**Integrated Overflow Abatement Plan**

**Vol. 3 - Sanitary Sewer Discharge Plan**

**Middle Fork Sewershed**

**Anchor Estates PS Elimination 1  
Vannah PS Elimination**

Preliminary - For Budget Development Only



- Documented SSO
- Suspected SSO
- Haulop Locations
- Pump Stations
- Proposed Pipe Solution
- WQTC
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 100 feet



Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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<b>Project Name</b>	Anchor Estates PS Elimination 2 - Anchor Estates #1 and #2 PS Elimination
<b>Project Number</b>	S_MI_MF_NB06_M_01_A_A - 1
<b>Modeled Area</b>	Middle Fork Beargrass Creek
<b>Branch or SSO ID</b>	MF06
<b>Project Type</b>	Diversion
<b>Receiving Stream</b>	Middle Fork Beargrass Creek
<b>Project Description</b>	This alternative includes 9440 LF of 8"-12" pipe at Anchor Estates #1 and #2 to eliminate both pump stations.
<b>Reason for Overflow</b>	Bypass Pipe at Vannah Way, Undersized Pumps at Anchor Estates #1 and #2.
<b>Design Parameters</b>	This solution is based on a 2.60 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$1,850,000
<b>Weighted Benefit/Cost Ratio</b>	31.14

Asset ID	SSO Start Date	Volume (Gal)
MSD0057-LS	1/1/2005	5000
00056-W	1/11/2014	25250
00056-W	1/13/2013	35650
MSD0057-LS	1/2/2004	5000
MSD0057-LS	1/22/2006	1300
MSD0057-LS	1/24/2002	5000
MSD0057-LS	1/3/2005	90000
MSD0057-LS	1/30/2002	1500
MSD0057-LS	1/4/2005	3000
MSD0057-LS	1/5/2004	3000
MSD0057-LS	1/6/2005	14000
MSD0057-LS	10/11/2002	3000
MSD0057-LS	10/14/2001	800
MSD0057-LS	10/19/2004	5000
00056-W	10/6/2013	4020
00056-W	11/10/2013	8750
MSD0057-LS	11/11/2004	5800
MSD0057-LS	11/19/2004	2000
MSD0057-LS	11/2/2004	10000
00056-W	11/22/2011	2750
MSD0057-LS	11/27/2001	200
MSD0057-LS	11/27/2003	2000
MSD0057-LS	11/28/2001	5000
MSD0057-LS	11/28/2003	6000
00056-W	11/28/2011	5840
MSD0057-LS	11/28/2011	9945
MSD0057-LS	11/29/2001	2500
MSD0057-LS	12/10/2003	2500
MSD0057-LS	12/15/2007	128250

**Project Name**    **Anchor Estates PS Elimination 2 - Anchor Estates #1 and #2 PS Elimination**

**Project Number**    **S\_MI\_MF\_NB06\_M\_01\_A\_A - 1**

00056-W	12/15/2007	7200
MSD0057-LS	12/16/2000	0
MSD0057-LS	12/16/2001	5000
MSD0057-LS	12/19/2002	19000
00056-W	12/22/2013	500
MSD0057-LS	12/30/2002	1400
MSD0057-LS	12/30/2004	10000
MSD0057-LS	12/31/2002	10000
00056-W	12/5/2011	37500
MSD0057-LS	12/8/2012	250
MSD0057-LS	2/15/2003	2000
00056-W	2/28/2011	10
MSD0057-LS	3/11/2013	25
MSD0057-LS	3/12/2006	700
MSD0057-LS	3/18/2013	2530
00056-W	3/18/2013	14600
MSD0057-LS	3/19/2002	1000
MSD0057-LS	3/19/2008	57000
00056-W	3/19/2008	16500
MSD0057-LS	3/26/2002	5000
00056-W	3/27/2008	21825
MSD0057-LS	3/27/2008	97800
MSD0057-LS	3/28/2005	12000
MSD0057-LS	3/4/2004	1500
MSD0057-LS	3/4/2004	3000
00056-W	3/4/2008	500
MSD0057-LS	3/4/2008	3000
00056-W	3/9/2011	53500
MSD0057-LS	4/1/2006	50
00056-W	4/12/2011	45500
MSD0057-LS	4/17/2003	500
MSD0057-LS	4/25/2003	2000
MSD0057-LS	4/30/2005	15000
00056-W	4/4/2008	25350
MSD0057-LS	4/4/2008	23850
MSD0057-LS	5/11/2008	1000
00056-W	5/13/2012	12925
MSD0057-LS	5/17/2002	20000
MSD0057-LS	5/17/2003	8000
00056-W	5/2/2010	43500
MSD0057-LS	5/2/2011	25
00056-W	5/2/2011	375
MSD0057-LS	5/25/2004	5000



**Project Name**     **Anchor Estates PS Elimination 2 - Anchor Estates #1 and #2 PS Elimination**

**Project Number**     **S\_MI\_MF\_NB06\_M\_01\_A\_A - 1**

MSD0057-LS	5/27/2004	1200
MSD0057-LS	5/28/2004	10000
MSD0057-LS	5/5/2003	5000
MSD0057-LS	6/2/2006	800
00056-W	6/23/2011	6975
00056-W	6/26/2013	21500
MSD0057-LS	7/17/2004	10000
00056-W	7/29/2009	1075
MSD0057-LS	7/29/2009	250
MSD0057-LS	8/30/2005	50
00056-W	8/4/2009	600
MSD0057-LS	9/2/2003	20000
MSD0057-LS	9/22/2006	3000
MSD0057-LS	9/27/2002	100000



# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

### Middle Fork Sewershed

#### Anchor Estates PS Elimination 2 Anchor Estates #1 & #2 PS Elimination

Preliminary - For Budget Development Only

- Documented SSO
- Suspected SSO
- Haulop Locations
- Pump Stations
- Proposed Pipe Solution
- WQTC
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

**Construct 9,440 LF of 8"-12" sewer  
to eliminate Anchor Estates #1 and #2 PSs**

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

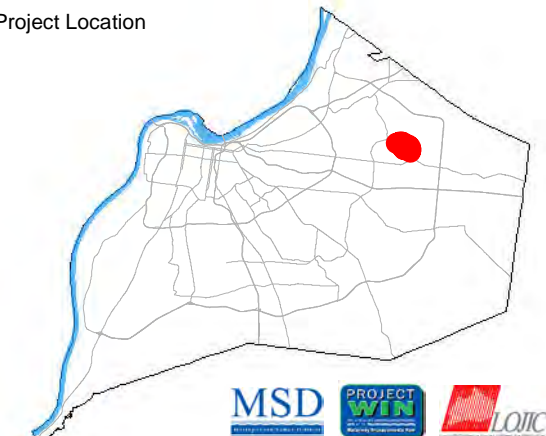
1 inch = 400 feet



Aerial Date:  
2009

Map Revision:  
April 9, 2012

Project Location



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<b>Project Name</b>	Goose Creek PS Improvements & Wet Weather Storage 1 - Devondale Wet Weather Storage
<b>Project Number</b>	S_MI_MF_NB04_M_03_B
<b>Modeled Area</b>	Middle Fork Beargrass Creek
<b>Branch or SSO ID</b>	MF04
<b>Project Type</b>	Storage & Force Main Upgrades
<b>Receiving Stream</b>	Goose Creek
<b>Project Description</b>	Construct 0.5 MG covered storage basin near Devondale Pump Station.
<b>Reason for Overflow</b>	Pump station capacity
<b>Design Parameters</b>	This solution is based on a 2.25 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$1,781,000
<b>Weighted Benefit/Cost Ratio</b>	11.00

Asset ID	SSO Start Date	Volume (Gal)
21628-W	1/1/2003	4500
21628-W	1/1/2003	4500
21628-W	1/1/2005	2000
MSD1024-PS	1/11/2014	5
43472	1/13/2013	16725
21628-W	1/24/2002	2000
MSD1024-PS	1/26/2012	52500
21628-W	1/3/2005	36000
21628-W	1/6/2005	30000
105936	10/6/2013	64000
43472	10/6/2013	37750
105936	11/17/2013	32500
43472	11/17/2013	6700
43472	11/22/2011	2520
21628-W	11/28/2011	28000
43472	11/28/2011	58500
21628-W	11/29/2001	400
43472	12/10/2012	1660
21628-W	12/15/2007	10800
21628-W	12/16/2000	0
21628-W	12/19/2002	8000
43472	12/21/2013	250
43472	12/22/2013	105500
43472	12/5/2011	9000
21628-W	12/5/2011	85500
105936	2/12/2013	100
43472	2/24/2011	15925
21628-W	2/25/2011	16475
21628-W	2/28/2011	1750
21628-W	2/6/2008	682500

**Project Name**     **Goose Creek PS Improvements & Wet Weather Storage 1 - Devondale Wet Weather Storage**

**Project Number**   **S\_MI\_MF\_NB04\_M\_03\_B**

21628-W	3/12/2006	500
62420	3/15/2011	100
43472	3/18/2008	200
21628-W	3/18/2008	37800
21628-W	3/19/2002	1000
91630	3/19/2008	5250
91629	3/19/2008	15750
46891	3/19/2008	246000
62418	3/19/2008	40000
21628-W	3/26/2002	6000
21628-W	3/27/2008	36000
21628-W	3/4/2008	20400
21628-W	3/9/2011	30000
105936	3/9/2011	326700
21628-W	4/11/2011	49500
MSD1024-PS	4/11/2011	9225
105936	4/12/2011	76500
21628-W	4/21/2006	1000
62418	4/23/2011	548500
43472	4/23/2011	112500
105936	4/24/2011	651000
43472	4/27/2011	38750
105936	4/27/2011	417500
62418	4/27/2011	231750
21628-W	4/28/2002	3000
21628-W	4/3/2008	18000
62418	4/4/2008	216000
105936	4/4/2008	43200
21628-W	5/13/2002	18000
21628-W	5/13/2012	1500
21628-W	5/2/2010	45000
43472	5/2/2010	51250
21628-W	5/28/2004	28000
46891	5/29/2012	1800
62418	5/3/2011	168000
105936	5/3/2011	268800
21628-W	5/5/2003	5000
21628-W	5/5/2003	5000
43472	5/8/2009	13000
21628-W	5/8/2009	20625
46891	6/15/2003	15000
21628-W	6/15/2003	500
43472	6/23/2011	8300

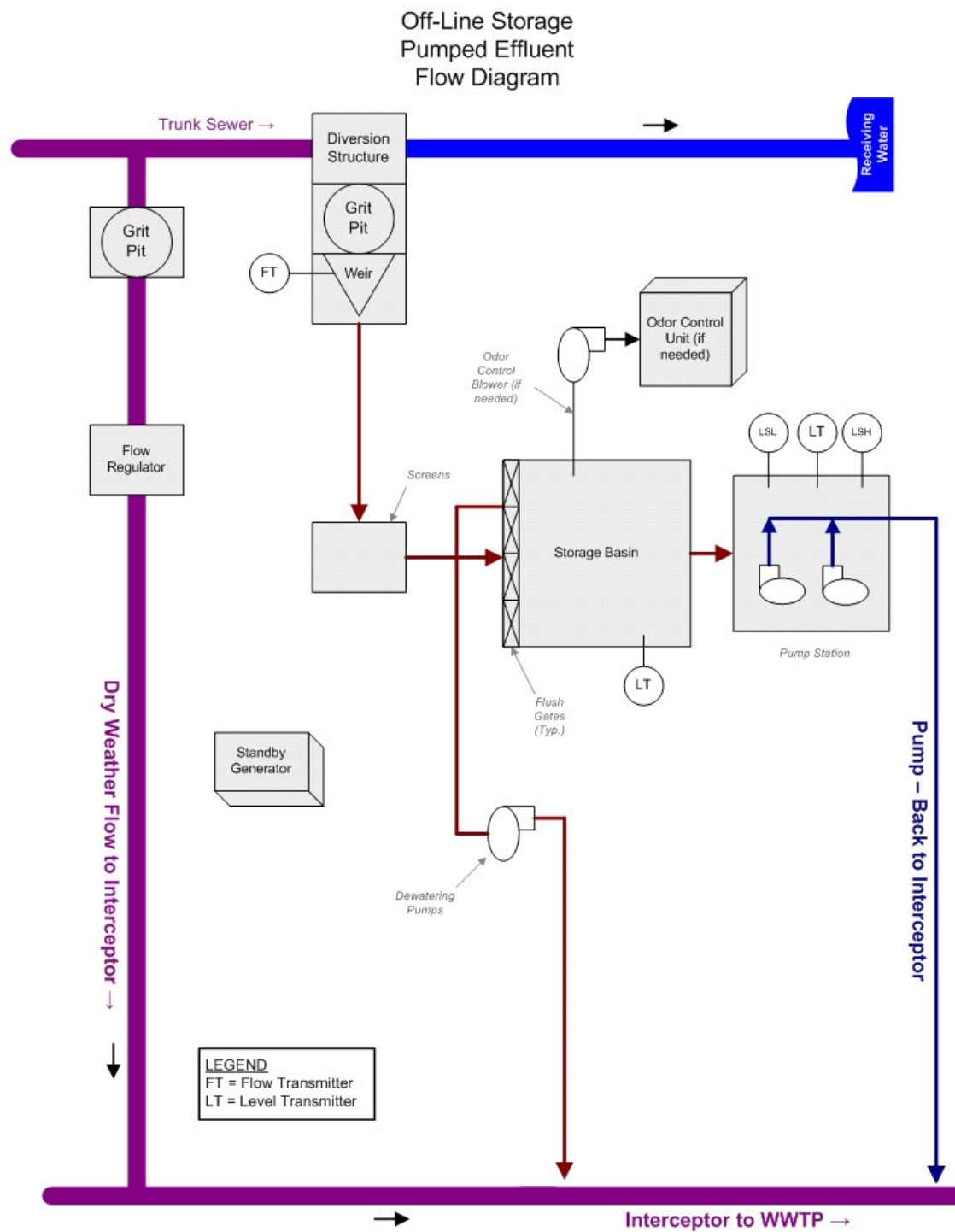


**Project Name** Goose Creek PS Improvements & Wet Weather Storage 1 - Devondale Wet Weather Storage

**Project Number** S\_MI\_MF\_NB04\_M\_03\_B

21628-W	6/23/2011	6000
21628-W	6/26/2013	625
105936	6/26/2013	122000
105936	6/27/2013	26000
21628-W	7/17/2004	10000
21628-W	7/29/2009	250
21628-W	8/4/2009	25000
105936	8/4/2009	1800
21628-W	9/2/2003	3500
21628-W	9/27/2002	3500

# Project Fact Sheet



















**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

**Middle Fork Sewershed  
Goose Creek PS Improvements &  
Wet Weather Storage 1  
Devondale Wet Weather Storage**

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  Proposed Pipe Solution
-  WQTC
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Proposed Storage Solution
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

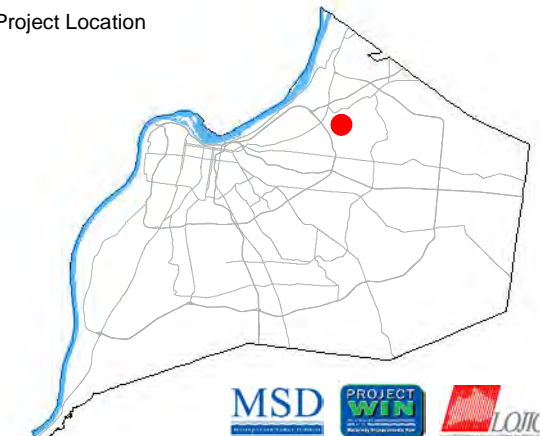
1 inch = 100 feet



Aerial Date:  
2009

Map Revision:  
April 9, 2012

Project Location



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*Off-line covered storage at  
Devondale PS (0.5 MG)*

21628-W  
DEVONDALE  
MSD0040-PS



<b>Project Name</b>	Goose Creek PS Improvements & Wet Weather Storage 2 - PS and FM Upgrades
<b>Project Number</b>	S_MI_MF_NB04_M_03_B
<b>Modeled Area</b>	Middle Fork Beargrass Creek
<b>Branch or SSO ID</b>	MF04
<b>Project Type</b>	Storage & Force Main Upgrades
<b>Receiving Stream</b>	Goose Creek
<b>Project Description</b>	This 5-year design level solution includes upsizing downstream 3,300 LF of FM Replacing 16" portion of GCPS with 20" FM. Upgrading Goose Creek PS to 7.95 MGD. Replacing Saurel Rd 4" FM with 6" FM.
<b>Reason for Overflow</b>	Pump station capacity
<b>Design Parameters</b>	This solution is based on a 2.25 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$5,777,000
<b>Weighted Benefit/Cost Ratio</b>	11.00

Asset ID	SSO Start Date	Volume (Gal)
21628-W	1/1/2003	4500
21628-W	1/1/2003	4500
21628-W	1/1/2005	2000
MSD1024-PS	1/11/2014	5
43472	1/13/2013	16725
21628-W	1/24/2002	2000
MSD1024-PS	1/26/2012	52500
21628-W	1/3/2005	36000
21628-W	1/6/2005	30000
105936	10/6/2013	64000
43472	10/6/2013	37750
105936	11/17/2013	32500
43472	11/17/2013	6700
43472	11/22/2011	2520
21628-W	11/28/2011	28000
43472	11/28/2011	58500
21628-W	11/29/2001	400
43472	12/10/2012	1660
21628-W	12/15/2007	10800
21628-W	12/16/2000	0
21628-W	12/19/2002	8000
43472	12/21/2013	250
43472	12/22/2013	105500
21628-W	12/5/2011	85500
43472	12/5/2011	9000
105936	2/12/2013	100
43472	2/24/2011	15925
21628-W	2/25/2011	16475



**Project Name**    **Goose Creek PS Improvements & Wet Weather Storage 2 - PS and FM Upgrades**

**Project Number**    **S\_MI\_MF\_NB04\_M\_03\_B**

21628-W	2/28/2011	1750
21628-W	2/6/2008	682500
21628-W	3/12/2006	500
62420	3/15/2011	100
21628-W	3/18/2008	37800
43472	3/18/2008	200
21628-W	3/19/2002	1000
91630	3/19/2008	5250
46891	3/19/2008	246000
91629	3/19/2008	15750
62418	3/19/2008	40000
21628-W	3/26/2002	6000
21628-W	3/27/2008	36000
21628-W	3/4/2008	20400
105936	3/9/2011	326700
21628-W	3/9/2011	30000
MSD1024-PS	4/11/2011	9225
21628-W	4/11/2011	49500
105936	4/12/2011	76500
21628-W	4/21/2006	1000
43472	4/23/2011	112500
62418	4/23/2011	548500
105936	4/24/2011	651000
105936	4/27/2011	417500
43472	4/27/2011	38750
62418	4/27/2011	231750
21628-W	4/28/2002	3000
21628-W	4/3/2008	18000
62418	4/4/2008	216000
105936	4/4/2008	43200
21628-W	5/13/2002	18000
21628-W	5/13/2012	1500
21628-W	5/2/2010	45000
43472	5/2/2010	51250
21628-W	5/28/2004	28000
46891	5/29/2012	1800
105936	5/3/2011	268800
62418	5/3/2011	168000
21628-W	5/5/2003	5000
21628-W	5/5/2003	5000
43472	5/8/2009	13000
21628-W	5/8/2009	20625
46891	6/15/2003	15000

**Project Name**    **Goose Creek PS Improvements & Wet Weather Storage 2 - PS and FM Upgrades**

**Project Number**    **S\_MI\_MF\_NB04\_M\_03\_B**








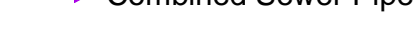






21628-W	6/15/2003	500
43472	6/23/2011	8300
21628-W	6/23/2011	6000
21628-W	6/26/2013	625
105936	6/26/2013	122000
105936	6/27/2013	26000
21628-W	7/17/2004	10000
21628-W	7/29/2009	250
105936	8/4/2009	1800
21628-W	8/4/2009	25000
21628-W	9/2/2003	3500
21628-W	9/27/2002	3500



**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

**Middle Fork Sewershed  
Goose Creek PS Improvements &  
Wet Weather Storage 2  
Pump Station & Force Main Upgrades**

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Proposed Pump Station Solution
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

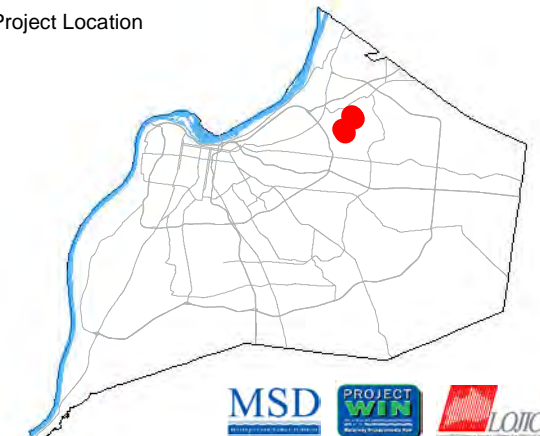
1 inch = 595 feet



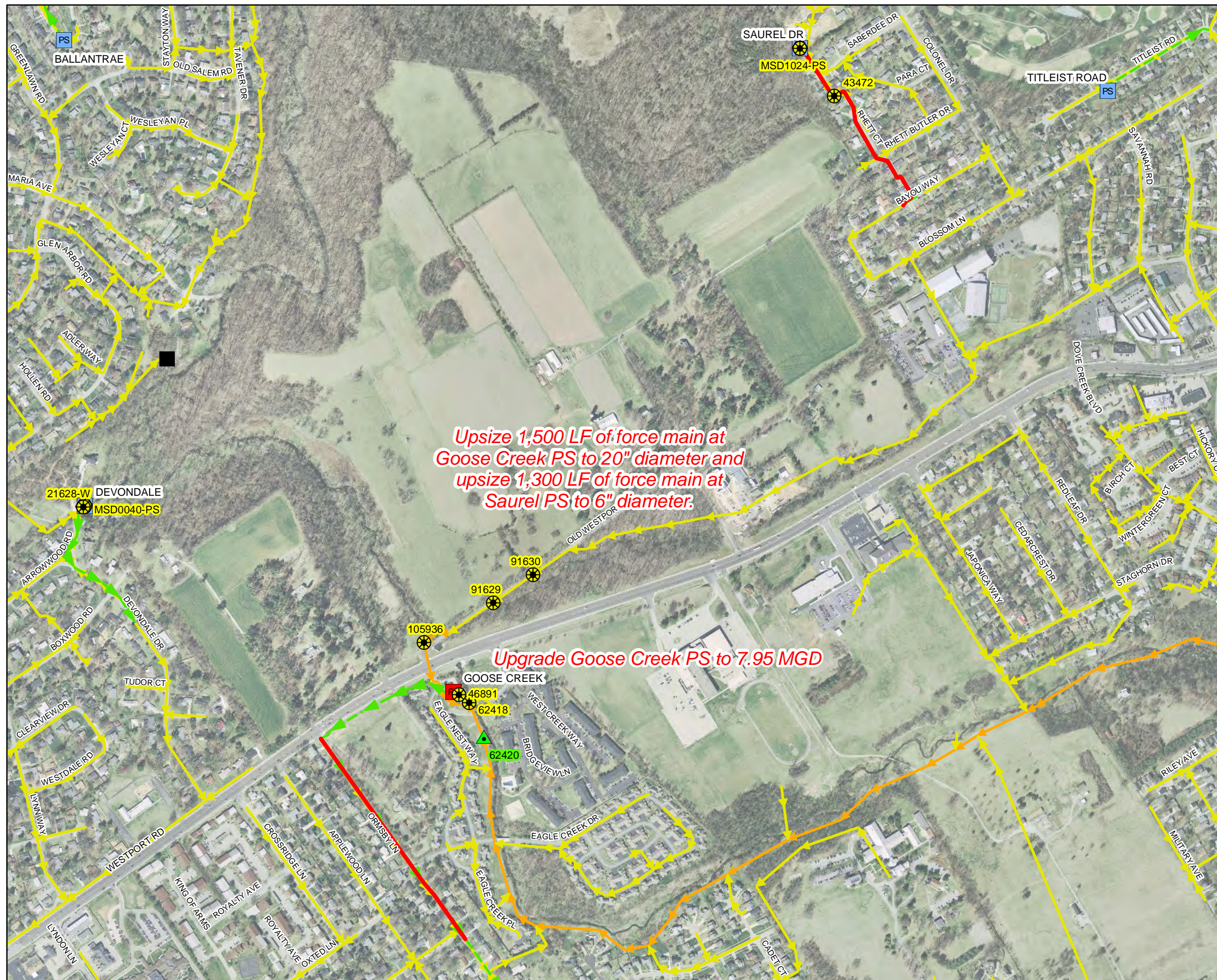
Aerial Date:  
2009

Map Revision:  
April 9, 2012

Project Location



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**Project Name**     **Hurstbourne I/I Investigation & Rehabilitation**

**Project Number**   **S\_MI\_MF\_NB07\_S\_07\_C**

**Modeled Area**             Middle Fork Beargrass Creek

**Branch or SSO ID**           MF07

**Project Type**                Infiltration Reduction

**Receiving Stream**         Middle Fork Beargrass Creek

**Project Description**        This location will be targeted for I/I source control (I/I rehab and private property program). Perform targeted SSES of 26,127 LF upstream of SSO at MH 01793. This accounts for 25% of upstream system.

**Reason for Overflow**        System Capacity

**Design Parameters**         This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**         N/A

**Estimated Capital Cost**     \$536,000




















**Weighted Benefit/Cost Ratio**   --

Asset ID	SSO Start Date	Volume (Gal)
67535	11/30/2011	100
67535	12/5/2011	82500
67535	5/3/2011	84500
67535	6/23/2011	100



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Middle Fork Sewershed  
 Solution ID # S\_MI\_MF\_NB07\_S\_07\_C  
 Hurstbourne I/I Investigation & Rehabilitation

**Preliminary - For Budget Development Only**  
**Legend**

-  Documented SSO
-  Suspected SSO
-  Haul Operation
-  Proposed Pump Station Solution
-  Pump Station
-  WWTP
-  Proposed Pipe Solution
-  Force Main
-  Collector < 12"
-  Interceptor => 12"
-  Combined Sewer Pipe
-  Proposed Off-line Storage
-  Road
-  Streams
-  Floodway
-  Small WWTP Service Area
-  Large WWTP Service Area
-  CSO Area
-  Metro Parks

*This location is targeted for source control  
 (I/I rehab and private property program)*

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

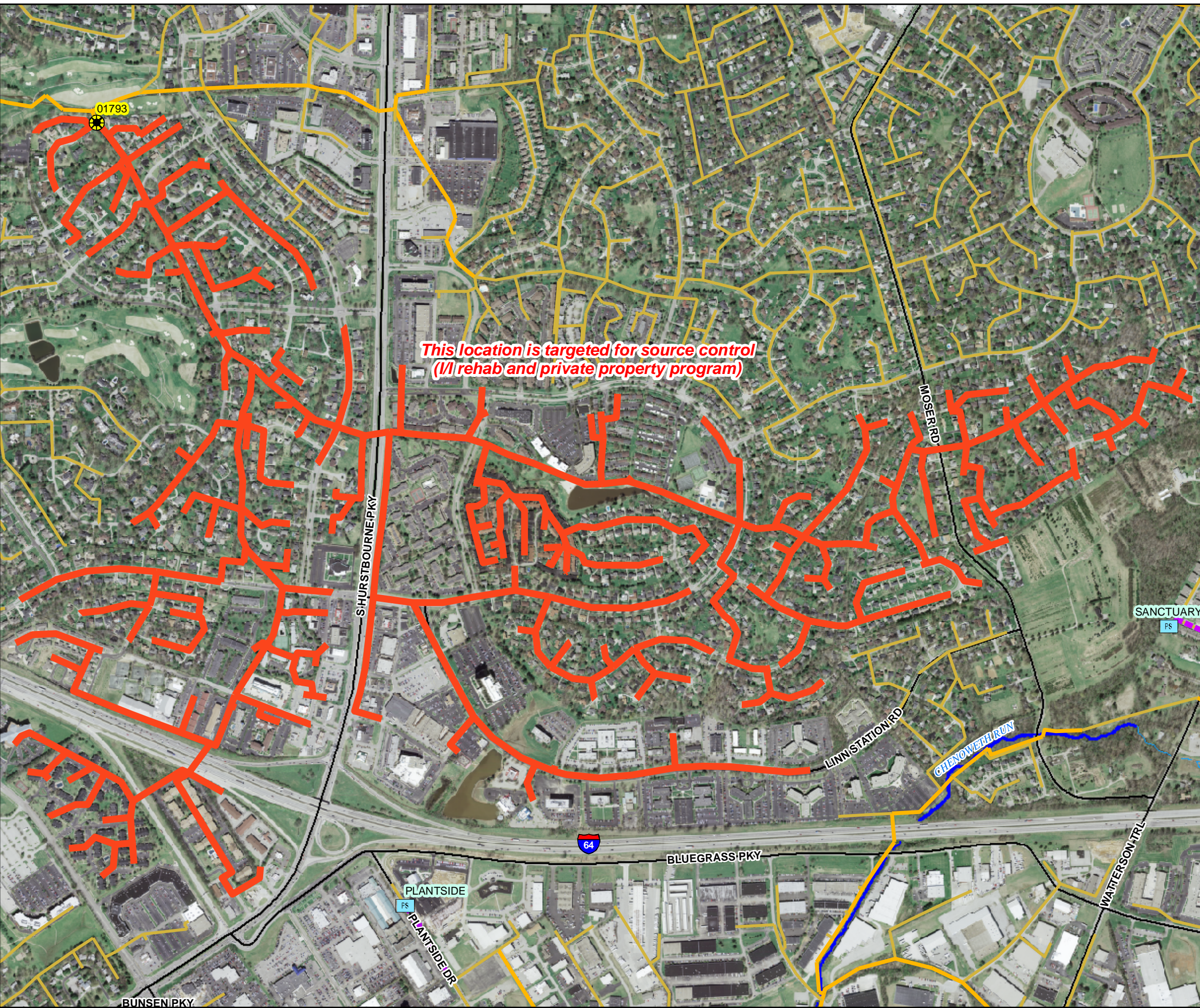
1 inch equals 900 feet  
 Scalable when printed on 11" X 17" paper



Some boundaries are uniquely symbolized within the map.  
 Map Revision  
 May 7, 2009  
 Aerial Date: 2006



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<b>Project Name</b>	Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin
<b>Project Number</b>	S_MISF_MF_NB01_M_01_C_A1
<b>Modeled Area</b>	Middle Fork Beargrass Creek
<b>Branch or SSO ID</b>	MF01
<b>Project Type</b>	Off-line Storage
<b>Receiving Stream</b>	Middle Fork Beargrass Creek, South Fork Beargrass Creek, Greasy Ditch, and Goose Creek
<b>Project Description</b>	Phase 1 of this project includes construction of a 3-cell off-line storage basin. The first two cells provide storage for the 1.82-inch cloudburst event, which was the recommended level of control resulting from the benefit cost evaluation. During design a more economical approach to expanding the available storage was identified, and this was included in the project as an bid alterantive. After bidding MSD decided to accept the alternate bid to construct a large third cell, which results in a level of control equal to the 10-year 24-hour storm event.
<b>Reason for Overflow</b>	System capacity
<b>Design Parameters</b>	The initial solution was based on a 1.82-inch cloudburst rain event. The final constructed configuration will accomodate the 10-year 24-hour rain event.
<b>Project Constraints</b>	Property Acquisition, Potential Wetlands at Buechel Site
<b>Estimated Capital Cost</b>	\$13,184,500
<b>Weighted Benefit/Cost Ratio</b>	1.26

Asset ID	SSO Start Date	Volume (Gal)
27005	1/10/2008	31050
08935-SM	1/10/2008	110880
27005	1/11/2014	6000
27005	1/13/2005	729000
47583	1/13/2013	87000
40559	1/13/2013	8250
51180	1/13/2013	26500
08935-SM	1/13/2013	8798306
45835	1/13/2013	102000
47582	1/13/2013	125000
51161	1/13/2013	42000
23211	1/13/2013	33500
51160	1/13/2013	27000
27005	1/13/2013	67500
84155	1/13/2013	30500
08935-SM	1/14/2007	4621000
90700	1/14/2013	100
47593	1/14/2013	6000
27005	1/15/2007	1539000
45835	1/15/2007	10260
08935-SM	1/17/2006	72000
27005	1/17/2006	20800
27005	1/2/2004	340000
08935-SM	1/21/2010	811385
27005	1/21/2010	48000

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

08935-SM	1/23/2006	156060
27005	1/23/2006	11400
08935-SM	1/24/2002	1000000
08935-SM	1/24/2010	242
40559	1/26/2012	15000
51161	1/26/2012	13000
23211	1/26/2012	14500
72288	1/26/2012	18000
47582	1/26/2012	82000
27005	1/26/2012	72000
90700	1/26/2012	36000
45835	1/26/2012	64000
47593	1/26/2012	27500
08935-SM	1/26/2012	253569
84155	1/26/2012	40500
51180	1/27/2012	100
51160	1/27/2012	22000
45835	1/3/2005	3726000
27005	1/3/2005	44800000
23211	1/3/2005	7590000
08935-SM	1/3/2005	10080000
08935-SM	1/4/2004	1700000
27005	1/4/2004	1900000
27005	10/18/2004	730000
08935-SM	10/18/2004	578000
45835	10/18/2004	102000
23211	10/18/2004	408000
08935-SM	10/22/2007	15120000
27005	10/22/2007	3726000
45835	10/23/2007	322080
08935-SM	10/27/2009	3078
08935-SM	10/27/2011	3071
08935-SM	10/28/2006	576000
08935-SM	10/31/2009	223896
47582	10/5/2013	208000
47583	10/5/2013	86500
51160	10/5/2013	270000
23211	10/5/2013	378000
27005	10/5/2013	125000
72289	10/5/2013	82000
08935-SM	10/5/2013	11307180
45835	10/5/2013	72000
90700	10/6/2013	62000

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

30376	10/6/2013	71000
84155	10/6/2013	55000
47593	10/6/2013	115000
51160	10/9/2009	1080
08935-SM	10/9/2009	1288
27005	10/9/2009	4200
45835	10/9/2009	4200
08935-SM	11/11/2004	430000
27005	11/11/2004	490000
47583	11/17/2013	108000
90700	11/17/2013	21000
47593	11/17/2013	45000
84155	11/17/2013	19500
45835	11/17/2013	92000
27005	11/17/2013	100000
08935-SM	11/17/2013	5019348
72289	11/17/2013	100
23211	11/17/2013	68400
51160	11/17/2013	199500
47582	11/17/2013	120000
23211	11/2/2004	1510000
45835	11/2/2004	29300
27005	11/2/2004	29300
08935-SM	11/2/2004	932000
47034	11/22/2011	650
27005	11/22/2011	52000
51161	11/22/2011	9000
08935-SM	11/22/2011	684854
51160	11/22/2011	27000
23211	11/22/2011	9000
45835	11/22/2011	6000
45835	11/25/2010	7200
27005	11/25/2010	1550
08935-SM	11/25/2010	1126398
08935-SM	11/28/2011	10071059
51161	11/28/2011	504000
47593	11/28/2011	3300
23211	11/28/2011	504000
51160	11/28/2011	76500
27005	11/28/2011	72500
45835	11/28/2011	91000
40559	11/28/2011	78500
72288	11/28/2011	87000



**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

08935-SM	11/29/2001	2000000
30376	11/29/2011	52500
90700	11/29/2011	12000
47582	11/30/2011	1000
45835	12/10/2012	9000
08935-SM	12/13/2007	41800
45835	12/13/2007	1400
27005	12/13/2007	12000
45835	12/15/2007	81000
27005	12/15/2007	2511000
08935-SM	12/15/2007	11095000
08935-SM	12/17/2001	2000000
08935-SM	12/19/2002	200000
08935-SM	12/21/2013	6282652
47582	12/21/2013	420000
47583	12/21/2013	355000
23211	12/22/2013	31000
45835	12/22/2013	55000
72289	12/22/2013	62000
84155	12/22/2013	12000
51160	12/22/2013	12000
27007	12/23/2013	100
45796	12/23/2013	100
08935-SM	12/24/2008	2128997
45835	12/24/2008	12000
47583	12/24/2008	135000
27005	12/24/2008	216000
08935-SM	12/26/2012	901
27005	12/27/2011	1900
45835	12/27/2011	2100
115183	12/5/2011	13500
115184	12/5/2011	100
115185	12/5/2011	100
84155	12/5/2011	33000
30376	12/5/2011	132000
51161	12/5/2011	780000
90700	12/5/2011	46500
51180	12/5/2011	432000
47582	12/5/2011	145000
45835	12/5/2011	345500
40559	12/5/2011	79500
23211	12/5/2011	72000
47593	12/5/2011	97500

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

72288	12/5/2011	135000
27005	12/5/2011	245000
51160	12/5/2011	346000
08935-SM	12/5/2011	10245414
40559	12/9/2012	15000
08935-SM	12/9/2012	464270
72289	12/9/2012	100
27005	12/9/2012	90000
08935-SM	2/12/2008	585268
27005	2/12/2008	9000
08935-SM	2/13/2007	720000
27005	2/13/2007	891000
23211	2/17/2000	0
08935-SM	2/22/2003	55000
45835	2/24/2011	42000
08935-SM	2/24/2011	7494807
23211	2/24/2011	36000
27005	2/24/2011	37000
51160	2/24/2011	44000
90700	2/25/2011	7950
47593	2/25/2011	14750
08935-SM	2/28/2011	31027
27005	2/28/2011	96500
45835	2/28/2011	100350
72288	2/29/2012	100
08935-SM	2/5/2008	1620000
27005	2/5/2010	23000
08935-SM	2/5/2010	272
45835	2/6/2008	432000
27005	2/6/2008	432000
47583	2/6/2008	117120
27005	3/1/2007	67500
08935-SM	3/1/2007	943200
08935-SM	3/10/2008	5574432
84155	3/10/2011	500
27005	3/11/2013	1600
08935-SM	3/11/2013	198695
45835	3/12/2006	286000
08935-SM	3/12/2006	4148000
27005	3/12/2006	702000
08935-SM	3/14/2007	97502
72288	3/16/2012	50
27005	3/17/2012	13500

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

15194	3/17/2012	2000
27005	3/17/2013	36000
45835	3/17/2013	37500
45835	3/18/2008	1302960
47583	3/18/2008	6318000
27005	3/18/2008	2403000
08935-SM	3/18/2008	16979740
47582	3/18/2013	108000
51161	3/18/2013	108000
84155	3/18/2013	30000
40559	3/18/2013	4900
08935-SM	3/18/2013	3203055
23211	3/18/2013	126000
47583	3/18/2013	108000
51160	3/18/2013	9000
08935-SM	3/19/2002	1000000
47604	3/19/2008	45000
90700	3/19/2008	5400
23211	3/19/2008	17820
47593	3/19/2008	837000
72288	3/23/2012	250
08935-SM	3/27/2005	1537000
08935-SM	3/27/2008	7225620
27005	3/27/2008	1309500
47583	3/27/2008	1458000
45835	3/27/2008	294000
45835	3/28/2005	111000
27005	3/28/2005	2100000
47593	3/28/2008	38880
47604	3/28/2008	6210
27005	3/31/2008	19500
45835	3/31/2008	15120
08935-SM	3/31/2008	19916
47583	3/4/2008	1296000
45835	3/4/2008	395280
08935-SM	3/4/2008	12397000
47603	3/4/2008	200
27005	3/4/2008	972000
27005	3/6/2011	100
90700	3/9/2011	72000
51160	3/9/2011	81000
08935-SM	3/9/2011	22584138
27005	3/9/2011	285000

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

23211	3/9/2011	25250
45835	3/9/2011	725000
47593	3/9/2011	69250
27005	4/1/2012	90000
45835	4/1/2012	63000
51160	4/1/2012	1800
40559	4/1/2012	43000
08935-SM	4/1/2012	303355
72288	4/1/2012	55000
45835	4/11/2011	2100250
27005	4/11/2011	1750250
08935-SM	4/11/2011	18668406
47593	4/12/2011	19500
51160	4/12/2011	95000
90700	4/12/2011	227250
47604	4/12/2011	142500
47034	4/12/2011	39250
84155	4/12/2011	45250
23211	4/12/2011	102500
115183	4/12/2011	9000
27005	4/13/2004	13000
27005	4/14/2007	108000
08935-SM	4/14/2007	367804
08935-SM	4/16/2011	1331416
08935-SM	4/19/2009	185884
08935-SM	4/20/2011	241203
08935-SM	4/21/2006	1656000
27005	4/21/2006	54000
45835	4/23/2011	1250000
47593	4/23/2011	42000
90700	4/23/2011	76250
08935-SM	4/23/2011	44938871
84155	4/23/2011	94550
51160	4/23/2011	3600000
23211	4/23/2011	130000
27005	4/23/2011	1650000
30376	4/27/2011	78000
47034	4/27/2011	49500
51161	4/27/2011	864000
115185	4/27/2011	46000
47582	4/28/2011	1750000
115183	4/28/2011	69500
08935-SM	4/3/2006	360000



**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

27005	4/3/2006	108000
08935-SM	4/3/2008	13948990
45835	4/3/2008	1218000
27005	4/3/2008	2268000
23211	4/4/2008	5724000
47593	4/4/2008	204000
23212	4/4/2008	9720
47583	4/4/2008	6156000
51161	4/4/2008	438000
51160	4/4/2008	55500
08935-SM	5/10/2013	10741
47582	5/10/2013	18250
27005	5/10/2013	10000
84155	5/10/2013	20500
47583	5/10/2013	205000
08935-SM	5/12/2010	1873
72288	5/13/2012	64000
51160	5/13/2012	4500
40559	5/13/2012	59000
27005	5/13/2012	105000
08935-SM	5/13/2012	1368241
23211	5/13/2012	4500
08935-SM	5/15/2008	521879
08935-SM	5/19/2005	468350
27005	5/19/2005	140000
45835	5/19/2005	140000
23211	5/2/2004	1400000
08935-SM	5/2/2004	875000
27005	5/2/2004	1500000
47583	5/2/2010	125000
47604	5/2/2010	29500
08935-SM	5/2/2010	17873159
51160	5/2/2010	288000
27005	5/2/2010	175000
90700	5/2/2010	31000
45835	5/2/2010	197000
47593	5/2/2010	136000
51160	5/2/2011	864000
51161	5/2/2011	432000
08935-SM	5/21/2010	456
27005	5/21/2010	1500
27005	5/23/2011	14000
27005	5/25/2004	1770000

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

23211	5/25/2004	1020000
08935-SM	5/25/2004	502000
08935-SM	5/26/2011	1342
27005	5/26/2011	9200
27005	5/27/2004	2900000
27005	5/27/2004	1640000
45835	5/27/2004	184000
08935-SM	5/27/2004	1925000
23211	5/27/2004	1040000
08935-SM	5/29/2012	1621039
72288	5/29/2012	126000
84155	5/29/2012	60000
72289	5/29/2012	60000
51161	5/29/2012	75000
47593	5/29/2012	72000
27005	5/29/2012	82000
40559	5/29/2012	126000
51160	5/29/2012	96000
23211	5/29/2012	105000
45835	5/29/2012	81500
51180	5/29/2012	1200
90700	5/29/2012	24000
84155	5/3/2011	67500
47593	5/3/2011	37500
30376	5/3/2011	29250
90700	5/3/2011	39500
47034	5/3/2011	51500
115185	5/3/2011	116000
23211	5/30/2004	2080000
45835	5/30/2004	281000
27005	5/30/2004	2710000
72288	5/31/2012	9500
27005	5/31/2012	7200
15194	5/5/2012	100
51160	5/8/2009	4500
08935-SM	5/8/2009	3867778
27005	5/8/2009	3975000
47583	5/8/2009	4500000
45835	5/8/2009	337500
90700	5/8/2009	540
47593	5/8/2009	540
08935-SM	6/1/2012	92118
45835	6/17/2013	50

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

27005	6/17/2013	50
08935-SM	6/17/2013	372637
08935-SM	6/18/2009	430000
45835	6/18/2009	9000
08935-SM	6/2/2006	1008000
45835	6/2/2006	57500
27005	6/2/2006	675000
51160	6/22/2011	129600
08935-SM	6/22/2011	5665357
51161	6/22/2011	408000
23211	6/22/2011	270000
47593	6/23/2011	100
47582	6/23/2011	145000
84155	6/23/2011	75000
27005	6/23/2011	84000
45835	6/23/2011	78500
45835	6/26/2013	165000
84155	6/26/2013	120000
47593	6/26/2013	112500
08935-SM	6/26/2013	6639301
40559	6/26/2013	30000
90700	6/26/2013	75000
51160	6/26/2013	126000
27005	6/26/2013	165000
47583	6/27/2013	64000
30376	6/27/2013	45000
23211	6/27/2013	84000
51180	6/27/2013	3000
08935-SM	6/28/2007	13579
45835	6/9/2010	9700
27005	6/9/2010	50
72289	7/1/2012	100
08935-SM	7/10/2004	220000
27005	7/10/2004	199500
27005	7/10/2013	4500
08935-SM	7/13/2010	217722
08935-SM	7/14/2006	792000
72288	7/15/2012	25
08935-SM	7/17/2004	220000
27005	7/17/2004	240000
08935-SM	7/20/2010	7463
72289	7/22/2013	100
45835	7/22/2013	10500

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

27005	7/22/2013	22000
08935-SM	7/29/2009	1350710
27005	7/29/2009	240000
47604	7/29/2009	34000
90700	7/29/2009	34000
47593	7/29/2009	240000
45835	7/29/2009	240000
27005	7/6/2013	100
08935-SM	7/6/2013	126702
47583	7/6/2013	32500
47582	7/6/2013	19000
08935-SM	8/14/2010	9
45796	8/17/2010	5
08935-SM	8/21/2007	4579
27005	8/30/2005	66000
45835	8/30/2005	60500
08935-SM	8/30/2005	1065000
45835	8/4/2009	320000
08935-SM	8/4/2009	6943977
47593	8/4/2009	111000
27005	8/4/2009	270000
47583	8/4/2009	54000
51160	8/4/2009	351360
08935-SM	8/7/2011	1147
45835	9/2/2003	650000
27005	9/2/2003	1900000
08935-SM	9/2/2003	1700000
72288	9/2/2012	150
08935-SM	9/20/2009	147609
27005	9/21/2009	520000
45835	9/21/2009	490000
27005	9/21/2013	100
27005	9/22/2006	5940000
08935-SM	9/22/2006	5544000
45835	9/22/2006	527040
84155	9/23/2006	0
51161	9/26/2011	71000
45835	9/26/2011	155000
08935-SM	9/26/2011	452913
27005	9/26/2011	172000
23211	9/26/2011	56500
51160	9/26/2011	17200
08935-SM	9/27/2002	100000



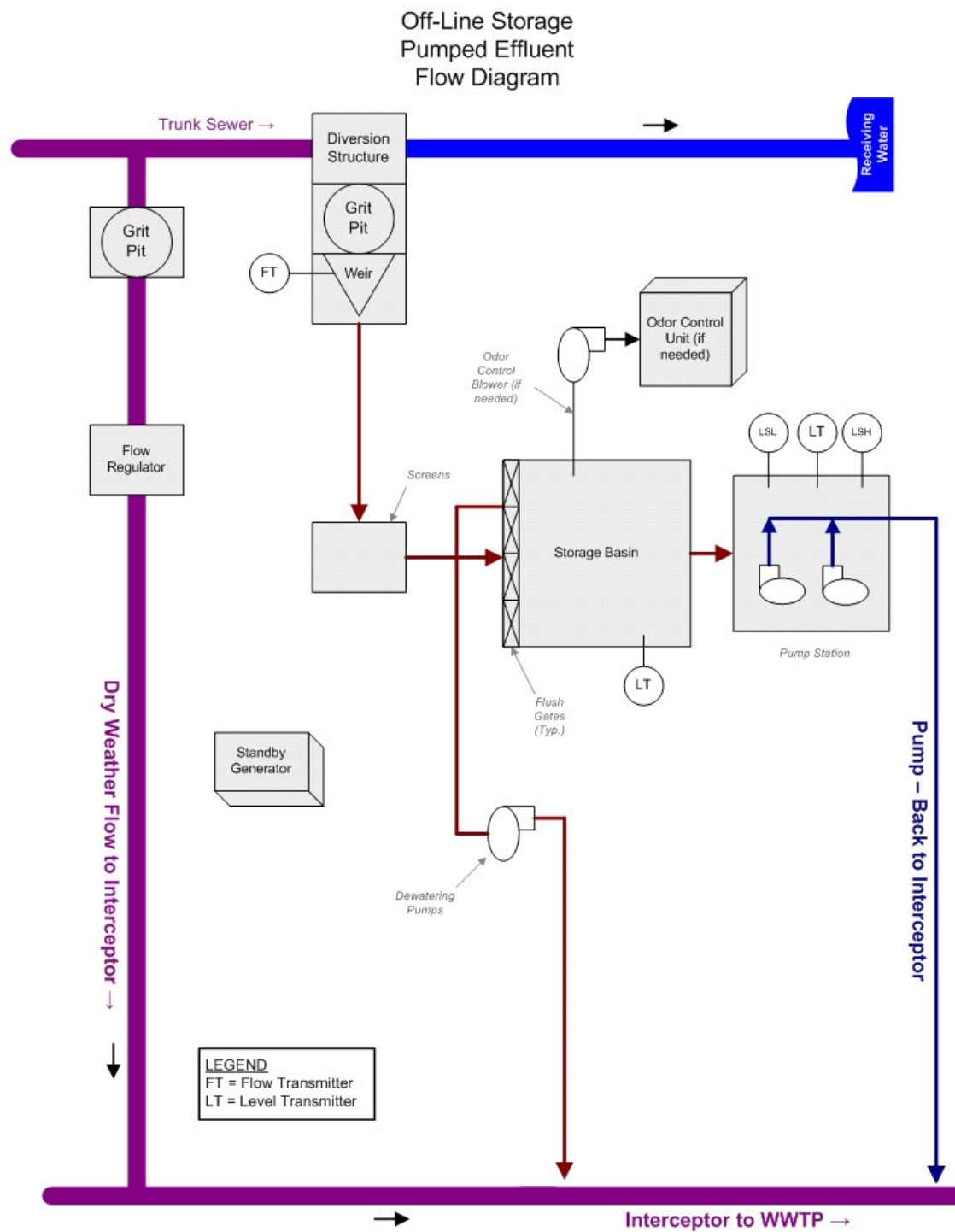
**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 1- Buechel Basin

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

08935-SM 9/3/2003 200000

72289 9/8/2012 50

# Project Fact Sheet





# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Middle Fork Sewershed  
Middle Fork Relief Interceptor,  
Wet Weather Storage and  
UMFLS Diversion 1 - Buechel Basin

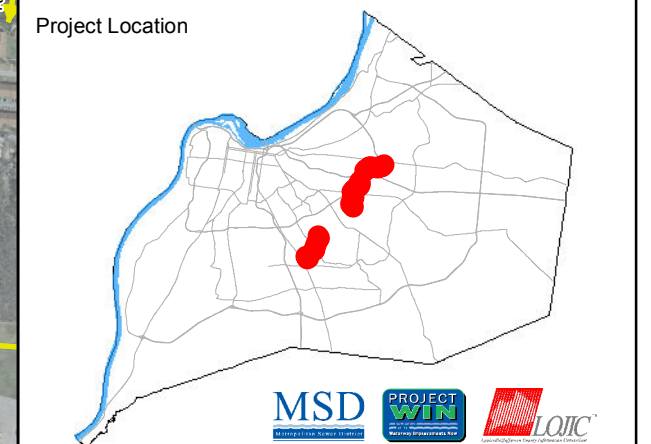
Preliminary - For Budget Development Only



- Documented SSO
- Suspected SSO
- Haulop Locations
- Pump Stations
- WQTC
- Proposed Pipe Solution
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Proposed Storage Solution
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,000 feet		Aerial Date: 2012	Map Revision: April 15, 2014
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<b>Project Name</b>	Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage
<b>Project Number</b>	S_MISF_MF_NB01_M_01_C_A1
<b>Modeled Area</b>	Middle Fork Beargrass Creek
<b>Branch or SSO ID</b>	MF01
<b>Project Type</b>	Off-line Storage & Pipe Upgrades
<b>Receiving Stream</b>	Middle Fork Beargrass Creek, South Fork Beargrass Creek, Greasy Ditch, and Goose Creek
<b>Project Description</b>	This alternative includes constructing 10,200 LF of 30" Force Main Diversion to Hikes Lane Interceptor from Ex UMFLS. Construct Middle Fork Relief Interceptor between Oxmoor and Middle Fork at Breckenridge. Construct 1.6 MG covered basin near Car Wash Site. Upsize Pipe D/S of MH 15138 to 18".
<b>Reason for Overflow</b>	System capacity
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	Property Acquisition, Stream Crossings for MFR1
<b>Estimated Capital Cost</b>	\$13,149,000
<b>Weighted Benefit/Cost Ratio</b>	1.26

Asset ID	SSO Start Date	Volume (Gal)
08935-SM	1/10/2008	110880
27005	1/10/2008	31050
27005	1/11/2014	6000
27005	1/13/2005	729000
51160	1/13/2013	27000
45835	1/13/2013	102000
08935-SM	1/13/2013	8798306
23211	1/13/2013	33500
51161	1/13/2013	42000
47582	1/13/2013	125000
40559	1/13/2013	8250
47583	1/13/2013	87000
51180	1/13/2013	26500
27005	1/13/2013	67500
84155	1/13/2013	30500
08935-SM	1/14/2007	4621000
47593	1/14/2013	6000
90700	1/14/2013	100
45835	1/15/2007	10260
27005	1/15/2007	1539000
08935-SM	1/17/2006	72000
27005	1/17/2006	20800
27005	1/2/2004	340000
08935-SM	1/21/2010	811385
27005	1/21/2010	48000
08935-SM	1/23/2006	156060
27005	1/23/2006	11400



**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

08935-SM	1/24/2002	1000000
08935-SM	1/24/2010	242
51161	1/26/2012	13000
40559	1/26/2012	15000
47582	1/26/2012	82000
45835	1/26/2012	64000
08935-SM	1/26/2012	253569
72288	1/26/2012	18000
23211	1/26/2012	14500
47593	1/26/2012	27500
90700	1/26/2012	36000
27005	1/26/2012	72000
84155	1/26/2012	40500
51160	1/27/2012	22000
51180	1/27/2012	100
45835	1/3/2005	3726000
08935-SM	1/3/2005	10080000
27005	1/3/2005	44800000
23211	1/3/2005	7590000
08935-SM	1/4/2004	1700000
27005	1/4/2004	1900000
27005	10/18/2004	730000
23211	10/18/2004	408000
45835	10/18/2004	102000
08935-SM	10/18/2004	578000
08935-SM	10/22/2007	15120000
27005	10/22/2007	3726000
45835	10/23/2007	322080
08935-SM	10/27/2009	3078
08935-SM	10/27/2011	3071
08935-SM	10/28/2006	576000
08935-SM	10/31/2009	223896
72289	10/5/2013	82000
47582	10/5/2013	208000
08935-SM	10/5/2013	11307180
51160	10/5/2013	270000
23211	10/5/2013	378000
45835	10/5/2013	72000
47583	10/5/2013	86500
27005	10/5/2013	125000
47593	10/6/2013	115000
30376	10/6/2013	71000
84155	10/6/2013	55000

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

90700	10/6/2013	62000
45835	10/9/2009	4200
51160	10/9/2009	1080
27005	10/9/2009	4200
08935-SM	10/9/2009	1288
27005	11/11/2004	490000
08935-SM	11/11/2004	430000
51160	11/17/2013	199500
72289	11/17/2013	100
47582	11/17/2013	120000
23211	11/17/2013	68400
45835	11/17/2013	92000
47593	11/17/2013	45000
08935-SM	11/17/2013	5019348
47583	11/17/2013	108000
90700	11/17/2013	21000
84155	11/17/2013	19500
27005	11/17/2013	100000
27005	11/2/2004	29300
45835	11/2/2004	29300
23211	11/2/2004	1510000
08935-SM	11/2/2004	932000
23211	11/22/2011	9000
51161	11/22/2011	9000
45835	11/22/2011	6000
51160	11/22/2011	27000
47034	11/22/2011	650
08935-SM	11/22/2011	684854
27005	11/22/2011	52000
08935-SM	11/25/2010	1126398
45835	11/25/2010	7200
27005	11/25/2010	1550
45835	11/28/2011	91000
51161	11/28/2011	504000
47593	11/28/2011	3300
72288	11/28/2011	87000
08935-SM	11/28/2011	10071059
23211	11/28/2011	504000
51160	11/28/2011	76500
40559	11/28/2011	78500
27005	11/28/2011	72500
08935-SM	11/29/2001	2000000
30376	11/29/2011	52500

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

90700	11/29/2011	12000
47582	11/30/2011	1000
45835	12/10/2012	9000
08935-SM	12/13/2007	41800
45835	12/13/2007	1400
27005	12/13/2007	12000
45835	12/15/2007	81000
08935-SM	12/15/2007	11095000
27005	12/15/2007	2511000
08935-SM	12/17/2001	2000000
08935-SM	12/19/2002	200000
47583	12/21/2013	355000
47582	12/21/2013	420000
08935-SM	12/21/2013	6282652
72289	12/22/2013	62000
23211	12/22/2013	31000
51160	12/22/2013	12000
45835	12/22/2013	55000
84155	12/22/2013	12000
45796	12/23/2013	100
27007	12/23/2013	100
47583	12/24/2008	135000
45835	12/24/2008	12000
08935-SM	12/24/2008	2128997
27005	12/24/2008	216000
08935-SM	12/26/2012	901
45835	12/27/2011	2100
27005	12/27/2011	1900
115183	12/5/2011	13500
115184	12/5/2011	100
51161	12/5/2011	780000
115185	12/5/2011	100
72288	12/5/2011	135000
47593	12/5/2011	97500
23211	12/5/2011	72000
51160	12/5/2011	346000
51180	12/5/2011	432000
40559	12/5/2011	79500
08935-SM	12/5/2011	10245414
45835	12/5/2011	345500
47582	12/5/2011	145000
30376	12/5/2011	132000
27005	12/5/2011	245000

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

90700	12/5/2011	46500
84155	12/5/2011	33000
40559	12/9/2012	15000
08935-SM	12/9/2012	464270
72289	12/9/2012	100
27005	12/9/2012	90000
08935-SM	2/12/2008	585268
27005	2/12/2008	9000
08935-SM	2/13/2007	720000
27005	2/13/2007	891000
23211	2/17/2000	0
08935-SM	2/22/2003	55000
51160	2/24/2011	44000
45835	2/24/2011	42000
08935-SM	2/24/2011	7494807
27005	2/24/2011	37000
23211	2/24/2011	36000
47593	2/25/2011	14750
90700	2/25/2011	7950
45835	2/28/2011	100350
08935-SM	2/28/2011	31027
27005	2/28/2011	96500
72288	2/29/2012	100
08935-SM	2/5/2008	1620000
27005	2/5/2010	23000
08935-SM	2/5/2010	272
47583	2/6/2008	117120
45835	2/6/2008	432000
27005	2/6/2008	432000
08935-SM	3/1/2007	943200
27005	3/1/2007	67500
08935-SM	3/10/2008	5574432
84155	3/10/2011	500
08935-SM	3/11/2013	198695
27005	3/11/2013	1600
08935-SM	3/12/2006	4148000
45835	3/12/2006	286000
27005	3/12/2006	702000
08935-SM	3/14/2007	97502
72288	3/16/2012	50
15194	3/17/2012	2000
27005	3/17/2012	13500
45835	3/17/2013	37500



**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

27005	3/17/2013	36000
45835	3/18/2008	1302960
47583	3/18/2008	6318000
27005	3/18/2008	2403000
08935-SM	3/18/2008	16979740
08935-SM	3/18/2013	3203055
51161	3/18/2013	108000
51160	3/18/2013	9000
47583	3/18/2013	108000
40559	3/18/2013	4900
23211	3/18/2013	126000
47582	3/18/2013	108000
84155	3/18/2013	30000
08935-SM	3/19/2002	1000000
47604	3/19/2008	45000
47593	3/19/2008	837000
23211	3/19/2008	17820
90700	3/19/2008	5400
72288	3/23/2012	250
08935-SM	3/27/2005	1537000
45835	3/27/2008	294000
47583	3/27/2008	1458000
27005	3/27/2008	1309500
08935-SM	3/27/2008	7225620
27005	3/28/2005	2100000
45835	3/28/2005	111000
47604	3/28/2008	6210
47593	3/28/2008	38880
45835	3/31/2008	15120
27005	3/31/2008	19500
08935-SM	3/31/2008	19916
47603	3/4/2008	200
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08935-SM	3/9/2011	22584138
51160	3/9/2011	81000
45835	3/9/2011	725000
47593	3/9/2011	69250
90700	3/9/2011	72000
27005	3/9/2011	285000

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

23211	3/9/2011	25250
72288	4/1/2012	55000
40559	4/1/2012	43000
45835	4/1/2012	63000
08935-SM	4/1/2012	303355
51160	4/1/2012	1800
27005	4/1/2012	90000
08935-SM	4/11/2011	18668406
45835	4/11/2011	2100250
27005	4/11/2011	1750250
47593	4/12/2011	19500
47604	4/12/2011	142500
47034	4/12/2011	39250
23211	4/12/2011	102500
51160	4/12/2011	95000
115183	4/12/2011	9000
90700	4/12/2011	227250
84155	4/12/2011	45250
27005	4/13/2004	13000
27005	4/14/2007	108000
08935-SM	4/14/2007	367804
08935-SM	4/16/2011	1331416
08935-SM	4/19/2009	185884
08935-SM	4/20/2011	241203
08935-SM	4/21/2006	1656000
27005	4/21/2006	54000
47593	4/23/2011	42000
23211	4/23/2011	130000
08935-SM	4/23/2011	44938871
51160	4/23/2011	3600000
45835	4/23/2011	1250000
27005	4/23/2011	1650000
90700	4/23/2011	76250
84155	4/23/2011	94550
47034	4/27/2011	49500
115185	4/27/2011	46000
51161	4/27/2011	864000
30376	4/27/2011	78000
47582	4/28/2011	1750000
115183	4/28/2011	69500
08935-SM	4/3/2006	360000
27005	4/3/2006	108000
45835	4/3/2008	1218000

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

08935-SM	4/3/2008	13948990
27005	4/3/2008	2268000
51161	4/4/2008	438000
47593	4/4/2008	204000
47583	4/4/2008	6156000
23212	4/4/2008	9720
23211	4/4/2008	5724000
51160	4/4/2008	55500
47582	5/10/2013	18250
47583	5/10/2013	205000
08935-SM	5/10/2013	10741
27005	5/10/2013	10000
84155	5/10/2013	20500
08935-SM	5/12/2010	1873
23211	5/13/2012	4500
08935-SM	5/13/2012	1368241
51160	5/13/2012	4500
40559	5/13/2012	59000
27005	5/13/2012	105000
72288	5/13/2012	64000
08935-SM	5/15/2008	521879
08935-SM	5/19/2005	468350
27005	5/19/2005	140000
45835	5/19/2005	140000
23211	5/2/2004	1400000
08935-SM	5/2/2004	875000
27005	5/2/2004	1500000
08935-SM	5/2/2010	17873159
47604	5/2/2010	29500
47583	5/2/2010	125000
45835	5/2/2010	197000
47593	5/2/2010	136000
51160	5/2/2010	288000
27005	5/2/2010	175000
90700	5/2/2010	31000
51160	5/2/2011	864000
51161	5/2/2011	432000
08935-SM	5/21/2010	456
27005	5/21/2010	1500
27005	5/23/2011	14000
08935-SM	5/25/2004	502000
27005	5/25/2004	1770000
23211	5/25/2004	1020000

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

08935-SM	5/26/2011	1342
27005	5/26/2011	9200
23211	5/27/2004	1040000
27005	5/27/2004	2900000
27005	5/27/2004	1640000
08935-SM	5/27/2004	1925000
45835	5/27/2004	184000
45835	5/29/2012	81500
72288	5/29/2012	126000
51180	5/29/2012	1200
72289	5/29/2012	60000
23211	5/29/2012	105000
40559	5/29/2012	126000
08935-SM	5/29/2012	1621039
47593	5/29/2012	72000
51160	5/29/2012	96000
51161	5/29/2012	75000
90700	5/29/2012	24000
84155	5/29/2012	60000
27005	5/29/2012	82000
115185	5/3/2011	116000
47034	5/3/2011	51500
47593	5/3/2011	37500
30376	5/3/2011	29250
90700	5/3/2011	39500
84155	5/3/2011	67500
27005	5/30/2004	2710000
23211	5/30/2004	2080000
45835	5/30/2004	281000
72288	5/31/2012	9500
27005	5/31/2012	7200
15194	5/5/2012	100
47593	5/8/2009	540
47583	5/8/2009	4500000
45835	5/8/2009	337500
27005	5/8/2009	3975000
90700	5/8/2009	540
51160	5/8/2009	4500
08935-SM	5/8/2009	3867778
08935-SM	6/1/2012	92118
45835	6/17/2013	50
08935-SM	6/17/2013	372637
27005	6/17/2013	50



**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

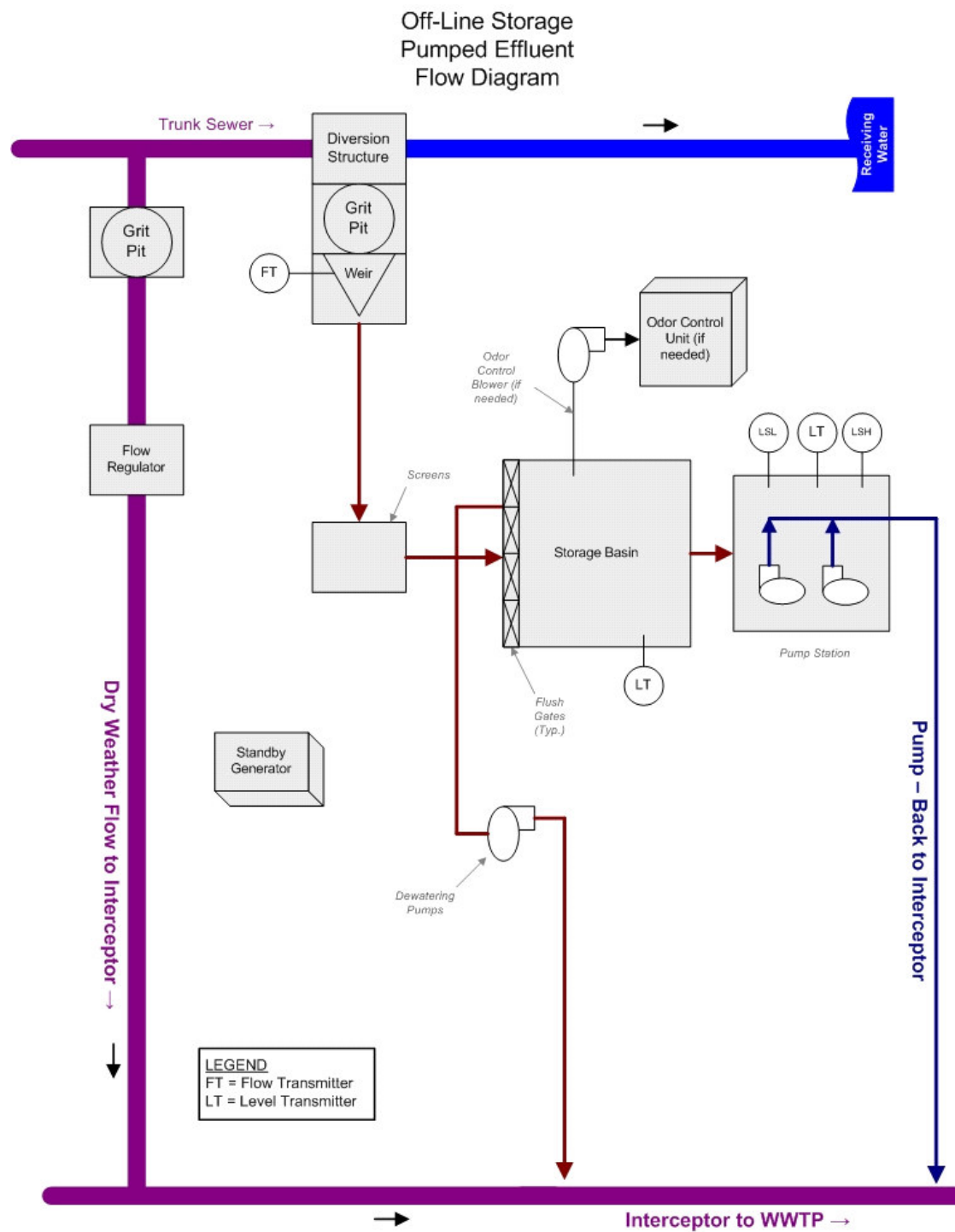
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51161	6/22/2011	408000
23211	6/22/2011	270000
08935-SM	6/22/2011	5665357
51160	6/22/2011	129600
47593	6/23/2011	100
47582	6/23/2011	145000
45835	6/23/2011	78500
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45835	6/26/2013	165000
08935-SM	6/26/2013	6639301
47593	6/26/2013	112500
84155	6/26/2013	120000
27005	6/26/2013	165000
90700	6/26/2013	75000
51180	6/27/2013	3000
47583	6/27/2013	64000
23211	6/27/2013	84000
30376	6/27/2013	45000
08935-SM	6/28/2007	13579
45835	6/9/2010	9700
27005	6/9/2010	50
72289	7/1/2012	100
27005	7/10/2004	199500
08935-SM	7/10/2004	220000
27005	7/10/2013	4500
08935-SM	7/13/2010	217722
08935-SM	7/14/2006	792000
72288	7/15/2012	25
27005	7/17/2004	240000
08935-SM	7/17/2004	220000
08935-SM	7/20/2010	7463
45835	7/22/2013	10500
72289	7/22/2013	100
27005	7/22/2013	22000
47604	7/29/2009	34000

**Project Name** Middle Fork Relief Interceptor, Wet Weather Storage, and UMFLS Diversion 2 - PS Diversion and Storage

**Project Number** S\_MISF\_MF\_NB01\_M\_01\_C\_A1

47593	7/29/2009	240000
45835	7/29/2009	240000
08935-SM	7/29/2009	1350710
27005	7/29/2009	240000
90700	7/29/2009	34000
08935-SM	7/6/2013	126702
47582	7/6/2013	19000
47583	7/6/2013	32500
27005	7/6/2013	100
08935-SM	8/14/2010	9
45796	8/17/2010	5
08935-SM	8/21/2007	4579
45835	8/30/2005	60500
27005	8/30/2005	66000
08935-SM	8/30/2005	1065000
47583	8/4/2009	54000
45835	8/4/2009	320000
47593	8/4/2009	111000
27005	8/4/2009	270000
51160	8/4/2009	351360
08935-SM	8/4/2009	6943977
08935-SM	8/7/2011	1147
27005	9/2/2003	1900000
08935-SM	9/2/2003	1700000
45835	9/2/2003	650000
72288	9/2/2012	150
08935-SM	9/20/2009	147609
45835	9/21/2009	490000
27005	9/21/2009	520000
27005	9/21/2013	100
08935-SM	9/22/2006	5544000
45835	9/22/2006	527040
27005	9/22/2006	5940000
84155	9/23/2006	0
45835	9/26/2011	155000
51161	9/26/2011	71000
23211	9/26/2011	56500
51160	9/26/2011	17200
08935-SM	9/26/2011	452913
27005	9/26/2011	172000
08935-SM	9/27/2002	100000
08935-SM	9/3/2003	200000
72289	9/8/2012	50

# Project Fact Sheet





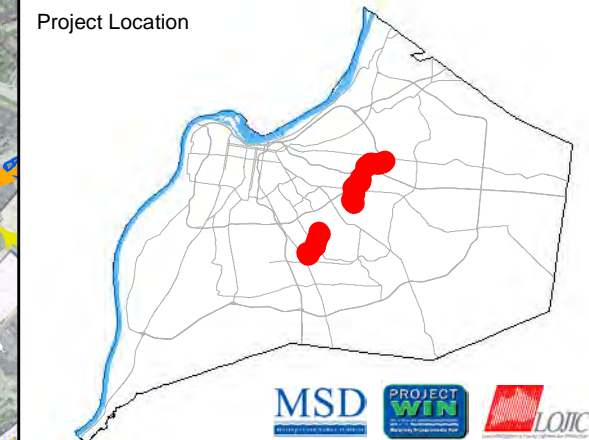
**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Middle Fork Sewershed**  
**Middle Fork Relief Interceptor,**  
**Wet Weather Storage and**  
**UMFLS Diversion 2 - PS Diversion and Storage**

Preliminary - For Budget Development Only

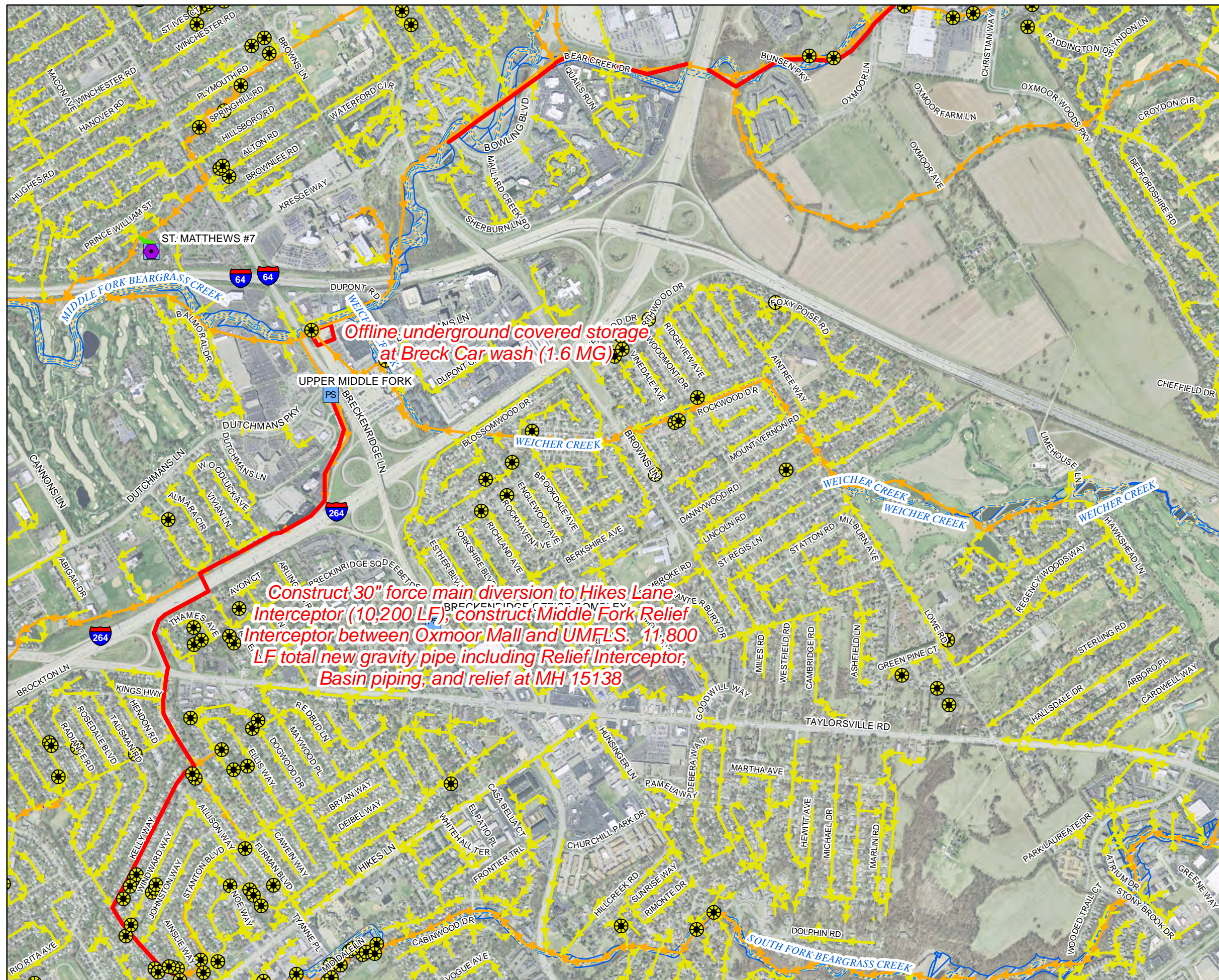
- Documented SSO
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General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,320 feet       Aerial Date: 2009    Map Revision: April 9, 2012



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Construct 30" force main diversion to Hikes Lane Interceptor (10,200 LF); construct Middle Fork Relief Interceptor between Oxmoor Mall and UMFLS. 11,800 LF total new gravity pipe including Relief Interceptor, Basin piping, and relief at MH 15138





<b>Project Name</b>	Beargrass Interceptor Rehab Ph. 2
<b>Project Number</b>	S_SD_MF_NB06_S_13_C
<b>Modeled Area</b>	Southeastern Diversion
<b>Branch or SSO ID</b>	NB06
<b>Project Type</b>	Pipe Rehab
<b>Receiving Stream</b>	South Fork Beargrass Creek
<b>Project Description</b>	This solution involves heavily cleaning 2,000 LF of 42" interceptor between MH 51594 and MH 73227.
<b>Reason for Overflow</b>	Obstructions and root masses
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$57,000
<b>Weighted Benefit/Cost Ratio</b>	--

Asset ID	SSO Start Date	Volume (Gal)
51594	1/11/2013	250
51594	1/13/2013	55000
51594	1/23/2012	2100
51594	1/26/2012	52500
51594	1/30/2013	3500
51594	10/1/2012	12000
51594	10/30/2013	3000
51594	10/5/2013	108000
51594	10/9/2009	9720
51594	11/15/2011	100
51594	11/17/2013	12600
51594	11/22/2011	9000
51594	11/25/2010	2200
51594	11/27/2011	24000
51594	12/22/2013	21000
51594	12/24/2008	6000
51594	12/27/2011	1350
51594	12/5/2011	144000
51594	12/7/2012	15000
51594	12/9/2012	6000
51594	2/24/2011	12000
51594	2/28/2011	19300
51594	2/29/2012	100
51594	2/5/2010	600
51594	3/11/2013	1200
51594	3/17/2012	7200
51594	3/18/2013	54000
51594	3/23/2012	1000
51594	3/5/2011	100

Project Name	Beargrass Interceptor Rehab Ph. 2	
Project Number	S_SD_MF_NB06_S_13_C	
51594	3/9/2011	65000
51594	4/1/2012	9000
51594	4/11/2011	196000
51594	4/16/2013	3750
51594	4/23/2011	197000
51594	4/28/2012	100
51594	4/9/2011	24525
51594	5/1/2010	72000
51594	5/1/2011	114000
51594	5/10/2013	9000
51594	5/13/2012	12600
51594	5/19/2005	50
51594	5/21/2010	9000
51594	5/23/2011	100
51594	5/23/2011	18000
51594	5/26/2011	4200
51594	5/29/2012	60000
51594	5/31/2012	10500
51594	5/5/2012	600
51594	5/5/2013	21600
51594	5/8/2011	100
51594	6/15/2011	100
51594	6/17/2013	3000
51594	6/21/2011	5000
51594	6/21/2013	50
51594	6/22/2011	18000
51594	6/26/2013	15000
51594	7/1/2012	100
51594	7/14/2012	2700
51594	7/19/2011	900
51594	7/19/2012	50
51594	7/22/2013	6000
51594	7/27/2012	50
51594	7/29/2009	27000
51594	8/12/2013	100
51594	8/16/2012	6300
51594	8/21/2013	100
51594	8/4/2009	42000
51594	8/7/2011	4800
51594	8/9/2013	100
51594	9/1/2012	100
51594	9/2/2012	100
51594	9/20/2009	18000

---

**Project Name** Beargrass Interceptor Rehab Ph. 2

**Project Number** S\_SD\_MF\_NB06\_S\_13\_C

51594	9/21/2013	19500
51594	9/26/2011	4400
51594	9/26/2012	4500
51594	9/5/2012	100
51594	9/8/2012	100



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Southeast Diversion**  
**Beargrass Interceptor Rehabilitation Ph. 2**

Preliminary - For Budget Development Only

- Documented SSO
- Suspected SSO
- Haulop Locations
- Pump Stations
- Proposed Pipe Solution
- WQTC
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

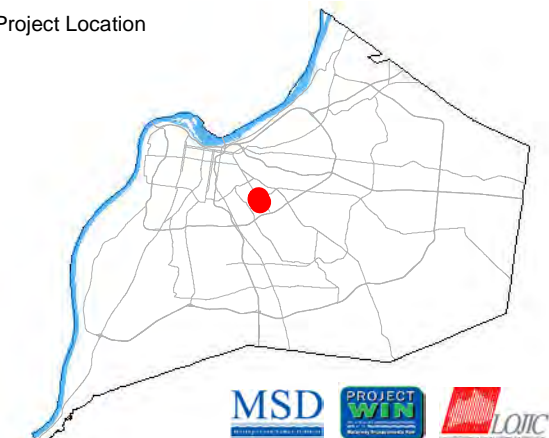
1 inch = 200 feet



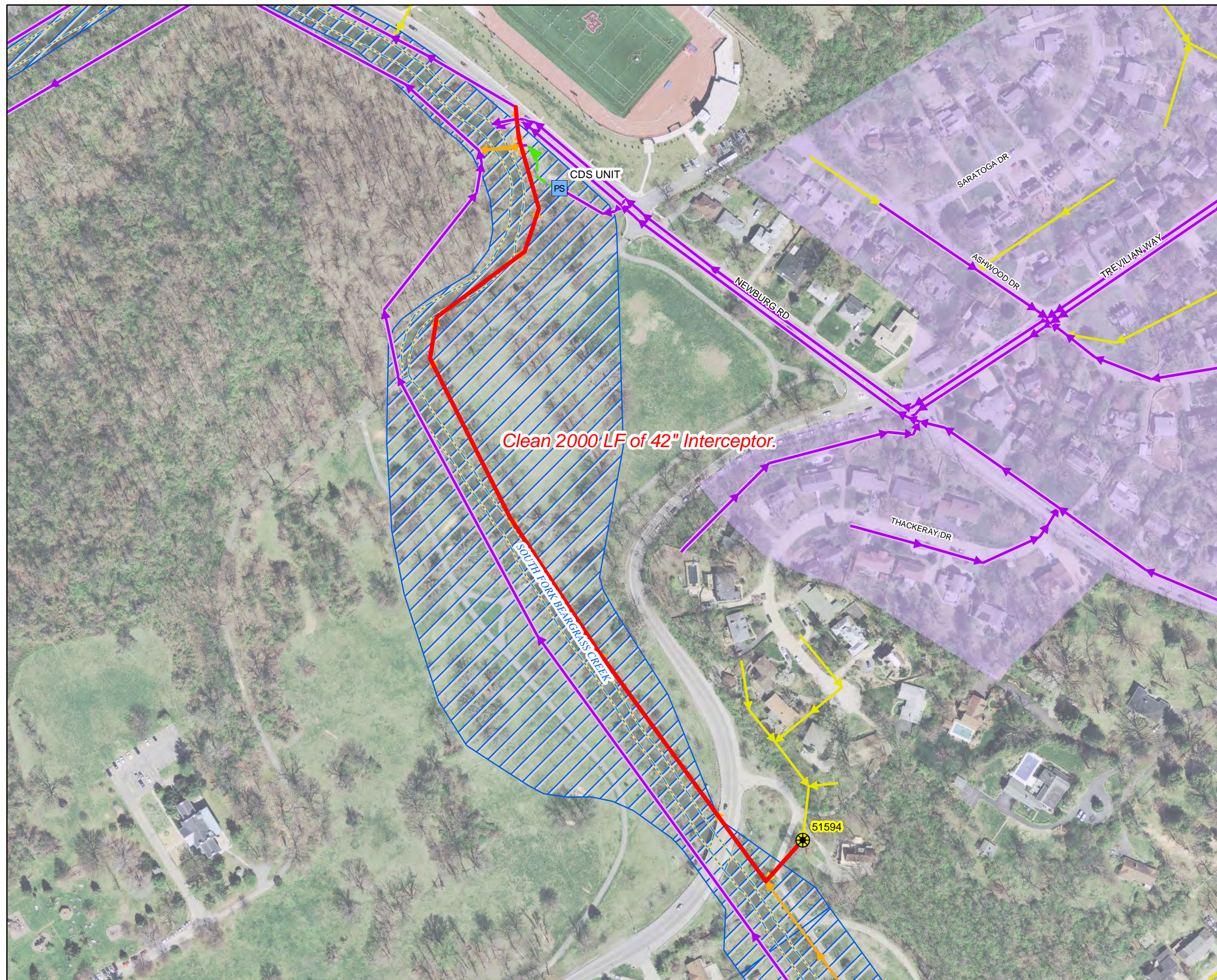
Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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Clean 2000 LF of 42" Interceptor.

SOUTH FORK BEARGRASS CREEK

CDS UNIT

PS

NEWBURG RD

SARATOGA DR

ASHWOOD DR

TREVILIAN WAY

THACKERAY DR

51594



<b>Project Name</b>	Klondike Interceptor
<b>Project Number</b>	S_SD_MF_NB04_S_01_B_A
<b>Modeled Area</b>	Southeastern Diversion
<b>Branch or SSO ID</b>	NB04
<b>Project Type</b>	Pipe Upgrades
<b>Receiving Stream</b>	South Fork Beargrass Creek
<b>Project Description</b>	This solution involves 2,830 LF of 30" gravity interceptor connecting to the Hikes Lane Interceptor where the Jeffersontown Branch 1 24" force main solution connects to the Hikes Lane Interceptor. The Southeast Diversion Branch 4 solution was priced with a 30" gravity interceptor constructed to the Hikes Lane Interceptor minus the cost of the 24" Jeffersontown force main along the same route.
<b>Reason for Overflow</b>	System Capacity
<b>Design Parameters</b>	This solution is based on a 2.25 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$558,000
<b>Weighted Benefit/Cost Ratio</b>	9.11

Asset ID	SSO Start Date	Volume (Gal)
25676	1/24/2002	100
25676	10/23/2007	459000
25676	10/3/2006	4680
66232	10/6/2013	37500
49513	10/6/2013	34500
25676	11/29/2011	22000
26650	11/29/2011	46000
25676	12/15/2007	351000
26650	12/5/2011	78500
25676	12/5/2011	57000
26651	12/5/2011	49500
66232	12/5/2011	62000
49513	12/5/2011	59500
25676	2/18/2000	0
25676	2/24/2011	19300
25676	3/12/2006	59800
25676	3/19/2008	20
26650	3/19/2008	150
25676	3/19/2008	380640
25676	3/4/2008	888300
26651	3/9/2011	145000
25676	3/9/2011	216250
26650	3/9/2011	124000
20644	4/12/2011	225000
26651	4/12/2011	179000
25676	4/12/2011	176500
26650	4/12/2011	156500

**Project Name** Klondike Interceptor

**Project Number** S\_SD\_MF\_NB04\_S\_01\_B\_A

26650	4/23/2011	99500
25676	4/23/2011	116000
49513	4/23/2011	83250
66232	4/23/2011	21500
20644	4/23/2011	255250
26651	4/23/2011	224000
25676	4/4/2008	452600
26651	4/4/2008	2511000
26650	5/2/2010	23000
25676	5/2/2010	110000
26651	5/2/2010	210000
49513	5/2/2010	72000
25676	5/3/2011	55000
20644	5/3/2011	114000
66232	5/3/2011	87500
26651	5/3/2011	102000
26650	5/3/2011	75000
49513	5/3/2011	72250
20644	6/22/2011	21500
49513	6/23/2011	26000
66232	6/23/2011	31500
25676	6/23/2011	32000
26650	6/23/2011	19000
25676	8/4/2009	110000
26650	8/4/2009	54000
25676	9/22/2006	4680



**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

**Southeast Diversion**

**Klondike Interceptor**

Preliminary - For Budget Development Only

- Documented SSO
- Suspected SSO
- Haulop Locations
- Pump Stations
- WQTC
- Proposed Pipe Solution
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Proposed Storage Solution
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

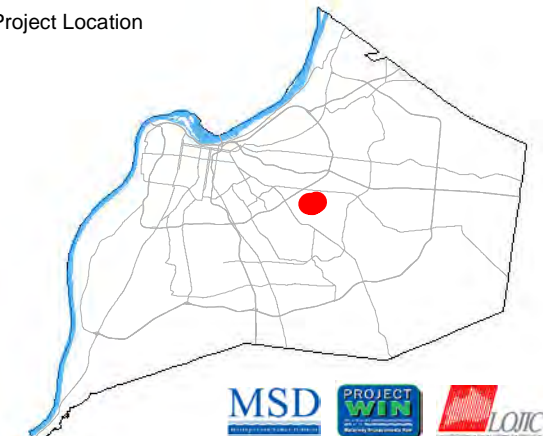
1 inch = 300 feet



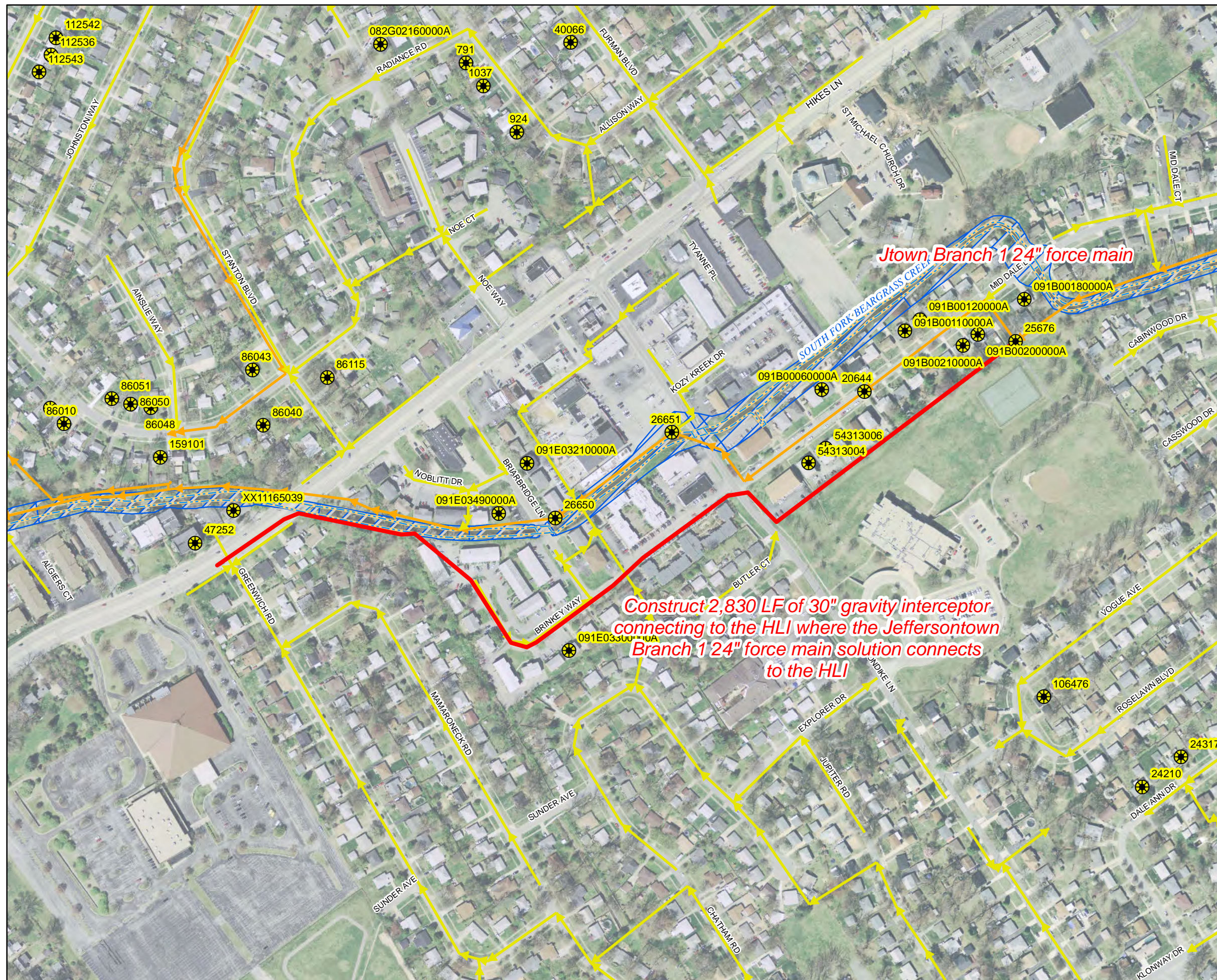
Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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**Project Name**     **Parkview Estates I/I Investigation & Rehabilitation**

**Project Number**     **S\_SD\_MF\_NB03\_S\_07\_C**

**Modeled Area**                     Southeastern Diversion

**Branch or SSO ID**                     NB03

**Project Type**                     Infiltration Reduction

**Receiving Stream**                     N/A

**Project Description**                     This location will be targeted for I/I source control (I/I rehab and private property program).

**Reason for Overflow**                     System Capacity

**Design Parameters**                     This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**                     N/A

**Estimated Capital Cost**                     \$285,000

**Weighted Benefit/Cost Ratio**                     --




















Asset ID	SSO Start Date	Volume (Gal)
47250	NO DATA	NO DATA



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Southeast Diversion  
 Solution ID # S\_SD\_MF\_NB03\_S\_07\_C  
 Parkview Estates I&I  
 Investigation & Rehabilitation

**Preliminary - For Budget Development Only**

**Legend**

-  Documented SSO
-  Suspected SSO
-  Haul Operation
-  Proposed Pump Station Solution
-  Pump Station
-  WWTP
-  Proposed Pipe Solution
-  Force Main
-  Collector < 12"
-  Interceptor => 12"
-  Combined Sewer Pipe
-  Proposed Off-line Storage
-  Road
-  Streams
-  Floodway
-  Small WWTP Service Area
-  Large WWTP Service Area
-  CSO Area
-  Metro Parks

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

1 inch equals 300 feet  
 Scalable when printed on 11" X 17" paper



Some boundaries are uniquely symbolized within the map.

Map Revision  
 May 7, 2009

Aerial Date: 2006



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<b>Project Name</b>	Sutherland Interceptor
<b>Project Number</b>	S_SD_MF_NB05_M_01_A
<b>Modeled Area</b>	Southeastern Diversion
<b>Branch or SSO ID</b>	NB05
<b>Project Type</b>	Pipe Upgrades
<b>Receiving Stream</b>	South Fork Beargrass Creek
<b>Project Description</b>	This alternative includes upsizing 10" interceptor to 670 LF of 18" and 1,070 LF of 15" interceptor along rear yards to eliminate Sutherland SSO possibly with pipe-bursting.
<b>Reason for Overflow</b>	System Capacity
<b>Design Parameters</b>	This solution is based on a 2.60 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$412,000
<b>Weighted Benefit/Cost Ratio</b>	32.71

Asset ID	SSO Start Date	Volume (Gal)
16649	1/13/2013	87906
16649	1/21/2010	240555
16649	1/24/2002	29000
16649	1/24/2010	269068
16649	1/26/2012	734325
16649	10/28/2009	44757
16649	10/31/2009	133357
16649	10/5/2013	75000
16649	10/9/2009	234426
16649	11/15/2011	133223
16649	11/17/2013	72000
16649	11/22/2011	219000
16649	11/25/2010	1350
16649	11/27/2011	944998
16649	11/30/2010	2635
16649	12/21/2013	26000
16649	12/24/2008	84000
16649	12/27/2011	71260
16649	12/5/2011	675369
16649	12/8/2009	70180
16649	2/1/2002	96000
16649	2/1/2011	320
16649	2/12/2008	74013
16649	2/24/2011	1429320
16649	2/28/2011	120120
16649	2/5/2010	241169
16649	2/6/2008	481013
16649	3/16/2012	2400
16649	3/17/2012	1500

Project Name	Sutherland Interceptor	
Project Number	S_SD_MF_NB05_M_01_A	
16649	3/18/2008	3058786
16649	3/19/2002	348000
16649	3/23/2012	1353678
16649	3/27/2008	1261809
16649	3/4/2008	1389212
16649	3/5/2011	78500
16649	3/8/2012	22543
16649	3/9/2011	245250
16649	4/11/2011	1259660
16649	4/19/2009	16548
16649	4/23/2011	1552249
16649	4/24/2010	7297
16649	4/27/2002	1
16649	4/29/2002	165000
16649	4/3/2009	8668
16649	5/1/2010	1130968
16649	5/12/2010	1000
16649	5/13/2002	318000
16649	5/16/2008	209000
16649	5/21/2010	200493
16649	5/23/2011	139591
16649	5/29/2012	32000
16649	5/8/2009	141974
16649	6/18/2009	20278
16649	6/22/2011	571551
16649	6/26/2009	268
16649	6/26/2013	3500
16649	6/9/2010	46884
16649	7/13/2010	1260
16649	7/27/2010	3750
16649	7/29/2009	35700
16649	7/30/2011	21254
16649	7/31/2010	1465
16649	8/13/2011	2625
16649	8/14/2010	780
16649	8/4/2009	568181
16649	8/7/2011	33386
16649	9/20/2009	47088
16649	9/26/2011	11885
















**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

**Southeast Diversion**


**Sutherland Interceptor**

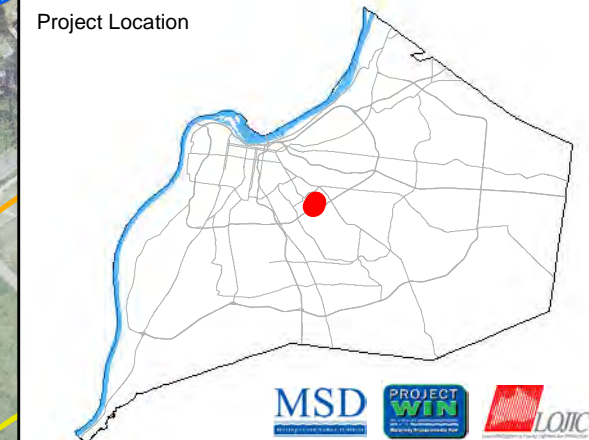
Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

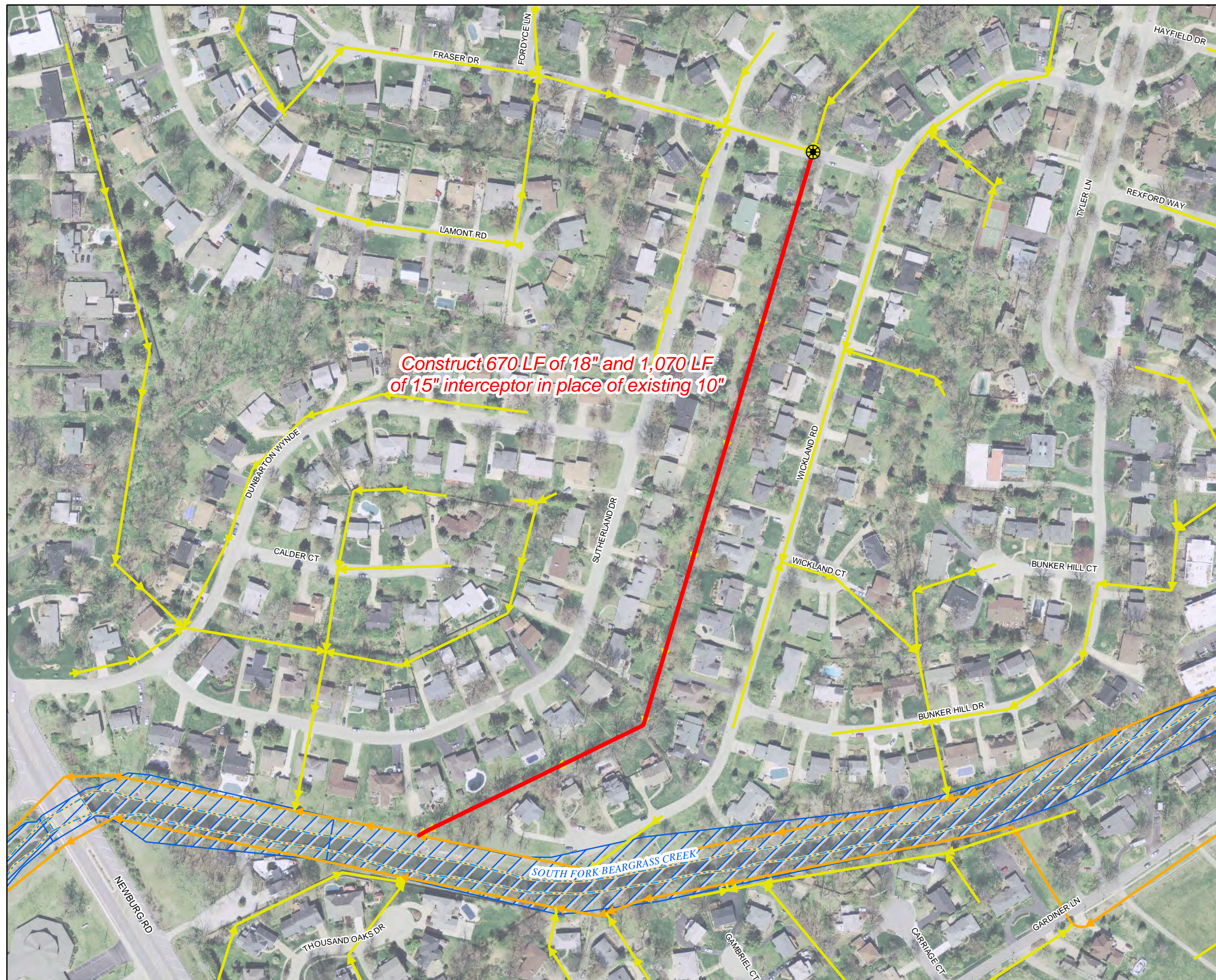
*Construct 670 LF of 18" and 1,070 LF of 15" interceptor in place of existing 10"*

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 200 feet		Aerial Date: 2009	Map Revision: April 9, 2012
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**Pond Creek  
Area**

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**Project Name**      **Avanti PS Elimination**

**Project Number**    **S\_PO\_WC\_PC07\_M\_01\_A**

**Modeled Area**              Pond Creek

**Branch or SSO ID**            PC07

**Project Type**                Diversion

**Receiving Stream**            Little Cedar Creek

**Project Description**        This alternative eliminates Avanti PS by constructing 150 LF of 8" pipe.

**Reason for Overflow**        Pump station capacity

**Design Parameters**        This solution is based on a 2.60 inch cloudburst rain event.

**Project Constraints**        N/A

**Estimated Capital Cost**     \$31,000

**Weighted Benefit/Cost Ratio**   1000.48




















Asset ID	SSO Start Date	Volume (Gal)
21229-W	NO DATA	NO DATA



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Pond Creek Sewershed  
 Solution ID # S\_PO\_WC\_PC07\_M\_01\_A  
 Avanti PS Elimination

**Preliminary - For Budget Development Only**

**Legend**

-  Documented SSO
-  Suspected SSO
-  Haul Operation
-  Proposed Pump Station Solution
-  Pump Station
-  WWTP
-  Proposed Pipe Solution
-  Force Main
-  Collector < 12"
-  Interceptor => 12"
-  Combined Sewer Pipe
-  Proposed Off-line Storage
-  Road
-  Streams
-  Floodway
-  Small WWTP Service Area
-  Large WWTP Service Area
-  CSO Area
-  Metro Parks

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

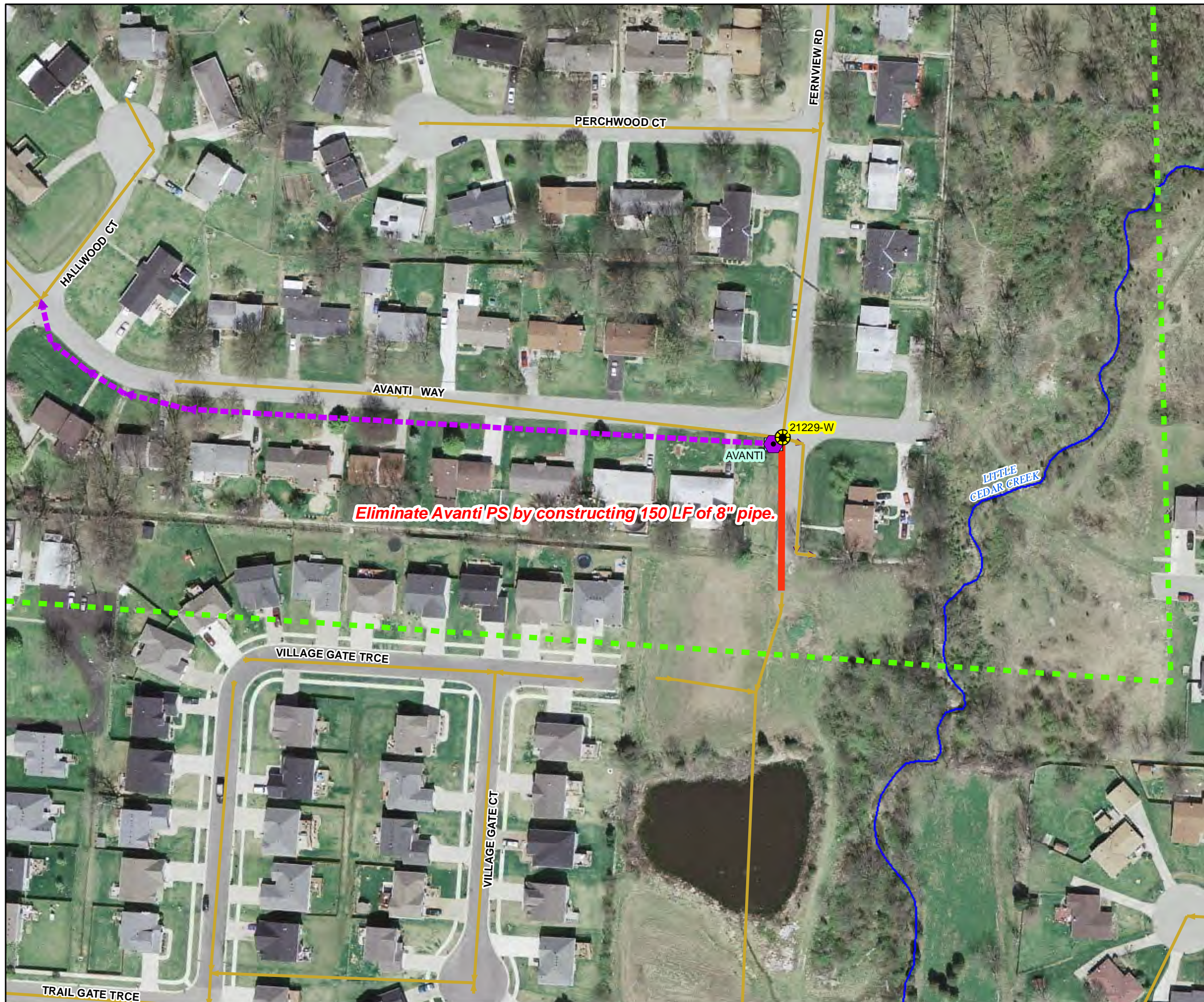
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 Scalable when printed on 11" X 17" paper



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 Map Revision  
 May 07, 2009  
 Aerial Date: 2006



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**Eliminate Avanti PS by constructing 150 LF of 8" pipe.**



<b>Project Name</b>	Caven Ave Pump Station Elimination
<b>Project Number</b>	S_PO_WC_PC09_M_09B_C
<b>Modeled Area</b>	Pond Creek
<b>Branch or SSO ID</b>	PC09
<b>Project Type</b>	PS Elimination
<b>Receiving Stream</b>	Pond Creek and Mud Creek
<b>Project Description</b>	This project includes the inspection and rehabilitation of the Caven Avenue Pump Station service area. The pump station will be eliminated and flow will diverted into newly constructed 10-inch sewer line to be connected to the Mud Creek Interceptor.
<b>Reason for Overflow</b>	System Capacity
<b>Design Parameters</b>	This solution is based on a 2.6 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$1,800,000
<b>Weighted Benefit/Cost Ratio</b>	155.27

Asset ID	SSO Start Date	Volume (Gal)
27116	1/11/2014	12000
27116	1/13/2013	261000
61687	1/13/2013	15000
61667	1/13/2013	120000
27116	1/26/2012	125000
27116	1/30/2013	66000
27116	10/1/2012	6375
27116	10/5/2013	6000
61667	10/6/2013	39000
27116	10/6/2013	43500
61687	10/6/2013	6000
27116	11/1/2013	3750
27116	11/15/2011	103500
27116	11/17/2013	31500
61687	11/22/2011	6000
27116	11/22/2011	135000
61667	11/22/2011	14250
27116	11/28/2011	212225
61687	11/28/2011	42250
61667	11/28/2011	84500
27116	12/20/2012	9000
MSD0133-PS	12/21/2013	22250
27116	12/21/2013	46750
27116	12/26/2012	33000
27116	12/27/2011	20000
27116	12/5/2011	217000
61687	12/5/2011	26175
61667	12/5/2011	105700

Project Name	Caven Ave Pump Station Elimination	
Project Number	S_PO_WC_PC09_M_09B_C	
27116	12/7/2012	42000
27116	12/9/2012	30000
27116	3/11/2013	66000
27116	3/17/2013	102000
27116	3/18/2012	17000
61687	3/23/2012	18000
27116	3/23/2012	5375
27116	3/23/2012	17750
61687	3/9/2011	100
61667	3/9/2011	15
27116	3/9/2012	200
27116	4/1/2012	24000
MSD0133-PS	4/4/2008	25500
27116	5/10/2013	60000
27116	5/13/2012	61000
61687	5/13/2012	31000
61667	5/13/2012	10625
17724	5/22/2005	60
27116	5/5/2012	22500
27116	5/5/2013	91000
27116	7/13/2011	100
27116	7/6/2011	5
27116	7/6/2013	30000
MSD0133-PS	8/4/2009	21250
27116	9/21/2013	108001
61687	9/26/2011	9000
17724	9/27/2003	15



**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

Derek R. Guthrie Sewershed

Caven Ave Pump Station Elimination

Preliminary - For Budget Development Only

- Documented SSO
- Suspected SSO
- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- MSD
- Proposed Pipe Solution
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Proposed Off-line Storage
- Streams
- Floodway
- Jefferson County Boundary

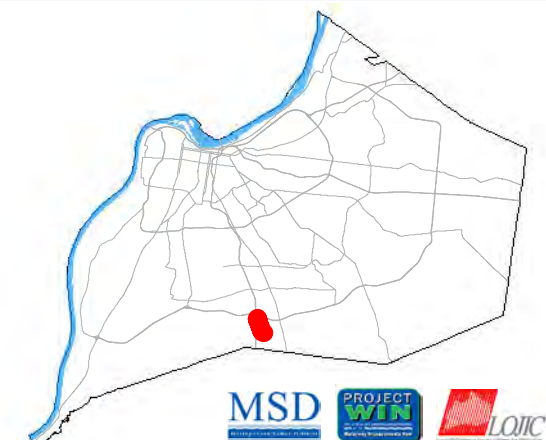
General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 500 feet

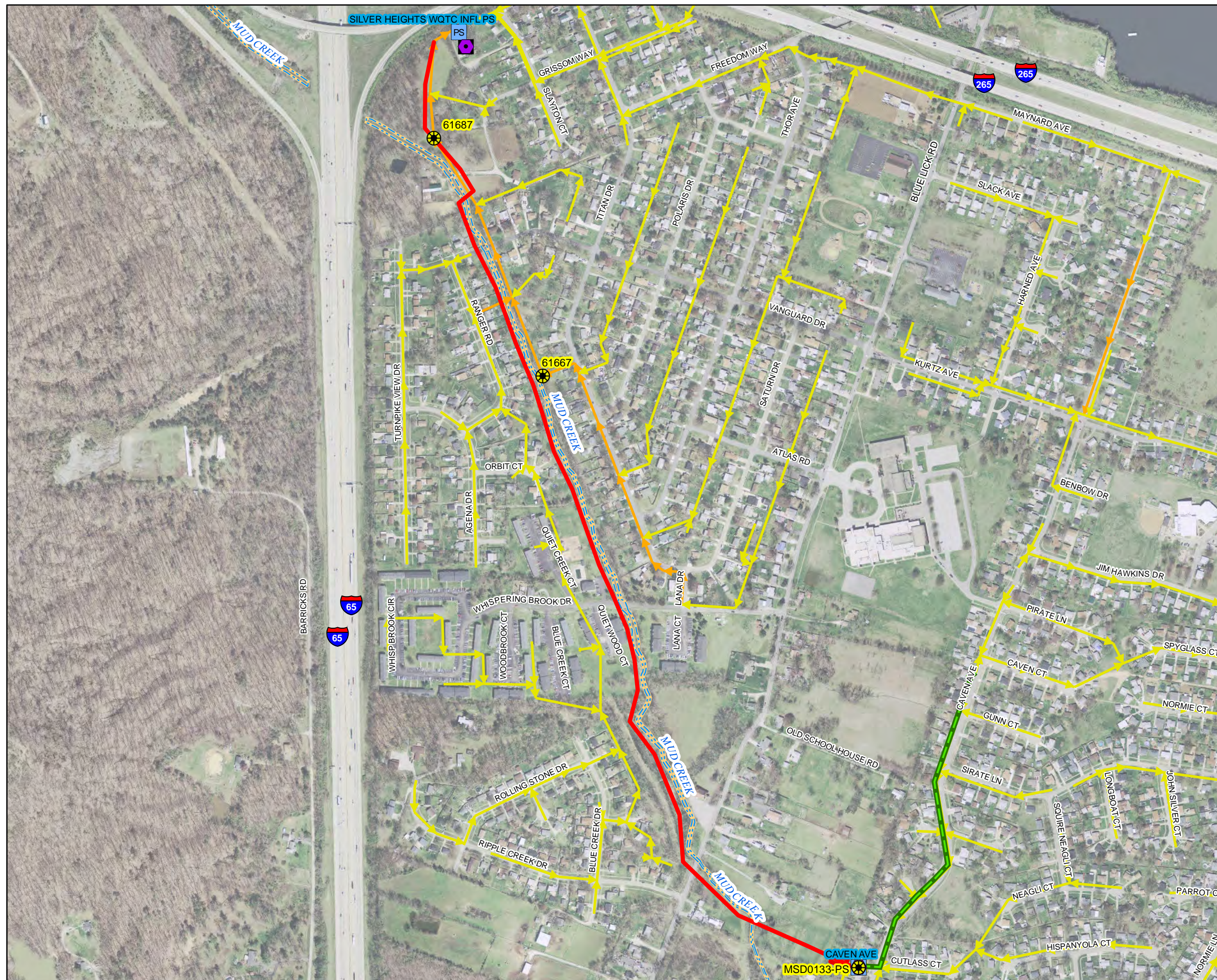


Aerial Date:  
2009

Map Revision:  
April 9, 2012



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**Project Name** Charleswood Interceptor Extension

**Project Number** S\_PO\_WC\_PC03\_M\_01\_C

**Modeled Area** Pond Creek

**Branch or SSO ID** PC03

**Project Type** Pipe Upgrades

**Receiving Stream** Fishpool Creek

**Project Description** This alternative includes upsizing 1,846 LF of open cut sewer (mostly in rock) downstream. This estimate does not include the Cooper Chapel PS elimination but the Charleswood Subdivision Interceptor will eliminate Cooper Chapel PS and require capacity increases downstream.

**Reason for Overflow** Pump station capacity

**Design Parameters** This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints** N/A

**Estimated Capital Cost** \$1,600,000

**Weighted Benefit/Cost Ratio** 62.84

Asset ID	SSO Start Date	Volume (Gal)
25479	1/13/2013	27500
MSD0130-PS	1/23/2006	7500
MSD0130-PS	1/24/2002	25000
25479	10/6/2013	20250
25480	11/11/2004	12000
25479	11/17/2013	7375
25479	11/22/2011	150
25479	11/28/2011	1200
25479	12/21/2013	1400
MSD0130-PS	12/21/2013	8250
25479	12/27/2011	750
25479	12/5/2011	30000
MSD0130-PS	3/11/2013	3125
25479	3/18/2013	3246
25479	5/13/2012	48375
MSD0130-PS	5/15/2008	3825
25480	5/2/2010	45900
25480	5/20/2005	1000
25479	5/5/2012	3500
25479	6/19/2011	640
MSD0130-PS	8/30/2005	2000
















**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

Pond Creek Sewershed

Charleswood Interceptor Extension

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  Proposed Pipe Solution
-  WQTC
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

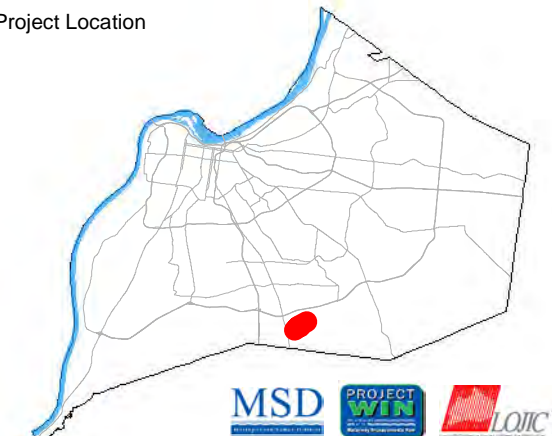
1 inch = 400 feet



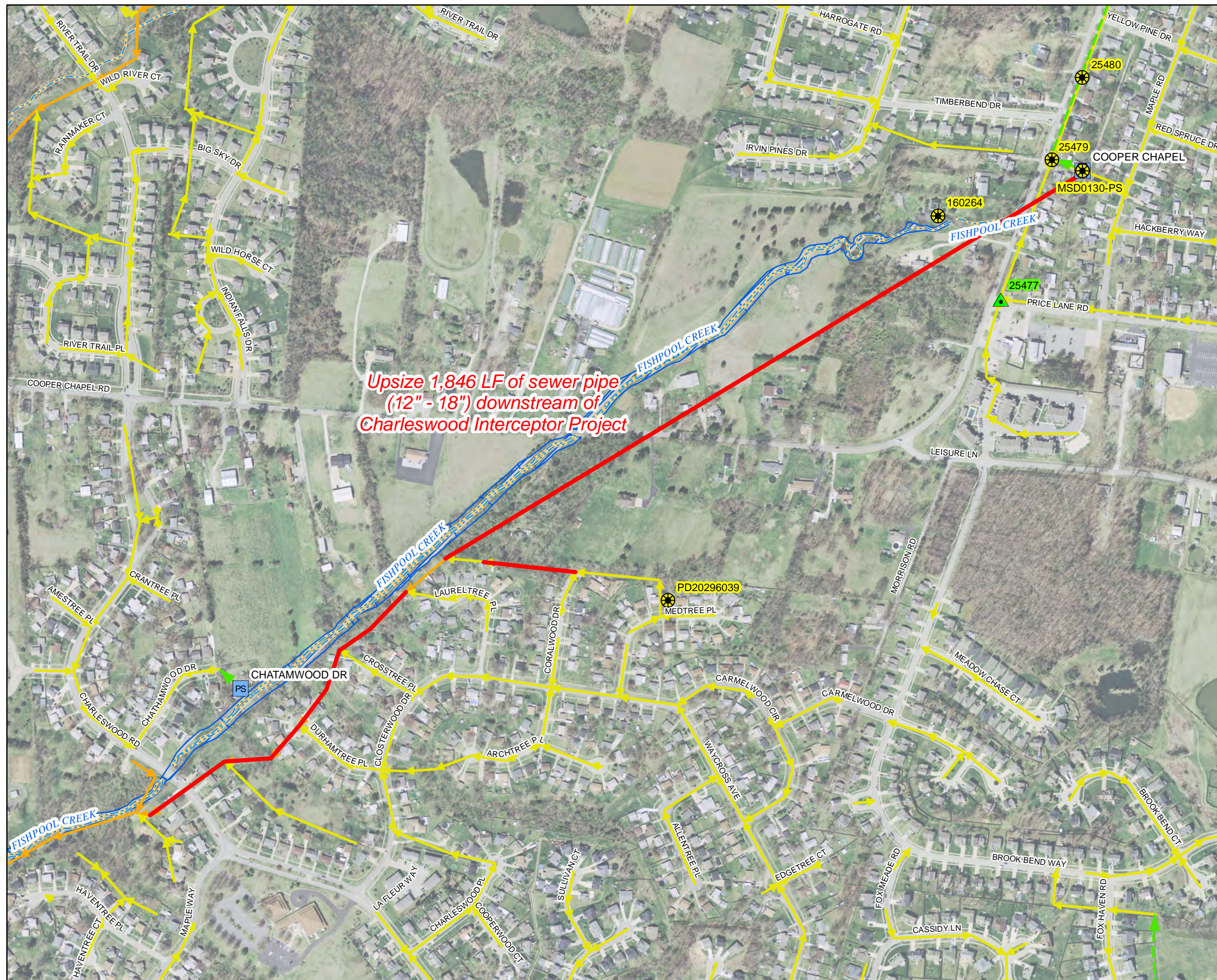
Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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<b>Project Name</b>	Cinderella PS Elimination
<b>Project Number</b>	S_PO_WC_PC04_M_01_C
<b>Modeled Area</b>	Pond Creek
<b>Branch or SSO ID</b>	PC04
<b>Project Type</b>	Diversion
<b>Receiving Stream</b>	Fishpool Creek and Manslick Branch
<b>Project Description</b>	This alternative eliminates Cinderella PS by constructing 2250 LF of 10" pipe. It will require 208 LF of tunneling under I-265.
<b>Reason for Overflow</b>	Pump station and system capacity
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$2,205,000
<b>Weighted Benefit/Cost Ratio</b>	43.86

Asset ID	SSO Start Date	Volume (Gal)
60679	1/13/2013	22750
MSD1013-PS	1/22/2006	2500
MSD1013-PS	1/27/2012	4700
35309	10/23/2007	650
35309	10/23/2007	21000
MSD1013-PS	10/6/2013	39750
MSD1013-PS	11/11/2004	16000
MSD1013-PS	11/2/2004	82000
60679	11/28/2011	17750
MSD1013-PS	11/29/2001	100000
60679	12/15/2007	8100
MSD1013-PS	12/17/2001	50000
MSD1013-PS	12/19/2002	15000
60679	12/22/2013	20500
MSD1013-PS	12/31/2002	50000
MSD1013-PS	12/31/2002	50000
60679	12/5/2011	145800
MSD1013-PS	2/22/2003	100000
60679	2/25/2011	83750
60679	2/25/2011	83750
60679	2/28/2011	11125
MSD1013-PS	3/18/2013	4625
MSD1013-PS	3/19/2002	50000
MSD1013-PS	3/19/2008	369000
60679	3/9/2011	38750
60679	4/12/2011	51000
60679	4/23/2011	54825
60679	4/27/2011	81000
MSD1013-PS	4/4/2008	96600

Project Name	Cinderella PS Elimination	
Project Number	S_PO_WC_PC04_M_01_C	
60679	5/13/2012	70000
MSD1013-PS	5/15/2008	38600
60679	5/26/2011	13250
60679	5/3/2011	99000
MSD1013-PS	5/30/2004	36000
MSD1013-PS	5/5/2012	10400
MSD1013-PS	8/30/2005	1000
MSD1013-PS	8/4/2009	9999
MSD1013-PS	9/26/2009	3300
MSD1013-PS	9/27/2002	15000
















**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

Pond Creek Sewershed

Cinderella PS Elimination

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

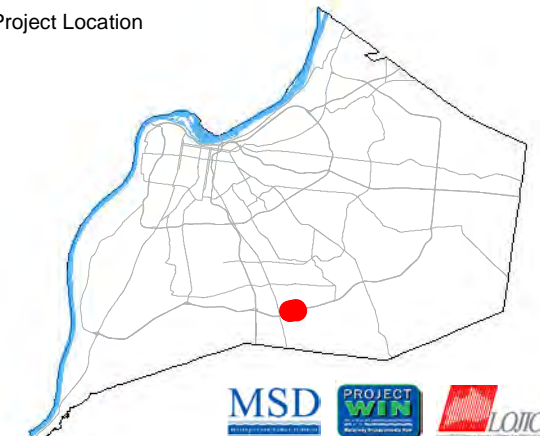
1 inch = 300 feet



Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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**Project Name**    **Edsel PS I/I Investigation & Rehabilitation**

**Project Number**    **S\_PO\_WC\_PC11\_M\_07\_C**

**Modeled Area**                      Pond Creek

**Branch or SSO ID**                      PC11

**Project Type**                              Infiltration Reduction

**Receiving Stream**                      Fern Creek

**Project Description**                      This location will be targeted for I/I source control (I/I rehab and private property program).

**Reason for Overflow**                      Pump station capacity and hydraulic bottlenecks

**Design Parameters**                      This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**                      N/A

**Estimated Capital Cost**                      \$367,000

**Weighted Benefit/Cost Ratio**                      --

Asset ID	SSO Start Date	Volume (Gal)
94009	2/25/2001	500
92099	2/25/2011	15750
92098	2/25/2011	15750
MSD1048-PS	3/19/2008	49500
MSD1048-PS	3/4/2008	94500
92099	3/9/2011	10400
94009	3/9/2011	10400
92098	4/12/2011	17550
92099	4/27/2011	127500
94009	4/27/2011	127500
MSD1048-PS	4/27/2011	25200
MSD1048-PS	4/4/2008	130500
92098	5/16/2008	3600
92099	5/2/2010	78900
92099	5/3/2011	8420
94009	5/3/2011	16840



# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Pond Creek Sewershed

Solution ID # S\_PO\_WC\_PC11\_M\_07\_C

Edsel PS I&I Investigation and Rehabilitation

**Preliminary - For Budget Development Only**

### Legend

- Documented SSO
- Suspected SSO
- Haul Operation
- Proposed Pump Station Solution
- Pump Station
- WWTP
- Proposed Pipe Solution
- Force Main
- Collector < 12"
- Interceptor => 12"
- Combined Sewer Pipe
- Proposed Off-line Storage
- Road
- Streams
- Floodway
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Metro Parks

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 400 feet  
Scalable when printed on 11" X 17" paper



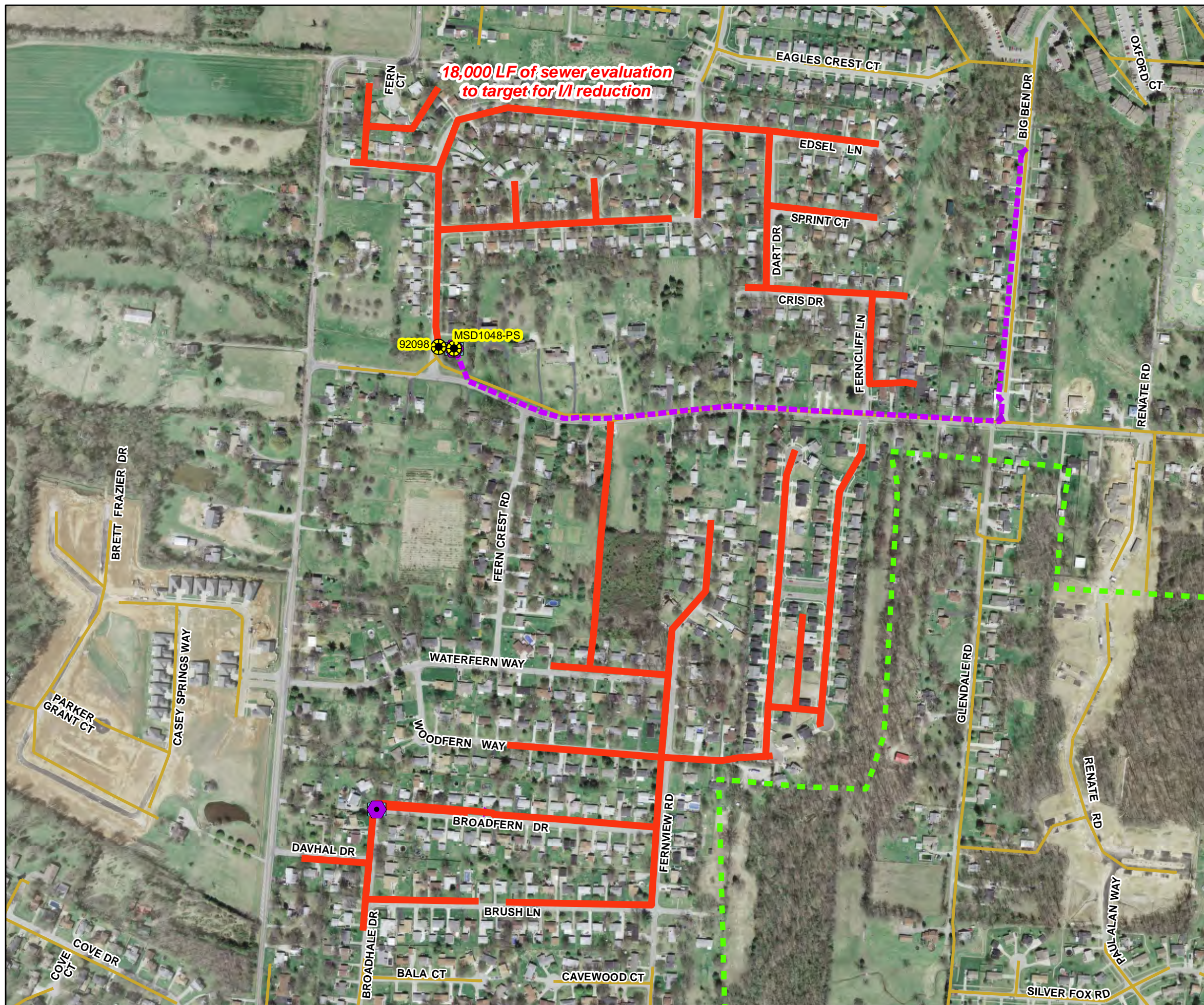
Some boundaries are uniquely symbolized within the map.

Map Revision  
May 07, 2009

Aerial Date: 2006



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






<b>Project Name</b>	Government Center PS Elimination
<b>Project Number</b>	S_PO_WC_PC06_M_01_C
<b>Modeled Area</b>	Pond Creek
<b>Branch or SSO ID</b>	PC06
<b>Project Type</b>	Off-line Storage & Pipe Upgrades
<b>Receiving Stream</b>	Pennsylvania Run
<b>Project Description</b>	This alternative eliminates Government Center PS by constructing 1,324 LF of 10" pipe. It will require 50 LF of tunneling.
<b>Reason for Overflow</b>	Pump station and system capacity
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$1,225,000
<b>Weighted Benefit/Cost Ratio</b>	44.91

Asset ID	SSO Start Date	Volume (Gal)
MSD0180-PS	1/3/2005	4700
MSD0180-PS	10/19/2004	20000
MSD0180-PS	11/11/2004	7000
MSD0180-PS	11/2/2004	27000
MSD0180-PS	12/16/2000	0
MSD0180-PS	12/19/2002	15000
MSD0180-PS	2/22/2003	300000
MSD0180-PS	2/24/2011	9999
MSD0180-PS	3/19/2002	50000
MSD0180-PS	3/19/2008	9825
MSD0180-PS	3/28/2005	1575
MSD0180-PS	4/4/2008	15590
MSD0180-PS	5/15/2008	12750
MSD0180-PS	5/2/2010	22300
MSD0180-PS	5/20/2005	1500
MSD0180-PS	5/28/2004	30000
MSD0180-PS	5/30/2004	30000
94541	7/29/2009	675
MSD0180-PS	7/29/2009	675
94542	7/29/2009	675
MSD0180-PS	8/30/2005	1000

**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Pond Creek Sewershed  
 Solution ID # S\_PO\_WC\_PC06\_M\_01\_C  
 Government Center PS Elimination

**Preliminary - For Budget Development Only**

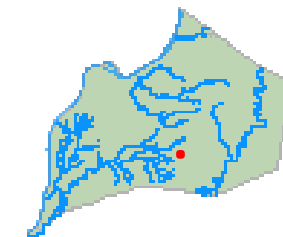
**Legend**

-  Documented SSO
-  Suspected SSO
-  Haul Operation
-  Proposed Pump Station Solution
-  Pump Station
-  WWTP
-  Proposed Pipe Solution
-  Force Main
-  Collector < 12"
-  Interceptor => 12"
-  Combined Sewer Pipe
-  Proposed Off-line Storage
-  Road
-  Streams
-  Floodway
-  Small WWTP Service Area
-  Large WWTP Service Area
-  CSO Area
-  Metro Parks

**Eliminate Government Center PS by  
 constructing 1,324 LF of 10" pipe.  
 50 LF of tunneling is required.**

**General representation of overflow  
 abatement solutions are for  
 preliminary planning purposes.  
 Alignments and locations may be  
 altered during design.**

1 inch = 200 feet  
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<b>Project Name</b>	Lantana PS #1 I/I Investigation and Rehabilitation
<b>Project Number</b>	S_PO_WC_PC05_M_07_C
<b>Modeled Area</b>	Pond Creek
<b>Branch or SSO ID</b>	PC05
<b>Project Type</b>	Infiltration Reduction
<b>Receiving Stream</b>	Pennsylvania Run
<b>Project Description</b>	This location will be targeted for I/I source control (I/I rehab and private property program). A full SSES will be performed upstream of Lantana PS.
<b>Reason for Overflow</b>	Pump station and system capacity
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$20,000
<b>Weighted Benefit/Cost Ratio</b>	--

Asset ID	SSO Start Date	Volume (Gal)
25484	1/13/2013	27000
MSD0101-PS	1/23/2006	7500
MSD0101-PS	1/24/2002	15000
25484	10/23/2007	37750
93719	10/23/2007	6200
25484	10/6/2013	10500
25484	11/17/2013	275
MSD0101-PS	11/2/2004	36000
25484	11/22/2011	2590
25484	11/28/2011	14600
93719	12/15/2007	5050
MSD0101-PS	12/16/2000	0
MSD0101-PS	12/19/2002	20000
25484	12/22/2013	350
25484	12/5/2011	60000
MSD0101-PS	2/22/2003	100000
MSD0101-PS	3/12/2006	10000
MSD0101-PS	3/18/2013	11250
MSD0101-PS	3/19/2002	50000
25484	3/19/2008	234000
93719	3/9/2011	48500
93719	4/12/2011	7750
25484	4/23/2011	12000
MSD0101-PS	4/25/2003	12000
25484	4/27/2011	432000
MSD0101-PS	5/2/2010	29000
93719	5/26/2011	1250
93719	5/3/2011	10200
MSD0101-PS	5/30/2004	57000



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**Project Name** Lantana PS #1 I/I Investigation and Rehabilitation

**Project Number** S\_PO\_WC\_PC05\_M\_07\_C




















MSD0101-PS	7/29/2009	10125
MSD0101-PS	8/30/2005	1000
MSD0101-PS	9/27/2002	10000



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Pond Creek Sewershed  
 Solution ID # S\_PO\_WC\_PC05\_M\_07\_C  
 Lantana #1 PS I/I Investigation & Rehabilitation

**Preliminary - For Budget Development Only**

**Legend**

-  Documented SSO
-  Suspected SSO
-  Haul Operation
-  Proposed Pump Station Solution
-  Pump Station
-  WWTP
-  Proposed Pipe Solution
-  Force Main
-  Collector < 12"
-  Interceptor => 12"
-  Combined Sewer Pipe
-  Proposed Off-line Storage
-  Road
-  Streams
-  Floodway
-  Small WWTP Service Area
-  Large WWTP Service Area
-  CSO Area
-  Metro Parks

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**Project Name**    [Lea Ann Way System Improvements](#)

**Project Number**    [S\\_PO\\_WC\\_PC08\\_M\\_01\\_C](#)

**Modeled Area**                      Pond Creek

**Branch or SSO ID**                      PC08

**Project Type**                              Pipe Upgrades and I&I Reductions

**Receiving Stream**                      Fern Creek and Northern Ditch

**Project Description**                      This project includes the construction of 3,255 LF of open cut sewer (12" to 18") to prevent overflows upstream of Lea Ann Way Pump Station. A full SSES for the Lea Ann Way service will be performed and significant sewer defects will be addressed. Flow monitoring will determine if the appropriate level of control has been met. If not, a new pump station may be built to divert flow from the low-lying Mile of Sunshine Drive area where the homes are at the highest risk of flooding due to surcharging. Additionally, a storage basin near the Lea Ann Way Pump Station may be constructed to achieve the level of control.

**Reason for Overflow**                      Pump station capacity

**Design Parameters**                      This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**                      N/A

**Estimated Capital Cost**                      \$827,000

**Weighted Benefit/Cost Ratio**                      49.01

Asset ID	SSO Start Date	Volume (Gal)
31073	1/11/2014	1625
31074	1/11/2014	1625
MSD1010-PS	1/13/2013	15250
MSD1200-PS	1/13/2013	32425
MSD1010-PS	1/13/2013	15250
MSD1010-PS	1/13/2013	15250
31074	1/13/2013	133740
31073	1/13/2013	27375
29948	1/13/2013	69750
MSD1010-PS	1/13/2013	4900
MSD1010-PS	1/26/2012	1040500
31073	1/26/2012	13000
31074	1/26/2012	13125
29948	1/26/2012	13500
29948	10/1/2012	4755
31073	10/1/2012	4500
31074	10/1/2012	9240
31073	10/5/2013	54510
29948	10/5/2013	8040
MSD1010-PS	10/5/2013	1125000
MSD1010-PS	10/5/2013	1125000
31074	10/5/2013	13980
MSD1010-PS	10/5/2013	60000
MSD1010-PS	10/5/2013	1125000
MSD1010-PS	11/17/2013	260000



Project Name	Lea Ann Way System Improvements	
Project Number	S_PO_WC_PC08_M_01_C	
31073	11/17/2013	20250
MSD1010-PS	11/17/2013	260000
29948	11/17/2013	9900
MSD1010-PS	11/17/2013	260000
31074	11/17/2013	48000
31073	11/22/2011	30015
31074	11/22/2011	10005
29948	11/22/2011	15250
29948	11/28/2011	87310
MSD1010-PS	11/28/2011	3756000
31074	11/28/2011	87310
31073	11/28/2011	43755
31073	12/10/2012	20000
31074	12/10/2012	12500
29948	12/10/2012	8500
MSD1010-PS	12/15/2007	1995000
31074	12/21/2013	36000
31073	12/22/2013	22500
29948	12/22/2013	10500
31074	12/26/2012	7380
31073	12/26/2012	7245
MSD1010-PS	12/5/2011	2964000
29948	12/5/2011	67740
31073	12/5/2011	33870
31074	12/5/2011	67740
31073	12/7/2012	21625
29948	12/7/2012	5000
31074	12/7/2012	19500
31074	12/8/2012	15000
31073	12/8/2012	12000
29948	12/8/2012	6000
31074	2/24/2011	11000
29948	2/24/2011	11000
31073	2/24/2011	11000
MSD1010-PS	2/25/2011	552000
31073	3/17/2012	3375
31074	3/17/2012	3375
MSD1010-PS	3/18/2013	662400
29948	3/18/2013	12000
31074	3/18/2013	12000
31073	3/18/2013	12000
MSD1010-PS	3/19/2008	3855000
29948	3/4/2008	100

Project Name	Lea Ann Way System Improvements	
Project Number	S_PO_WC_PC08_M_01_C	
MSD1010-PS	3/4/2008	2697000
29948	3/9/2011	40875
31074	3/9/2011	40825
31073	3/9/2011	3450
MSD1010-PS	3/9/2011	4935000
31073	3/9/2011	9225
29948	4/1/2012	1250
31073	4/1/2012	1425
31074	4/1/2012	2850
29948	4/11/2011	43200
31074	4/11/2011	43300
31073	4/11/2011	43250
MSD1010-PS	4/12/2011	432000
MSD1010-PS	4/12/2011	1143000
MSD1010-PS	4/12/2011	432000
MSD1010-PS	4/12/2011	1143000
MSD1010-PS	4/23/2011	350000
31074	4/23/2011	1890
29948	4/23/2011	1890
31073	4/23/2011	1890
MSD1010-PS	4/23/2011	56250
MSD1010-PS	4/23/2011	315000
MSD1010-PS	4/23/2011	126000
MSD1010-PS	4/24/2011	1860000
MSD1010-PS	4/24/2011	744000
31073	4/24/2011	7750
MSD1010-PS	4/24/2011	720000
MSD1010-PS	4/24/2011	1800000
29948	4/24/2011	6300
31074	4/24/2011	7750
31074	4/27/2011	40500
29948	4/27/2011	40500
MSD1010-PS	4/4/2008	6276200
29948	4/4/2008	50
31074	5/13/2012	25260
29948	5/13/2012	11125
31073	5/13/2012	24990
MSD1010-PS	5/16/2008	297000
MSD1010-PS	5/2/2010	2720000
31074	5/2/2010	23050
31073	5/2/2010	23000
29948	5/2/2010	23000
31073	5/3/2011	18700

Project Name	Lea Ann Way System Improvements	
Project Number	S_PO_WC_PC08_M_01_C	
29948	5/3/2011	18700
31074	5/3/2011	18700
MSD1010-PS	5/3/2011	828000
MSD1010-PS	5/3/2011	738000
MSD1010-PS	5/3/2011	1230000
MSD1010-PS	5/3/2011	861000
29948	5/8/2009	360
29948	6/18/2009	6600
MSD1010-PS	6/23/2011	193500
MSD1010-PS	6/23/2011	193500
MSD1010-PS	6/23/2011	193500
31073	6/26/2013	4250
29948	6/26/2013	5250
31074	6/26/2013	4500
MSD1010-PS	7/29/2009	30000
MSD1010-PS	8/4/2009	468000
31073	9/21/2013	23040
31074	9/21/2013	34560

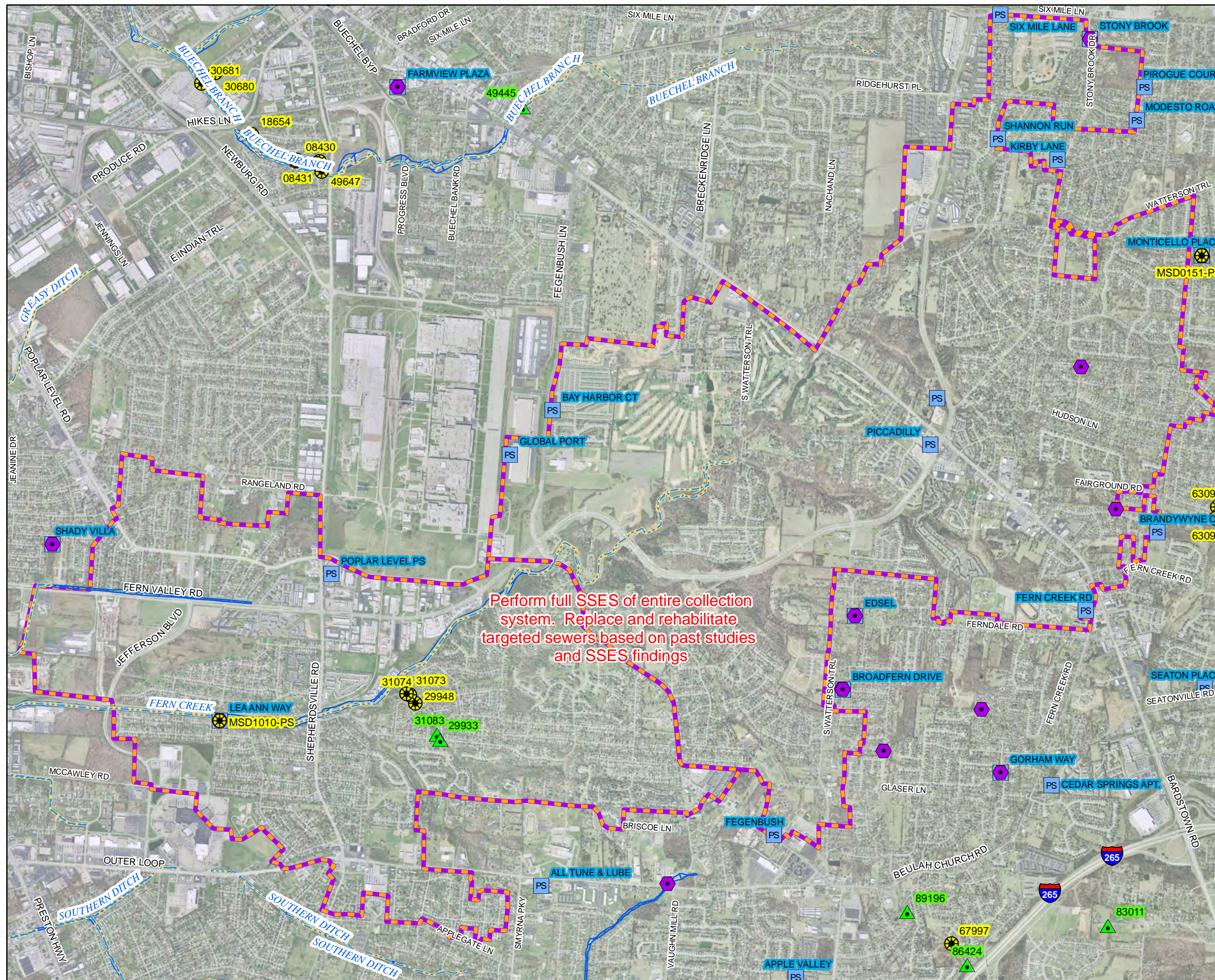


**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan**

**Pond Creek Sewershed**

**Lea Ann Way PS System Improvement**

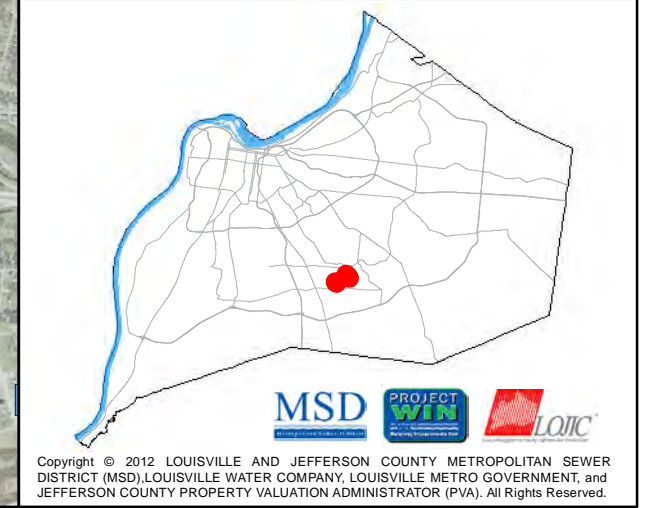
Preliminary - For Budget Development Only



- Documented SSO
- Suspected SSO
- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- MSD
- Streams
- Floodway
- SSES Area
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 2,448 feet Aerial Date: 2009 Map Revision: April 9, 2012





**Project Name**    **Leven PS Elimination**

**Project Number**    **S\_PO\_WC\_PC10\_M\_01\_C**

**Modeled Area**                      Pond Creek

**Branch or SSO ID**                      PC10

**Project Type**                              Diversion

**Receiving Stream**                      Pennsylvania Run

**Project Description**                      This alternative eliminates Leven PS by constructing 890 LF of 10" pipe. Existing PS and FM will remain functional but dormant to allow for monitoring downstream impacts of the new diversion. If no impacts are noted, the PS will be eliminated and FM taken out of service. If downstream impacts arise, the PS will be reconfigured to supplement the capacity of the new diversion line.

**Reason for Overflow**                      Pump station capacity and hydraulic bottlenecks

**Design Parameters**                      This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**                      N/A

**Estimated Capital Cost**                      \$376,000

**Weighted Benefit/Cost Ratio**                      95.93

<b>Asset ID</b>	<b>SSO Start Date</b>	<b>Volume (Gal)</b>
36419	11/29/2011	775
36419	NO DATA	NO DATA



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Pond Creek Sewershed  
 Solution ID # S\_PO\_WC\_PC10\_M\_01\_C  
 Leven PS Elimination

**Preliminary - For Budget Development Only**

**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- Proposed Pump Station Solution
- Pump Station
- WWTP
- Proposed Pipe Solution
- Force Main
- Collector < 12"
- Interceptor => 12"
- Combined Sewer Pipe
- Proposed Off-line Storage
- Road
- Streams
- Floodway
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Metro Parks

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

1 inch = 100 feet  
 Scalable when printed on 11" X 17" paper



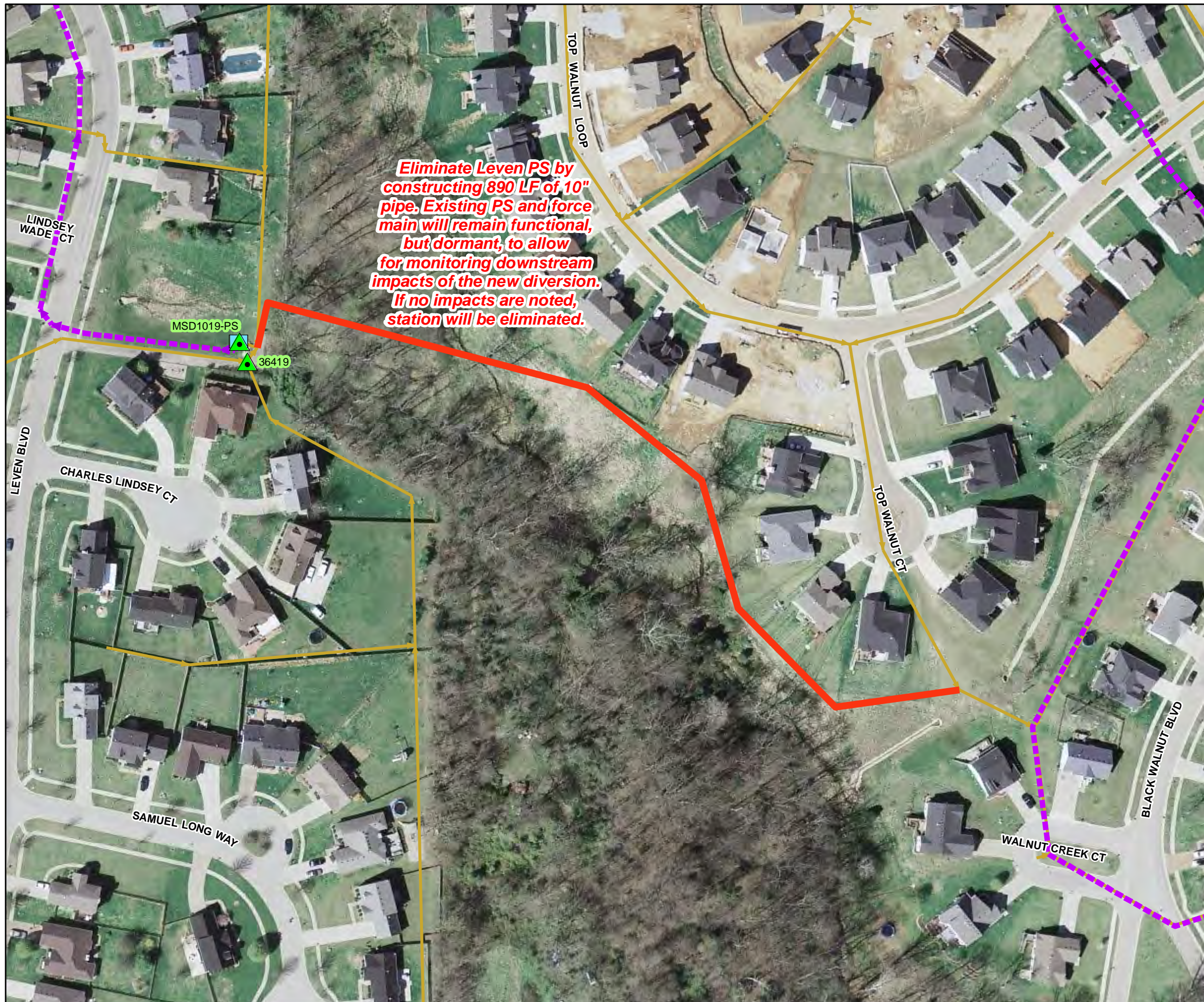
Some boundaries are uniquely symbolized within the map.

Map Revision  
 May 7, 2009

Aerial Date: 2006



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**Ohio River Force  
Main Area**

**Project Name**     Derington Ct. PS I/I Investigation & Rehabilitation

**Project Number**   S\_OR\_MF\_NB03\_S\_07\_C

**Modeled Area**             ORFM

**Branch or SSO ID**         NB03

**Project Type**             Infiltration Reduction

**Receiving Stream**         Goose Creek

**Project Description**       This location will be targeted for I/I source control (I/I rehab and private property program).

**Reason for Overflow**       Pump station capacity

**Design Parameters**        This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**        N/A

**Estimated Capital Cost**     \$265,000

**Weighted Benefit/Cost Ratio**  --

Asset ID	SSO Start Date	Volume (Gal)
MSD0095-PS	1/1/2003	3000
MSD0095-PS	3/19/2008	20500
MSD0095-PS	3/4/2008	400
MSD0095-PS	4/4/2008	54000
MSD0095-PS	5/8/2009	3800
20155	7/29/2009	2625
20155	8/4/2009	5500



# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Ohio River Force Main Sewershed




















Solution ID # S\_OR\_MF\_NB03\_S\_07\_C

Derington Ct. PS I&I

Investigation & Rehabilitation

**Preliminary - For Budget Development Only**

### Legend

-  Documented SSO
-  Suspected SSO
-  Haul Operation
-  Proposed Pump Station Solution
-  Pump Station
-  WWTP
-  Proposed Pipe Solution
-  Force Main
-  Collector < 12"
-  Interceptor => 12"
-  Combined Sewer Pipe
-  Proposed Off-line Storage
-  Road
-  Streams
-  Floodway
-  Small WWTP Service Area
-  Large WWTP Service Area
-  CSO Area
-  Metro Parks

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

1 inch equals 300 feet  
Scalable when printed on 11" X 17" paper



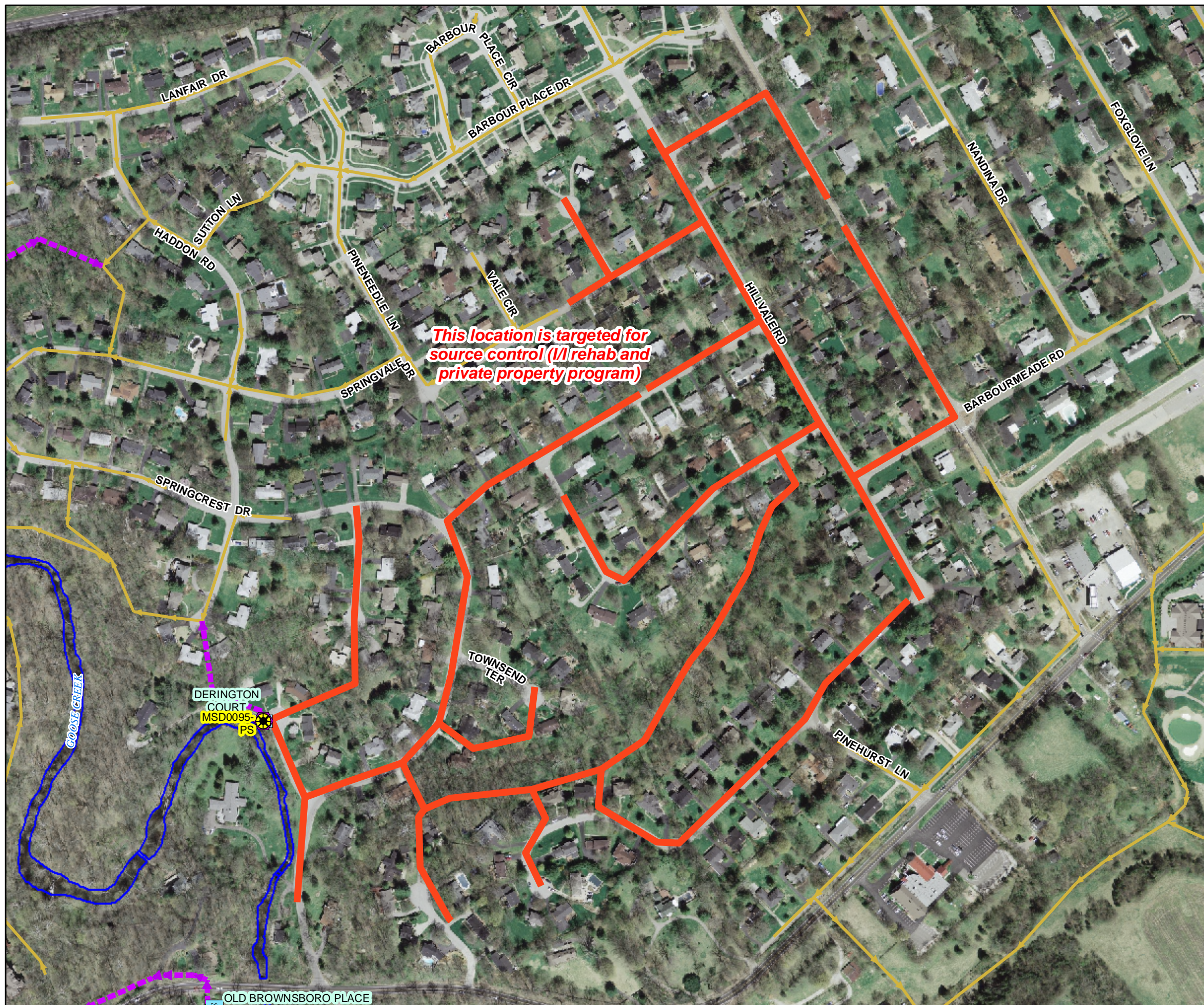
Some boundaries are uniquely symbolized within the map.

Map Revision  
May 7, 2009

Aerial Date: 2006



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**Project Name** Leland Road SSO Investigation

**Project Number** S\_OR\_MF\_NB02\_S\_13\_C

**Modeled Area** ORFM

**Branch or SSO ID** NB02

**Project Type** Pipe Upgrades

**Receiving Stream** Cherrywood Creek

**Project Description** The overflow at Leland Road had only been documented to overflow once. The overflow location was monitored for three years and no additional overflows were witnessed. As such, no further action for overflow mitigation will be undertaken.

**Reason for Overflow** Hydraulic bottleneck

**Design Parameters** Project Eliminated.

**Project Constraints** Project Eliminated

**Estimated Capital Cost** Project Eliminated

**Weighted Benefit/Cost Ratio** Project Eliminated

Asset ID	SSO Start Date	Volume (Gal)
96020	3/12/2006	20



# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Ohio River Force Main Sewershed

Solution ID # S\_OR\_MF\_NB02\_S\_13\_C

Leland Rd SSO Investigation

**Preliminary - For Budget Development Only**

### Legend

- Documented SSO
- Suspected SSO
- Haul Operation
- Proposed Pump Station Solution
- Pump Station
- WWTP
- Proposed Pipe Solution
- Force Main
- Collector < 12"
- Interceptor => 12"
- Combined Sewer Pipe
- Proposed Off-line Storage
- Road
- Streams
- Floodway
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Metro Parks

**Perform periodic condition assessment for three years and monitor location during rain events.**

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

1 inch equals 300 feet  
Scalable when printed on 11" X 17" paper



Some boundaries are uniquely symbolized within the map.

Map Revision  
May 7, 2009

Aerial Date: 2006



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<b>Project Name</b>	Mellwood System Improvements & PS Elimination - Mellwood PS and FM Improvements
<b>Project Number</b>	S_OR_MF_NB01_M_01_B
<b>Modeled Area</b>	ORFM
<b>Branch or SSO ID</b>	NB01
<b>Project Type</b>	Pump Station Upgrades, Pipe Upgrades, & Diversion
<b>Receiving Stream</b>	Muddy Fork Beargrass Creek
<b>Project Description</b>	This alternative includes a total pump station upgrade to 3.5 MGD and replacement of approximately 1,240 LF of 6" of force main with 15" for Mellwood Ave PS (PS needs to be flood-proofed due to its proximity to the Ohio River).
<b>Reason for Overflow</b>	Pump station capacity & system capacity
<b>Design Parameters</b>	This solution is based on a 2.25 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$2,168,000
<b>Weighted Benefit/Cost Ratio</b>	26.97

Asset ID	SSO Start Date	Volume (Gal)
26752	1/13/2013	77500
41374	1/13/2013	27000
MSD0023-PS	1/14/2007	100
MSD0023-PS	1/16/2007	1000
MSD0023-PS	1/16/2007	25
MSD0023-PS	1/2/2004	0
MSD0023-PS	1/22/2010	12750
MSD0023-PS	1/25/2010	1800
26752	1/26/2012	67500
MSD0023-PS	1/4/2004	12000
MSD0023-PS	1/4/2004	0
MSD0023-PS	1/4/2004	68400
MSD0023-PS	10/23/2007	14400
26752	10/5/2013	226000
41374	10/6/2013	74500
26752	11/17/2013	79500
26752	11/22/2011	32000
41374	11/28/2011	504000
26752	11/28/2011	758000
MSD0023-PS	11/29/2011	9999
MSD0023-PS	12/13/2007	20500
MSD0023-PS	12/15/2007	151200
MSD0006-PS	12/19/2002	115500
41374	12/22/2013	62000
26752	12/5/2011	504000
26752	12/9/2012	32000
41374	2/25/2011	157000
41374	2/28/2011	7950



**Project Name** Mellwood System Improvements & PS Elimination - Mellwood PS and FM Improvements

**Project Number** S\_OR\_MF\_NB01\_M\_01\_B














MSD0023-PS	2/3/2004	156000
MSD0023-PS	2/5/2004	714000
MSD0023-PS	2/5/2010	9000
MSD0023-PS	2/6/2008	120750
MSD0023-PS	3/10/2011	9999
MSD0023-PS	3/18/2008	936000
26752	3/18/2013	65500
41374	3/18/2013	27000
MSD0007-PS	3/20/2002	3000
MSD0007-PS	3/26/2002	2000
41374	3/27/2008	100
MSD0023-PS	3/27/2008	225000
MSD0023-PS	3/4/2008	67500
26752	3/9/2011	315000
41374	3/9/2011	263000
26752	4/1/2012	2025
41374	4/11/2011	34500
MSD0023-PS	4/13/2004	150000
MSD0023-PS	4/13/2011	9999
MSD0023-PS	4/14/2007	1500
MSD0023-PS	4/19/2009	12000
MSD0023-PS	4/22/2011	9999
41374	4/23/2011	1750000
MSD0023-PS	4/25/2004	81000
26752	4/26/2011	156000
MSD0023-PS	4/3/2008	456000
MSD0023-PS	4/3/2009	6750
MSD0023-PS	5/1/2004	1495200
26752	5/12/2010	100
MSD0023-PS	5/16/2008	9000
MSD0023-PS	5/16/2009	7750
41374	5/2/2010	57000
MSD0023-PS	5/2/2010	81000
26752	5/2/2010	97000
26752	5/26/2011	3200
MSD0023-PS	5/27/2004	2196000
26752	5/29/2012	35000
26752	5/3/2011	215000
MSD0023-PS	5/31/2004	1434000
MSD0010-PS	5/5/2003	7000
26752	5/8/2011	100
26752	6/23/2011	345000
26752	6/26/2013	6500

Project Name	Mellwood System Improvements & PS Elimination - Mellwood PS and FM Improvements	
Project Number	S_OR_MF_NB01_M_01_B	
41374	6/27/2013	7500
26752	7/29/2009	260000
MSD0023-PS	7/29/2009	999999999
MSD0023-PS	7/31/2009	16500
MSD0023-PS	8/11/2009	4000
MSD0023-PS	8/30/2005	200
26752	8/4/2009	340000
MSD0007-PS	8/4/2009	9999
41374	8/4/2009	240000
MSD0023-PS	8/4/2009	9999
MSD0006-PS	9/15/2002	30000
MSD0007-PS	9/20/2002	2000
41374	9/26/2011	126500
26752	9/26/2011	156000
MSD0006-PS	9/27/2002	2000



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Ohio River Force Main Sewershed  
**Mellwood System Improvements & PS Eliminations 1 - Mellwood PS & Force Main**

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

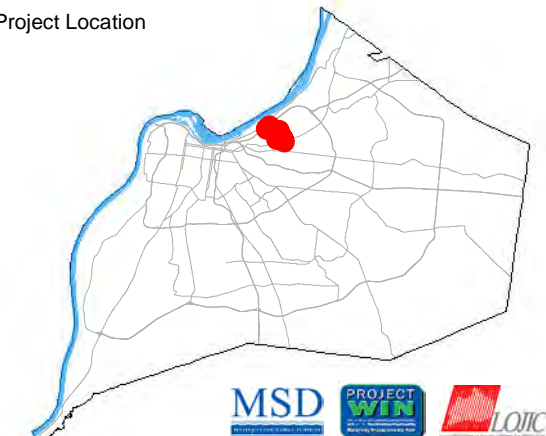
1 inch = 200 feet



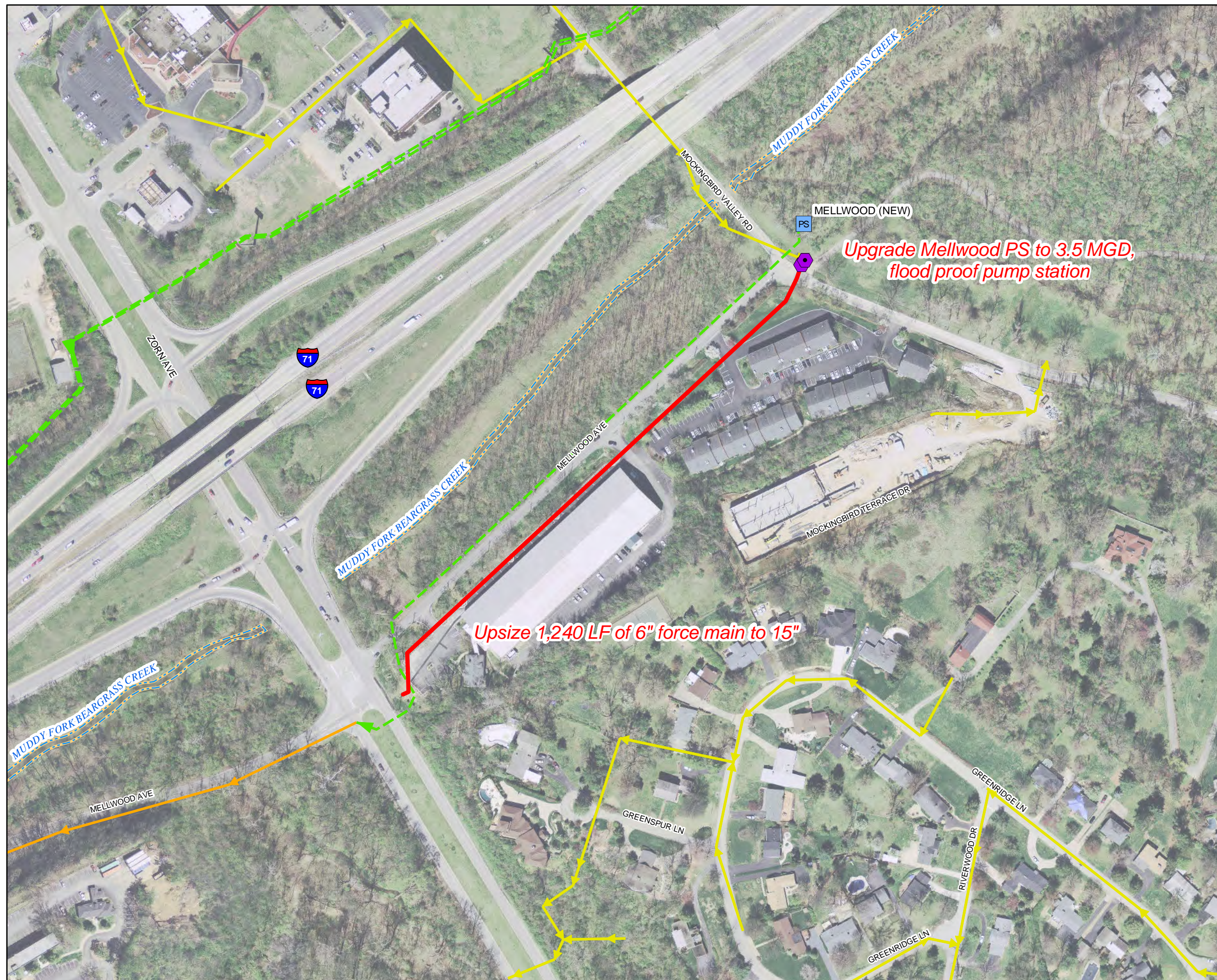
Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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<b>Project Name</b>	Mellwood System Improvements & PS Elimination - Winton and Mockingbird Valley Elimination
<b>Project Number</b>	S_OR_MF_NB01_M_01_B
<b>Modeled Area</b>	ORFM
<b>Branch or SSO ID</b>	NB01
<b>Project Type</b>	Pump Station Upgrades, Pipe Upgrades, & Diversion
<b>Receiving Stream</b>	Muddy Fork Beargrass Creek
<b>Project Description</b>	This alternative includes the replacement of approximately 1,890 LF of 8" gravity sewer flowing into Mockingbird Valley PS, installation of 400 LF of 8" pipe for Winton Diversion and 2210 LF of 15" pipe for Mockingbird Diversion. 300 LF of the sewer is tunneled. Winton and Mockingbird Valley pump stations will be eliminated.
<b>Reason for Overflow</b>	Pump station capacity & system capacity
<b>Design Parameters</b>	This solution is based on a 2.25 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$887,000
<b>Weighted Benefit/Cost Ratio</b>	26.97

Asset ID	SSO Start Date	Volume (Gal)
26752	1/13/2013	77500
41374	1/13/2013	27000
MSD0023-PS	1/14/2007	100
MSD0023-PS	1/16/2007	25
MSD0023-PS	1/16/2007	1000
MSD0023-PS	1/2/2004	0
MSD0023-PS	1/22/2010	12750
MSD0023-PS	1/25/2010	1800
26752	1/26/2012	67500
MSD0023-PS	1/4/2004	12000
MSD0023-PS	1/4/2004	0
MSD0023-PS	1/4/2004	68400
MSD0023-PS	10/23/2007	14400
26752	10/5/2013	226000
41374	10/6/2013	74500
26752	11/17/2013	79500
26752	11/22/2011	32000
26752	11/28/2011	758000
41374	11/28/2011	504000
MSD0023-PS	11/29/2011	9999
MSD0023-PS	12/13/2007	20500
MSD0023-PS	12/15/2007	151200
MSD0006-PS	12/19/2002	115500
41374	12/22/2013	62000
26752	12/5/2011	504000
26752	12/9/2012	32000
41374	2/25/2011	157000

**Project Name** Mellwood System Improvements & PS Elimination - Winton and Mockingbird Valley Elimination

**Project Number** S\_OR\_MF\_NB01\_M\_01\_B

41374	2/28/2011	7950
MSD0023-PS	2/3/2004	156000
MSD0023-PS	2/5/2004	714000
MSD0023-PS	2/5/2010	9000
MSD0023-PS	2/6/2008	120750
MSD0023-PS	3/10/2011	9999
MSD0023-PS	3/18/2008	936000
26752	3/18/2013	65500
41374	3/18/2013	27000
MSD0007-PS	3/20/2002	3000
MSD0007-PS	3/26/2002	2000
MSD0023-PS	3/27/2008	225000
41374	3/27/2008	100
MSD0023-PS	3/4/2008	67500
41374	3/9/2011	263000
26752	3/9/2011	315000
26752	4/1/2012	2025
41374	4/11/2011	34500
MSD0023-PS	4/13/2004	150000
MSD0023-PS	4/13/2011	9999
MSD0023-PS	4/14/2007	1500
MSD0023-PS	4/19/2009	12000
MSD0023-PS	4/22/2011	9999
41374	4/23/2011	1750000
MSD0023-PS	4/25/2004	81000
26752	4/26/2011	156000
MSD0023-PS	4/3/2008	456000
MSD0023-PS	4/3/2009	6750
MSD0023-PS	5/1/2004	1495200
26752	5/12/2010	100
MSD0023-PS	5/16/2008	9000
MSD0023-PS	5/16/2009	7750
41374	5/2/2010	57000
MSD0023-PS	5/2/2010	81000
26752	5/2/2010	97000
26752	5/26/2011	3200
MSD0023-PS	5/27/2004	2196000
26752	5/29/2012	35000
26752	5/3/2011	215000
MSD0023-PS	5/31/2004	1434000
MSD0010-PS	5/5/2003	7000
26752	5/8/2011	100
26752	6/23/2011	345000

**Project Name** Mellwood System Improvements & PS Elimination - Winton and Mockingbird Valley Elimination

**Project Number** S\_OR\_MF\_NB01\_M\_01\_B

26752	6/26/2013	6500
41374	6/27/2013	7500
26752	7/29/2009	260000
MSD0023-PS	7/29/2009	99999999
MSD0023-PS	7/31/2009	16500
MSD0023-PS	8/11/2009	4000
MSD0023-PS	8/30/2005	200
41374	8/4/2009	240000
26752	8/4/2009	340000
MSD0007-PS	8/4/2009	9999
MSD0023-PS	8/4/2009	9999
MSD0006-PS	9/15/2002	30000
MSD0007-PS	9/20/2002	2000
41374	9/26/2011	126500
26752	9/26/2011	156000
MSD0006-PS	9/27/2002	2000
















# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Ohio River Force Main Sewershed  
Mellwood System Improvements &  
PS Eliminations 2 - Winton Ave /  
Mockingbird Valley PS Eliminations

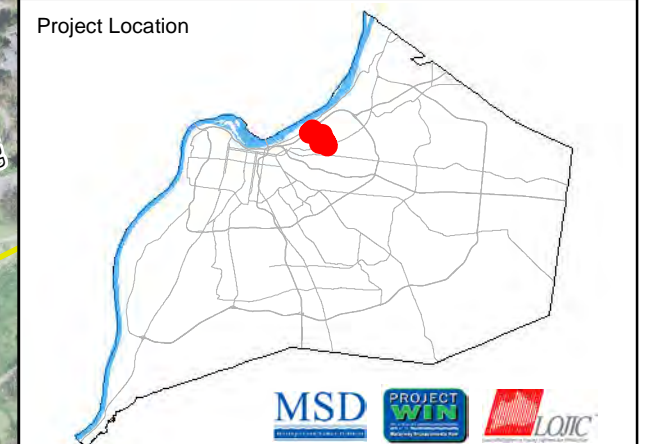
Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

**Construct 2,210 LF of 15" sewer to eliminate Mockingbird Valley PS and 400 LF of 8" sewer to eliminate Winton Ave PS. Upsize 1,890 LF of 8" sewer to 10"-12" upstream of Mockingbird Valley PS**

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 400 feet      N      Aerial Date: 2009      Map Revision: April 9, 2012



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<b>Project Name</b>	Prospect #1 - WQTC Eliminations
<b>Project Number</b>	S_OR_MF_NB04_M_03_B_B
<b>Modeled Area</b>	ORFM
<b>Branch or SSO ID</b>	NB04
<b>Project Type</b>	Pump Station & Pipe Upgrades
<b>Receiving Stream</b>	Goose Creek, Little Goose Creek, Harrods Creek, Muddy Fork Beargrass Creek, and Ohio River
<b>Project Description</b>	Construct new Harrods Creek Interceptor, including 15,000 LF of 24"-42" sewer and 3400 LF of 6" force main to eliminate 5 Prospect WQTCs. Also includes construction of two new PSs. Eliminate Deep Creek PS by constructing 130 LF of 8" sewer to new Harrods Creek Interceptor. Elimination of the WQTC is a requirement of the Amended Consent Decree.
<b>Reason for Overflow</b>	ORFM and pump station capacity
<b>Design Parameters</b>	This solution is based on a 2.25 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$17,247,000
<b>Weighted Benefit/Cost Ratio</b>	1.69

Asset ID	SSO Start Date	Volume (Gal)
MSD1063-PS	1/1/2005	6000
MSD0183-PS	1/1/2005	6000
MSD1063-PS	1/13/2005	5000
40880	1/13/2013	174000
MSD0192-PS	1/13/2013	70875
65623	1/13/2013	67500
89791	1/13/2013	21000
MSD0183-PS	1/14/2007	100
40872	1/21/2010	12450
MSD1063-PS	1/22/2006	500
MSD1063-PS	1/24/2002	6000
MSD0192-PS	1/24/2002	100000
MSD1063-PS	1/26/2012	36375
89791	1/27/2012	7400
MSD0186-PS	1/27/2012	37000
40880	1/27/2012	6020
40879	1/27/2012	181500
65623	1/27/2012	6200
22436	1/3/2005	90000
MSD0183-PS	1/3/2005	120000
40870	1/3/2005	81000
MSD1063-PS	1/3/2005	3000
MSD0192-PS	1/3/2005	105000
MSD1063-PS	1/30/2002	1000
MSD1063-PS	1/4/2004	3000
MSD0183-PS	1/4/2005	75000
MSD1063-PS	1/4/2005	110000

<b>Project Name</b>	<b>Prospect #1 - WQTC Eliminations</b>	
<b>Project Number</b>	<b>S_OR_MF_NB04_M_03_B_B</b>	
MSD0183-PS	1/5/2005	100000
MSD0193-PS	1/6/2005	14000
MSD1063-PS	1/7/2005	1200
MSD0183-PS	1/7/2005	2000
MSD1063-PS	10/14/2001	4000
MSD0183-PS	10/22/2007	300
MSD0192-PS	10/23/2007	75000
40870	10/23/2007	75000
MSD1063-PS	10/27/2004	2000
65623	10/6/2013	47500
MSD0186-PS	10/6/2013	5850
MSD1063-PS	10/6/2013	92100
MSD1063-PS	11/11/2004	11000
MSD0192-PS	11/15/2005	30000
MSD1063-PS	11/15/2005	500
MSD0183-PS	11/15/2005	15000
40871	11/16/2011	11750
40872	11/16/2011	11750
65623	11/17/2013	78000
40880	11/17/2013	62250
MSD0192-PS	11/17/2013	20550
MSD1063-PS	11/19/2004	5000
MSD1063-PS	11/2/2004	5000
MSD0183-PS	11/2/2004	15000
40871	11/22/2011	232500
65623	11/22/2011	4100
MSD1063-PS	11/22/2011	7080
40872	11/22/2011	232500
40871	11/25/2010	38750
40872	11/25/2010	310000
MSD1063-PS	11/28/2001	3000
MSD1063-PS	11/28/2005	1200
65623	11/28/2011	18000
40872	11/28/2011	549000
89791	11/28/2011	18000
MSD1063-PS	11/28/2011	62250
40871	11/28/2011	549000
40871	11/30/2010	97500
40872	11/30/2010	146250
40872	12/15/2007	81000
22436	12/15/2007	30000
MSD0192-PS	12/16/2000	0
MSD1063-PS	12/16/2000	0



<b>Project Name</b>	<b>Prospect #1 - WQTC Eliminations</b>	
<b>Project Number</b>	<b>S_OR_MF_NB04_M_03_B_B</b>	
MSD1063-PS	12/16/2007	25500
40870	12/19/2002	50000
MSD1063-PS	12/19/2002	13200
MSD0192-PS	12/19/2002	100000
40879	12/2/2010	100
40879	12/22/2013	131500
42680	12/22/2013	30000
89791	12/22/2013	19500
65623	12/22/2013	60000
40870	12/24/2008	2400
89646	12/27/2011	91500
40879	12/28/2011	5
MSD1063-PS	12/30/2002	600
MSD1063-PS	12/30/2002	600
MSD1063-PS	12/30/2004	12000
MSD1063-PS	12/31/2002	6000
MSD0183-PS	12/31/2004	10000
65623	12/5/2011	123000
89791	12/5/2011	52000
40871	12/5/2011	962500
40872	12/5/2011	962500
MSD1063-PS	12/5/2011	34750
65633	12/5/2011	70500
MSD1063-PS	2/15/2001	1500
MSD1063-PS	2/15/2003	4000
MSD1063-PS	2/24/2011	2450
40871	2/25/2011	36000
40872	2/25/2011	216090
65633	2/25/2011	54500
40872	2/28/2011	10500
40871	2/28/2011	8750
MSD1063-PS	2/3/2004	15000
40871	2/4/2010	5
MSD1063-PS	2/5/2004	15000
MSD1063-PS	2/5/2010	150
40872	2/6/2008	5400
MSD0123-PS	2/6/2008	36750
MSD1063-PS	3/11/2006	500
MSD1063-PS	3/12/2006	1000
40872	3/12/2011	167500
40871	3/12/2011	16750
40872	3/18/2008	108000
MSD1063-PS	3/18/2008	11625

Project Name	Prospect #1 - WQTC Eliminations	
Project Number	S_OR_MF_NB04_M_03_B_B	
40871	3/18/2008	312200
MSD0183-PS	3/18/2008	114000
40880	3/18/2012	183400
40879	3/18/2012	183400
MSD0186-PS	3/18/2013	11700
89791	3/18/2013	8500
40879	3/18/2013	146250
MSD1063-PS	3/19/2008	76000
42680	3/19/2008	162000
MSD0192-PS	3/20/2002	60000
MSD1044-PS	3/20/2002	4500
MSD0183-PS	3/20/2002	4000
40880	3/24/2012	95500
40879	3/24/2012	271250
MSD0186-PS	3/24/2012	21000
MSD0183-PS	3/26/2002	12000
MSD0192-PS	3/26/2002	20000
MSD1063-PS	3/26/2002	1500
MSD1044-PS	3/26/2002	1500
MSD1063-PS	3/27/2005	2400
40872	3/27/2008	342000
MSD0183-PS	3/28/2005	50000
40870	3/28/2005	10000
MSD0192-PS	3/4/2008	72000
MSD1063-PS	3/4/2008	15000
40871	3/4/2008	18000
40872	3/4/2008	204000
40872	3/5/2011	30000
40871	3/5/2011	30000
40872	3/9/2011	630000
42680	3/9/2011	37500
40871	3/9/2011	126000
MSD1063-PS	3/9/2011	22720
40879	4/1/2012	227250
MSD0186-PS	4/1/2012	13200
40880	4/1/2012	530250
40871	4/11/2011	123625
MSD1063-PS	4/11/2011	25125
40872	4/11/2011	989000
89791	4/12/2011	17000
65633	4/12/2011	330000
42680	4/12/2011	198000
MSD1063-PS	4/2/2006	100

Project Name	Prospect #1 - WQTC Eliminations	
Project Number	S_OR_MF_NB04_M_03_B_B	
MSD1063-PS	4/21/2002	4500
MSD0183-PS	4/21/2006	2000
65633	4/23/2011	183750
MSD1063-PS	4/23/2011	73950
89791	4/23/2011	72000
40871	4/23/2011	1429875
40872	4/23/2011	2859750
MSD1063-PS	4/25/2003	2000
MSD1063-PS	4/25/2004	3000
MSD1063-PS	4/27/2002	3000
65633	4/27/2011	137400
65623	4/27/2011	113500
MSD0193-PS	4/27/2011	27125
MSD0193-PS	4/4/2008	12000
40871	4/4/2008	120000
MSD0183-PS	4/4/2008	18000
40872	4/4/2008	360000
65633	4/4/2008	204000
MSD1063-PS	4/4/2008	14400
65635	4/4/2008	25500
MSD1063-PS	5/1/2004	15000
65633	5/11/2009	1500
MSD1063-PS	5/13/2002	2000
40880	5/13/2012	313750
40879	5/13/2012	94125
MSD0186-PS	5/13/2012	62750
65623	5/13/2012	10500
40871	5/2/2010	51750
40872	5/2/2010	103500
MSD0183-PS	5/2/2010	31500
65633	5/2/2010	112000
MSD1063-PS	5/2/2011	23040
MSD1063-PS	5/25/2004	8000
MSD1063-PS	5/27/2004	90000
MSD1063-PS	5/27/2004	30000
40870	5/28/2004	18000
MSD0183-PS	5/28/2004	300000
40879	5/29/2012	1800
89791	5/29/2012	48000
40880	5/29/2012	47800
MSD0186-PS	5/29/2012	1700
MSD1063-PS	5/3/2008	18000
65623	5/3/2011	2200



<b>Project Name</b>	<b>Prospect #1 - WQTC Eliminations</b>	
<b>Project Number</b>	<b>S_OR_MF_NB04_M_03_B_B</b>	
89791	5/3/2011	72000
MSD0193-PS	5/3/2011	54000
65633	5/3/2011	33000
MSD1063-PS	5/30/2004	15000
MSD1063-PS	5/5/2003	5000
40870	5/8/2009	18000
MSD0183-PS	5/8/2009	9500
MSD1063-PS	5/8/2009	8400
MSD0192-PS	6/14/2003	50000
MSD0183-PS	6/15/2003	18000
89791	6/23/2011	23000
40871	6/23/2011	75000
40872	6/23/2011	125000
42680	6/23/2011	5
65623	6/23/2011	41000
89791	6/26/2013	24000
40879	6/27/2013	43000
40880	6/27/2013	2760
MSD0186-PS	6/27/2013	14205
MSD0183-PS	6/6/2002	3000
MSD0192-PS	6/6/2002	10000
MSD1063-PS	6/6/2002	5000
MSD0183-PS	6/7/2003	1000
40872	7/13/2010	32000
MSD0183-PS	7/14/2006	43000
MSD0183-PS	7/17/2004	800000
MSD1063-PS	7/29/2009	450
65633	7/29/2009	10250
40872	7/29/2009	216000
MSD0183-PS	7/29/2009	250
MSD1063-PS	7/30/2009	61875
40872	7/31/2009	225000
MSD1063-PS	8/30/2005	250
MSD0192-PS	8/30/2005	150
MSD1063-PS	8/4/2009	5625
40872	8/4/2009	9999
65633	8/4/2009	102000
MSD1063-PS	9/1/2003	25000
MSD1063-PS	9/15/2002	800
40870	9/20/2009	39600
MSD0183-PS	9/23/2006	12000
MSD1063-PS	9/23/2006	10000
MSD0192-PS	9/23/2006	16000

Project Name	Prospect #1 - WQTC Eliminations	
Project Number	S_OR_MF_NB04_M_03_B_B	
40872	9/26/2011	33500
40871	9/26/2011	10050
MSD1063-PS	9/26/2011	26250
89791	9/26/2011	1400
MSD1063-PS	9/27/2002	1200
MSD0192-PS	9/27/2002	360000
40870	9/27/2002	10000
MSD0123-PS	9/27/2002	4000
MSD0183-PS	9/27/2002	5000
MSD1063-PS	9/27/2003	3000
MSD0183-PS	9/27/2003	25000



**Integrated Overflow Abatement Plan**

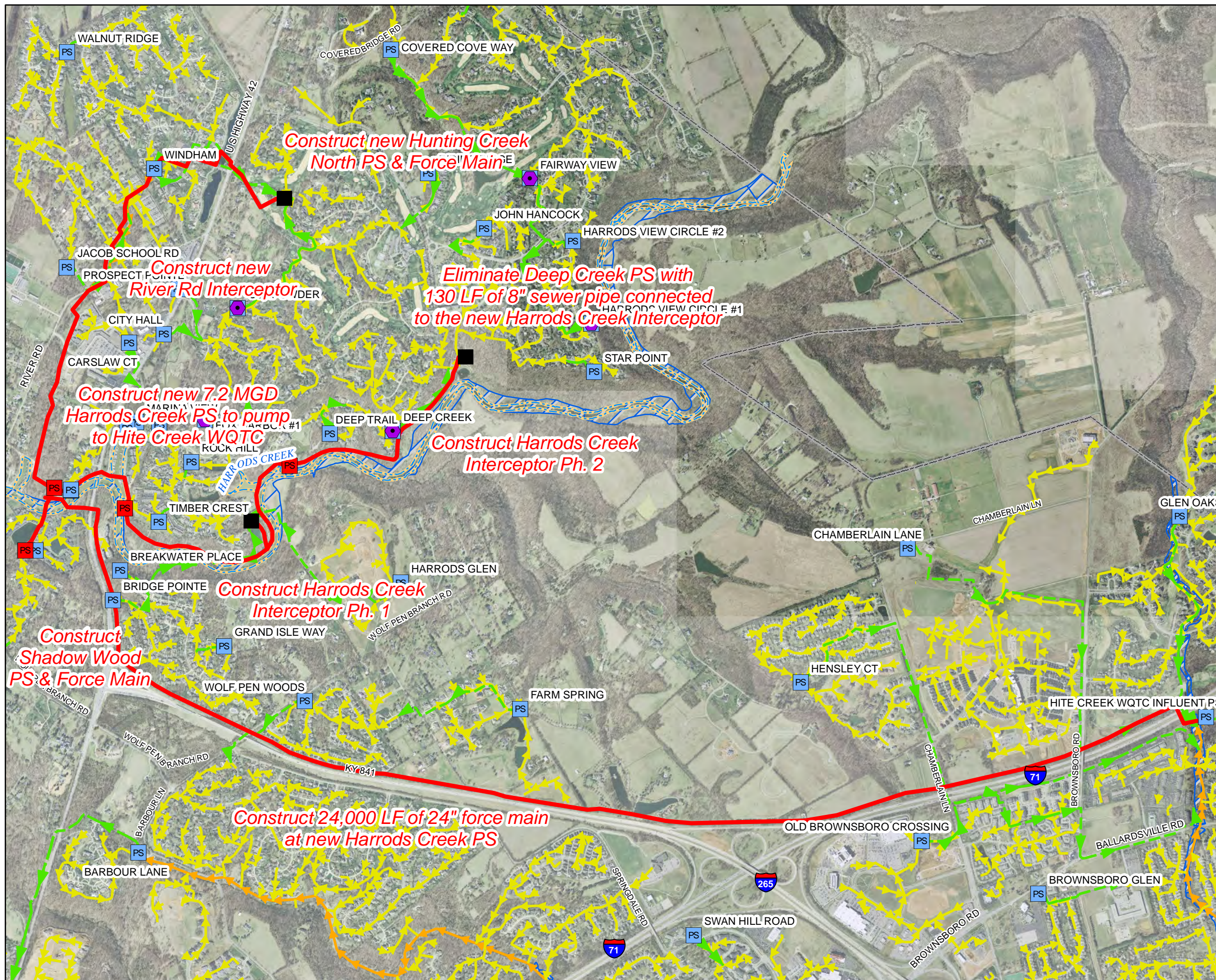
**Vol. 3 - Sanitary Sewer Discharge Plan**

Ohio River Force Main Sewershed

Prospect #1 - WQTC Eliminations

Prospect #2 - Harrods Creek PS

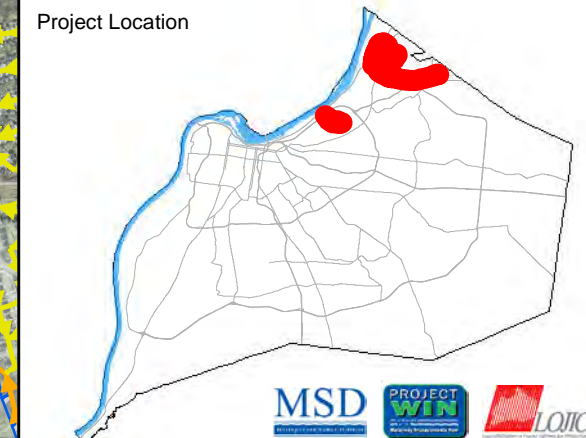
Preliminary - For Budget Development Only



- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- WQTC
- Proposed Pipe Solution
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,708 feet Aerial Date: 2009 Map Revision: April 9, 2012



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<b>Project Name</b>	Prospect #2 - Harrods Creek PS and FM
<b>Project Number</b>	S_OR_MF_NB04_M_03_B_B
<b>Modeled Area</b>	ORFM
<b>Branch or SSO ID</b>	NB04
<b>Project Type</b>	Pump Station & Pipe Upgrades
<b>Receiving Stream</b>	Goose Creek, Little Goose Creek, Harrods Creek, Muddy Fork Beargrass Creek, and Ohio River
<b>Project Description</b>	Construct new 7.2 MGD Harrods Creek PS and 24,000 LF of 24" force main to pump flow to the Hite Creek WQTC.
<b>Reason for Overflow</b>	ORFM and pump station capacity
<b>Design Parameters</b>	This solution is based on a 2.25 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$9,621,000
<b>Weighted Benefit/Cost Ratio</b>	1.69

Asset ID	SSO Start Date	Volume (Gal)
MSD1063-PS	1/1/2005	6000
MSD0183-PS	1/1/2005	6000
MSD1063-PS	1/13/2005	5000
65623	1/13/2013	67500
40880	1/13/2013	174000
89791	1/13/2013	21000
MSD0192-PS	1/13/2013	70875
MSD0183-PS	1/14/2007	100
40872	1/21/2010	12450
MSD1063-PS	1/22/2006	500
MSD0192-PS	1/24/2002	100000
MSD1063-PS	1/24/2002	6000
MSD1063-PS	1/26/2012	36375
89791	1/27/2012	7400
65623	1/27/2012	6200
40880	1/27/2012	6020
MSD0186-PS	1/27/2012	37000
40879	1/27/2012	181500
22436	1/3/2005	90000
40870	1/3/2005	81000
MSD0183-PS	1/3/2005	120000
MSD0192-PS	1/3/2005	105000
MSD1063-PS	1/3/2005	3000
MSD1063-PS	1/30/2002	1000
MSD1063-PS	1/4/2004	3000
MSD0183-PS	1/4/2005	75000
MSD1063-PS	1/4/2005	110000
MSD0183-PS	1/5/2005	100000
MSD0193-PS	1/6/2005	14000

<b>Project Name</b>	<b>Prospect #2 - Harrods Creek PS and FM</b>	
<b>Project Number</b>	<b>S_OR_MF_NB04_M_03_B_B</b>	
MSD0183-PS	1/7/2005	2000
MSD1063-PS	1/7/2005	1200
MSD1063-PS	10/14/2001	4000
MSD0183-PS	10/22/2007	300
MSD0192-PS	10/23/2007	75000
40870	10/23/2007	75000
MSD1063-PS	10/27/2004	2000
MSD1063-PS	10/6/2013	92100
65623	10/6/2013	47500
MSD0186-PS	10/6/2013	5850
MSD1063-PS	11/11/2004	11000
MSD0192-PS	11/15/2005	30000
MSD0183-PS	11/15/2005	15000
MSD1063-PS	11/15/2005	500
40872	11/16/2011	11750
40871	11/16/2011	11750
65623	11/17/2013	78000
40880	11/17/2013	62250
MSD0192-PS	11/17/2013	20550
MSD1063-PS	11/19/2004	5000
MSD0183-PS	11/2/2004	15000
MSD1063-PS	11/2/2004	5000
40871	11/22/2011	232500
65623	11/22/2011	4100
40872	11/22/2011	232500
MSD1063-PS	11/22/2011	7080
40871	11/25/2010	38750
40872	11/25/2010	310000
MSD1063-PS	11/28/2001	3000
MSD1063-PS	11/28/2005	1200
89791	11/28/2011	18000
40871	11/28/2011	549000
65623	11/28/2011	18000
40872	11/28/2011	549000
MSD1063-PS	11/28/2011	62250
40871	11/30/2010	97500
40872	11/30/2010	146250
40872	12/15/2007	81000
22436	12/15/2007	30000
MSD1063-PS	12/16/2000	0
MSD0192-PS	12/16/2000	0
MSD1063-PS	12/16/2007	25500
MSD0192-PS	12/19/2002	100000

Project Name	Prospect #2 - Harrods Creek PS and FM	
Project Number	S_OR_MF_NB04_M_03_B_B	
40870	12/19/2002	50000
MSD1063-PS	12/19/2002	13200
40879	12/2/2010	100
40879	12/22/2013	131500
42680	12/22/2013	30000
65623	12/22/2013	60000
89791	12/22/2013	19500
40870	12/24/2008	2400
89646	12/27/2011	91500
40879	12/28/2011	5
MSD1063-PS	12/30/2002	600
MSD1063-PS	12/30/2002	600
MSD1063-PS	12/30/2004	12000
MSD1063-PS	12/31/2002	6000
MSD0183-PS	12/31/2004	10000
65633	12/5/2011	70500
40871	12/5/2011	962500
40872	12/5/2011	962500
89791	12/5/2011	52000
65623	12/5/2011	123000
MSD1063-PS	12/5/2011	34750
MSD1063-PS	2/15/2001	1500
MSD1063-PS	2/15/2003	4000
MSD1063-PS	2/24/2011	2450
40872	2/25/2011	216090
40871	2/25/2011	36000
65633	2/25/2011	54500
40872	2/28/2011	10500
40871	2/28/2011	8750
MSD1063-PS	2/3/2004	15000
40871	2/4/2010	5
MSD1063-PS	2/5/2004	15000
MSD1063-PS	2/5/2010	150
MSD0123-PS	2/6/2008	36750
40872	2/6/2008	5400
MSD1063-PS	3/11/2006	500
MSD1063-PS	3/12/2006	1000
40872	3/12/2011	167500
40871	3/12/2011	16750
MSD0183-PS	3/18/2008	114000
40872	3/18/2008	108000
40871	3/18/2008	312200
MSD1063-PS	3/18/2008	11625



<b>Project Name</b>	<b>Prospect #2 - Harrods Creek PS and FM</b>	
<b>Project Number</b>	<b>S_OR_MF_NB04_M_03_B_B</b>	
40880	3/18/2012	183400
40879	3/18/2012	183400
MSD0186-PS	3/18/2013	11700
89791	3/18/2013	8500
40879	3/18/2013	146250
MSD1063-PS	3/19/2008	76000
42680	3/19/2008	162000
MSD0183-PS	3/20/2002	4000
MSD0192-PS	3/20/2002	60000
MSD1044-PS	3/20/2002	4500
40880	3/24/2012	95500
40879	3/24/2012	271250
MSD0186-PS	3/24/2012	21000
MSD1063-PS	3/26/2002	1500
MSD1044-PS	3/26/2002	1500
MSD0192-PS	3/26/2002	20000
MSD0183-PS	3/26/2002	12000
MSD1063-PS	3/27/2005	2400
40872	3/27/2008	342000
40870	3/28/2005	10000
MSD0183-PS	3/28/2005	50000
40871	3/4/2008	18000
MSD0192-PS	3/4/2008	72000
MSD1063-PS	3/4/2008	15000
40872	3/4/2008	204000
40872	3/5/2011	30000
40871	3/5/2011	30000
40872	3/9/2011	630000
MSD1063-PS	3/9/2011	22720
42680	3/9/2011	37500
40871	3/9/2011	126000
40879	4/1/2012	227250
40880	4/1/2012	530250
MSD0186-PS	4/1/2012	13200
40871	4/11/2011	123625
MSD1063-PS	4/11/2011	25125
40872	4/11/2011	989000
89791	4/12/2011	17000
42680	4/12/2011	198000
65633	4/12/2011	330000
MSD1063-PS	4/2/2006	100
MSD1063-PS	4/21/2002	4500
MSD0183-PS	4/21/2006	2000

<b>Project Name</b>	<b>Prospect #2 - Harrods Creek PS and FM</b>	
<b>Project Number</b>	<b>S_OR_MF_NB04_M_03_B_B</b>	
89791	4/23/2011	72000
40871	4/23/2011	1429875
MSD1063-PS	4/23/2011	73950
65633	4/23/2011	183750
40872	4/23/2011	2859750
MSD1063-PS	4/25/2003	2000
MSD1063-PS	4/25/2004	3000
MSD1063-PS	4/27/2002	3000
65633	4/27/2011	137400
MSD0193-PS	4/27/2011	27125
65623	4/27/2011	113500
65633	4/4/2008	204000
MSD0183-PS	4/4/2008	18000
MSD0193-PS	4/4/2008	12000
65635	4/4/2008	25500
40871	4/4/2008	120000
40872	4/4/2008	360000
MSD1063-PS	4/4/2008	14400
MSD1063-PS	5/1/2004	15000
65633	5/11/2009	1500
MSD1063-PS	5/13/2002	2000
MSD0186-PS	5/13/2012	62750
40880	5/13/2012	313750
65623	5/13/2012	10500
40879	5/13/2012	94125
MSD0183-PS	5/2/2010	31500
65633	5/2/2010	112000
40872	5/2/2010	103500
40871	5/2/2010	51750
MSD1063-PS	5/2/2011	23040
MSD1063-PS	5/25/2004	8000
MSD1063-PS	5/27/2004	90000
MSD1063-PS	5/27/2004	30000
40870	5/28/2004	18000
MSD0183-PS	5/28/2004	300000
40879	5/29/2012	1800
40880	5/29/2012	47800
89791	5/29/2012	48000
MSD0186-PS	5/29/2012	1700
MSD1063-PS	5/3/2008	18000
89791	5/3/2011	72000
MSD0193-PS	5/3/2011	54000
65623	5/3/2011	2200

Project Name	Prospect #2 - Harrods Creek PS and FM	
Project Number	S_OR_MF_NB04_M_03_B_B	
65633	5/3/2011	33000
MSD1063-PS	5/30/2004	15000
MSD1063-PS	5/5/2003	5000
MSD1063-PS	5/8/2009	8400
MSD0183-PS	5/8/2009	9500
40870	5/8/2009	18000
MSD0192-PS	6/14/2003	50000
MSD0183-PS	6/15/2003	18000
89791	6/23/2011	23000
40871	6/23/2011	75000
65623	6/23/2011	41000
40872	6/23/2011	125000
42680	6/23/2011	5
89791	6/26/2013	24000
40880	6/27/2013	2760
MSD0186-PS	6/27/2013	14205
40879	6/27/2013	43000
MSD0183-PS	6/6/2002	3000
MSD1063-PS	6/6/2002	5000
MSD0192-PS	6/6/2002	10000
MSD0183-PS	6/7/2003	1000
40872	7/13/2010	32000
MSD0183-PS	7/14/2006	43000
MSD0183-PS	7/17/2004	800000
40872	7/29/2009	216000
MSD0183-PS	7/29/2009	250
MSD1063-PS	7/29/2009	450
65633	7/29/2009	10250
MSD1063-PS	7/30/2009	61875
40872	7/31/2009	225000
MSD1063-PS	8/30/2005	250
MSD0192-PS	8/30/2005	150
65633	8/4/2009	102000
MSD1063-PS	8/4/2009	5625
40872	8/4/2009	9999
MSD1063-PS	9/1/2003	25000
MSD1063-PS	9/15/2002	800
40870	9/20/2009	39600
MSD0183-PS	9/23/2006	12000
MSD0192-PS	9/23/2006	16000
MSD1063-PS	9/23/2006	10000
40872	9/26/2011	33500
89791	9/26/2011	1400



Project Name	Prospect #2 - Harrods Creek PS and FM	
Project Number	S_OR_MF_NB04_M_03_B_B	
40871	9/26/2011	10050
MSD1063-PS	9/26/2011	26250
MSD0123-PS	9/27/2002	4000
MSD0183-PS	9/27/2002	5000
MSD1063-PS	9/27/2002	1200
40870	9/27/2002	10000
MSD0192-PS	9/27/2002	360000
MSD1063-PS	9/27/2003	3000
MSD0183-PS	9/27/2003	25000



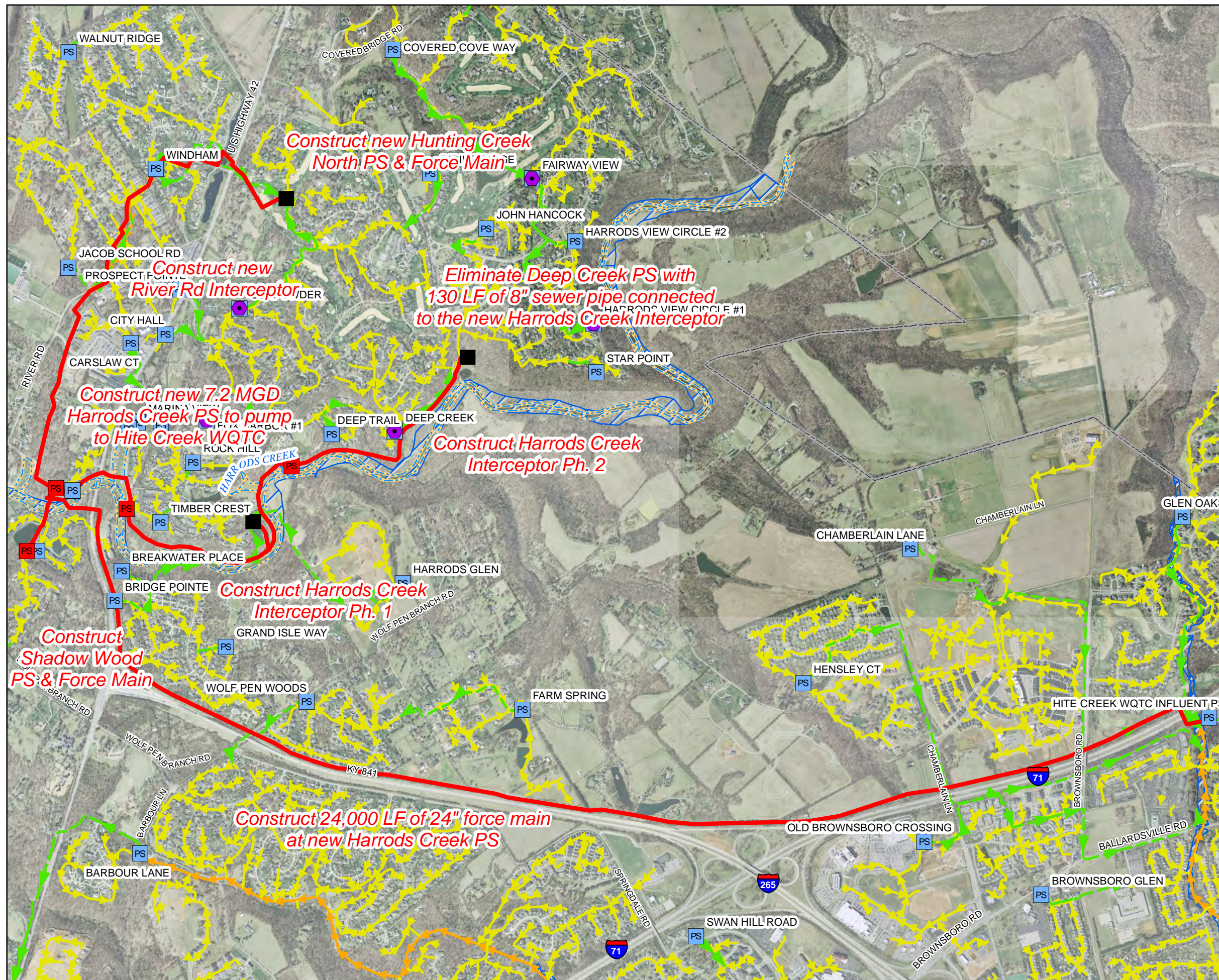
**Integrated Overflow Abatement Plan**

**Vol. 3 - Sanitary Sewer Discharge Plan**

Ohio River Force Main Sewershed

Prospect #1 - WQTC Eliminations  
Prospect #2 - Harrods Creek PS

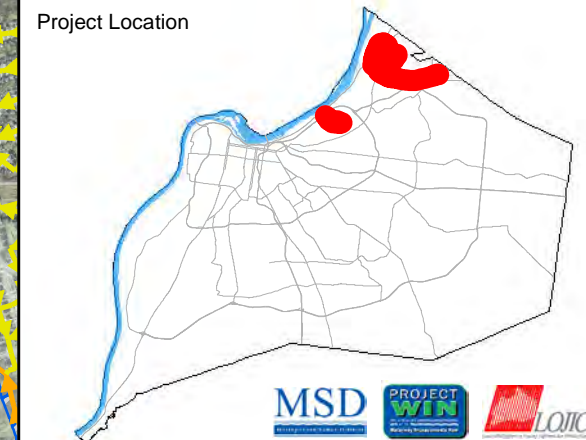
Preliminary - For Budget Development Only



- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- WQTC
- Proposed Pipe Solution
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,708 feet       Aerial Date: 2009    Map Revision: April 9, 2012



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<b>Project Name</b>	Prospect #3 - ORFM System Improvemetsns
<b>Project Number</b>	S_OR_MF_NB04_M_03_B_B
<b>Modeled Area</b>	ORFM
<b>Branch or SSO ID</b>	NB04
<b>Project Type</b>	Pump Station & Pipe Upgrades
<b>Receiving Stream</b>	Goose Creek, Ohio River
<b>Project Description</b>	Upsize 8,350 LF of interceptor upstream of Muddy Fork PS to 27". Upgrade pumps at Muddy Fork, Winding Falls/Phoenix Hill PS and New Market PS. Upsize force main from Muddy Fork PS to 24".
<b>Reason for Overflow</b>	ORFM and pump station capacity
<b>Design Parameters</b>	This solution is based on a 2.25 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$4,500,000
<b>Weighted Benefit/Cost Ratio</b>	4.8

Asset ID	SSO Start Date	Volume (Gal)
MSD0183-PS	1/1/2005	6000
MSD1063-PS	1/1/2005	6000
MSD1063-PS	1/13/2005	5000
89791	1/13/2013	21000
65623	1/13/2013	67500
40880	1/13/2013	174000
MSD0192-PS	1/13/2013	70875
MSD0183-PS	1/14/2007	100
40872	1/21/2010	12450
MSD1063-PS	1/22/2006	500
MSD0192-PS	1/24/2002	100000
MSD1063-PS	1/24/2002	6000
MSD1063-PS	1/26/2012	36375
MSD0186-PS	1/27/2012	37000
40880	1/27/2012	6020
89791	1/27/2012	7400
65623	1/27/2012	6200
40879	1/27/2012	181500
MSD0192-PS	1/3/2005	105000
MSD1063-PS	1/3/2005	3000
22436	1/3/2005	90000
40870	1/3/2005	81000
MSD0183-PS	1/3/2005	120000
MSD1063-PS	1/30/2002	1000
MSD1063-PS	1/4/2004	3000
MSD1063-PS	1/4/2005	110000
MSD0183-PS	1/4/2005	75000
MSD0183-PS	1/5/2005	100000
MSD0193-PS	1/6/2005	14000



<b>Project Name</b>	<b>Prospect #3 - ORFM System Improvemetrns</b>	
<b>Project Number</b>	<b>S_OR_MF_NB04_M_03_B_B</b>	
MSD1063-PS	1/7/2005	1200
MSD0183-PS	1/7/2005	2000
MSD1063-PS	10/14/2001	4000
MSD0183-PS	10/22/2007	300
40870	10/23/2007	75000
MSD0192-PS	10/23/2007	75000
MSD1063-PS	10/27/2004	2000
65623	10/6/2013	47500
MSD1063-PS	10/6/2013	92100
MSD0186-PS	10/6/2013	5850
MSD1063-PS	11/11/2004	11000
MSD1063-PS	11/15/2005	500
MSD0192-PS	11/15/2005	30000
MSD0183-PS	11/15/2005	15000
40871	11/16/2011	11750
40872	11/16/2011	11750
65623	11/17/2013	78000
MSD0192-PS	11/17/2013	20550
40880	11/17/2013	62250
MSD1063-PS	11/19/2004	5000
MSD0183-PS	11/2/2004	15000
MSD1063-PS	11/2/2004	5000
65623	11/22/2011	4100
MSD1063-PS	11/22/2011	7080
40871	11/22/2011	232500
40872	11/22/2011	232500
40871	11/25/2010	38750
40872	11/25/2010	310000
MSD1063-PS	11/28/2001	3000
MSD1063-PS	11/28/2005	1200
40872	11/28/2011	549000
65623	11/28/2011	18000
89791	11/28/2011	18000
MSD1063-PS	11/28/2011	62250
40871	11/28/2011	549000
40871	11/30/2010	97500
40872	11/30/2010	146250
22436	12/15/2007	30000
40872	12/15/2007	81000
MSD1063-PS	12/16/2000	0
MSD0192-PS	12/16/2000	0
MSD1063-PS	12/16/2007	25500
40870	12/19/2002	50000

Project Name	Prospect #3 - ORFM System Improvemetrns	
Project Number	S_OR_MF_NB04_M_03_B_B	
MSD1063-PS	12/19/2002	13200
MSD0192-PS	12/19/2002	100000
40879	12/2/2010	100
89791	12/22/2013	19500
40879	12/22/2013	131500
65623	12/22/2013	60000
42680	12/22/2013	30000
40870	12/24/2008	2400
89646	12/27/2011	91500
40879	12/28/2011	5
MSD1063-PS	12/30/2002	600
MSD1063-PS	12/30/2002	600
MSD1063-PS	12/30/2004	12000
MSD1063-PS	12/31/2002	6000
MSD0183-PS	12/31/2004	10000
65633	12/5/2011	70500
40871	12/5/2011	962500
40872	12/5/2011	962500
89791	12/5/2011	52000
MSD1063-PS	12/5/2011	34750
65623	12/5/2011	123000
MSD1063-PS	2/15/2001	1500
MSD1063-PS	2/15/2003	4000
MSD1063-PS	2/24/2011	2450
40872	2/25/2011	216090
40871	2/25/2011	36000
65633	2/25/2011	54500
40872	2/28/2011	10500
40871	2/28/2011	8750
MSD1063-PS	2/3/2004	15000
40871	2/4/2010	5
MSD1063-PS	2/5/2004	15000
MSD1063-PS	2/5/2010	150
MSD0123-PS	2/6/2008	36750
40872	2/6/2008	5400
MSD1063-PS	3/11/2006	500
MSD1063-PS	3/12/2006	1000
40871	3/12/2011	16750
40872	3/12/2011	167500
40871	3/18/2008	312200
MSD0183-PS	3/18/2008	114000
40872	3/18/2008	108000
MSD1063-PS	3/18/2008	11625

Project Name	Prospect #3 - ORFM System Improvemetrns	
Project Number	S_OR_MF_NB04_M_03_B_B	
40879	3/18/2012	183400
40880	3/18/2012	183400
89791	3/18/2013	8500
MSD0186-PS	3/18/2013	11700
40879	3/18/2013	146250
MSD1063-PS	3/19/2008	76000
42680	3/19/2008	162000
MSD0183-PS	3/20/2002	4000
MSD1044-PS	3/20/2002	4500
MSD0192-PS	3/20/2002	60000
MSD0186-PS	3/24/2012	21000
40879	3/24/2012	271250
40880	3/24/2012	95500
MSD1063-PS	3/26/2002	1500
MSD1044-PS	3/26/2002	1500
MSD0183-PS	3/26/2002	12000
MSD0192-PS	3/26/2002	20000
MSD1063-PS	3/27/2005	2400
40872	3/27/2008	342000
40870	3/28/2005	10000
MSD0183-PS	3/28/2005	50000
MSD1063-PS	3/4/2008	15000
MSD0192-PS	3/4/2008	72000
40871	3/4/2008	18000
40872	3/4/2008	204000
40872	3/5/2011	30000
40871	3/5/2011	30000
42680	3/9/2011	37500
40871	3/9/2011	126000
MSD1063-PS	3/9/2011	22720
40872	3/9/2011	630000
40879	4/1/2012	227250
MSD0186-PS	4/1/2012	13200
40880	4/1/2012	530250
40871	4/11/2011	123625
MSD1063-PS	4/11/2011	25125
40872	4/11/2011	989000
89791	4/12/2011	17000
65633	4/12/2011	330000
42680	4/12/2011	198000
MSD1063-PS	4/2/2006	100
MSD1063-PS	4/21/2002	4500
MSD0183-PS	4/21/2006	2000



<b>Project Name</b>	<b>Prospect #3 - ORFM System Improvemetrns</b>	
<b>Project Number</b>	<b>S_OR_MF_NB04_M_03_B_B</b>	
40871	4/23/2011	1429875
65633	4/23/2011	183750
89791	4/23/2011	72000
MSD1063-PS	4/23/2011	73950
40872	4/23/2011	2859750
MSD1063-PS	4/25/2003	2000
MSD1063-PS	4/25/2004	3000
MSD1063-PS	4/27/2002	3000
MSD0193-PS	4/27/2011	27125
65633	4/27/2011	137400
65623	4/27/2011	113500
65633	4/4/2008	204000
65635	4/4/2008	25500
MSD0183-PS	4/4/2008	18000
40872	4/4/2008	360000
MSD0193-PS	4/4/2008	12000
MSD1063-PS	4/4/2008	14400
40871	4/4/2008	120000
MSD1063-PS	5/1/2004	15000
65633	5/11/2009	1500
MSD1063-PS	5/13/2002	2000
40879	5/13/2012	94125
40880	5/13/2012	313750
65623	5/13/2012	10500
MSD0186-PS	5/13/2012	62750
MSD0183-PS	5/2/2010	31500
40872	5/2/2010	103500
65633	5/2/2010	112000
40871	5/2/2010	51750
MSD1063-PS	5/2/2011	23040
MSD1063-PS	5/25/2004	8000
MSD1063-PS	5/27/2004	90000
MSD1063-PS	5/27/2004	30000
40870	5/28/2004	18000
MSD0183-PS	5/28/2004	300000
MSD0186-PS	5/29/2012	1700
89791	5/29/2012	48000
40880	5/29/2012	47800
40879	5/29/2012	1800
MSD1063-PS	5/3/2008	18000
65633	5/3/2011	33000
89791	5/3/2011	72000
65623	5/3/2011	2200








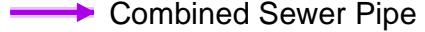






<b>Project Name</b>	<b>Prospect #3 - ORFM System Improvemetrns</b>	
<b>Project Number</b>	<b>S_OR_MF_NB04_M_03_B_B</b>	
MSD0193-PS	5/3/2011	54000
MSD1063-PS	5/30/2004	15000
MSD1063-PS	5/5/2003	5000
40870	5/8/2009	18000
MSD1063-PS	5/8/2009	8400
MSD0183-PS	5/8/2009	9500
MSD0192-PS	6/14/2003	50000
MSD0183-PS	6/15/2003	18000
40872	6/23/2011	125000
40871	6/23/2011	75000
65623	6/23/2011	41000
42680	6/23/2011	5
89791	6/23/2011	23000
89791	6/26/2013	24000
40879	6/27/2013	43000
40880	6/27/2013	2760
MSD0186-PS	6/27/2013	14205
MSD0192-PS	6/6/2002	10000
MSD1063-PS	6/6/2002	5000
MSD0183-PS	6/6/2002	3000
MSD0183-PS	6/7/2003	1000
40872	7/13/2010	32000
MSD0183-PS	7/14/2006	43000
MSD0183-PS	7/17/2004	800000
MSD1063-PS	7/29/2009	450
40872	7/29/2009	216000
MSD0183-PS	7/29/2009	250
65633	7/29/2009	10250
MSD1063-PS	7/30/2009	61875
40872	7/31/2009	225000
MSD1063-PS	8/30/2005	250
MSD0192-PS	8/30/2005	150
40872	8/4/2009	9999
MSD1063-PS	8/4/2009	5625
65633	8/4/2009	102000
MSD1063-PS	9/1/2003	25000
MSD1063-PS	9/15/2002	800
40870	9/20/2009	39600
MSD1063-PS	9/23/2006	10000
MSD0192-PS	9/23/2006	16000
MSD0183-PS	9/23/2006	12000
40871	9/26/2011	10050
MSD1063-PS	9/26/2011	26250

Project Name	Prospect #3 - ORFM System Improvemets	
Project Number	S_OR_MF_NB04_M_03_B_B	
40872	9/26/2011	33500
89791	9/26/2011	1400
40870	9/27/2002	10000
MSD0123-PS	9/27/2002	4000
MSD1063-PS	9/27/2002	1200
MSD0192-PS	9/27/2002	360000
MSD0183-PS	9/27/2002	5000
MSD0183-PS	9/27/2003	25000
MSD1063-PS	9/27/2003	3000



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Ohio River Force Main Sewershed  
 Prospect #3 - ORFM System Improvements

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Proposed Pump Station Solution
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

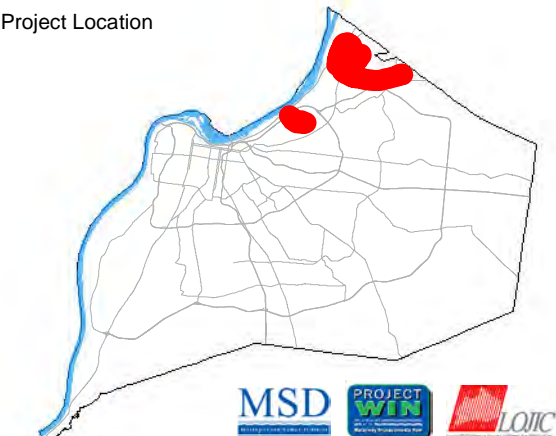
1 inch = 1,000 feet



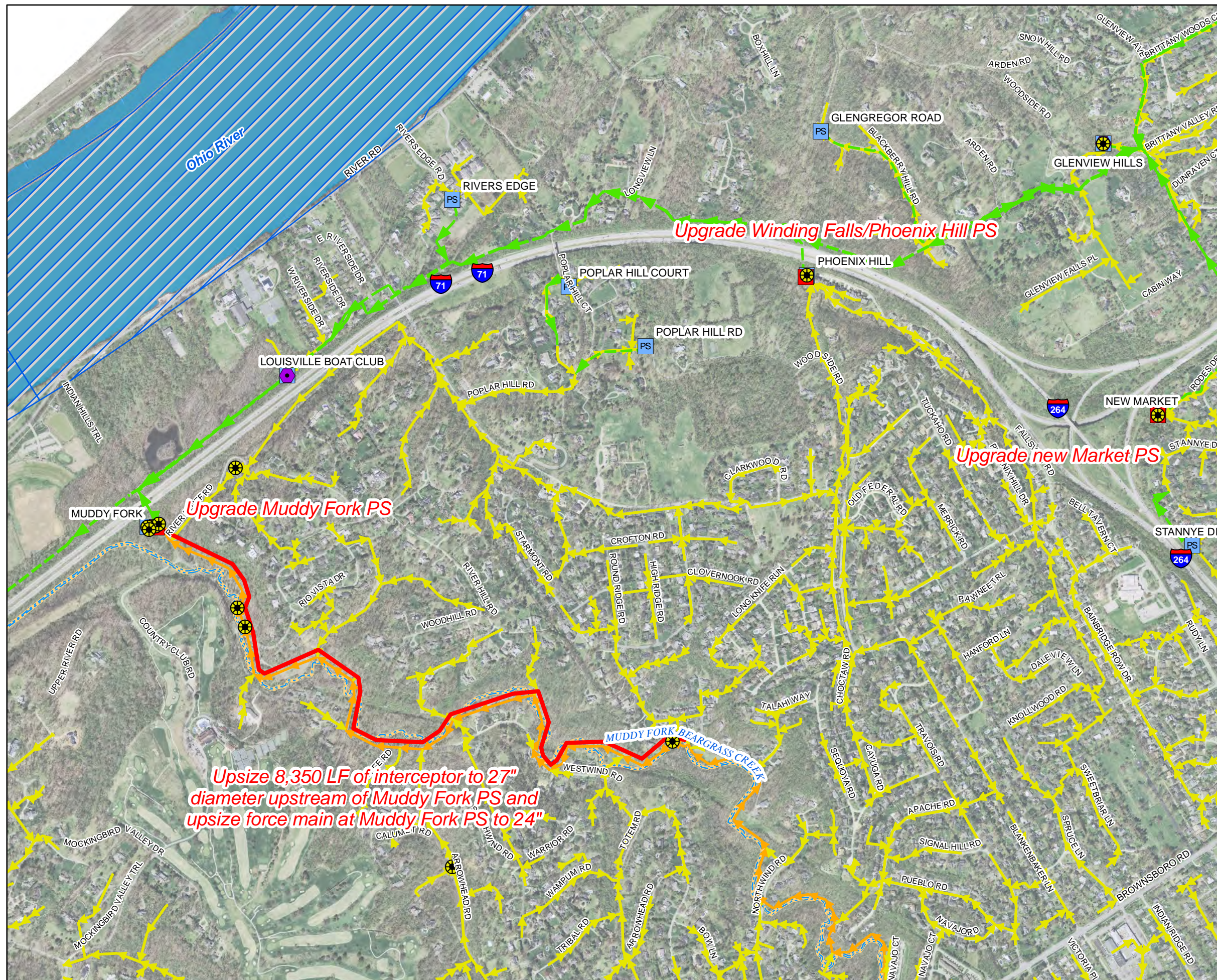
Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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**Mill Creek  
Area**

<b>Project Name</b>	East Rockford PS Relocation
<b>Project Number</b>	S_MC_WC_NB02_S_03_C
<b>Modeled Area</b>	Mill Creek
<b>Branch or SSO ID</b>	NB02
<b>Project Type</b>	Pump Station Replacement and Relocation
<b>Receiving Stream</b>	Mill Creek
<b>Project Description</b>	Relocate and replace East Rockford PS at 300 GPM. 150 LF of 4" force main will be replaced. Additional 150 LF of 10" gravity improvements required to relocate PS.
<b>Reason for Overflow</b>	Surface flooding
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$1,044,000
<b>Weighted Benefit/Cost Ratio</b>	--




















Asset ID	SSO Start Date	Volume (Gal)
04699-W	12/15/2007	0
04699-W	2/25/2011	9999
04699-W	3/9/2011	9999
04699-W	4/11/2011	9999
04699-W	5/8/2009	5000
04699-W	6/18/2009	2000
04699-W	6/23/2011	9999
04699-W	8/4/2009	9999
04699-W	9/21/2009	9999
04699-W	9/26/2011	9999



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Mill Creek Sewershed  
 Solution ID # S\_MC\_WC\_NB02\_S\_03\_C  
 East Rockford PS Relocation

**Preliminary - For Budget Development Only**

**Legend**

-  Documented SSO
-  Suspected SSO
-  Haul Operation
-  Proposed Pump Station Solution
-  Pump Station
-  WWTP
-  Proposed Pipe Solution
-  Force Main
-  Collector < 12"
-  Interceptor => 12"
-  Combined Sewer Pipe
-  Proposed Off-line Storage
-  Road
-  Streams
-  Floodway
-  Small WWTP Service Area
-  Large WWTP Service Area
-  CSO Area
-  Metro Parks

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

1 inch = 100 feet  
 Scalable when printed on 11" X 17" paper



Some boundaries are uniquely symbolized within the map.

Map Revision  
 May 07, 2009  
 Aerial Date: 2006



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<b>Project Name</b>	Shively Interceptor
<b>Project Number</b>	S_MC_WC_NB01_M_01_A
<b>Modeled Area</b>	Mill Creek
<b>Branch or SSO ID</b>	NB01
<b>Project Type</b>	Pipe Upgrades
<b>Receiving Stream</b>	Mill Creek and Heatherfield Ditch
<b>Project Description</b>	Construct 18,830 LF of new gravity sewers (10" – 27") to eliminate pump stations. This is the Shively Interceptor capital improvement project.
<b>Reason for Overflow</b>	Pump station capacity (hydraulic bottleneck & backwater effects)
<b>Design Parameters</b>	This solution is based on a 2.60 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$16,419,000
<b>Weighted Benefit/Cost Ratio</b>	6.7

Asset ID	SSO Start Date	Volume (Gal)
MSD0047-PS	1/24/2002	144000
81814-W	1/24/2002	180000
MSD0047-PS	1/3/2005	198000
MSD0047-PS	10/18/2004	115500
MSD0047-PS	11/10/2002	72000
MSD0047-PS	11/11/2004	214500
MSD0047-PS	12/16/2000	0
MSD0050-PS	12/16/2000	0
MSD0047-PS	12/16/2001	54500
MSD0047-PS	12/19/2002	156000
MSD0047-PS	2/25/2011	117000
81814-W	3/19/2008	11500
MSD0047-PS	3/26/2002	144000
MSD0050-PS	3/9/2011	36250
MSD0047-PS	3/9/2011	112750
MSD0044-PS	3/9/2011	39500
MSD0044-PS	4/12/2011	28750
MSD0043-PS	4/12/2011	69750
MSD0047-PS	4/12/2011	79750
MSD0047-PS	4/25/2003	103500
MSD0050-PS	4/27/2011	162000
MSD0047-PS	4/27/2011	162000
MSD0049-PS	4/27/2011	108000
MSD0047-PS	4/28/2002	12000
MSD0047-PS	4/4/2008	426000
MSD0047-PS	5/13/2002	72030
81814-W	5/17/2003	45000
MSD0047-PS	5/17/2003	63000
81814-W	5/2/2010	217500

Project Name	Shively Interceptor	
Project Number	S_MC_WC_NB01_M_01_A	
MSD0047-PS	5/2/2010	216000
MSD0047-PS	5/25/2004	35000
MSD0050-PS	5/26/2011	300
MSD0047-PS	5/27/2004	99000
MSD0047-PS	5/27/2004	12250
MSD0047-PS	5/27/2004	26500
MSD0049-PS	5/29/2012	9999
MSD0047-PS	5/5/2003	81000
81814-W	5/8/2009	5000
MSD0049-PS	6/22/2011	9999
MSD0047-PS	7/22/2001	40500
MSD0047-PS	8/2/2003	90000
MSD0047-PS	8/30/2005	143000
81814-W	8/4/2009	9999
MSD0016-PS	8/4/2009	1375
MSD0047-PS	9/2/2003	18000
MSD0049-PS	9/26/2011	9999
MSD0047-PS	9/27/2002	365000



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Mill Creek Sewershed  
 Solution ID # S\_MC\_WC\_NB01\_M\_01\_A  
 Shively Interceptor

**Preliminary - For Budget Development Only**

**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- Proposed Pump Station Solution
- Pump Station
- WWTP
- Proposed Pipe Solution
- Force Main
- Collector < 12"
- Interceptor => 12"
- Combined Sewer Pipe
- Proposed Off-line Storage
- Road
- Streams
- Floodway
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Metro Parks

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 800 feet  
 Scalable when printed on 11" X 17" paper



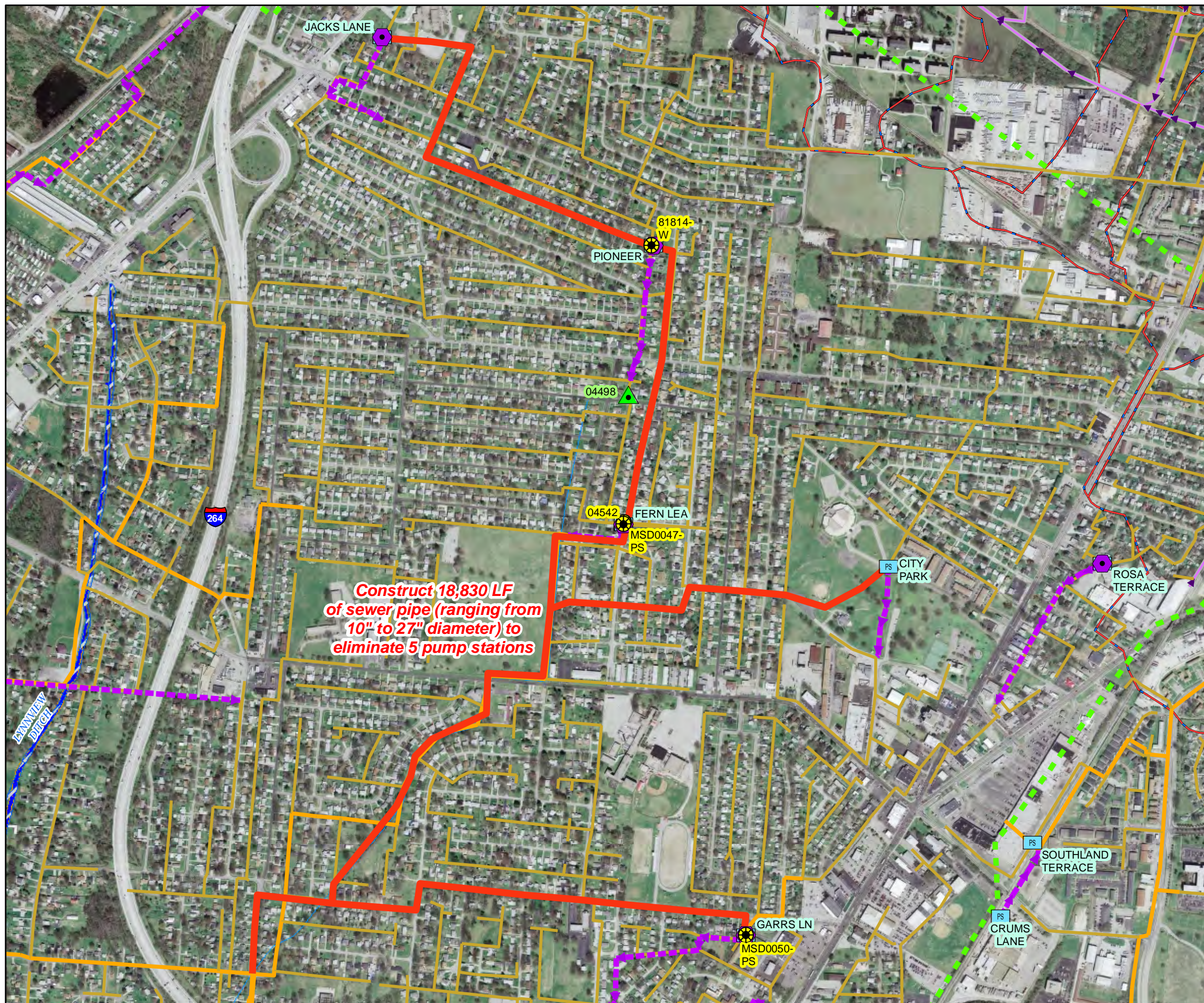
Some boundaries are uniquely symbolized within the map.

Map Revision  
 May 07, 2009

Aerial Date: 2006



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<b>Project Name</b>	Camp Taylor System Improvements Phase 1 - SSES
<b>Project Number</b>	S_SF_MF_30917_M_09_A
<b>Modeled Area</b>	CSO
<b>Branch or SSO ID</b>	30917
<b>Project Type</b>	SSES
<b>Receiving Stream</b>	South Fork Beargrass Creek, Muddy Fork Beargrass Creek, and Camp Taylor Ditch
<b>Project Description</b>	This phase is a special study which includes a full SSES of the entire Camp Taylor area.
<b>Reason for Overflow</b>	System capacity and poor system conditions in some areas
<b>Design Parameters</b>	Estimated capital costs include all four phases.
<b>Project Constraints</b>	Some overflow volumes were estimated using regression equation not by a hydraulic model.
<b>Estimated Capital Cost</b>	\$28,279,000
<b>Weighted Benefit/Cost Ratio</b>	Unavailable at this time

Asset ID	SSO Start Date	Volume (Gal)
99259	1/13/2013	28000
66349	1/13/2013	57500
104231	1/13/2013	58500
36763	1/13/2013	40500
13943	1/13/2013	37500
44397	1/14/2007	9000
44397	1/17/2006	6800
44397	1/23/2006	2300
104223	1/23/2012	5100
104231	1/26/2012	12600
13943	1/27/2012	21000
44397	1/3/2005	266800
104231	10/1/2012	1880
44397	10/18/2004	10000
104231	10/23/2007	3000
44397	10/23/2007	8640
99259	10/30/2013	6000
13946	10/30/2013	6000
66349	10/30/2013	1500
36763	10/30/2013	1500
66349	10/5/2013	7200
99259	10/5/2013	1500
104231	10/5/2013	180000
13943	10/5/2013	1500
13931	10/5/2013	32000
36763	10/5/2013	4200
13946	10/6/2013	24000
51301	10/9/2009	540
13943	10/9/2009	554



**Project Name**    **Camp Taylor System Improvements Phase 1 - SSES**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

104231	10/9/2009	108000
13946	11/17/2013	72000
99259	11/17/2013	4800
66349	11/17/2013	75000
36763	11/17/2013	33600
13943	11/17/2013	1500
104231	11/22/2011	27000
13943	11/25/2010	780
104231	11/25/2010	1200
13943	11/28/2011	31000
104231	11/28/2011	39000
104231	11/30/2010	9000
44397	12/15/2007	7020
104231	12/15/2007	600
104231	12/22/2013	15000
13946	12/22/2013	49500
13931	12/22/2013	9000
99259	12/22/2013	5700
36763	12/22/2013	39000
13943	12/22/2013	3000
13943	12/5/2011	21000
104231	12/5/2011	399000
104231	12/8/2012	900
13943	12/8/2012	180
13943	12/9/2012	1500
104231	12/9/2012	21000
66349	12/9/2012	2400
44397	2/13/2007	1980
13943	2/24/2011	6000
104231	2/24/2011	11950
104231	2/28/2011	10900
44397	3/1/2007	2160
44397	3/12/2006	52900
104231	3/17/2012	16800
13943	3/17/2012	1800
66349	3/18/2013	7200
104231	3/18/2013	108000
99259	3/18/2013	720
36763	3/18/2013	1440
13943	3/18/2013	1320
13943	3/19/2008	250
44397	3/19/2008	27540
104231	3/23/2012	1000

**Project Name**    **Camp Taylor System Improvements Phase 1 - SSES**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

44397	3/27/2008	16740
13931	3/4/2008	6000
44397	3/4/2008	10800
13943	3/5/2011	100
44396	3/9/2011	31250
13943	3/9/2011	327500
104231	3/9/2011	264000
104231	4/1/2012	54000
13943	4/1/2012	720
44396	4/1/2012	3600
44396	4/11/2011	365250
13943	4/11/2011	345500
104231	4/11/2011	385500
99259	4/12/2011	100
44397	4/14/2007	6210
104231	4/19/2013	150
44397	4/21/2006	36800
104231	4/23/2011	845000
44396	4/23/2011	5500
13943	4/23/2011	17000
36763	4/23/2011	194000
99259	4/27/2011	36000
66349	4/27/2011	36000
44397	4/3/2007	5940
44397	4/4/2008	79500
13943	4/4/2008	250
44396	4/4/2008	79500
104231	5/1/2010	573120
13943	5/1/2011	32000
104231	5/1/2011	152000
13943	5/10/2013	900
104231	5/10/2013	10800
66349	5/10/2013	1800
104231	5/12/2010	1300
104231	5/13/2012	72000
13943	5/13/2012	1800
44397	5/15/2008	12750
44397	5/19/2005	210000
99259	5/2/2010	4320
104223	5/2/2010	36000
44396	5/2/2010	77760
51301	5/2/2010	144000
104223	5/20/2005	40

**Project Name**    **Camp Taylor System Improvements Phase 1 - SSES**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

104231	5/21/2010	105000
13943	5/21/2010	4500
51301	5/21/2010	9000
13943	5/23/2011	1200
104231	5/23/2011	36000
104231	5/26/2011	5500
44397	5/27/2004	14000
13931	5/29/2012	1200
44396	5/29/2012	30000
13943	5/29/2012	27500
104231	5/29/2012	140000
44396	5/3/2011	162000
44397	5/30/2004	208000
104231	5/31/2012	11500
13943	5/31/2012	3500
104231	5/5/2012	250
104231	5/5/2013	7200
13946	5/6/2011	100
104231	5/8/2009	27000
13943	5/8/2009	360
104231	6/15/2011	100
44397	6/2/2006	50600
104231	6/22/2011	96000
13943	6/22/2011	4500
66349	6/22/2011	15000
13931	6/23/2011	100
13943	6/26/2013	1500
104231	6/26/2013	6000
36763	6/26/2013	4500
104231	7/13/2010	500
44397	7/14/2006	9720
13943	7/14/2012	360
104231	7/14/2012	6300
44397	7/19/2007	1620
104231	7/19/2012	3000
13943	7/20/2011	420
44396	7/20/2011	100
104231	7/20/2011	4500
99259	7/22/2013	1000
36763	7/22/2013	3000
13943	7/22/2013	1000
66349	7/22/2013	12000
104231	7/22/2013	40500



**Project Name**    **Camp Taylor System Improvements Phase 1 - SSES**

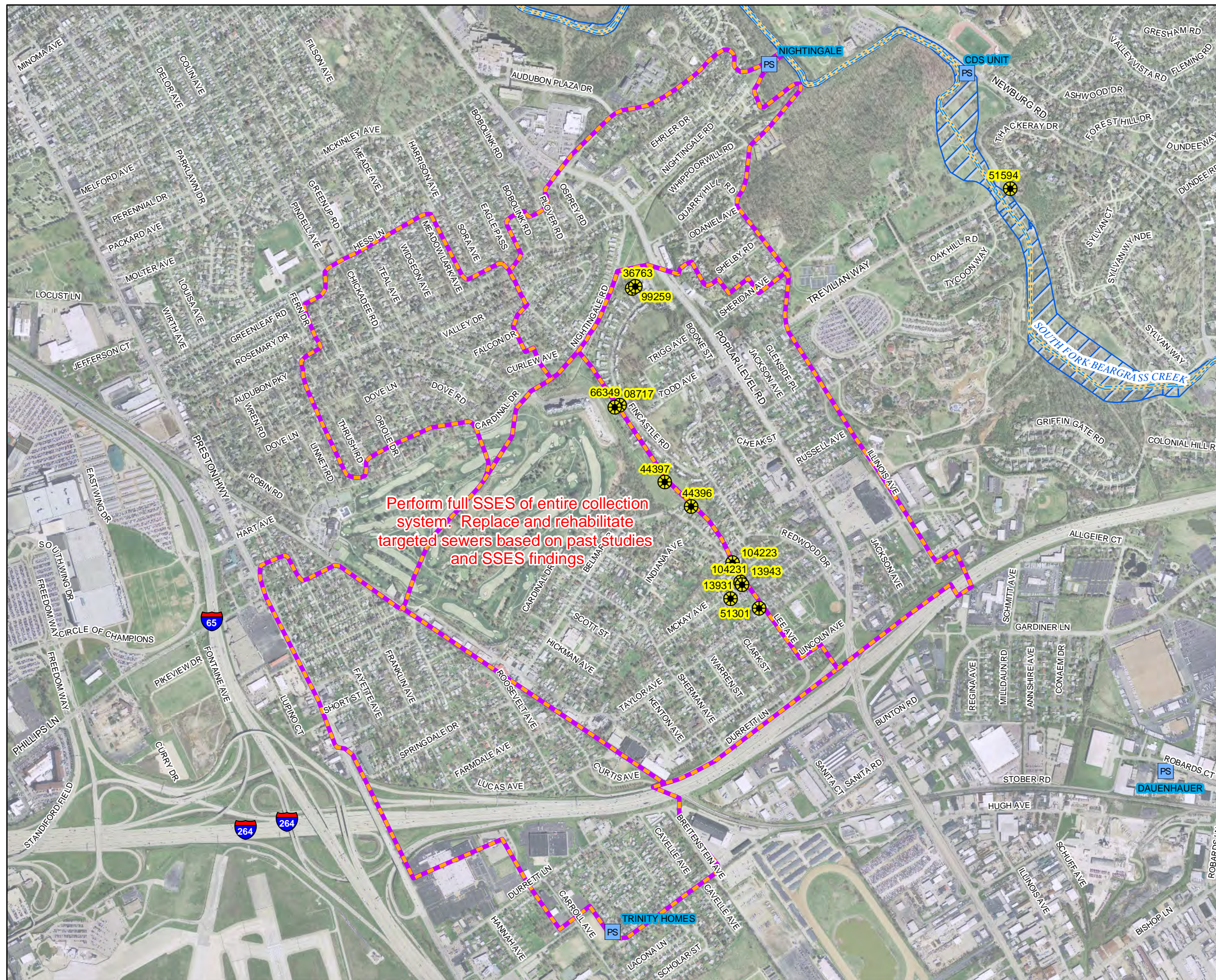
**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

13931	7/22/2013	100
104231	7/27/2012	50
36763	7/29/2009	1800
44396	7/29/2009	15000
99259	7/29/2009	1800
104231	7/29/2009	75000
13943	8/12/2013	100
36763	8/12/2013	100
36763	8/21/2013	100
104231	8/21/2013	100
44397	8/30/2005	9200
51301	8/4/2009	144000
44396	8/4/2009	144000
13943	8/4/2009	4320
104231	8/4/2009	351360
99259	8/4/2009	144000
13931	8/4/2009	77760
36763	8/4/2009	77760
66349	8/4/2009	77760
13943	8/7/2011	1500
104231	8/7/2011	18000
99259	8/9/2013	100
104231	9/1/2012	100
13943	9/20/2009	3000
104231	9/20/2009	52500
51301	9/20/2009	21000
44397	9/22/2006	9900
44396	9/26/2011	5550
104231	9/26/2011	4800
13943	9/26/2011	1100
104231	9/5/2012	100



**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan  
Combined Sewer System  
Camp Taylor System Improvements**

Preliminary - For Budget Development Only



Perform full SSES of entire collection system. Replace and rehabilitate targeted sewers based on past studies and SSES findings

- Documented SSO
- Suspected SSO
- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- MSD
- Streams
- Floodway
- SSES Area
- Jefferson County Boundary

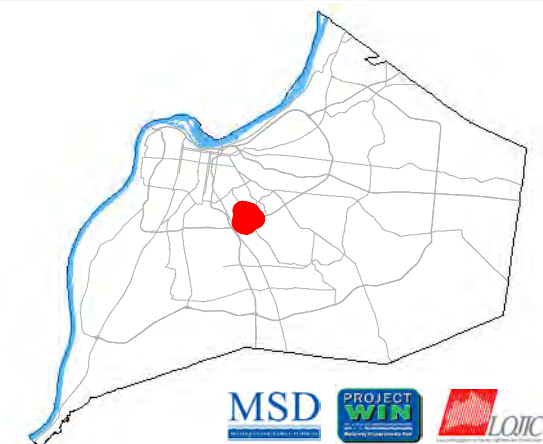
General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,123 feet



Aerial Date: 2009

Map Revision: April 9, 2012



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<b>Project Name</b>	Camp Taylor System Improvements Phase 2 - Sewer Replacement and Rehabilitation
<b>Project Number</b>	S_SF_MF_30917_M_09_A
<b>Modeled Area</b>	CSO
<b>Branch or SSO ID</b>	30917
<b>Project Type</b>	Sewer Replacement and Rehabilitation
<b>Receiving Stream</b>	South Fork Beargrass Creek, Muddy Fork Beargrass Creek, and Camp Taylor Ditch
<b>Project Description</b>	This alternative includes replacement of target sewers based on past studies and historical work orders.
<b>Reason for Overflow</b>	System capacity and poor system conditions in some areas
<b>Design Parameters</b>	This solution is based on a 2.60 inch cloudburst rain event. Estimated capital costs include all four phases.
<b>Project Constraints</b>	Some overflow volumes were estimated using regression equation not by a hydraulic model.
<b>Estimated Capital Cost</b>	\$28,279,000
<b>Weighted Benefit/Cost Ratio</b>	Unavailable at this time

Asset ID	SSO Start Date	Volume (Gal)
99259	1/13/2013	28000
66349	1/13/2013	57500
104231	1/13/2013	58500
36763	1/13/2013	40500
13943	1/13/2013	37500
44397	1/14/2007	9000
44397	1/17/2006	6800
44397	1/23/2006	2300
104223	1/23/2012	5100
104231	1/26/2012	12600
13943	1/27/2012	21000
44397	1/3/2005	266800
104231	10/1/2012	1880
44397	10/18/2004	10000
104231	10/23/2007	3000
44397	10/23/2007	8640
99259	10/30/2013	6000
13946	10/30/2013	6000
66349	10/30/2013	1500
36763	10/30/2013	1500
66349	10/5/2013	7200
99259	10/5/2013	1500
104231	10/5/2013	180000
13943	10/5/2013	1500
13931	10/5/2013	32000
36763	10/5/2013	4200
13946	10/6/2013	24000
51301	10/9/2009	540



**Project Name**    **Camp Taylor System Improvements Phase 2 - Sewer Replacement and Rehabilitation**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

13943	10/9/2009	554
104231	10/9/2009	108000
13946	11/17/2013	72000
99259	11/17/2013	4800
66349	11/17/2013	75000
36763	11/17/2013	33600
13943	11/17/2013	1500
104231	11/22/2011	27000
13943	11/25/2010	780
104231	11/25/2010	1200
13943	11/28/2011	31000
104231	11/28/2011	39000
104231	11/30/2010	9000
44397	12/15/2007	7020
104231	12/15/2007	600
104231	12/22/2013	15000
13946	12/22/2013	49500
13931	12/22/2013	9000
99259	12/22/2013	5700
36763	12/22/2013	39000
13943	12/22/2013	3000
13943	12/5/2011	21000
104231	12/5/2011	399000
104231	12/8/2012	900
13943	12/8/2012	180
13943	12/9/2012	1500
104231	12/9/2012	21000
66349	12/9/2012	2400
44397	2/13/2007	1980
13943	2/24/2011	6000
104231	2/24/2011	11950
104231	2/28/2011	10900
44397	3/1/2007	2160
44397	3/12/2006	52900
104231	3/17/2012	16800
13943	3/17/2012	1800
66349	3/18/2013	7200
104231	3/18/2013	108000
99259	3/18/2013	720
36763	3/18/2013	1440
13943	3/18/2013	1320
13943	3/19/2008	250
44397	3/19/2008	27540

**Project Name**    **Camp Taylor System Improvements Phase 2 - Sewer Replacement and Rehabilitation**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

104231	3/23/2012	1000
44397	3/27/2008	16740
13931	3/4/2008	6000
44397	3/4/2008	10800
13943	3/5/2011	100
44396	3/9/2011	31250
13943	3/9/2011	327500
104231	3/9/2011	264000
104231	4/1/2012	54000
13943	4/1/2012	720
44396	4/1/2012	3600
44396	4/11/2011	365250
13943	4/11/2011	345500
104231	4/11/2011	385500
99259	4/12/2011	100
44397	4/14/2007	6210
104231	4/19/2013	150
44397	4/21/2006	36800
104231	4/23/2011	845000
44396	4/23/2011	5500
13943	4/23/2011	17000
36763	4/23/2011	194000
99259	4/27/2011	36000
66349	4/27/2011	36000
44397	4/3/2007	5940
44397	4/4/2008	79500
13943	4/4/2008	250
44396	4/4/2008	79500
104231	5/1/2010	573120
13943	5/1/2011	32000
104231	5/1/2011	152000
13943	5/10/2013	900
104231	5/10/2013	10800
66349	5/10/2013	1800
104231	5/12/2010	1300
104231	5/13/2012	72000
13943	5/13/2012	1800
44397	5/15/2008	12750
44397	5/19/2005	210000
99259	5/2/2010	4320
104223	5/2/2010	36000
44396	5/2/2010	77760
51301	5/2/2010	144000

**Project Name**    **Camp Taylor System Improvements Phase 2 - Sewer Replacement and Rehabilitation**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

104223	5/20/2005	40
104231	5/21/2010	105000
13943	5/21/2010	4500
51301	5/21/2010	9000
13943	5/23/2011	1200
104231	5/23/2011	36000
104231	5/26/2011	5500
44397	5/27/2004	14000
13931	5/29/2012	1200
44396	5/29/2012	30000
13943	5/29/2012	27500
104231	5/29/2012	140000
44396	5/3/2011	162000
44397	5/30/2004	208000
104231	5/31/2012	11500
13943	5/31/2012	3500
104231	5/5/2012	250
104231	5/5/2013	7200
13946	5/6/2011	100
104231	5/8/2009	27000
13943	5/8/2009	360
104231	6/15/2011	100
44397	6/2/2006	50600
104231	6/22/2011	96000
13943	6/22/2011	4500
66349	6/22/2011	15000
13931	6/23/2011	100
13943	6/26/2013	1500
104231	6/26/2013	6000
36763	6/26/2013	4500
104231	7/13/2010	500
44397	7/14/2006	9720
13943	7/14/2012	360
104231	7/14/2012	6300
44397	7/19/2007	1620
104231	7/19/2012	3000
13943	7/20/2011	420
44396	7/20/2011	100
104231	7/20/2011	4500
99259	7/22/2013	1000
36763	7/22/2013	3000
13943	7/22/2013	1000
66349	7/22/2013	12000



**Project Name**    **Camp Taylor System Improvements Phase 2 - Sewer Replacement and Rehabilitation**

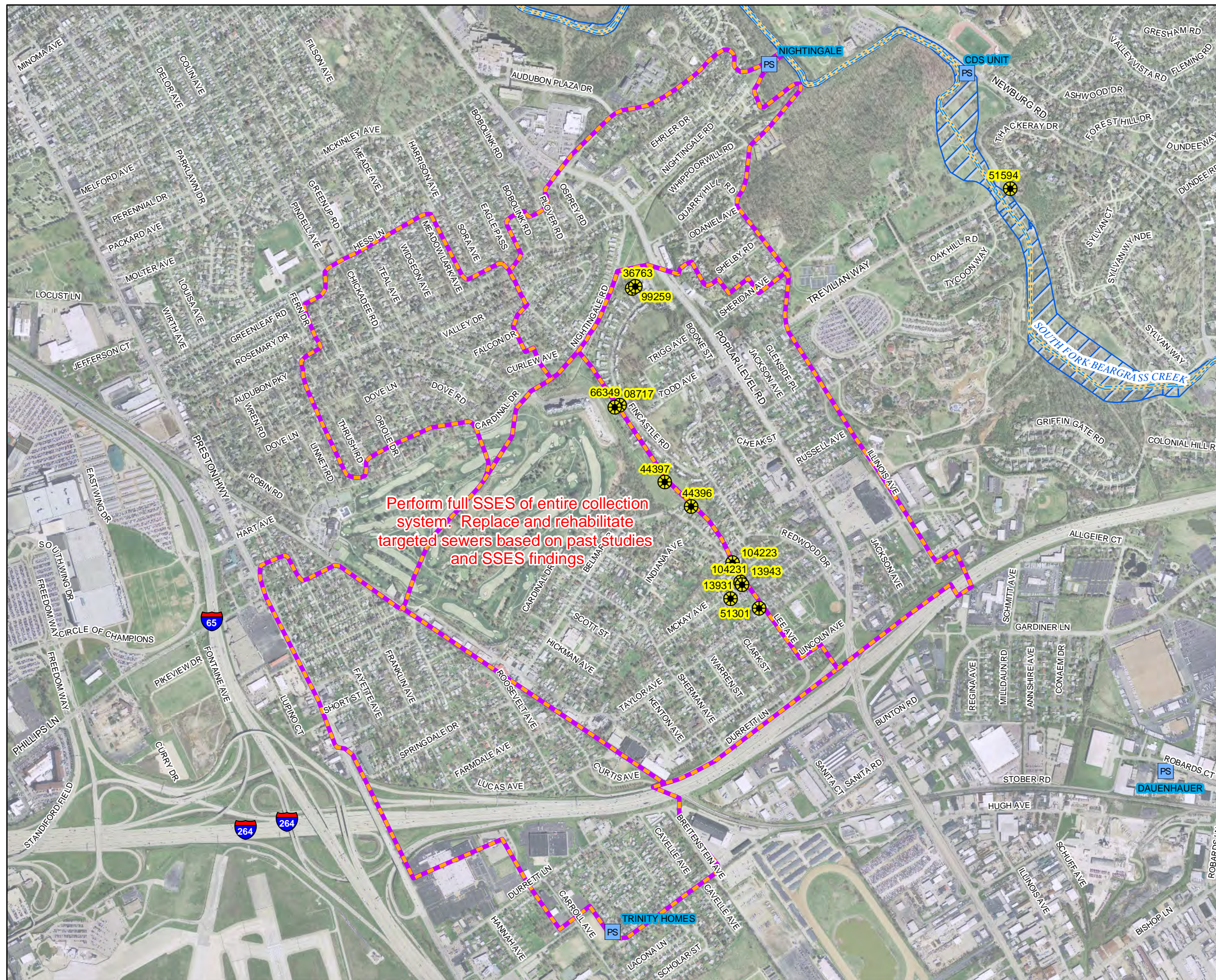
**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

104231	7/22/2013	40500
13931	7/22/2013	100
104231	7/27/2012	50
36763	7/29/2009	1800
44396	7/29/2009	15000
99259	7/29/2009	1800
104231	7/29/2009	75000
13943	8/12/2013	100
36763	8/12/2013	100
36763	8/21/2013	100
104231	8/21/2013	100
44397	8/30/2005	9200
51301	8/4/2009	144000
44396	8/4/2009	144000
13943	8/4/2009	4320
104231	8/4/2009	351360
99259	8/4/2009	144000
13931	8/4/2009	77760
36763	8/4/2009	77760
66349	8/4/2009	77760
13943	8/7/2011	1500
104231	8/7/2011	18000
99259	8/9/2013	100
104231	9/1/2012	100
13943	9/20/2009	3000
104231	9/20/2009	52500
51301	9/20/2009	21000
44397	9/22/2006	9900
44396	9/26/2011	5550
104231	9/26/2011	4800
13943	9/26/2011	1100
104231	9/5/2012	100



**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan  
Combined Sewer System  
Camp Taylor System Improvements**

Preliminary - For Budget Development Only

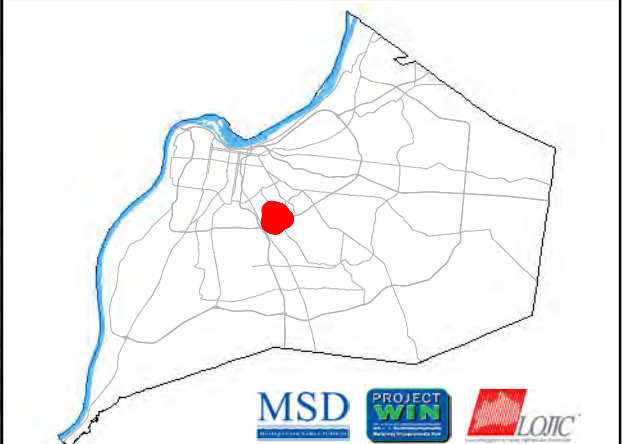


Perform full SSES of entire collection system. Replace and rehabilitate targeted sewers based on past studies and SSES findings

- Documented SSO
- Suspected SSO
- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- MSD
- Streams
- Floodway
- SSES Area
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,123 feet       Aerial Date: 2009    Map Revision: April 9, 2012



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<b>Project Name</b>	Camp Taylor System Improvements 3 - Sewer Replacement & Sewer Rehabilitation
<b>Project Number</b>	S_SF_MF_30917_M_09_A
<b>Modeled Area</b>	CSO
<b>Branch or SSO ID</b>	30917
<b>Project Type</b>	Sewer Replacement and Sewer Rehabilitation
<b>Receiving Stream</b>	South Fork Beargrass Creek, Muddy Fork Beargrass Creek, and Camp Taylor Ditch
<b>Project Description</b>	Phase 2 of replacement of target sewers after full SSES. Additional rehabilitation of sewers based on SSES findings.
<b>Reason for Overflow</b>	System capacity and poor system conditions in some areas
<b>Design Parameters</b>	This solution is based on a 2.60 inch cloudburst rain event. Estimated capital costs include all four phases.
<b>Project Constraints</b>	Some overflow volumes were estimated using regression equation not by a hydraulic model.
<b>Estimated Capital Cost</b>	\$28,279,000
<b>Weighted Benefit/Cost Ratio</b>	Unavailable at this time

Asset ID	SSO Start Date	Volume (Gal)
66349	1/13/2013	57500
13943	1/13/2013	37500
36763	1/13/2013	40500
99259	1/13/2013	28000
104231	1/13/2013	58500
44397	1/14/2007	9000
44397	1/17/2006	6800
44397	1/23/2006	2300
104223	1/23/2012	5100
104231	1/26/2012	12600
13943	1/27/2012	21000
44397	1/3/2005	266800
104231	10/1/2012	1880
44397	10/18/2004	10000
104231	10/23/2007	3000
44397	10/23/2007	8640
66349	10/30/2013	1500
36763	10/30/2013	1500
99259	10/30/2013	6000
13946	10/30/2013	6000
66349	10/5/2013	7200
13931	10/5/2013	32000
13943	10/5/2013	1500
104231	10/5/2013	180000
36763	10/5/2013	4200
99259	10/5/2013	1500
13946	10/6/2013	24000
51301	10/9/2009	540



**Project Name**    **Camp Taylor System Improvements 3 - Sewer Replacement & Sewer Rehabilitation**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

13943	10/9/2009	554
104231	10/9/2009	108000
66349	11/17/2013	75000
13946	11/17/2013	72000
99259	11/17/2013	4800
36763	11/17/2013	33600
13943	11/17/2013	1500
104231	11/22/2011	27000
13943	11/25/2010	780
104231	11/25/2010	1200
104231	11/28/2011	39000
13943	11/28/2011	31000
104231	11/30/2010	9000
104231	12/15/2007	600
44397	12/15/2007	7020
13943	12/22/2013	3000
99259	12/22/2013	5700
13931	12/22/2013	9000
36763	12/22/2013	39000
13946	12/22/2013	49500
104231	12/22/2013	15000
13943	12/5/2011	21000
104231	12/5/2011	399000
13943	12/8/2012	180
104231	12/8/2012	900
104231	12/9/2012	21000
13943	12/9/2012	1500
66349	12/9/2012	2400
44397	2/13/2007	1980
104231	2/24/2011	11950
13943	2/24/2011	6000
104231	2/28/2011	10900
44397	3/1/2007	2160
44397	3/12/2006	52900
104231	3/17/2012	16800
13943	3/17/2012	1800
104231	3/18/2013	108000
66349	3/18/2013	7200
99259	3/18/2013	720
36763	3/18/2013	1440
13943	3/18/2013	1320
44397	3/19/2008	27540
13943	3/19/2008	250

**Project Name**    **Camp Taylor System Improvements 3 - Sewer Replacement & Sewer Rehabilitation**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

104231	3/23/2012	1000
44397	3/27/2008	16740
13931	3/4/2008	6000
44397	3/4/2008	10800
13943	3/5/2011	100
13943	3/9/2011	327500
44396	3/9/2011	31250
104231	3/9/2011	264000
44396	4/1/2012	3600
104231	4/1/2012	54000
13943	4/1/2012	720
13943	4/11/2011	345500
44396	4/11/2011	365250
104231	4/11/2011	385500
99259	4/12/2011	100
44397	4/14/2007	6210
104231	4/19/2013	150
44397	4/21/2006	36800
13943	4/23/2011	17000
104231	4/23/2011	845000
44396	4/23/2011	5500
36763	4/23/2011	194000
99259	4/27/2011	36000
66349	4/27/2011	36000
44397	4/3/2007	5940
44397	4/4/2008	79500
44396	4/4/2008	79500
13943	4/4/2008	250
104231	5/1/2010	573120
104231	5/1/2011	152000
13943	5/1/2011	32000
66349	5/10/2013	1800
13943	5/10/2013	900
104231	5/10/2013	10800
104231	5/12/2010	1300
13943	5/13/2012	1800
104231	5/13/2012	72000
44397	5/15/2008	12750
44397	5/19/2005	210000
99259	5/2/2010	4320
104223	5/2/2010	36000
44396	5/2/2010	77760
51301	5/2/2010	144000

**Project Name**    **Camp Taylor System Improvements 3 - Sewer Replacement & Sewer Rehabilitation**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

104223	5/20/2005	40
104231	5/21/2010	105000
51301	5/21/2010	9000
13943	5/21/2010	4500
13943	5/23/2011	1200
104231	5/23/2011	36000
104231	5/26/2011	5500
44397	5/27/2004	14000
13931	5/29/2012	1200
104231	5/29/2012	140000
13943	5/29/2012	27500
44396	5/29/2012	30000
44396	5/3/2011	162000
44397	5/30/2004	208000
13943	5/31/2012	3500
104231	5/31/2012	11500
104231	5/5/2012	250
104231	5/5/2013	7200
13946	5/6/2011	100
13943	5/8/2009	360
104231	5/8/2009	27000
104231	6/15/2011	100
44397	6/2/2006	50600
104231	6/22/2011	96000
66349	6/22/2011	15000
13943	6/22/2011	4500
13931	6/23/2011	100
36763	6/26/2013	4500
104231	6/26/2013	6000
13943	6/26/2013	1500
104231	7/13/2010	500
44397	7/14/2006	9720
13943	7/14/2012	360
104231	7/14/2012	6300
44397	7/19/2007	1620
104231	7/19/2012	3000
44396	7/20/2011	100
104231	7/20/2011	4500
13943	7/20/2011	420
104231	7/22/2013	40500
13931	7/22/2013	100
13943	7/22/2013	1000
36763	7/22/2013	3000



**Project Name**    **Camp Taylor System Improvements 3 - Sewer Replacement & Sewer Rehabilitation**

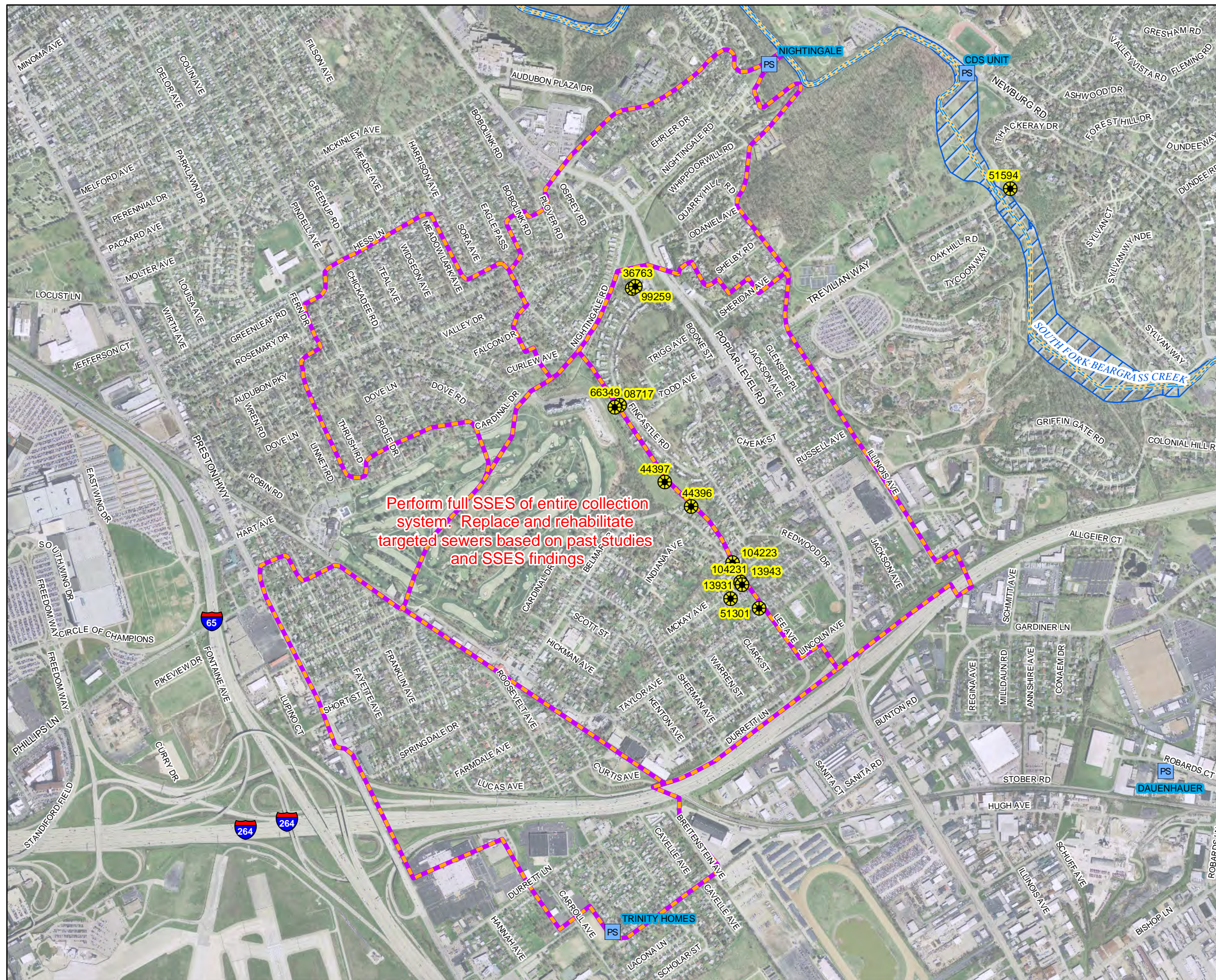
**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

66349	7/22/2013	12000
99259	7/22/2013	1000
104231	7/27/2012	50
104231	7/29/2009	75000
44396	7/29/2009	15000
99259	7/29/2009	1800
36763	7/29/2009	1800
36763	8/12/2013	100
13943	8/12/2013	100
104231	8/21/2013	100
36763	8/21/2013	100
44397	8/30/2005	9200
104231	8/4/2009	351360
51301	8/4/2009	144000
99259	8/4/2009	144000
44396	8/4/2009	144000
13943	8/4/2009	4320
36763	8/4/2009	77760
66349	8/4/2009	77760
13931	8/4/2009	77760
13943	8/7/2011	1500
104231	8/7/2011	18000
99259	8/9/2013	100
104231	9/1/2012	100
13943	9/20/2009	3000
104231	9/20/2009	52500
51301	9/20/2009	21000
44397	9/22/2006	9900
44396	9/26/2011	5550
13943	9/26/2011	1100
104231	9/26/2011	4800
104231	9/5/2012	100



**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan  
Combined Sewer System  
Camp Taylor System Improvements**

Preliminary - For Budget Development Only

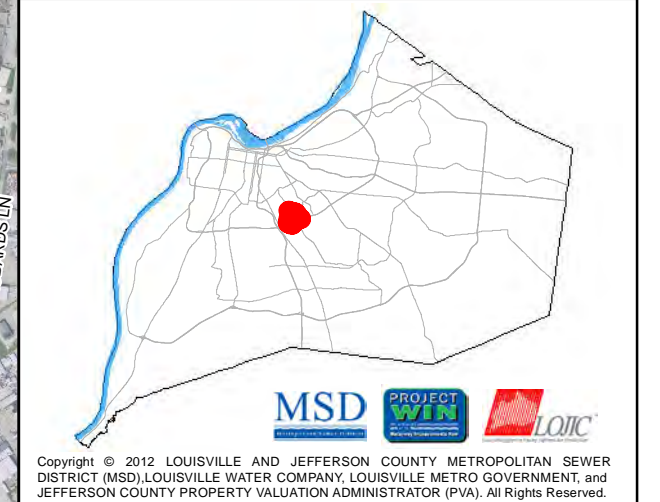


- Documented SSO
- Suspected SSO
- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- MSD
- Streams
- Floodway
- SSES Area
- Jefferson County Boundary

**Perform full SSES of entire collection system. Replace and rehabilitate targeted sewers based on past studies and SSES findings**

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,123 feet		Aerial Date: 2009	Map Revision: April 9, 2012
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<b>Project Name</b>	Camp Taylor System Improvements Phase 4 - Storage Basin and Sewer Upsize
<b>Project Number</b>	S_SF_MF_30917_M_09_A
<b>Modeled Area</b>	CSO
<b>Branch or SSO ID</b>	30917
<b>Project Type</b>	Sewer Replacement and Storage Basin
<b>Receiving Stream</b>	South Fork Beargrass Creek, Muddy Fork Beargrass Creek, and Camp Taylor Ditch
<b>Project Description</b>	This alternative includes additional rehab of sewers based on SSES findings and constructing an off-line pumped 0.038 MG storage basin at the PS to store excess wet weather flows, 3,395 LF of 8" sewer to convey flow to basin. Flow monitoring and system monitoring will be performed in the Camp Taylor system after rehab is complete. If the system is operating with no overflows at a 2.6-inch storm, no storage basin will be constructed. Documentation of this analysis will be submitted to the appropriate regulatory agencies.
<b>Reason for Overflow</b>	System capacity and poor system conditions in some areas
<b>Design Parameters</b>	This solution is based on a 2.60 inch cloudburst rain event. Estimated capital costs include all four phases.
<b>Project Constraints</b>	Some overflow volumes were estimated using regression equation not by a hydraulic model.
<b>Estimated Capital Cost</b>	\$28,279,000
<b>Weighted Benefit/Cost Ratio</b>	Unavailable at this time

Asset ID	SSO Start Date	Volume (Gal)
99259	1/13/2013	28000
66349	1/13/2013	57500
104231	1/13/2013	58500
36763	1/13/2013	40500
13943	1/13/2013	37500
44397	1/14/2007	9000
44397	1/17/2006	6800
44397	1/23/2006	2300
104223	1/23/2012	5100
104231	1/26/2012	12600
13943	1/27/2012	21000
44397	1/3/2005	266800
104231	10/1/2012	1880
44397	10/18/2004	10000
104231	10/23/2007	3000
44397	10/23/2007	8640
99259	10/30/2013	6000
13946	10/30/2013	6000
66349	10/30/2013	1500
36763	10/30/2013	1500
66349	10/5/2013	7200
99259	10/5/2013	1500
104231	10/5/2013	180000
13943	10/5/2013	1500
13931	10/5/2013	32000



**Project Name**    **Camp Taylor System Improvements Phase 4 - Storage Basin and Sewer Upsize**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

36763	10/5/2013	4200
13946	10/6/2013	24000
51301	10/9/2009	540
13943	10/9/2009	554
104231	10/9/2009	108000
13946	11/17/2013	72000
99259	11/17/2013	4800
66349	11/17/2013	75000
36763	11/17/2013	33600
13943	11/17/2013	1500
104231	11/22/2011	27000
13943	11/25/2010	780
104231	11/25/2010	1200
13943	11/28/2011	31000
104231	11/28/2011	39000
104231	11/30/2010	9000
44397	12/15/2007	7020
104231	12/15/2007	600
104231	12/22/2013	15000
13946	12/22/2013	49500
13931	12/22/2013	9000
99259	12/22/2013	5700
36763	12/22/2013	39000
13943	12/22/2013	3000
13943	12/5/2011	21000
104231	12/5/2011	399000
104231	12/8/2012	900
13943	12/8/2012	180
13943	12/9/2012	1500
104231	12/9/2012	21000
66349	12/9/2012	2400
44397	2/13/2007	1980
13943	2/24/2011	6000
104231	2/24/2011	11950
104231	2/28/2011	10900
44397	3/1/2007	2160
44397	3/12/2006	52900
104231	3/17/2012	16800
13943	3/17/2012	1800
66349	3/18/2013	7200
104231	3/18/2013	108000
99259	3/18/2013	720
36763	3/18/2013	1440

**Project Name**    **Camp Taylor System Improvements Phase 4 - Storage Basin and Sewer Upsize**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

13943	3/18/2013	1320
13943	3/19/2008	250
44397	3/19/2008	27540
104231	3/23/2012	1000
44397	3/27/2008	16740
13931	3/4/2008	6000
44397	3/4/2008	10800
13943	3/5/2011	100
44396	3/9/2011	31250
13943	3/9/2011	327500
104231	3/9/2011	264000
104231	4/1/2012	54000
13943	4/1/2012	720
44396	4/1/2012	3600
44396	4/11/2011	365250
13943	4/11/2011	345500
104231	4/11/2011	385500
99259	4/12/2011	100
44397	4/14/2007	6210
104231	4/19/2013	150
44397	4/21/2006	36800
104231	4/23/2011	845000
44396	4/23/2011	5500
13943	4/23/2011	17000
36763	4/23/2011	194000
99259	4/27/2011	36000
66349	4/27/2011	36000
44397	4/3/2007	5940
44397	4/4/2008	79500
13943	4/4/2008	250
44396	4/4/2008	79500
104231	5/1/2010	573120
13943	5/1/2011	32000
104231	5/1/2011	152000
13943	5/10/2013	900
104231	5/10/2013	10800
66349	5/10/2013	1800
104231	5/12/2010	1300
104231	5/13/2012	72000
13943	5/13/2012	1800
44397	5/15/2008	12750
44397	5/19/2005	210000
99259	5/2/2010	4320

**Project Name**    **Camp Taylor System Improvements Phase 4 - Storage Basin and Sewer Upsize**

**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

104223	5/2/2010	36000
44396	5/2/2010	77760
51301	5/2/2010	144000
104223	5/20/2005	40
104231	5/21/2010	105000
13943	5/21/2010	4500
51301	5/21/2010	9000
13943	5/23/2011	1200
104231	5/23/2011	36000
104231	5/26/2011	5500
44397	5/27/2004	14000
13931	5/29/2012	1200
44396	5/29/2012	30000
13943	5/29/2012	27500
104231	5/29/2012	140000
44396	5/3/2011	162000
44397	5/30/2004	208000
104231	5/31/2012	11500
13943	5/31/2012	3500
104231	5/5/2012	250
104231	5/5/2013	7200
13946	5/6/2011	100
104231	5/8/2009	27000
13943	5/8/2009	360
104231	6/15/2011	100
44397	6/2/2006	50600
104231	6/22/2011	96000
13943	6/22/2011	4500
66349	6/22/2011	15000
13931	6/23/2011	100
13943	6/26/2013	1500
104231	6/26/2013	6000
36763	6/26/2013	4500
104231	7/13/2010	500
44397	7/14/2006	9720
13943	7/14/2012	360
104231	7/14/2012	6300
44397	7/19/2007	1620
104231	7/19/2012	3000
13943	7/20/2011	420
44396	7/20/2011	100
104231	7/20/2011	4500
99259	7/22/2013	1000



**Project Name**    **Camp Taylor System Improvements Phase 4 - Storage Basin and Sewer Upsize**

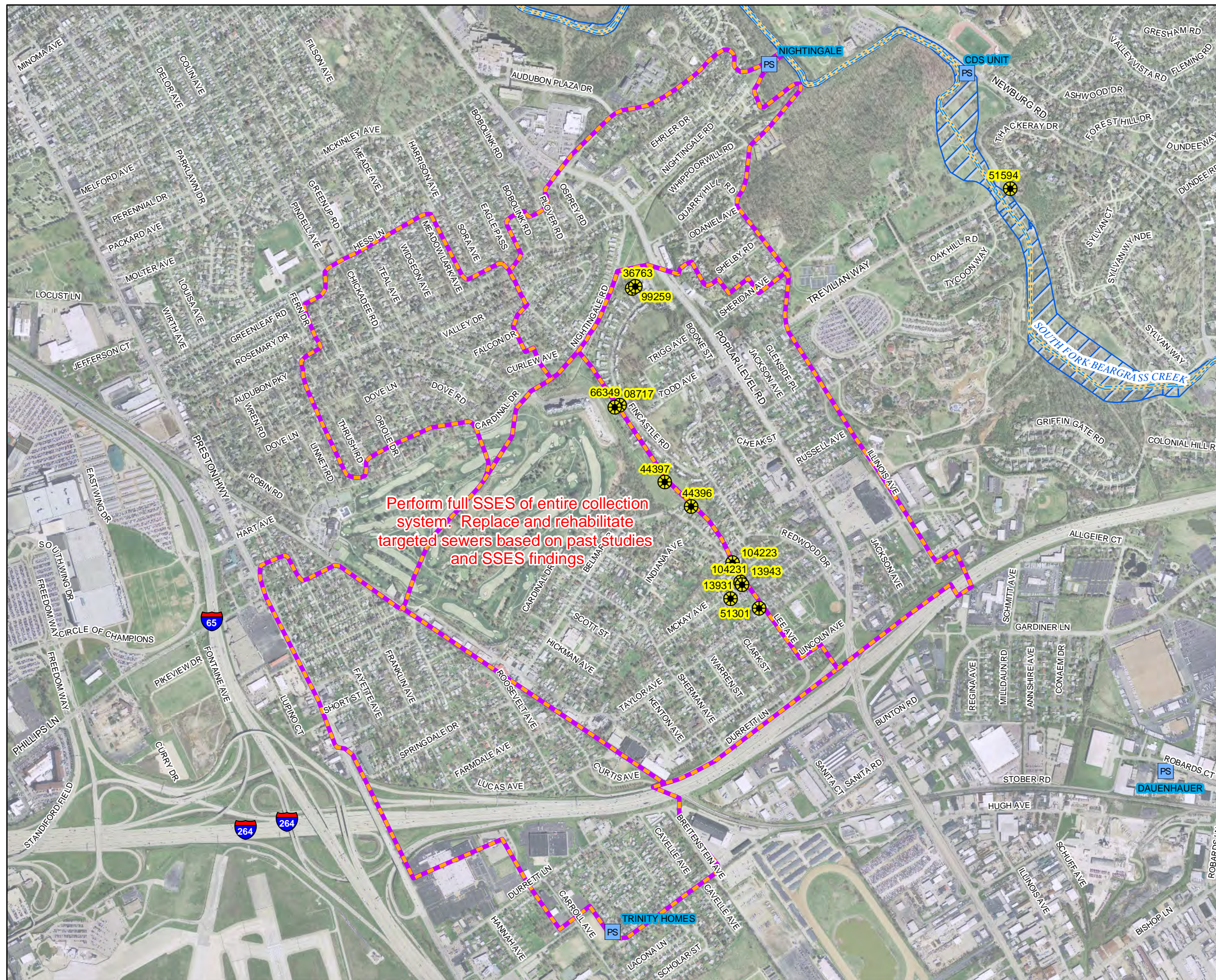
**Project Number**    **S\_SF\_MF\_30917\_M\_09\_A**

36763	7/22/2013	3000
13943	7/22/2013	1000
66349	7/22/2013	12000
104231	7/22/2013	40500
13931	7/22/2013	100
104231	7/27/2012	50
36763	7/29/2009	1800
44396	7/29/2009	15000
99259	7/29/2009	1800
104231	7/29/2009	75000
13943	8/12/2013	100
36763	8/12/2013	100
36763	8/21/2013	100
104231	8/21/2013	100
44397	8/30/2005	9200
51301	8/4/2009	144000
44396	8/4/2009	144000
13943	8/4/2009	4320
104231	8/4/2009	351360
99259	8/4/2009	144000
13931	8/4/2009	77760
36763	8/4/2009	77760
66349	8/4/2009	77760
13943	8/7/2011	1500
104231	8/7/2011	18000
99259	8/9/2013	100
104231	9/1/2012	100
13943	9/20/2009	3000
104231	9/20/2009	52500
51301	9/20/2009	21000
44397	9/22/2006	9900
44396	9/26/2011	5550
104231	9/26/2011	4800
13943	9/26/2011	1100
104231	9/5/2012	100



**Integrated Overflow Abatement Plan  
Vol. 3 - Sanitary Sewer Discharge Plan  
Combined Sewer System  
Camp Taylor System Improvements**

Preliminary - For Budget Development Only

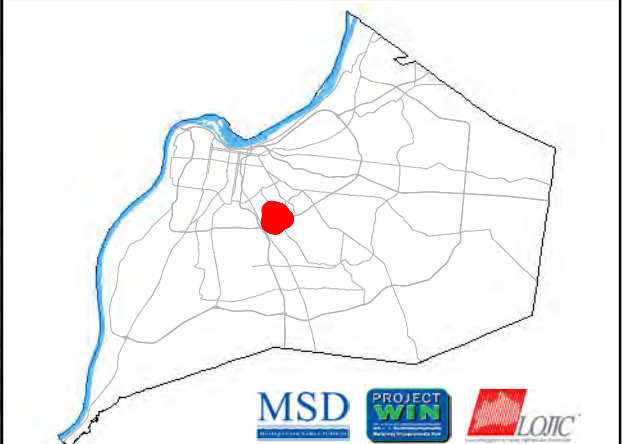


- Documented SSO
- Suspected SSO
- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- MSD
- Streams
- Floodway
- SSES Area
- Jefferson County Boundary

**Perform full SSES of entire collection system. Replace and rehabilitate targeted sewers based on past studies and SSES findings**

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,123 feet       Aerial Date: 2009    Map Revision: April 9, 2012



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**Project Name**     **Hazelwood PS I/I Investigation & Rehabilitation**

**Project Number**     **S\_MC\_MF\_55665\_S\_07\_C**

**Modeled Area**                     CSO

**Branch or SSO ID**                 55665

**Project Type**                        Infiltration Reduction

**Receiving Stream**                 Upper Mill Creek

**Project Description**                This location will be targeted for I/I source control (I/I rehab and private property program).

**Reason for Overflow**                Pump Station capacity

**Design Parameters**                 This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**                 N/A

**Estimated Capital Cost**             \$173,000

**Weighted Benefit/Cost Ratio**        --

Asset ID	SSO Start Date	Volume (Gal)
55665	3/19/2008	28000
55665	4/12/2011	43000
55667	4/12/2011	43000
55665	4/24/2011	25
55665	4/27/2011	18000
55667	4/27/2011	18000
55665	5/3/2011	8400
55665	6/23/2011	5010



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Combined Sewer System  
 Solution ID # S\_MC\_MF\_55665\_S\_07\_C  
 Hazelwood PS I&I Investigation & Rehabilitation

**Preliminary - For Budget Development Only**

**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- Proposed Pump Station Solution
- Pump Station
- WWTP
- Proposed Pipe Solution
- Force Main
- Collector < 12"
- Interceptor => 12"
- Combined Sewer Pipe
- Proposed Off-line Storage
- Road
- Streams
- Floodway
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Metro Parks

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1 inch equals 200 feet  
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Some boundaries are uniquely symbolized within the map.  
 Map Revision  
 May 7, 2009  
 Aerial Date: 2006



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<b>Project Name</b>	Sonne PS I/I Investigation & Rehabilitation
<b>Project Number</b>	S_OR_MF_42007_S_07_C
<b>Modeled Area</b>	CSO
<b>Branch or SSO ID</b>	MSD0042-PS
<b>Project Type</b>	Infiltration Reduction
<b>Receiving Stream</b>	Paddy Run
<b>Project Description</b>	This location will be targeted for I/I source control (I/I rehab and private property program).
<b>Reason for Overflow</b>	System capacity
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$265,000
<b>Weighted Benefit/Cost Ratio</b>	--

Asset ID	SSO Start Date	Volume (Gal)
MSD0042-PS	1/3/2005	90000
MSD0042-PS	10/18/2004	184500
MSD0042-PS	11/10/2002	405000
MSD0042-PS	11/11/2004	114000
MSD0042-PS	11/29/2001	99000
MSD0042-PS	12/15/2007	317850
MSD0042-PS	12/16/2000	0
MSD0042-PS	12/16/2001	54000
MSD0042-PS	12/22/2013	5
MSD0042-PS	3/26/2002	175000
MSD0042-PS	4/25/2003	99000
MSD0042-PS	4/26/2002	226000
MSD0042-PS	4/28/2002	54000
MSD0042-PS	4/4/2008	308700
MSD0042-PS	5/11/2003	45000
MSD0042-PS	5/13/2002	162000
MSD0042-PS	5/2/2010	187500
MSD0042-PS	5/25/2004	38500
MSD0042-PS	5/26/2011	300
MSD0042-PS	5/27/2004	25550
MSD0042-PS	5/29/2012	1950
MSD0042-PS	5/5/2003	81000
MSD0042-PS	8/30/2005	169500
MSD0042-PS	8/4/2009	20220
MSD0042-PS	9/1/2003	27000
MSD0042-PS	9/26/2011	6100




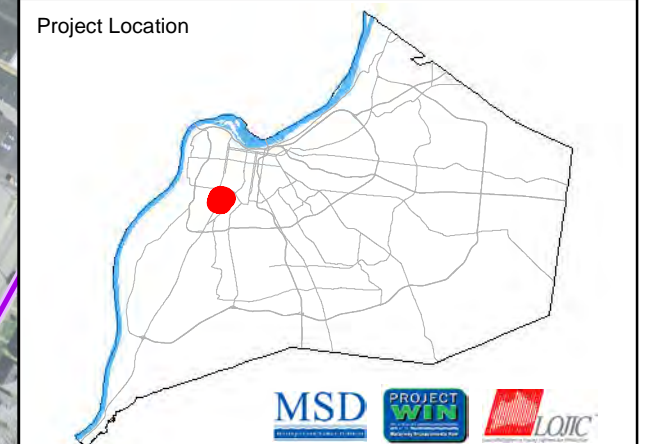
**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
**Combined Sewer System**  
**Sonne PS I&I Investigation & Rehabilitation**

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 300 feet            Aerial Date: 2009      Map Revision: April 9, 2012



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**Small WQTC  
Areas**

**Project Name** Fairway View PS Improvements

**Project Number** S\_HC\_HS\_NB01\_S\_03\_C\_A

**Modeled Area** Hunting Creek South WQTC

**Branch or SSO ID** NB01

**Project Type** Pump Station Upgrades

**Receiving Stream** Harrods Creek

**Project Description** This alternative includes upgrading pumps at Fairway View PS to discharge: 100, 100, and 120 GPM (previously 88 GPM each).

**Reason for Overflow** Pump station capacity

**Design Parameters** This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints** N/A

**Estimated Capital Cost** \$167,000

**Weighted Benefit/Cost Ratio** 10.32

Asset ID	SSO Start Date	Volume (Gal)
MSD1065-PS	10/14/2002	500
MSD1065-PS	3/19/2008	8400
MSD1065-PS	6/9/2003	300



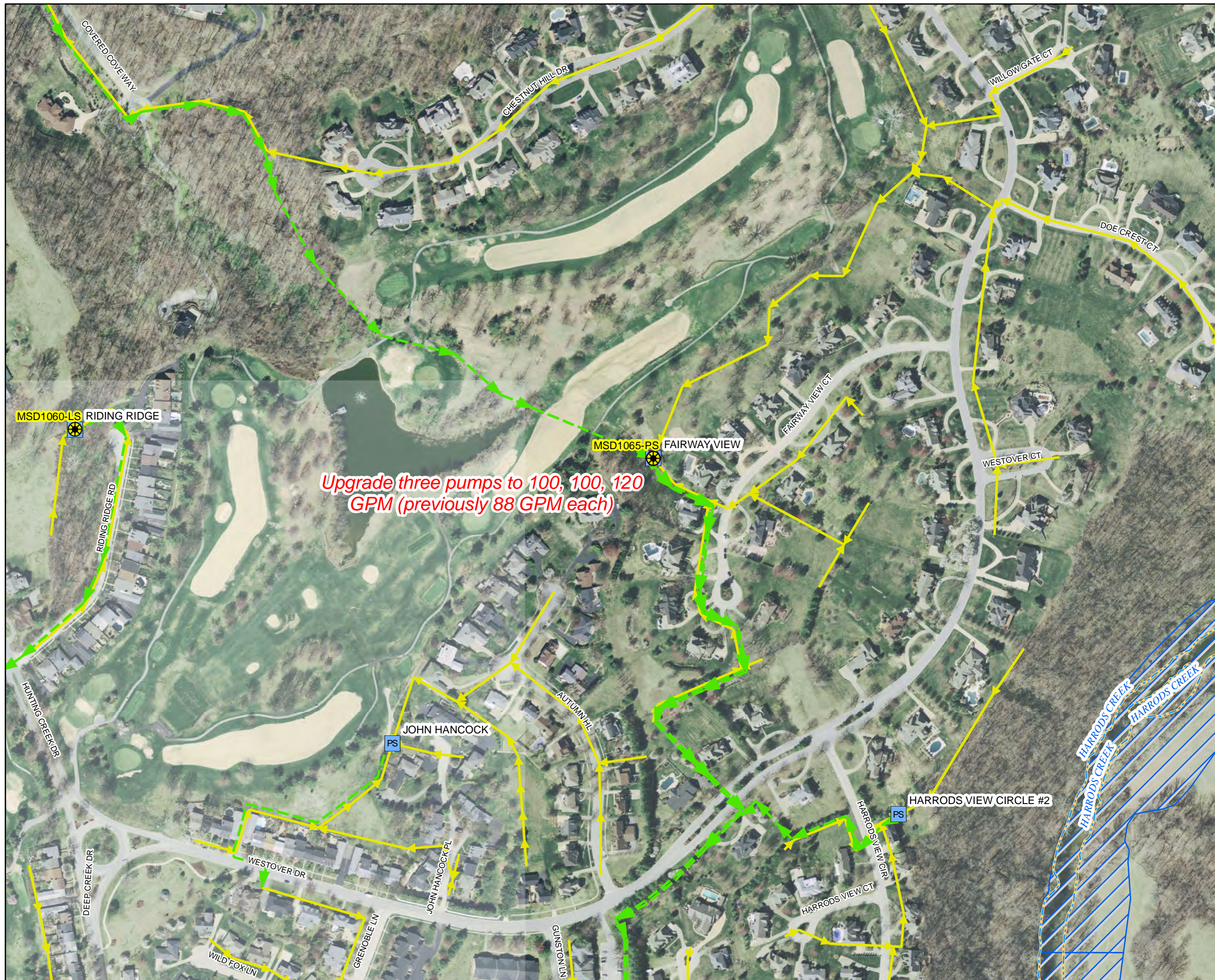
# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Hunting Creek South Sewershed

Fairway View PS Improvements

Preliminary - For Budget Development Only



- Documented SSO
- Suspected SSO
- Haulop Locations
- Pump Stations
- Proposed Pipe Solution
- WQTC
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 300 feet



Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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**Project Name**      Fox Harbor Inline Storage

**Project Number**    S\_HC\_HN\_NB03\_S\_09A\_A\_A

**Modeled Area**            Hunting Creek North

**Branch or SSO ID**        NB03

**Project Type**            Inline Storage

**Receiving Stream**        Harrods Creek

**Project Description**      This alternative includes replacing two 8" (total 133 LF) pipes upstream and east of the Fox Harbor #2 LS with 24" and 60" pipes respectively. For Fox Harbor #1: Install (194 LF of 24" to 54") parallel storage pipes upstream of the lift station and lower the upstream invert of that pipe (which will require a new drop MH).

**Reason for Overflow**      Pump station capacities

**Design Parameters**        This solution is based on a 2.60 inch cloudburst rain event.

**Project Constraints**        N/A

**Estimated Capital Cost**    \$328,000

**Weighted Benefit/Cost Ratio** 87.55

Asset ID	SSO Start Date	Volume (Gal)
62769	NO DATA	NO DATA



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Hunting Creek North Sewershed  
 Solution ID # S\_HC\_HN\_NB03\_S\_09A\_A\_A  
 Fox Harbor Inline Storage

**Preliminary - For Budget Development Only**  
**Legend**

- Documented SSO
- Suspected SSO
- Haul Operation
- Proposed Pump Station Solution
- Pump Station
- WWTP
- Proposed Pipe Solution
- Force Main
- Collector < 12"
- Interceptor => 12"
- Combined Sewer Pipe
- Proposed Off-line Storage
- Road
- Streams
- Floodway
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Metro Parks

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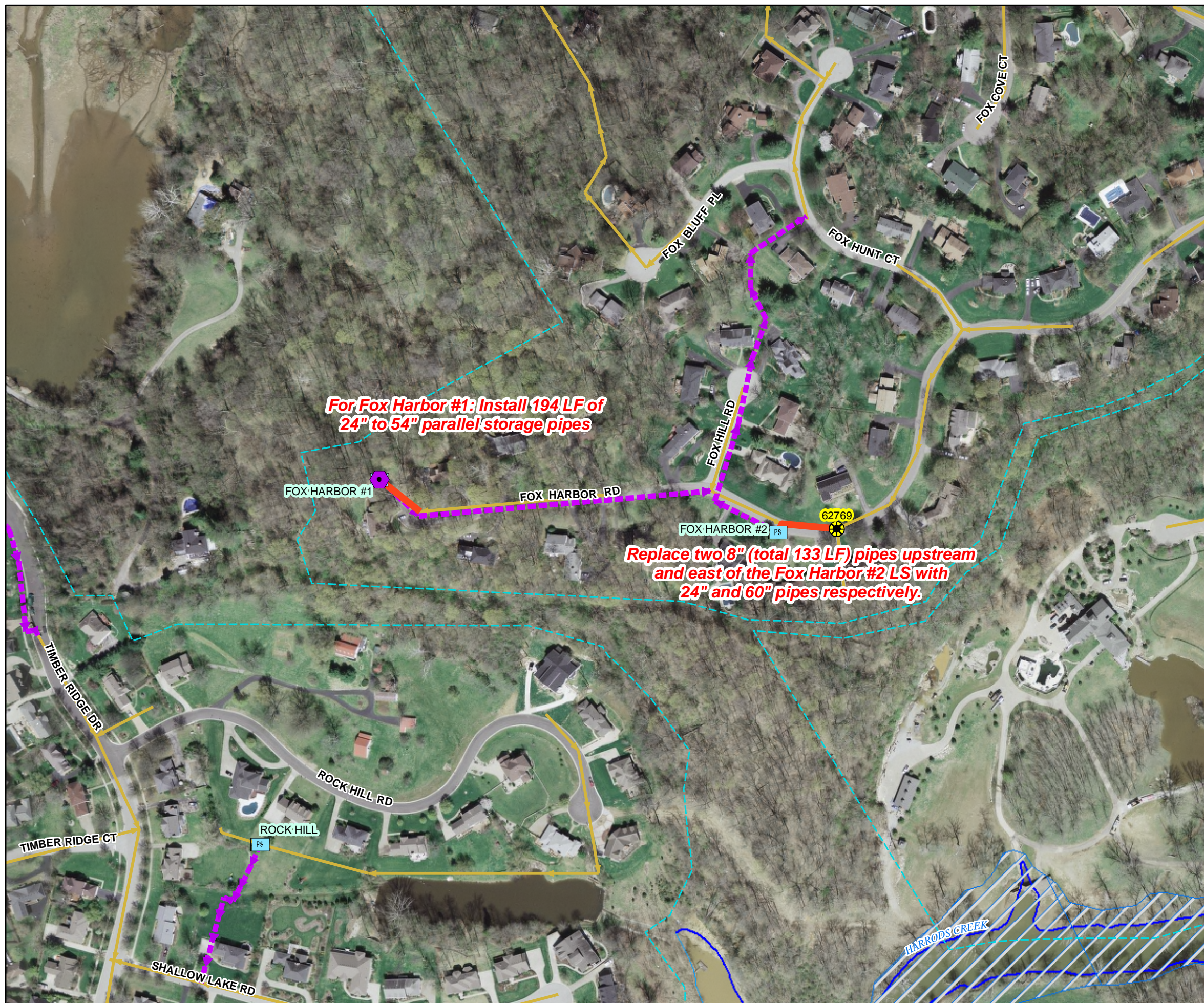
Some boundaries are uniquely symbolized within the map.

Map Revision  
 May 7, 2009

Aerial Date: 2006



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<b>Project Name</b>	Gunpowder PS Inline Storage
<b>Project Number</b>	S_HC_HN_NB02_S_09A_C_B
<b>Modeled Area</b>	Hunting Creek North WQTC
<b>Branch or SSO ID</b>	NB02
<b>Project Type</b>	Inline Storage
<b>Receiving Stream</b>	Harrods Creek
<b>Project Description</b>	This alternative includes replacing 120 LF of 8" with 60" in-line storage pipe. In addition, 28 LF of pipe upgrades will be needed.
<b>Reason for Overflow</b>	Pump station capacity
<b>Design Parameters</b>	This solution is based on a 1.82 inch cloudburst rain event.
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$176,000
<b>Weighted Benefit/Cost Ratio</b>	78.71

Asset ID	SSO Start Date	Volume (Gal)
MSD1055-LS	1/1/2005	1000
MSD1055-LS	1/24/2002	600
MSD1055-LS	1/3/2005	95000
MSD1055-LS	1/4/2005	4000
MSD1055-LS	1/5/2005	50000
MSD1055-LS	11/11/2004	5490
MSD1055-LS	12/16/2000	0
MSD1055-LS	12/19/2002	6000
MSD1055-LS	3/28/2005	1200
MSD1055-LS	4/21/2002	3000
MSD1055-LS	4/23/2011	36000
MSD1055-LS	4/23/2011	9000
MSD1055-LS	4/5/2006	5000
MSD1055-LS	5/19/2005	6000
MSD1055-LS	5/27/2004	2500
MSD1055-LS	5/3/2011	92100
MSD1055-LS	5/30/2004	10000
MSD1055-LS	5/5/2003	2000
MSD1055-LS	6/6/2002	3000
MSD1055-LS	7/14/2006	9000
MSD1055-LS	9/26/2011	267000
MSD1055-LS	9/27/2002	3000



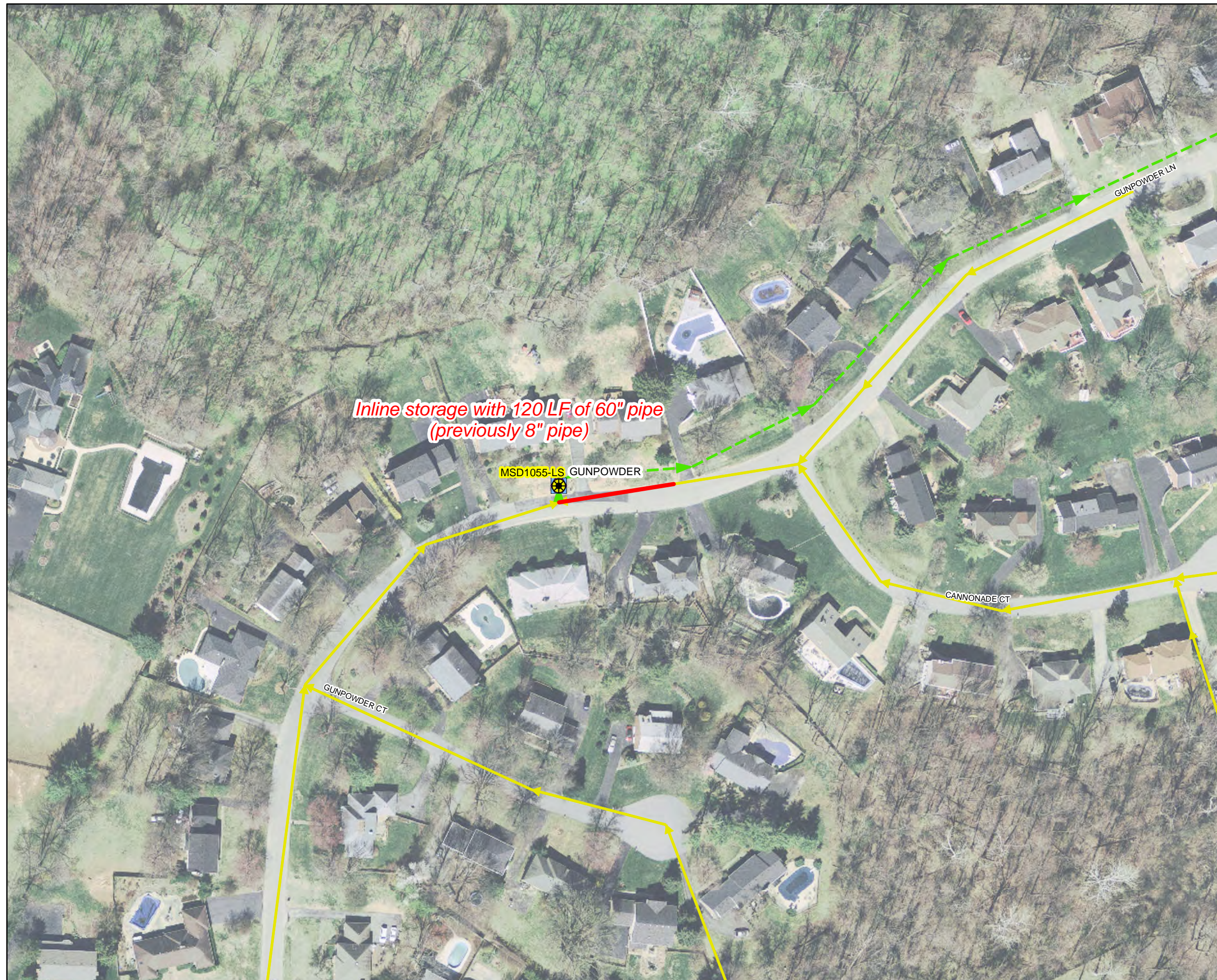
# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Hunting Creek North Sewershed

Gunpowder PS Inline Storage

Preliminary - For Budget Development Only



- Documented SSO
- Suspected SSO
- Haulop Locations
- Proposed Pump Station Solution
- Pump Stations
- WQTC
- Proposed Pipe Solution
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

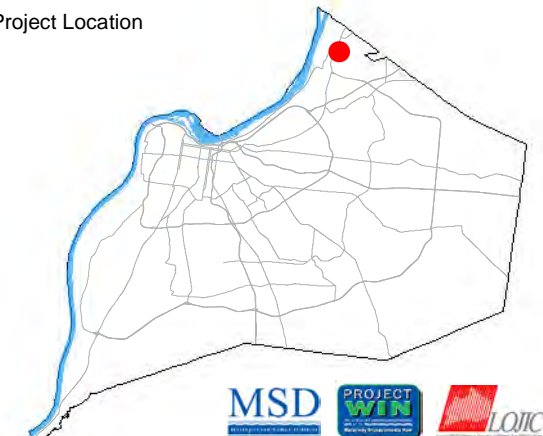
1 inch = 100 feet



Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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**Project Name**     Lake Forest PS SSO Investigation

**Project Number**     S\_FF\_LF\_NB01\_S\_13\_C\_A

**Modeled Area**             Lake Forest

**Branch or SSO ID**             NB01

**Project Type**                 Pump Station Upgrades

**Receiving Stream**             Floyds Fork

**Project Description**             This alternative includes installing two new pumps at the Lake Forest from 83 GPM to discharge 122 GPM. This would give the station a peak flow capacity of 0.34 MGD.

**Reason for Overflow**             Pump station capacity

**Design Parameters**             This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**             Family residences very close to proposed construction

**Estimated Capital Cost**             \$77,000

**Weighted Benefit/Cost Ratio**             28.57




















Asset ID	SSO Start Date	Volume (Gal)
MSD1169-LS	NO DATA	NO DATA



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Lake Forest Sewershed  
 Solution ID # S\_FF\_LF\_NB01\_S\_13\_C\_A  
 Lake Forest PS SSO Investigation

**Preliminary - For Budget Development Only**

**Legend**

-  Documented SSO
-  Suspected SSO
-  Haul Operation
-  Proposed Pump Station Solution
-  Pump Station
-  WWTP
-  Proposed Pipe Solution
-  Force Main
-  Collector < 12"
-  Interceptor => 12"
-  Combined Sewer Pipe
-  Proposed Off-line Storage
-  Road
-  Streams
-  Floodway
-  Small WWTP Service Area
-  Large WWTP Service Area
-  CSO Area
-  Metro Parks

**Monitor the Lake Forest PS during rain events for the next three years according to SORP protocols.**

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

1 inch equals 600 feet  
 Scalable when printed on 11" X 17" paper



Some boundaries are uniquely symbolized within the map.

Map Revision  
 May 20, 2009  
 Aerial Date: 2006



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**Project Name** Lucas Lane PS Inline Storage

**Project Number** S\_FF\_BT\_NB01\_S\_09A\_C\_A

**Modeled Area** Berrytown

**Branch or SSO ID** NB01

**Project Type** Inline Storage

**Receiving Stream** Goose Creek

**Project Description** This alternative includes installing two 90 LF long 54" wide parallel storage pipes that branch off the gravity main prior to the Lucas Lane PS. The invert must be lowered and upgraded to a 36" pipe.

**Reason for Overflow** Pump station capacity

**Design Parameters** This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints** N/A

**Estimated Capital Cost** \$183,000

**Weighted Benefit/Cost Ratio** 112.86

Asset ID	SSO Start Date	Volume (Gal)
MSD0199-LS	3/12/2006	5000



# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Berrytown Sewershed

Solution ID # S\_FF\_BT\_NB01\_S\_09A\_C\_A

Lucas Ln. PS Inline Storage

### Preliminary - For Budget Development Only

#### Legend

- Documented SSO
- Suspected SSO
- Haul Operation
- Proposed Pump Station Solution
- Pump Station
- WWTP
- Proposed Pipe Solution
- Force Main
- Collector < 12"
- Interceptor => 12"
- Combined Sewer Pipe
- Proposed Off-line Storage
- Road
- Streams
- Floodway
- Small WWTP Service Area
- Large WWTP Service Area
- CSO Area
- Metro Parks

**Replace 90 LF of 8" pipe upstream of the Lucas Lane Pump Station with a 54" pipe and install an additional 90 LF of 54" pipe parallel to it to provide inline storage. Lower the invert of the influent 8" pipe to PS and replace with a 36" pipe.**

**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

1 inch equals 100 feet  
Scalable when printed on 11" X 17" paper



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Map Revision  
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Aerial Date: 2006



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**Project Name**     **Riding Ridge PS Improvements**

**Project Number**   **S\_HC\_HN\_NB01\_S\_03\_C\_A**

**Modeled Area**                     Hunting Creek North

**Branch or SSO ID**                     NB01

**Project Type**                         Pump Station Upgrades

**Receiving Stream**                     Harrods Creek

**Project Description**                     This alternative includes upgrading pumps at Riding Ridge PS from 17 GPM to 26 GPM. This will give the PS a peak pumping rate capacity of 0.075 MGD.

**Reason for Overflow**                     Pump station capacity

**Design Parameters**                     This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**                     N/A

**Estimated Capital Cost**                     \$27,000














**Weighted Benefit/Cost Ratio**                     52.02

Asset ID	SSO Start Date	Volume (Gal)
MSD1060-LS	1/1/2003	1000
MSD1060-LS	1/27/2012	7250
MSD1060-LS	1/3/2005	4000
MSD1060-LS	12/16/2000	0
MSD1060-LS	12/19/2002	7500
MSD1060-LS	12/5/2011	7500
MSD1060-LS	3/18/2008	10200
MSD1060-LS	3/26/2002	500
MSD1060-LS	3/27/2008	600
MSD1060-LS	4/12/2011	450
MSD1060-LS	4/23/2011	52250
MSD1060-LS	4/4/2008	5200
MSD1060-LS	5/30/2004	3500
MSD1060-LS	6/6/2002	1000



**Integrated Overflow Abatement Plan**  
**Vol. 3 - Sanitary Sewer Discharge Plan**  
 Hunting Creek North Sewershed  
 Riding Ridge PS Improvements

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Proposed Pump Station Solution
-  Pump Stations
-  WQTC
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

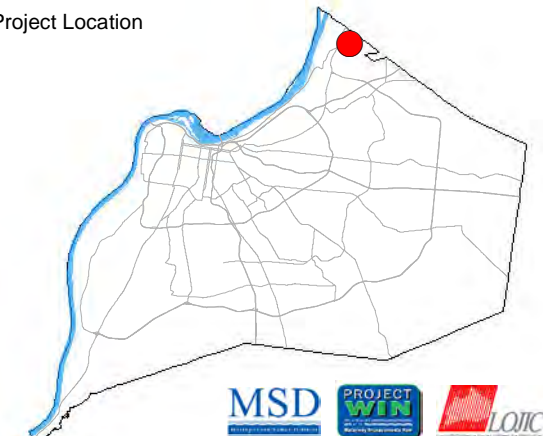
1 inch = 200 feet



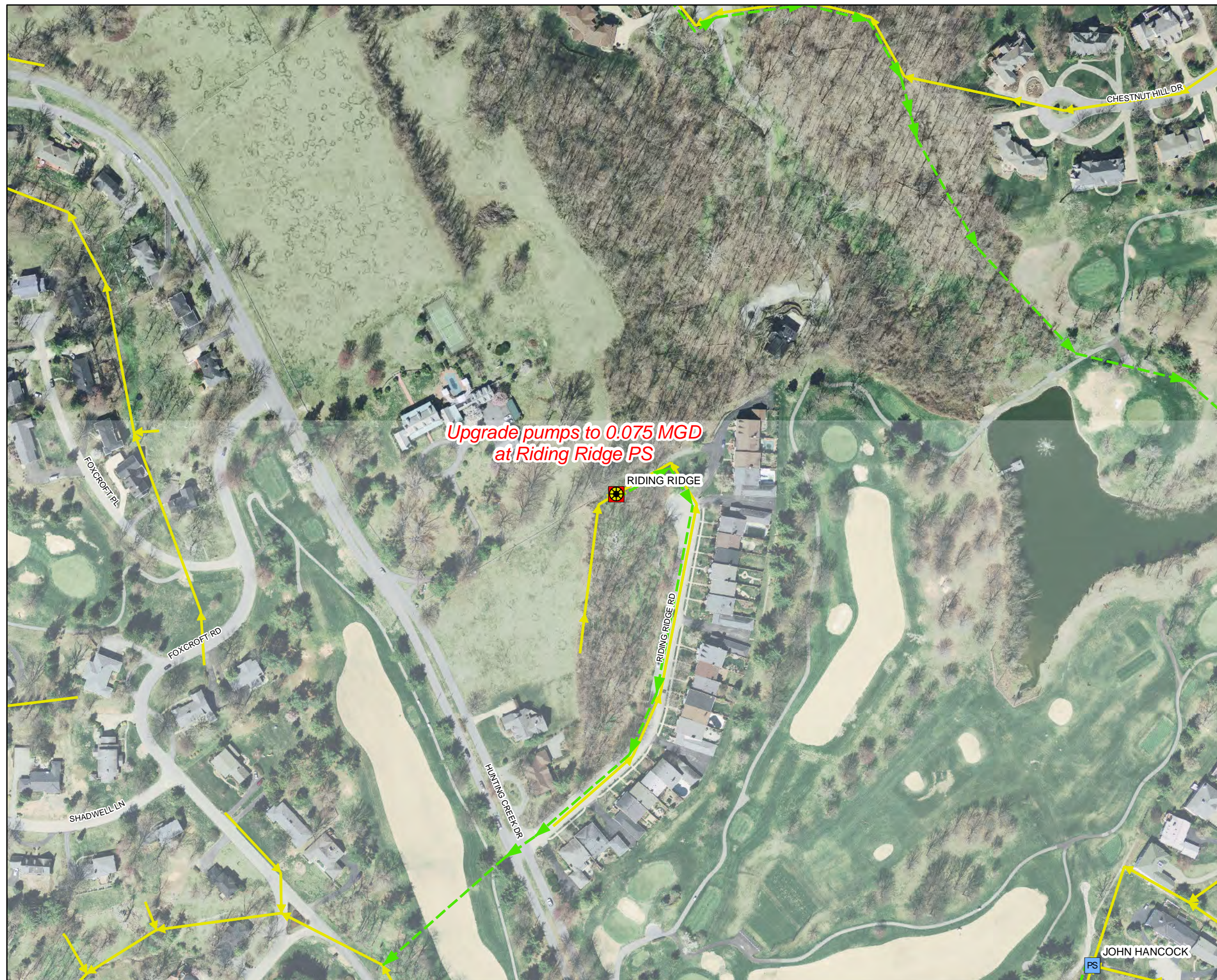
Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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**Project Name**     **St. Rene Rd. PS Inline Storage**

**Project Number**   **S\_FF\_CH\_NB01\_S\_09A\_C\_A**

**Modeled Area**             Chenoweth Hills

**Branch or SSO ID**         CH01

**Project Type**             Inline Storage

**Receiving Stream**         Chenoweth Run

**Project Description**       This alternative includes replacing 42 LF of 8" with 48" pipe just upstream of the PS.

**Reason for Overflow**       Pump station capacity

**Design Parameters**        This solution is based on a 1.82 inch cloudburst rain event.

**Project Constraints**        N/A

**Estimated Capital Cost**     \$30,000

**Weighted Benefit/Cost Ratio**   212.00

Asset ID	SSO Start Date	Volume (Gal)
94187	3/19/2008	4380













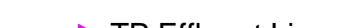



# Integrated Overflow Abatement Plan

## Vol. 3 - Sanitary Sewer Discharge Plan

Chenoweth Hills Sewershed

St. Rene Rd. PS Inline Storage

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  TP Effluent Lines
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

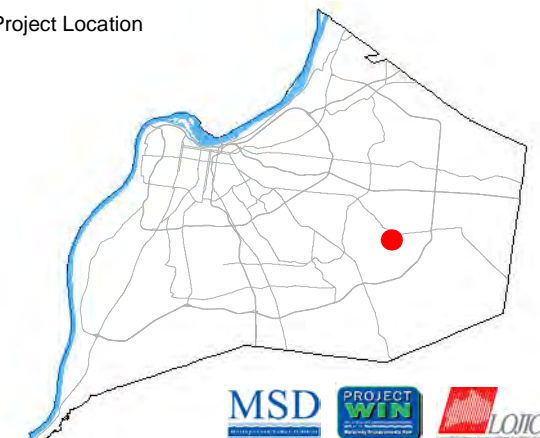
1 inch = 100 feet



Aerial Date:  
2009

Map Revision:  
April 9, 2012

Project Location



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<b>Project Name</b>	Beechwood Village Sanitary Sewer Replacement
<b>Project Number</b>	BVSSR
<b>Modeled Area</b>	N/A
<b>Branch or SSO ID</b>	N/A
<b>Project Type</b>	Sewer Replacement
<b>Receiving Stream</b>	Upper Sinking Fork
<b>Project Description</b>	This project involves replacement or rehabilitation of the entire service area, encompassing 23,700 LF of sewer and 580 customer service connections. Existing sewers will be rehabilitated with a cured-in-place liner. Existing service connections will be completely replaced by repiping the interior service piping to eliminate basement discharge by gravity and remove all clean water connections to the sanitary sewer system. The project will be completed in two phases, east and west.
<b>Reason for Overflow</b>	System Capacity and Inflow/Infiltration
<b>Design Parameters</b>	N/A
<b>Project Constraints</b>	Sinking Fork Relief Sewer must be completed first
<b>Estimated Capital Cost</b>	\$11,800,000
<b>Weighted Benefit/Cost Ratio</b>	N/A

Asset ID	SSO Start Date	Volume (Gal)
21156	1/10/2008	518700
21061	1/10/2008	240000
21153	1/10/2008	470600
21153	1/14/2007	3839000
21061	1/14/2007	885500
21101	1/14/2007	3875300
21156	1/14/2007	3494000
21061	1/15/2007	990000
21101	1/2/2004	55000
21153	1/2/2004	1580000
21101	1/2/2004	610000
21156	1/2/2004	856000
21153	1/23/2006	748500
21156	1/23/2006	1317500
21156	1/4/2004	2380000
21153	1/4/2004	2380000
21061	1/4/2004	790000
21101	10/18/2004	600000
21156	10/18/2004	700000
21153	10/18/2004	600000
21153	10/23/2007	3759800
21156	10/23/2007	4493100
21061	10/23/2007	3028200
21101	10/23/2007	5197600
21061	10/9/2009	272700
21156	10/9/2009	1263500

**Project Name**    **Beechwood Village Sanitary Sewer Replacement**

**Project Number**    **BVSSR**

21153	10/9/2009	472100
21156	11/11/2004	900000
21101	11/11/2004	867000
21153	11/2/2004	1423000
21156	11/2/2004	1442800
21061	11/2/2004	1327500
21101	11/2/2004	2079200
21153	11/29/2001	3173500
21101	11/29/2001	2623500
21156	11/29/2001	2761000
21061	12/13/2007	524600
21156	12/13/2007	1159500
21101	12/13/2007	1335500
21153	12/13/2007	1123000
21156	12/15/2007	4066100
21101	12/15/2007	5422600
21153	12/15/2007	3512600
21061	12/15/2007	3147300
21156	12/16/2000	0
21061	12/16/2000	0
21153	12/16/2000	0
21101	12/16/2000	0
21156	12/16/2001	654500
21153	12/16/2001	660000
21061	12/16/2001	522500
21061	12/17/2001	355300
21101	12/17/2001	1180000
21156	12/17/2001	2048000
21153	12/17/2001	2000000
21101	12/18/2001	346500
21101	12/19/2002	1996500
21153	12/19/2002	1031800
21061	12/19/2002	877800
21156	12/19/2002	2381500
21153	12/20/2002	1307900
21061	12/20/2002	1399200
21156	12/24/2008	944300
21153	12/24/2008	572700
21101	12/24/2008	711500
21061	12/24/2008	120700
21061	12/31/2004	11093000
21156	12/31/2004	15000000
21153	12/31/2004	15000000



**Project Name**    **Beechwood Village Sanitary Sewer Replacement**

**Project Number**    **BVSSR**

21101	12/31/2004	15000000
21101	2/13/2007	992200
21153	2/13/2007	521000
21156	2/13/2007	556200
21101	2/17/2000	0
21156	2/17/2000	0
21061	2/17/2000	0
21153	2/17/2000	0
21153	2/5/2004	660000
21156	2/5/2004	363000
21101	2/6/2004	363000
21156	2/6/2008	2792000
21153	2/6/2008	2438800
21061	2/6/2008	2413600
21101	2/6/2008	3131800
21153	2/9/2004	627000
21153	3/1/2007	742700
21156	3/1/2007	768000
21061	3/12/2000	1414000
21101	3/12/2006	4888000
21156	3/12/2006	4207500
21153	3/12/2006	4853500
21061	3/13/2006	1176000
21153	3/14/2007	201100
21156	3/14/2007	289100
21101	3/18/2008	6700300
21156	3/18/2008	6803800
21061	3/18/2008	4635800
21153	3/18/2008	6426500
21101	3/19/2002	2893000
21156	3/19/2002	3289000
21153	3/19/2002	2428800
21061	3/19/2002	2220500
21156	3/27/2008	4350500
21153	3/27/2008	1229700
21061	3/27/2008	1180400
21101	3/27/2008	4426200
21101	3/28/2005	2000000
21153	3/28/2005	1514000
21061	3/28/2005	1514000
21156	3/28/2005	1514000
21061	3/28/2008	1773000
21153	3/28/2008	1904500

**Project Name**    **Beechwood Village Sanitary Sewer Replacement**

**Project Number**    **BVSSR**

21153	3/4/2004	266000
21153	3/4/2008	3752400
21061	3/4/2008	3338900
21156	3/4/2008	4456900
21101	3/4/2008	4972000
21153	4/14/2007	364400
21156	4/14/2007	408000
21101	4/21/2006	1656000
21061	4/21/2006	912000
21153	4/21/2006	1470500
21156	4/21/2006	1120000
21101	4/3/2008	10905400
21153	4/3/2008	4944900
21156	4/3/2008	6652000
21101	4/3/2008	100
21061	4/3/2008	4948200
21156	5/15/2008	1113000
21061	5/15/2008	552500
21101	5/15/2008	182000
21153	5/15/2008	1225900
21153	5/19/2004	1336500
21156	5/2/2010	3962700
21061	5/2/2010	170000
21101	5/2/2010	5385400
21153	5/26/2004	430000
21156	5/26/2004	430000
21061	5/27/2004	3570000
21153	5/27/2004	3600000
21156	5/29/2004	3800000
21061	5/31/2004	1200000
21153	5/31/2004	466000
21101	5/5/2003	1254000
21153	5/5/2003	1336500
21061	5/5/2003	561000
21156	5/5/2003	1292500
21153	5/8/2009	1056100
21156	5/8/2009	1564200
21101	5/8/2009	1494300
21061	5/8/2009	846300
21101	6/1/2004	200000
21101	6/14/2003	500000
21061	6/14/2003	340000
21153	6/14/2003	400000

**Project Name**    **Beechwood Village Sanitary Sewer Replacement**

**Project Number**    **BVSSR**













21156	6/14/2003	340000
21101	6/15/2003	1060000
21061	6/15/2003	860000
21101	6/16/2003	860000
21156	6/18/2009	1451100
21061	6/18/2009	365700
21101	6/18/2009	391400
21153	6/18/2009	389500
21101	6/2/2006	482500
21153	6/2/2006	845000
21156	6/2/2006	1054000
21061	6/2/2006	466000
21153	7/14/2006	438500
21156	7/14/2006	637700
21061	7/14/2006	367200
21101	7/14/2006	695700
21101	7/29/2009	761500
21153	7/29/2009	428200
21156	7/29/2009	652800
21061	7/29/2009	436700
21153	8/30/2005	466000
21061	8/30/2005	908800
21101	8/30/2005	1713100
21156	8/30/2005	1626000
21153	8/4/2009	2974300
21061	8/4/2009	2641000
21156	8/4/2009	3630400
21101	8/4/2009	5319800
21101	9/1/2003	4630000
21156	9/1/2003	2640000
21153	9/1/2003	2570000
21061	9/1/2003	2570000
21101	9/23/2006	4674000
21153	9/23/2006	3527500
21061	9/23/2006	1884500
21156	9/23/2006	3514500
21101	9/27/2002	1056000
21153	9/27/2002	1105500
21156	9/27/2002	1104000
21061	9/27/2002	995500



**Integrated Overflow Abatement Plan  
Interim Sanitary Sewer Discharge Plan**

**Beechwood Village  
Sanitary Sewer Replacements**

**Legend**

-  Documented SSO
-  Suspected SSO
-  WWTP
-  Pump Station
-  Force Main
-  Force Main non MSD
-  MSD Sewer
-  non msd pipes
-  Combined Sewer Pipe
-  Streams
-  Beechwood Village
-  Metro Parks



**General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.**

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Map Revision  
May 07, 2009

Aerial Date: 2006



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<b>Project Name</b>	Derek R. Guthrie WQTC Wet Weather Facility
<b>Project Number</b>	DRGWQTC
<b>Modeled Area</b>	N/A
<b>Branch or SSO ID</b>	N/A
<b>Project Type</b>	WQTC Upgrade
<b>Receiving Stream</b>	Mill Creek, Black Pond Creek, Alvey Ditch, and the Ohio River
<b>Project Description</b>	This project includes improvements to the Derek R. Guthrie WQTC to allow treatment of all wet weather flow from other SSDP system improvements. The secondary treatment wet weather peak flow capacity will be expanded to 200 MGD, and a wet weather pump station, short-term detention basin and flow equalization basin will be added to increase the overall wet weather peak flow capacity to over 300 MGD. Facilities added to the secondary treatment system include a new raw wastewater pump station, expanded grit removal facilities, a new aeration basin, six new secondary clarifiers, and expanded disinfection facilities.
<b>Reason for Overflow</b>	Treatment Plant Capacity
<b>Design Parameters</b>	N/A
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$102,700,000
<b>Weighted Benefit/Cost Ratio</b>	N/A

Asset ID	SSO Start Date	Volume (Gal)
22370	1/13/2013	95000000
32682	1/13/2013	9999
32688	1/24/2002	375000
MSD0277	10/13/2011	824099
MSD0277	10/17/2006	5000000
59169	10/23/2007	3024000
22385	10/23/2007	3024000
32682	10/23/2007	3240000
32682	10/6/2013	855000
32682	11/28/2011	410000
22370	12/16/2011	25
22370	12/16/2011	5
32688	12/17/2001	900000
22370	12/19/2002	24624000
22385	12/21/2011	5
32682	12/21/2013	100000
MSD0277	12/31/2009	1500000
32682	12/5/2011	565000
32682	2/25/2011	1975000
59169	3/12/2006	1600000
22370	3/12/2006	1700000
32682	3/12/2006	1700000
22385	3/12/2006	1600000
59169	3/19/2008	1377000
22385	3/19/2008	162000

**Project Name** Derek R. Guthrie WQTC Wet Weather Facility

**Project Number** DRGWQTC














32682	3/19/2008	1944000
32688	3/20/2002	5430000
32682	3/4/2008	1944000
22385	3/4/2008	1728000
59169	3/4/2008	1620000
22370	3/9/2011	725000
32682	3/9/2011	1630750
32682	4/12/2011	135000
22370	4/12/2011	2365000
32682	4/23/2011	1900000
32688	4/27/2002	0
22370	4/27/2011	2150000
32682	4/27/2011	2300000
32688	4/29/2002	5760000
32682	4/4/2008	3132000
22370	4/4/2008	8016000
32688	5/13/2002	3300000
22370	5/2/2010	1000
59169	5/2/2010	1000
22385	5/2/2010	1000
32682	5/2/2010	1300
32688	5/2/2010	1000
22370	5/3/2011	1750000
MSD0277	6/19/2011	596409
MSD0277	6/19/2011	364000
22370	7/29/2009	320000
32682	8/4/2009	27000



**Integrated Overflow Abatement Plan  
Interim Sanitary Sewer Discharge Plan**

Derek R. Guthrie WQTC

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 200 feet



Aerial Date: 2012

Map Revision: April 9, 2012

Project Location



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Equalization Basin

100 MGD Conventional Wet Weather Secondary Treatment

MSD0277

GUTHRIE WQTC RWPS (INFLUENT PS)

LOWER RIVER RD

MILL CREEK



<b>Project Name</b>	Hikes Lane Interceptor and Highgate Springs
<b>Project Number</b>	HLIHSPS
<b>Modeled Area</b>	N/A
<b>Branch or SSO ID</b>	N/A
<b>Project Type</b>	Pump Station Elimination and New Interceptor
<b>Receiving Stream</b>	South Fork Beargrass Creek and Wedgewood Ditch
<b>Project Description</b>	This project includes improvements to the Hikes Point Sewer System and eliminates the Highgate Springs Pump Station. In the general Hikes Point area includes improvements of 3,500 LF of new or replacement sewers, and decommissioning the Highgate Springs Pump Station. The new Hikes Lane Interceptor consists of 10,000 LF of 72-inch sewer that connects to Southeastern Interceptor.
<b>Reason for Overflow</b>	System and Pump Station Capacity
<b>Design Parameters</b>	N/A
<b>Project Constraints</b>	N/A
<b>Estimated Capital Cost</b>	\$21,216,000
<b>Weighted Benefit/Cost Ratio</b>	N/A

Asset ID	SSO Start Date	Volume (Gal)
18595	1/10/2008	197600
18471	1/10/2008	420000
17571	1/10/2008	204100
MSD0012-PS	1/10/2008	1134600
18483	1/10/2008	299000
30680	1/13/2013	19000
18505	1/14/2007	1045000
17571	1/14/2007	830500
18595	1/14/2007	763400
18471	1/14/2007	3351700
MSD0012-PS	1/14/2007	372000
18483	1/14/2007	1221000
17571	1/15/2007	748000
18595	1/15/2007	359700
18505	1/15/2007	572000
18483	1/15/2007	1276000
MSD0012-PS	1/17/2006	1674000
MSD0012-PS	1/2/2004	2052696
17571	1/2/2004	1287000
MSD0012-PS	1/2/2005	41268000
MSD0012-PS	1/21/2010	171600
MSD0012-PS	1/22/2006	1153200
17571	1/23/2006	928600
18471	1/23/2006	1158700
MSD0012-PS	1/24/2002	4333800
MSD0012-PS	1/24/2010	357552

<b>Project Name</b>	<b>Hikes Lane Interceptor and Highgate Springs</b>	
<b>Project Number</b>	<b>HLIHSPS</b>	
48886	1/26/2012	12500
MSD0012-PS	1/26/2012	2767245
18483	1/26/2012	852100
18595	1/26/2012	381300
18471	1/26/2012	926200
18299	1/26/2012	6200
48885	1/26/2012	10500
30680	1/3/2005	151800
18471	1/4/2004	1700600
17571	1/4/2004	891000
MSD0012-PS	1/4/2004	4568904
18483	1/4/2004	808500
18505	1/5/2004	770000
18595	1/5/2004	759000
18471	10/18/2004	790000
MSD0012-PS	10/18/2004	684000
30681	10/18/2004	23100
17571	10/18/2004	860000
18505	10/19/2004	132000
18483	10/19/2004	400000
MSD0012-PS	10/22/2007	16128000
17571	10/23/2007	2745600
18483	10/23/2007	3482700
18595	10/23/2007	3198300
18471	10/23/2007	3809700
30680	10/23/2007	4320
18505	10/23/2007	2809500
MSD0012-PS	10/31/2009	415740
48885	10/6/2013	2000
18299	10/6/2013	2500
30680	10/6/2013	22500
18595	10/9/2009	590100
18505	10/9/2009	446600
18483	10/9/2009	564300
17571	10/9/2009	528200
18471	10/9/2009	1067200
MSD0012-PS	10/9/2009	1627860
MSD0012-PS	11/11/2004	3283200
17571	11/15/2005	88000
MSD0012-PS	11/15/2011	28601
18471	11/19/2004	266000
MSD0012-PS	11/19/2004	296400
18595	11/2/2004	548500



<b>Project Name</b>	<b>Hikes Lane Interceptor and Highgate Springs</b>	
<b>Project Number</b>	<b>HLIHSPS</b>	
18471	11/2/2004	990000
18505	11/2/2004	1054100
17571	11/2/2004	1518900
18483	11/2/2004	790000
30680	11/2/2004	29300
18595	11/22/2011	150100
18471	11/22/2011	387600
MSD0012-PS	11/22/2011	102895
18483	11/22/2011	290700
MSD0012-PS	11/25/2010	117450
18471	11/28/2001	2216400
18471	11/28/2011	4618300
MSD0012-PS	11/28/2011	2783916
18505	11/28/2011	2078300
48885	11/28/2011	58500
18302	11/28/2011	37500
18483	11/28/2011	2288200
48886	11/28/2011	55800
18299	11/28/2011	55000
49673	11/28/2011	54500
18595	11/28/2011	1922800
17571	11/29/2001	1826000
18505	11/29/2001	2046000
18483	11/29/2001	1661000
MSD0012-PS	11/29/2001	17019000
MSD0012-PS	11/30/2010	25299
18471	12/13/2007	1200600
18595	12/13/2007	247000
17571	12/13/2007	117000
MSD0012-PS	12/13/2007	3780000
18483	12/13/2007	549600
18595	12/15/2007	2681300
18471	12/15/2007	3881800
18505	12/15/2007	2434900
17571	12/15/2007	2020600
MSD0012-PS	12/15/2007	21146450
49672	12/15/2007	648000
30680	12/15/2007	8100
18483	12/15/2007	3180500
18595	12/16/2000	0
18471	12/16/2000	0
18505	12/16/2000	0
18483	12/16/2000	0

Project Name	Hikes Lane Interceptor and Highgate Springs	
Project Number	HLIHSPS	
17571	12/16/2000	0
MSD0012-PS	12/16/2000	1
18483	12/16/2001	484000
18471	12/16/2001	467500
18505	12/16/2001	456500
18595	12/16/2001	385000
17571	12/16/2001	330000
MSD0012-PS	12/17/2001	11606400
18483	12/17/2001	1122000
18505	12/17/2001	1467000
17571	12/17/2001	266200
18595	12/17/2001	1474000
18471	12/17/2001	742500
18471	12/19/2002	1749000
18595	12/19/2002	1448700
MSD0012-PS	12/19/2002	4836000
17571	12/19/2002	1463000
18505	12/19/2002	1427800
18483	12/19/2002	1402500
MSD0012-PS	12/22/2011	75944
18471	12/24/2008	638600
18483	12/24/2008	508800
MSD0012-PS	12/24/2008	14587
17571	12/24/2008	204000
MSD0012-PS	12/28/2011	556
17571	12/30/2004	33000
MSD0012-PS	12/31/2002	16293000
18471	12/31/2004	15000000
18595	12/31/2004	10964600
17571	12/31/2004	9419280
18483	12/31/2004	10955800
18505	12/31/2004	10827300
MSD0012-PS	12/31/2006	46500
73111	12/5/2011	110000
49672	12/5/2011	61000
49673	12/5/2011	54500
48886	12/5/2011	46000
MSD0012-PS	12/5/2011	3124766
48885	12/5/2011	33000
18134	12/5/2011	54500
18483	12/5/2011	3374700
18505	12/5/2011	1999500
18302	12/5/2011	81000

<b>Project Name</b>	<b>Hikes Lane Interceptor and Highgate Springs</b>	
<b>Project Number</b>	<b>HLIHSPS</b>	
18595	12/5/2011	2097600
18471	12/5/2011	4399800
MSD0012-PS	12/9/2007	259200
MSD0012-PS	2/1/2002	1800000
18483	2/12/2008	620100
MSD0012-PS	2/12/2008	1469400
18505	2/13/2007	565000
18471	2/13/2007	8417000
MSD0012-PS	2/13/2007	1562400
MSD0012-PS	2/15/2001	576600
MSD0012-PS	2/16/2008	183000
18471	2/17/2000	0
18595	2/17/2000	0
17571	2/17/2000	0
18505	2/17/2000	0
18483	2/17/2000	0
MSD0012-PS	2/17/2008	130200
MSD0012-PS	2/21/2003	14322000
MSD0012-PS	2/24/2007	279000
18483	2/24/2007	272800
18471	2/24/2007	239000
18505	2/24/2007	268800
MSD0012-PS	2/24/2011	718650
18483	2/24/2011	1071100
49672	2/24/2011	32500
18505	2/24/2011	323000
48885	2/24/2011	19250
18471	2/24/2011	1552900
30681	2/24/2011	17500
MSD0012-PS	2/28/2011	753350
18505	2/28/2011	444600
49672	2/28/2011	10
18595	2/28/2011	305900
18471	2/28/2011	1908000
18299	2/28/2011	25
18483	2/28/2011	1732200
MSD0012-PS	2/5/2008	5566980
MSD0012-PS	2/5/2010	125580
18483	2/6/2008	1725400
17571	2/6/2008	838500
18471	2/6/2008	2080400
18595	2/6/2008	790400
MSD0012-PS	3/1/2007	9300



<b>Project Name</b>	<b>Hikes Lane Interceptor and Highgate Springs</b>	
<b>Project Number</b>	<b>HLIHSPS</b>	
18483	3/1/2007	891000
18505	3/1/2007	170500
18471	3/1/2007	1017500
18595	3/12/2006	1400000
18505	3/12/2006	1704000
30680	3/12/2006	69000
MSD0012-PS	3/12/2006	6937800
18471	3/12/2006	3996000
17571	3/12/2006	1309000
18483	3/12/2006	1744000
MSD0012-PS	3/15/2008	93000
MSD0012-PS	3/17/2012	829169
18595	3/18/2008	462800
18595	3/18/2008	208000
17571	3/18/2008	1088100
MSD0012-PS	3/18/2008	23361600
49672	3/18/2008	344040
18471	3/18/2008	5640800
18483	3/18/2008	5207700
18595	3/19/2002	3179000
18505	3/19/2002	1705000
17571	3/19/2002	2651000
18471	3/19/2002	3030500
MSD0012-PS	3/19/2002	4968600
18483	3/19/2002	2112000
30680	3/19/2008	15660
49224	3/19/2008	100
18595	3/19/2008	2542400
17571	3/19/2008	2775000
18505	3/19/2008	2569800
MSD0012-PS	3/27/2008	11718000
18471	3/27/2008	722900
18595	3/27/2008	674700
18483	3/27/2008	909000
17571	3/27/2008	647400
18483	3/28/2005	860000
18505	3/28/2005	1652000
17571	3/28/2005	922000
18471	3/28/2005	1580000
MSD0012-PS	3/28/2005	750000
18595	3/28/2005	1056000
17571	3/28/2008	1211000
18471	3/28/2008	1882600

<b>Project Name</b>	<b>Hikes Lane Interceptor and Highgate Springs</b>	
<b>Project Number</b>	<b>HLIHSPS</b>	
18595	3/28/2008	1050000
30680	3/28/2008	540
18505	3/28/2008	396500
18483	3/28/2008	1828200
MSD0012-PS	3/4/2004	892800
49672	3/4/2008	97200
30680	3/4/2008	10260
18595	3/4/2008	1950300
18483	3/4/2008	3139000
MSD0012-PS	3/4/2008	14805600
18505	3/4/2008	2462400
17571	3/4/2008	1855100
18471	3/4/2008	3794400
MSD0012-PS	3/5/2011	4673
MSD0012-PS	3/9/2008	2399400
73111	3/9/2011	56000
30680	3/9/2011	76500
18299	3/9/2011	700
18297	3/9/2011	50
48888	3/9/2011	150
18471	3/9/2011	5044200
48885	3/9/2011	146250
49672	3/9/2011	174000
18483	3/9/2011	4810700
18595	3/9/2011	2485200
MSD0012-PS	3/9/2011	4646371
18302	3/9/2011	300
30681	3/9/2011	211000
18505	3/9/2011	2779600
MSD0012-PS	4/1/2012	109243
MSD0012-PS	4/11/2008	223200
18595	4/11/2011	1826900
48885	4/11/2011	2550750
18483	4/11/2011	3881100
MSD0012-PS	4/11/2011	10111163
18505	4/11/2011	1661400
18471	4/11/2011	4696600
73111	4/12/2011	362000
48886	4/12/2011	2500500
49672	4/12/2011	213250
18302	4/12/2011	153250
30681	4/12/2011	226000
18299	4/12/2011	175000

<b>Project Name</b>	<b>Hikes Lane Interceptor and Highgate Springs</b>	
<b>Project Number</b>	<b>HLIHSPS</b>	
MSD0012-PS	4/13/2004	129000
18471	4/14/2007	432000
MSD0012-PS	4/19/2006	2027400
MSD0012-PS	4/19/2009	39000
18471	4/20/2003	561000
MSD0012-PS	4/20/2003	1458600
MSD0012-PS	4/20/2006	2976000
18471	4/21/2006	1536000
18483	4/21/2006	712000
17571	4/21/2006	769500
18595	4/21/2006	814400
18505	4/21/2006	344000
18505	4/23/2011	8051900
18595	4/23/2011	4191400
73111	4/23/2011	126000
48886	4/23/2011	64000
18471	4/23/2011	9737700
18483	4/23/2011	7797400
MSD0012-PS	4/23/2011	31709427
18134	4/23/2011	71000
18299	4/23/2011	6200
49673	4/23/2011	117500
49224	4/23/2011	99500
18302	4/23/2011	145000
30680	4/23/2011	122000
48885	4/23/2011	648000
18505	4/27/2011	3582900
18483	4/27/2011	6001900
18134	4/27/2011	44000
49672	4/27/2011	125500
18595	4/27/2011	2838200
18471	4/27/2011	6423100
MSD0012-PS	4/3/2006	745000
18483	4/3/2008	5045000
MSD0012-PS	4/3/2008	25682880
18595	4/3/2008	3865900
18471	4/3/2008	5090000
18505	4/3/2008	4999500
17571	4/3/2008	4230500
49224	4/4/2008	180000
49236	4/4/2008	150
49672	4/4/2008	810000
49672	4/4/2008	100



<b>Project Name</b>	<b>Hikes Lane Interceptor and Highgate Springs</b>	
<b>Project Number</b>	<b>HLIHSPS</b>	
30680	4/4/2008	33480
18434	4/4/2008	300
18134	4/4/2008	100
49673	4/4/2008	23250
18434	4/4/2008	250
MSD0012-PS	5/1/2010	9894300
MSD0012-PS	5/13/2012	557347
18483	5/13/2012	492100
18471	5/13/2012	619500
MSD0012-PS	5/15/2008	3896700
17571	5/15/2008	240500
18595	5/15/2008	559000
18471	5/15/2008	1050900
18505	5/15/2008	260000
18483	5/15/2008	767600
MSD0012-PS	5/19/2005	63240
49672	5/2/2010	250
30680	5/2/2010	61000
18505	5/2/2010	1901900
18471	5/2/2010	5119600
49673	5/2/2010	2900
18483	5/2/2010	4329500
18302	5/2/2010	41000
48885	5/2/2010	24000
30681	5/2/2010	27000
18595	5/2/2010	2011100
18595	5/2/2011	2312800
18595	5/2/2011	317300
18483	5/2/2011	4058700
18483	5/2/2011	465700
18302	5/2/2011	162000
49673	5/2/2011	87000
48885	5/2/2011	540000
18471	5/2/2011	559100
73111	5/2/2011	102000
18471	5/2/2011	4919000
48886	5/2/2011	108000
MSD0012-PS	5/21/2010	538200
MSD0012-PS	5/23/2011	131400
MSD0012-PS	5/25/2004	186000
17571	5/25/2004	130000
18471	5/25/2004	130000
18471	5/26/2011	532000

<b>Project Name</b>	<b>Hikes Lane Interceptor and Highgate Springs</b>	
<b>Project Number</b>	<b>HLIHSPS</b>	
18483	5/26/2011	485500
18595	5/26/2011	602300
MSD0012-PS	5/26/2011	575723
18595	5/27/2004	1256000
17571	5/27/2004	4000000
18483	5/27/2004	1500000
18505	5/27/2004	5940000
MSD0012-PS	5/27/2004	1470000
30680	5/28/2004	100
MSD0012-PS	5/29/2012	524307
18483	5/29/2012	986800
18471	5/29/2012	822600
49673	5/29/2012	12000
18505	5/29/2012	295700
18299	5/29/2012	45000
48885	5/29/2012	9000
MSD0012-PS	5/3/2008	37200
18134	5/3/2011	7650
49672	5/3/2011	99500
30680	5/3/2011	10000
18505	5/3/2011	1918900
49224	5/3/2011	108000
18483	5/30/2004	1190000
30680	5/30/2004	42000
18595	5/30/2004	2500000
18471	5/30/2004	1124000
17571	5/31/2004	1900000
MSD0012-PS	5/31/2012	1146953
18595	5/5/2003	407000
18595	5/5/2003	874500
17571	5/5/2003	396000
MSD0012-PS	5/5/2003	5000000
18471	5/5/2003	973500
MSD0012-PS	5/6/2002	641000
18595	5/8/2009	180700
17571	5/8/2009	552100
MSD0012-PS	5/8/2009	606098
MSD0012-PS	6/18/2009	132600
18471	6/18/2009	74100
18483	6/18/2009	232900
17571	6/2/2006	332000
18471	6/2/2006	1089000
18483	6/2/2006	411000

<b>Project Name</b>	<b>Hikes Lane Interceptor and Highgate Springs</b>	
<b>Project Number</b>	<b>HLIHSPS</b>	
18505	6/2/2006	394500
18595	6/2/2006	159500
MSD0012-PS	6/2/2006	744000
MSD0012-PS	6/21/2011	3061
18471	6/22/2011	2672200
18505	6/22/2011	1740100
18483	6/22/2011	2333500
18595	6/22/2011	1141900
49673	6/22/2011	22000
MSD0012-PS	6/22/2011	1536754
18299	6/23/2011	5000
73111	6/23/2011	32000
30680	6/23/2011	144000
18302	6/23/2011	54000
48886	6/23/2011	36000
48885	6/23/2011	36000
MSD0012-PS	6/9/2010	11313
18471	7/14/2006	177100
17571	7/14/2006	266000
MSD0012-PS	7/14/2006	483600
MSD0012-PS	7/29/2009	97500
18471	7/29/2009	93800
18483	7/29/2009	69600
17571	7/29/2009	173500
MSD0012-PS	8/30/2005	1934400
17571	8/30/2005	317700
17571	8/30/2005	834000
18483	8/30/2005	1106600
18471	8/30/2005	1201000
30680	8/30/2005	9200
18595	8/30/2005	916500
18505	8/30/2005	423100
17571	8/31/2005	315545
17571	8/4/2009	1847100
MSD0012-PS	8/4/2009	3931200
18302	8/4/2009	72000
30681	8/4/2009	72000
18471	8/4/2009	2477400
30680	8/4/2009	150000
49672	8/4/2009	120000
49673	8/4/2009	120000
18505	8/4/2009	644600
48885	8/4/2009	648000



<b>Project Name</b>	<b>Hikes Lane Interceptor and Highgate Springs</b>	
<b>Project Number</b>	<b>HLIHSPS</b>	
18595	8/4/2009	2093300
18483	8/4/2009	1869500
17571	9/1/2003	2780000
MSD0012-PS	9/2/2003	9820800
18483	9/2/2003	990000
18471	9/2/2003	3710000
18505	9/2/2003	340000
18595	9/2/2003	1260000
MSD0012-PS	9/20/2009	21870
MSD0012-PS	9/22/2006	9486000
30680	9/23/2006	10800
18471	9/23/2006	4060000
18299	9/23/2006	50600
17571	9/23/2006	2643800
48885	9/23/2006	0
49672	9/23/2006	3960
18505	9/23/2006	2086700
18595	9/23/2006	2235000
18483	9/23/2006	254200
18483	9/26/2011	95000
MSD0012-PS	9/26/2011	90630
18471	9/26/2011	309800
18595	9/26/2011	138700
18483	9/27/2002	1025500
18595	9/27/2002	1001000
18471	9/27/2002	1025500
18505	9/27/2002	1061500
17571	9/27/2002	1120000
MSD0012-PS	9/27/2002	1310000
MSD0012-PS	9/28/2006	372000



**Integrated Overflow Abatement Plan  
Interim Sanitary Sewer Discharge Plan**

**Hikes Lane Interceptor and  
Highgate Springs Pump Station**

Preliminary - For Budget Development Only

- Documented SSO
- Suspected SSO
- Haulop Locations
- Pump Stations
- WQTC
- Proposed Pipe Solution
- Combined Sewer Pipe
- Force Main
- Collector < 12"
- Interceptor >= 12"
- Streams
- Floodway
- Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,068 feet



Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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Solution:  
New Relief Sewer

Solution:  
Increase Capacity

Solution:  
Remove Hydraulic  
Constriction

Solution:  
- Offload portion of flow tributary to HSPS  
to New Hikes Lane Interceptor  
- Decommission HSPS

Solution:  
- Construct 10,000 LF of 72" Interceptor

Southeast Diversion Structure



**Project Name**     Northern Ditch Diversion Interceptor

**Project Number**     NDDI

**Modeled Area**                     N/A

**Branch or SSO ID**                     N/A

**Project Type**                     New Interceptor / WQTC Elimination

**Receiving Stream**                     Northern Ditch

**Project Description**                     This project includes construction of a new Northern Ditch Diversion Interceptor which will allow flow from upstream projects to reach the Derek R. Guthrie WQTC. The project consists of 13,000 LF of 84 inch pipe constructed along Greasy Ditch from the Northern Ditch Pump Station to the Pond Creek Interceptor.

**Reason for Overflow**                     System Capacity

**Design Parameters**                     N/A

**Project Constraints**                     Project is dependent on Derek R. Guthrie WQTC Improvements.

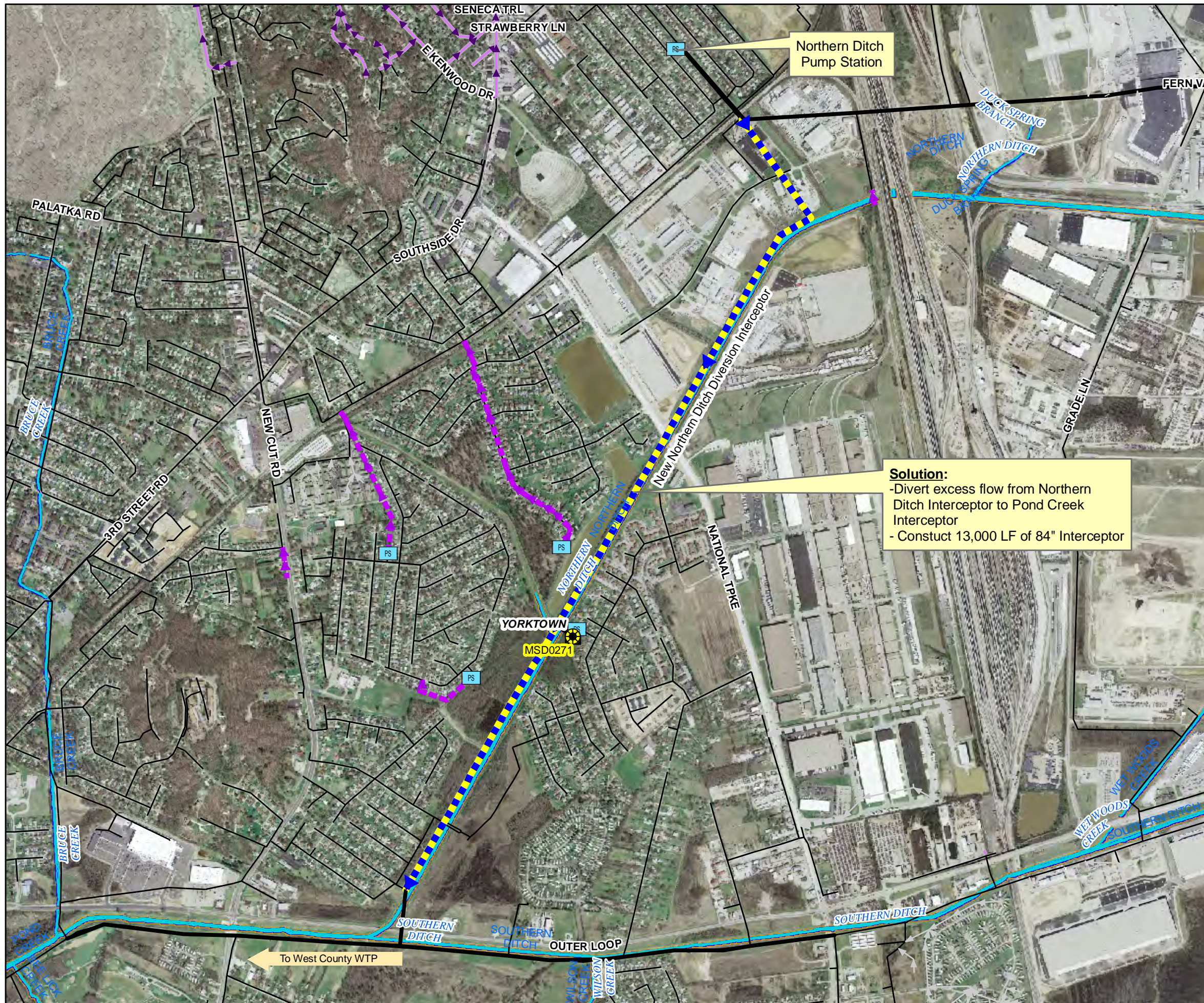
**Estimated Capital Cost**                     \$20,397,000

**Weighted Benefit/Cost Ratio**                     N/A

Asset ID	SSO Start Date	Volume (Gal)
MSD0271	NO DATA	NO DATA



**Integrated Overflow Abatement Plan**  
**Interim Sanitary Sewer Discharge Plan**  
**Northern Ditch Diversion Interceptor**



- Legend**
- Documented SSO
  - Suspected SSO
  - WWTP
  - Pump Station
  - New Construction
  - Force Main
  - Force Main non MSD
  - MSD Sewer
  - Non MSD Pipes
  - Combined Sewer Pipe
  - Streams
  - Hikes Point
  - Metro Parks

**Solution:**  
 -Divert excess flow from Northern Ditch Interceptor to Pond Creek Interceptor  
 - Construct 13,000 LF of 84" Interceptor

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 1,300 feet  
 Scalable when printed on 11" X 17" paper



Some boundaries are uniquely symbolized within the map.  
 Map Revision  
 May 07, 2009  
 Aerial Date: 2006



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<b>Project Name</b>	Sinking Fork Relief Sewer
<b>Project Number</b>	SFRS
<b>Modeled Area</b>	N/A
<b>Branch or SSO ID</b>	N/A
<b>Project Type</b>	New Relief Sewer
<b>Receiving Stream</b>	Middle Fork Beargrass Creek and Upper Sinking Fork
<b>Project Description</b>	This project includes conveying flow from some of the new Beechwood Village sewers and providing additional wet weather capacity downstream of the Beechwood Village East area to accommodate upstream SSDP projects. The project includes installing 2,800 LF of 24-inch relief sewer.
<b>Reason for Overflow</b>	System Capacity
<b>Design Parameters</b>	N/A
<b>Project Constraints</b>	Project is subject to a potential change due to upstream projects
<b>Estimated Capital Cost</b>	\$1,690,000
<b>Weighted Benefit/Cost Ratio</b>	N/A

Asset ID	SSO Start Date	Volume (Gal)
25012	1/3/2005	9639000
25012	10/23/2007	1701000
63319	10/23/2007	2052000
63319	12/15/2007	183000
25012	12/15/2007	2187000
25012	2/6/2008	900
25012	3/12/2006	297000
63319	3/19/2008	33750
21103	3/19/2008	50
63319	3/28/2008	6480
25012	3/28/2008	74520
63319	3/4/2008	59940
25012	3/4/2008	186000
25012	4/4/2008	252000
63319	4/4/2008	34500
25012	5/27/2004	350000
25012	8/4/2009	81000
63319	9/23/2006	3960
25012	9/23/2006	116640



**Integrated Overflow Abatement Plan**  
**Interim Sanitary Sewer Discharge Plan**  
**Sinking Fork Relief Sewer**



- Legend**
- Documented SSO
  - Suspected SSO
  - WWTP
  - Pump Station
  - New Construction
  - Force Main
  - Force Main non MSD
  - MSD Sewer
  - non msd pipes
  - Combined Sewer Pipe
  - Streams
  - Beechwood Village
  - Metro Parks

**Solution:**  
 - Construct 2,800 LF of 24" Interceptor

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

1 inch = 350 feet  
 Scalable when printed on 11" X 17" paper



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 Map Revision  
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 Aerial Date: 2006



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<b>Project Name</b>	Southeastern Diversion Structure and Interceptor
<b>Project Number</b>	SDSI
<b>Modeled Area</b>	N/A
<b>Branch or SSO ID</b>	N/A
<b>Project Type</b>	New relief sewer and flow control modifications
<b>Receiving Stream</b>	South Fork Beargrass Creek
<b>Project Description</b>	This project includes improvements to the Southeast Diversion Structure for increased flows due to the Hikes Lane Interceptor and other Final SSDP projects. The project will consist of a new parallel Southeastern Interceptor relief sewer, two flow control junction boxes, and modifications to the existing Southeastern Diversion Structure (including removing control weirs and reprogramming Real Time Control gates).
<b>Reason for Overflow</b>	System Capacity
<b>Design Parameters</b>	N/A
<b>Project Constraints</b>	Project is subject to a potential change due to upstream projects
<b>Estimated Capital Cost</b>	\$1,744,000
<b>Weighted Benefit/Cost Ratio</b>	N/A

Asset ID	SSO Start Date	Volume (Gal)
72571-X	1/10/2008	140940
18654	1/13/2013	26000
63779	1/14/2007	6000
72571-X	1/14/2007	2856000
49647	1/14/2007	12960
72571-X	1/17/2006	4186730
72571-X	1/21/2010	715687
72571-X	1/22/2006	3702240
63779	1/24/2002	1000000
72571-X	1/24/2002	5000000
63779	1/3/2005	14520000
72571-X	1/3/2005	16500000
49647	1/3/2005	5346000
63779	10/18/2004	23100
72571-X	10/18/2004	10650000
72571-X	10/22/2007	2736000
49647	10/23/2007	756000
63779	10/23/2007	1863000
72571-X	10/27/2004	7400000
72571-X	10/28/2009	224
72571-X	10/31/2009	1627
18654	10/6/2013	78000
72571-X	10/9/2009	930
72571-X	11/1/2004	41900000
72571-X	11/11/2004	29000000
72571-X	11/19/2004	30890000

**Project Name** Southeastern Diversion Structure and Interceptor

**Project Number** SDSI

63779	11/2/2004	3680000
49647	11/2/2004	29300
72571-X	11/20/2011	22095
72571-X	11/22/2011	108564
72571-X	11/25/2010	843051
72571-X	11/28/2011	1606767
49647	11/29/2001	1000000
72571-X	11/29/2001	10000000
72571-X	12/13/2007	28500
63779	12/15/2007	247050
72571-X	12/15/2007	5241000
49647	12/15/2007	823500
49647	12/17/2001	1000000
72571-X	12/17/2001	10000000
63779	12/19/2002	150000
72571-X	12/19/2002	300000
72571-X	12/2/2007	1500
72571-X	12/24/2008	536275
72571-X	12/5/2011	2046000
18654	12/5/2011	69000
72571-X	12/8/2009	16206
72571-X	2/1/2002	3600000
63779	2/1/2002	42000
72571-X	2/12/2008	29119
63779	2/17/2000	0
72571-X	2/22/2003	10000000
63779	2/22/2003	55000
72571-X	2/24/2011	1509071
72571-X	2/28/2011	1427596
49647	2/28/2011	13500
72571-X	2/4/2006	4250000
72571-X	2/5/2008	1200000
72571-X	2/5/2010	535724
63779	2/6/2008	1800
49647	2/6/2008	1800
72571-X	3/1/2007	247680
72571-X	3/12/2006	7492000
49647	3/12/2006	4160000
72571-X	3/18/2008	3623670
72571-X	3/19/2002	1000000
63779	3/19/2002	500000
63779	3/19/2008	945000
49647	3/19/2008	468480

**Project Name** Southeastern Diversion Structure and Interceptor

**Project Number** SDSI

72571-X	3/27/2005	5928000
63779	3/28/2008	1242
72571-X	3/28/2008	183170
49647	3/28/2008	1242
63779	3/4/2008	850500
49647	3/4/2008	945000
72571-X	3/4/2008	3403000
72571-X	3/9/2011	1577116
72571-X	4/1/2006	1000000
72571-X	4/11/2011	2099532
63779	4/12/2011	645000
72571-X	4/19/2009	195618
72571-X	4/2/2006	3750000
72571-X	4/20/2006	4500000
72571-X	4/23/2011	7329855
18654	4/27/2011	113500
72571-X	4/3/2008	3124240
30701	4/4/2008	81000
30702	4/4/2008	81000
49647	4/4/2008	790560
63779	4/4/2008	1458000
63779	5/15/2008	12000
72571-X	5/15/2008	1679510
49647	5/15/2008	12000
72571-X	5/19/2005	2802282
72571-X	5/2/2004	7000000
18654	5/2/2010	97000
72571-X	5/2/2010	2772175
72571-X	5/2/2011	2907260
72571-X	5/21/2010	279825
72571-X	5/23/2011	211860
72571-X	5/25/2004	44900000
72571-X	5/26/2011	260867
63779	5/27/2004	30000
49647	5/27/2004	30000
18654	5/3/2011	90500
63779	5/30/2004	5100000
49647	5/30/2004	219000
72571-X	5/5/2003	6000000
72571-X	5/8/2009	1377881
72571-X	6/18/2009	5900000
72571-X	6/19/2006	3000000
72571-X	6/2/2006	5750000



**Project Name** Southeastern Diversion Structure and Interceptor

**Project Number** SDSI














72571-X	6/22/2011	1056810
18654	6/22/2011	27000
72571-X	6/28/2007	159206
72571-X	6/9/2010	349912
72571-X	7/10/2004	3000000
72571-X	7/13/2004	3100000
72571-X	7/13/2010	26793
72571-X	7/14/2006	2988000
72571-X	7/17/2004	12000000
72571-X	7/17/2011	96362
72571-X	7/29/2009	1829875
72571-X	8/14/2010	1
72571-X	8/21/2007	12470
72571-X	8/28/2005	17928
72571-X	8/30/2005	3536000
18654	8/4/2009	22680
72571-X	8/4/2009	7278984
49647	9/2/2003	400000
63779	9/2/2003	10000
63779	9/2/2003	270000
72571-X	9/2/2003	10000000
72571-X	9/2/2003	8900000
72571-X	9/20/2009	1060533
72571-X	9/22/2006	19173000
63779	9/23/2006	7560000
49647	9/23/2006	1701000
72571-X	9/26/2011	268696
63779	9/27/2002	150000
72571-X	9/27/2002	100000



**Integrated Overflow Abatement Plan  
Interim Sanitary Sewer Discharge Plan**

**Southeastern Diversion  
Structure and Interceptor**

Preliminary - For Budget Development Only

-  Documented SSO
-  Suspected SSO
-  Haulop Locations
-  Pump Stations
-  WQTC
-  Proposed Pipe Solution
-  Combined Sewer Pipe
-  Force Main
-  Collector < 12"
-  Interceptor >= 12"
-  Streams
-  Floodway
-  Jefferson County Boundary

General representation of overflow abatement solutions are for preliminary planning purposes. Alignments and locations may be altered during design.

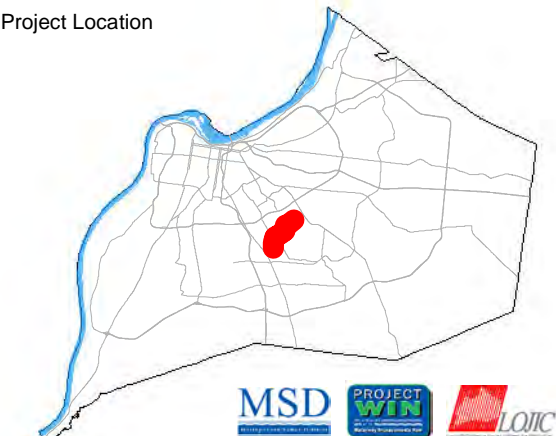
1 inch = 1,000 feet



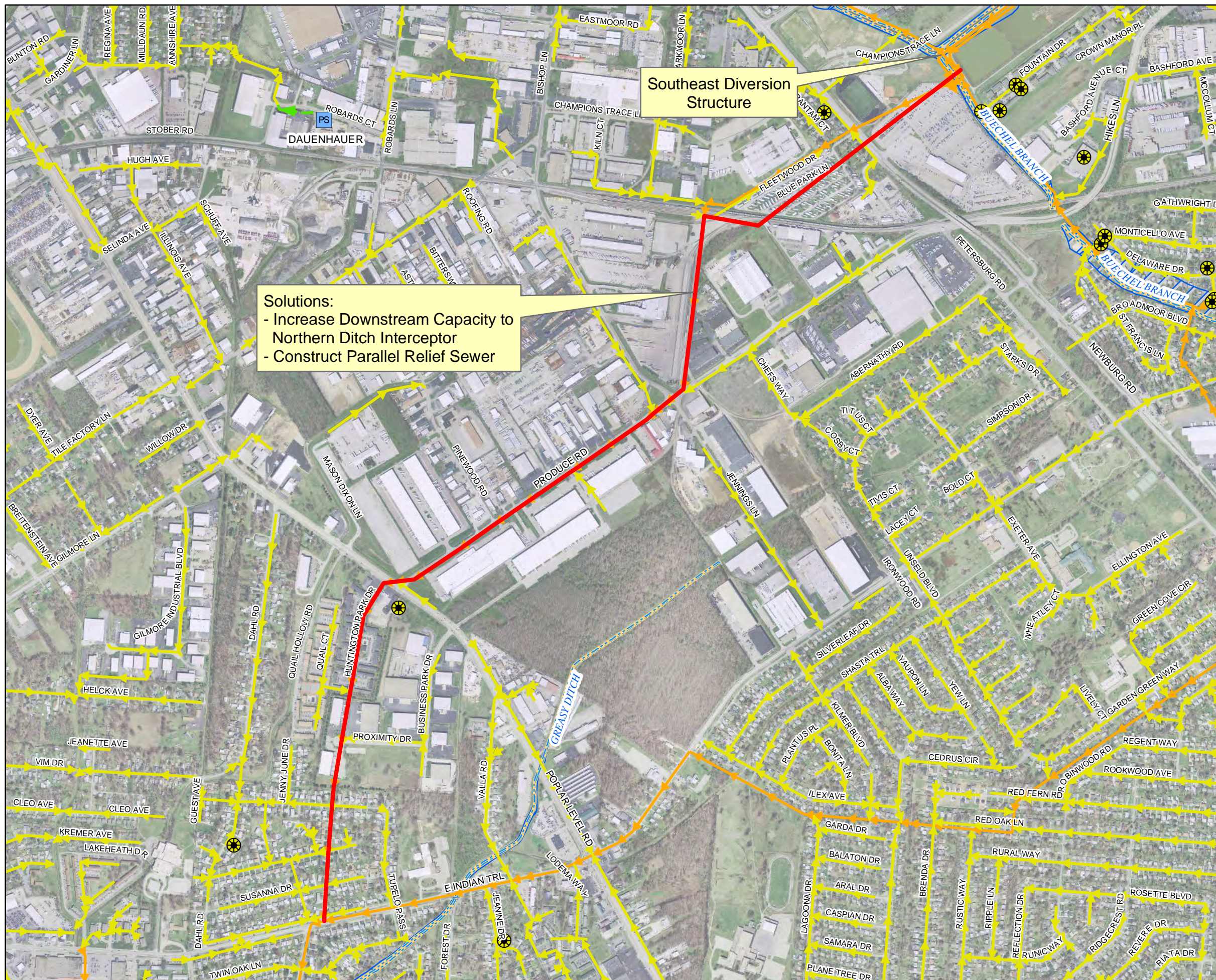
Aerial Date: 2009

Map Revision: April 9, 2012

Project Location



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**Southeast Diversion  
Structure**

**Solutions:**  
 - Increase Downstream Capacity to Northern Ditch Interceptor  
 - Construct Parallel Relief Sewer